

GOV DOC

BRA

1521

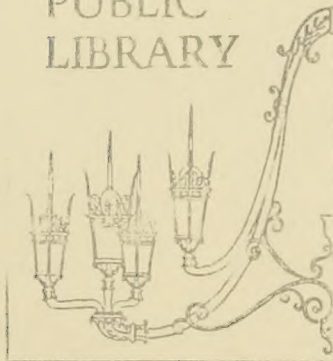
Nov.

1984

Vol. 2



BOSTON  
PUBLIC  
LIBRARY







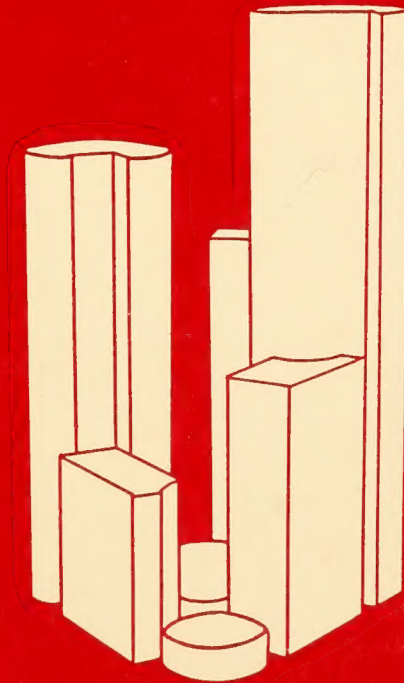


# FINAL BOSTON REDEVELOPMENT AUTHORITY ENVIRONMENTAL IMPACT REPORT

GOVDOC

BRA  
1521  
NOV.  
1984  
Vol. 2 ✓

## International Place at Fort Hill Square



VOLUME II

South Station  
H111  
IP-FEIR

Prepared for The Chiofaro Company

Prepared by HMM Associates, Vanasse/Hangen Associates,  
Colorado State University, Cosentini Associates and Haley & Aldrich, Inc.



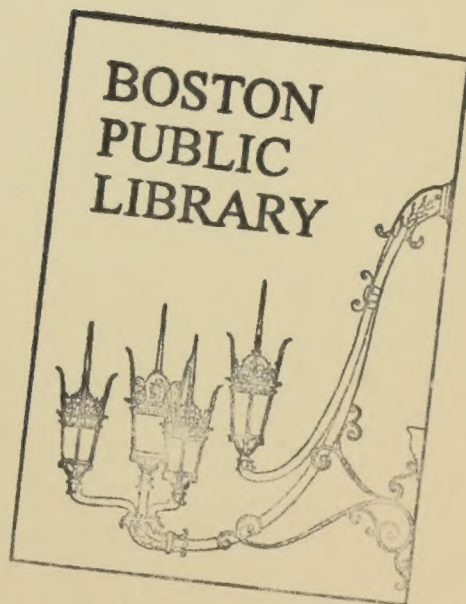
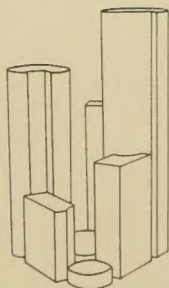


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# Technical Appendix

*Another version of This  
is also on This number.*







APPENDIX  
TABLE OF CONTENTS

TRANSPORTATION

AIR QUALITY

PEDESTRIAN WIND

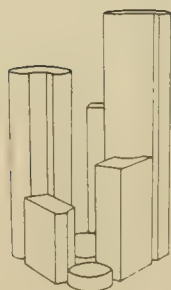




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# Transportation







TRAFFIC COUNT VOLUMES





## TRANSPORTATION TECHNICAL APPENDIX

### LIST OF CONTENTS

Traffic Count Volumes  
Level of Service Analyses  
Traffic Signal Permits  
Air Quality Data  
Rapid Transit Ridership  
Commuter Rail Ridership  
Rapid Transit Capacity  
Excerpt From Previous Report

- "3.2 LAND USE" Third Harbor Tunnel, Interstate 90/Central Artery,  
Interstate 93 DEIR, Dated June, 1983.
  - "2.0 TRAFFIC FORECASTING PROCEDURE" Third Harbor Tunnel Project,  
Interstate 90 Supplement to the DEIR, Dated December, 1982.
  - "Downtown Crossing: Auto Restricted Zone in Boston"  
Final Report Dated July, 1982.
  - "Parking in Central Boston: Meeting the Access Needs of a Growing  
Downtown" Dated December, 1983.
- APPENDIX C
  - APPENDIX D

# TRAFFIC MOVEMENT SUMMARY TABLE

ON Congress Street & Franklin Street CITY OR TOWN Boston Proper

7/25/79 DAY OF WEEK Wed. WEATHER Fair RECORDER E.B.

TIME STARTS -- M	Congress St.		Franklin St.										TOTAL HALF HOURLY TALLY
	Southbound		Westbound										
	S		R	L		S							
00-7:30	182		27	26		13							248
30-8:00	214		33	22		26							295
00-8:30	233		43	30		52							358
30-9:00	222		60	44		73							399
00-9:30	199		37	36		71							343
30-10:00	194		62	37		38							331
00-10:30	189		48	35		48							320
30-11:00	228		52	41		51							372
00-11:30	244		61	42		43							390
30-12:00	231		45	47		55							378
00-12:30	245		56	48		44							393
30-1:00	253		62	46		46							407
00-1:30	194		54	51		41							326
30-2:00	201		55	34		39							329
00-2:30	195		51	35		45							326
30-3:00	220		42	32		48							340
00-3:30	223		46	41		51							361
30-4:00	234		54	47		56							391
00-4:30	241		61	57		63							416
30-5:00	247		69	59		67							442
00-5:30	253		73	43		71							447
30-6:00	224		69	40		72							405
00-6:30													
30-7:00													
00-7:30													
30-8:00													
00-8:30													
30-9:00													
00-9:30													
30-10:00													
00-10:30													
30-11:00													
TOTAL	1514		1160	873		1113							GRAND TOTAL
TOTAL OF S.B.	6008		1986										8000

INT. NO.

DATE 8/1&2/79 DAY OF WEEK Wed-Thur

## INTERSECTION TURNING MOVEMENT COUNT

#36 BR. 4

VEHICLES COUNTED	
ALL	X
PASS. CARS	
TRUCKS	(X)

\*

Congress Street

N.E. TELEPHONE CO.

High Street

High Street

R<sub>1</sub>

V<sub>S</sub>

S

V<sub>L</sub>

Keystone Building

Congress Street

WEATHER

Fair

COUNT TAKEN  
BY

W.C.

LENGTH OF COUNT

TIME

NUMBER  
OF HOURS

7am to 6pm

11

STREET		ENTERING VOLUME	FLOW PERCENT
High St.	SB	4620	38
Congress St.	EB	7675	62
		12295	10

COMMENTS



# TRAFFIC MOVEMENT SUMMARY TABLE

ION Congress Street & High Street CITY OR TOWN Boston Proper

E 8/1&2/79 DAY OF WEEK Wed-Thur WEATHER Fair RECORDER W.C.

TIME STARTS -- M	High Street			Congress Street								TOTAL HALF HOURLY TALLY
	Southbound			Eastbound								
	L		S	S		R						
7:00-7:30	45		83	147		26						301
7:30-8:00	106		119	176		40						441
8:00-8:30	175		185	207		76						643
8:30-9:00	126		204	229		78						637
9:00-9:30	91		218	228		93						630
9:30-10:00	67		187	209		77						540
10:00-10:30	57		152	181		83						473
10:30-11:00	54		126	183		74						431
11:00-11:30	51		126	213		61						451
11:30-12:00	66		141	229		73						509
12:00-12:30	85		179	317		77						658
12:30-1:00	48		117	215		53						433
1:00-1:30	73		96	244		53						466
1:30-2:00	55		122	230		37						444
2:00-2:30	55		117	279		68						519
2:30-3:00	70		145	320		81						616
3:00-3:30	72		116	325		75						588
3:30-4:00	74		103	345		72						594
4:00-4:30	75		97	400		71						643
4:30-5:00	84		111	444		92						731
5:00-5:30	75		95	545		67						782
5:30-6:00	71		100	545		67						759
6:00-6:30												
6:30-7:00												
7:00-7:30												
7:30-8:00												
8:00-8:30												
8:30-9:00												
9:00-9:30												
9:30-10:00												
10:00-10:30												
10:30-11:00												
TOTAL	1361		2939	6181		1494						GRAND TOTAL 14275
TOTAL OF L S & R	4420			7675								12295

INT. NO.

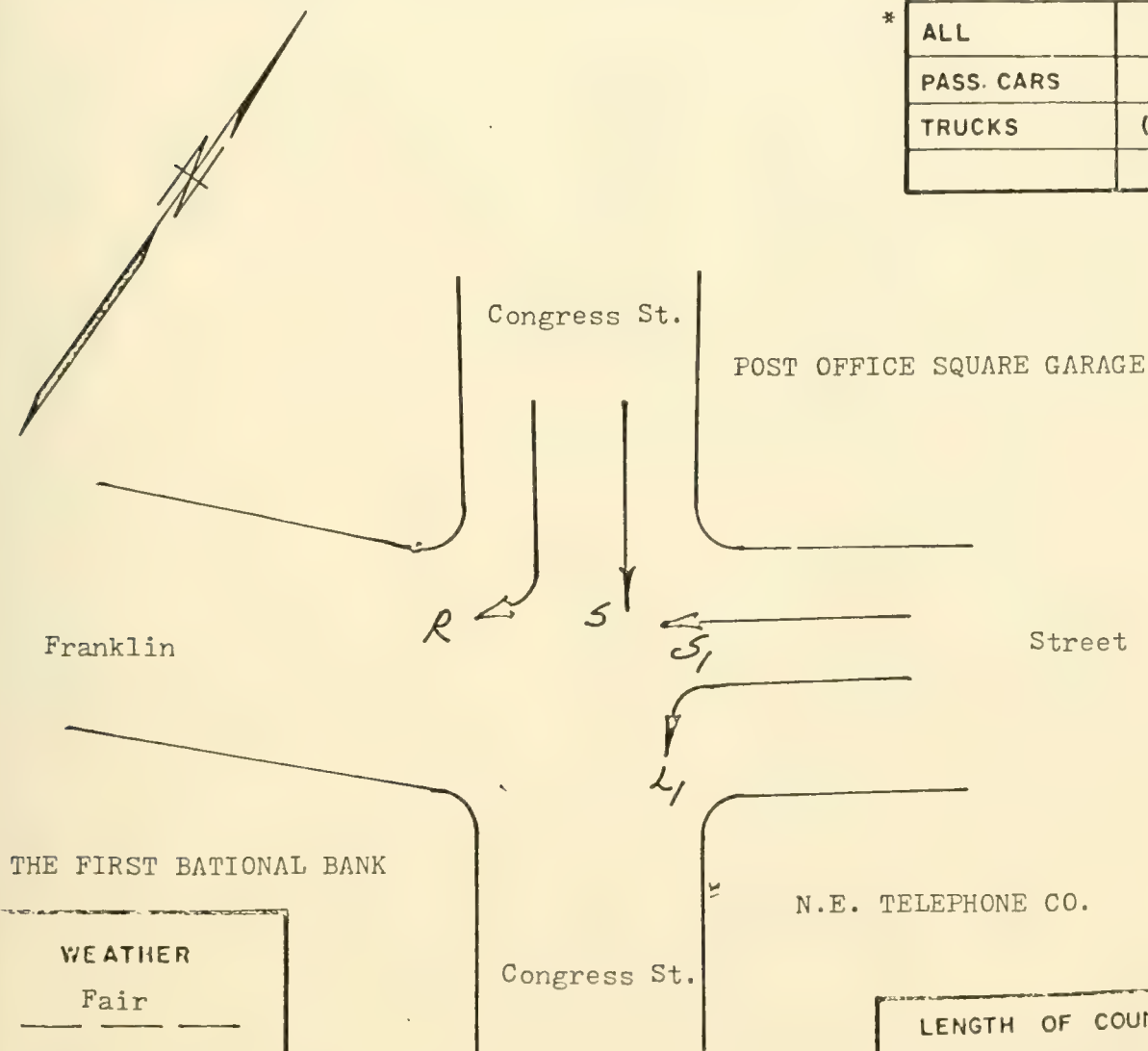
Franklin Street

DATE 7/25/79 DAY OF WEEK Wed.

### INTERSECTION TURNING MOVEMENT COUNT

#35 BRA 362

VEHICLES COUNTED	
ALL	X
PASS. CARS	
TRUCKS	(X)



THE FIRST NATIONAL BANK

N.E. TELEPHONE CO.

## WEATHER

Fair

COUNT TAKEN  
BY  
E.B.

LENGTH OF COUNT

TIME

NUMBER  
OF HOURS

7am-6pm

11 hours

STREET		ENTERING VOLUME	FLOW PERCENT	COMMENTS			
Congress St.	SB	6026	75				
Franklin St.	NB	1986	25				
101st		8012	100				

ION Congress Street & High Street CITY OR TOWN Boston Proper

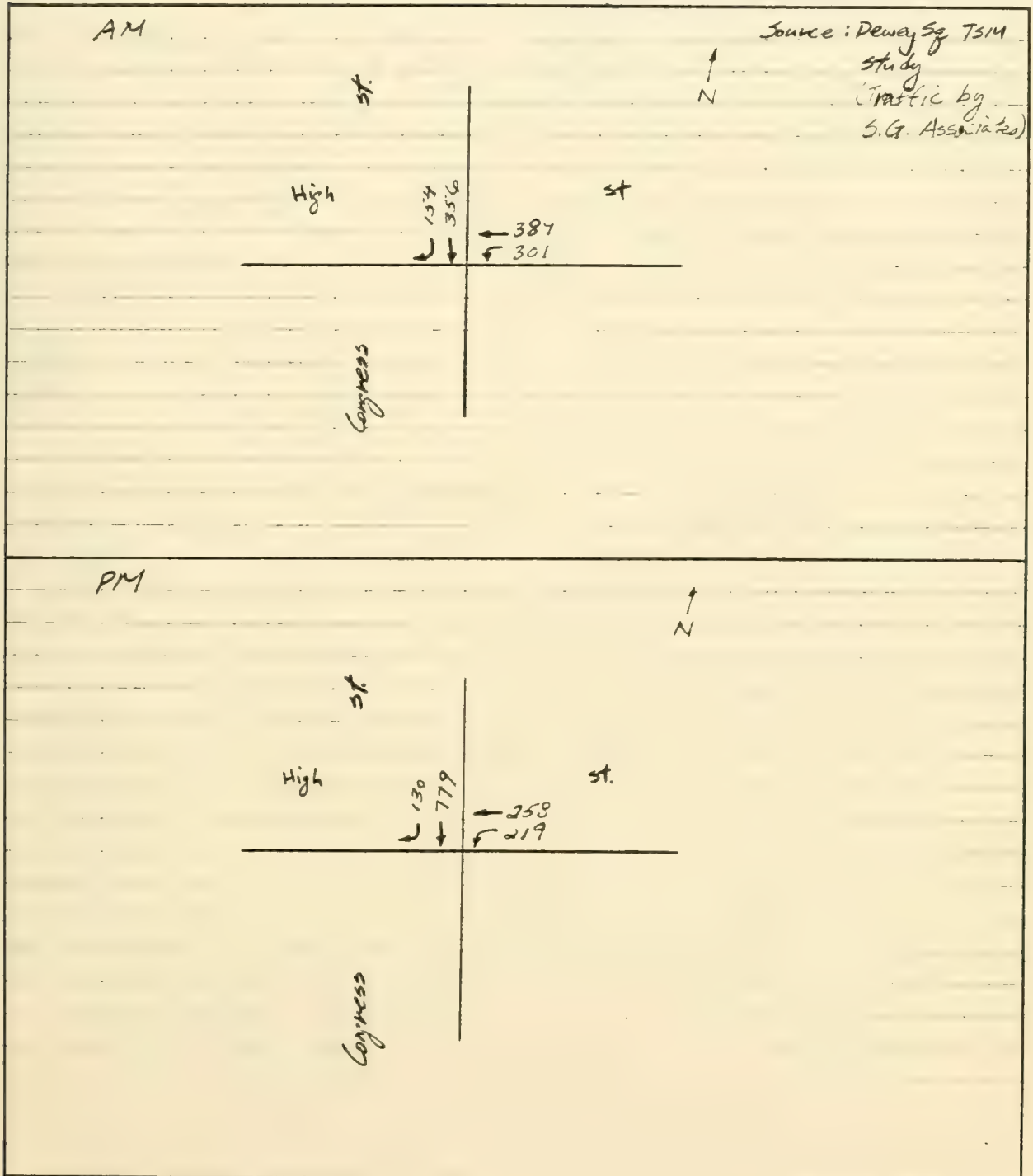
E 8/1&2/79 DAY OF WEEK Wed-Thur WEATHER Fair RECORDER W.C.

TIME STARTS -- M	High Street		Congress Street								TOTAL HALF HOURLY TALLY
	Southbound		Eastbound								
	L	S	S	R							
7:00-7:30	45	83	147	26							301
7:30-8:00	106	119	176	40							441
8:00-8:30	175	185	207	76							643
8:30-9:00	126	204	229	78							637
9:00-9:30	91	218	228	93							630
9:30-10:00	67	187	209	77							540
10:00-10:30	57	152	181	83							473
10:30-11:00	54	126	183	74							431
11:00-11:30	51	126	213	61							451
11:30-12:00	66	141	229	73							509
12:00-12:30	85	179	317	77							658
12:30-1:00	48	117	215	53							433
1:00-1:30	73	96	244	53							466
1:30-2:00	55	122	230	37							444
2:00-2:30	55	117	279	68							519
2:30-3:00	70	145	320	81							616
3:00-3:30	72	116	325	75							588
3:30-4:00	74	103	315	72							594
4:00-4:30	25	97	400	71							643
4:30-5:00	84	111	444	92							731
5:00-5:30	75	95	545	67							782
5:30-6:00	77	100	515	67							759
6:00-6:30											
6:30-7:00											
7:00-7:30											
7:30-8:00											
8:00-8:30											
8:30-9:00											
9:00-9:30											
9:30-10:00											
10:00-10:30											
10:30-11:00											
TOTAL	1531	2939	6181	1494							GRAND TOTAL 12275
TOTAL OF L S R L	4520		7675								12275

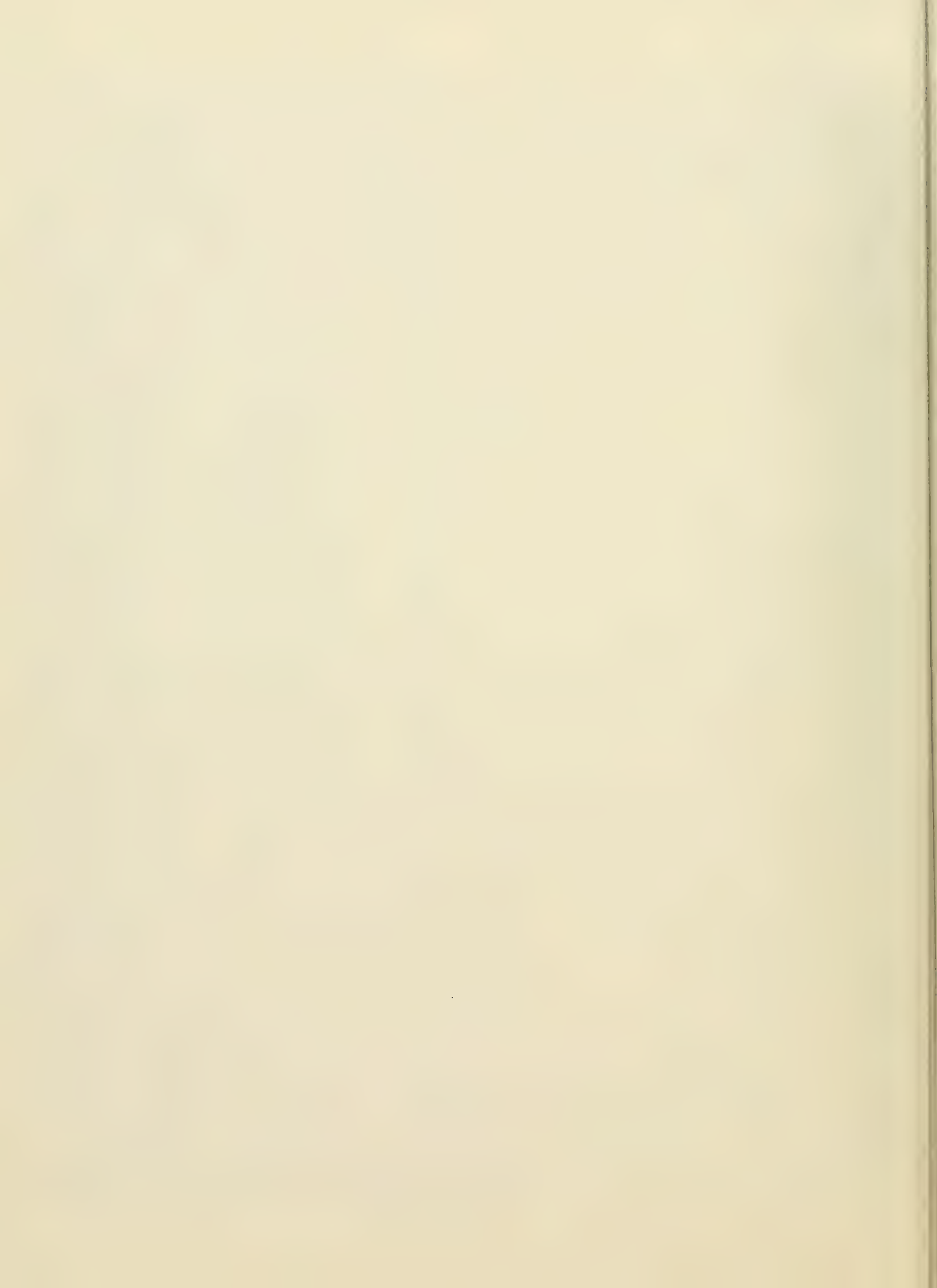


**Vanasse / Hangen Engineering, Inc.**  
Consulting Engineers & Planners  
184 High Street, Boston, Massachusetts 02110  
617 / 482-1870

JOB: International Place JOB No. 0923  
LOCATION: \_\_\_\_\_ SHEET \_\_\_\_\_ OF \_\_\_\_\_  
CALCULATED BY: AG DATE \_\_\_\_\_  
CHECKED BY: \_\_\_\_\_ DATE \_\_\_\_\_  
TITLE Turning Movement Counts







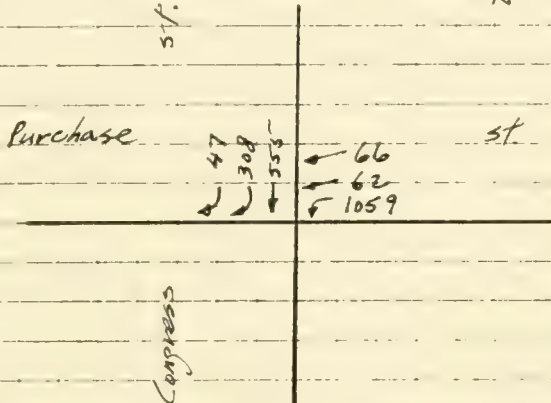


**Vanasse / Hangen Engineering, Inc.**  
Consulting Engineers & Planners  
184 High Street, Boston, Massachusetts 02110  
617 / 482-1870

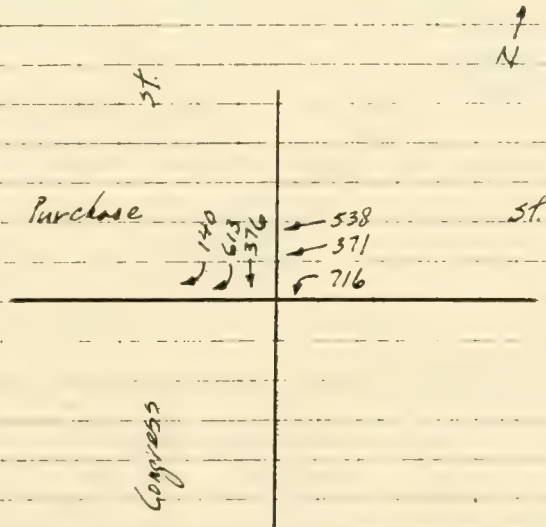
JOB: International Place JOB No. 0923  
LOCATION: \_\_\_\_\_ SHEET \_\_\_\_\_ OF \_\_\_\_\_  
CALCULATED BY: BG DATE \_\_\_\_\_  
CHECKED BY: \_\_\_\_\_ DATE \_\_\_\_\_  
TITLE: Turning Movement Counts

AM

Source: Third Harbor EIR



PM



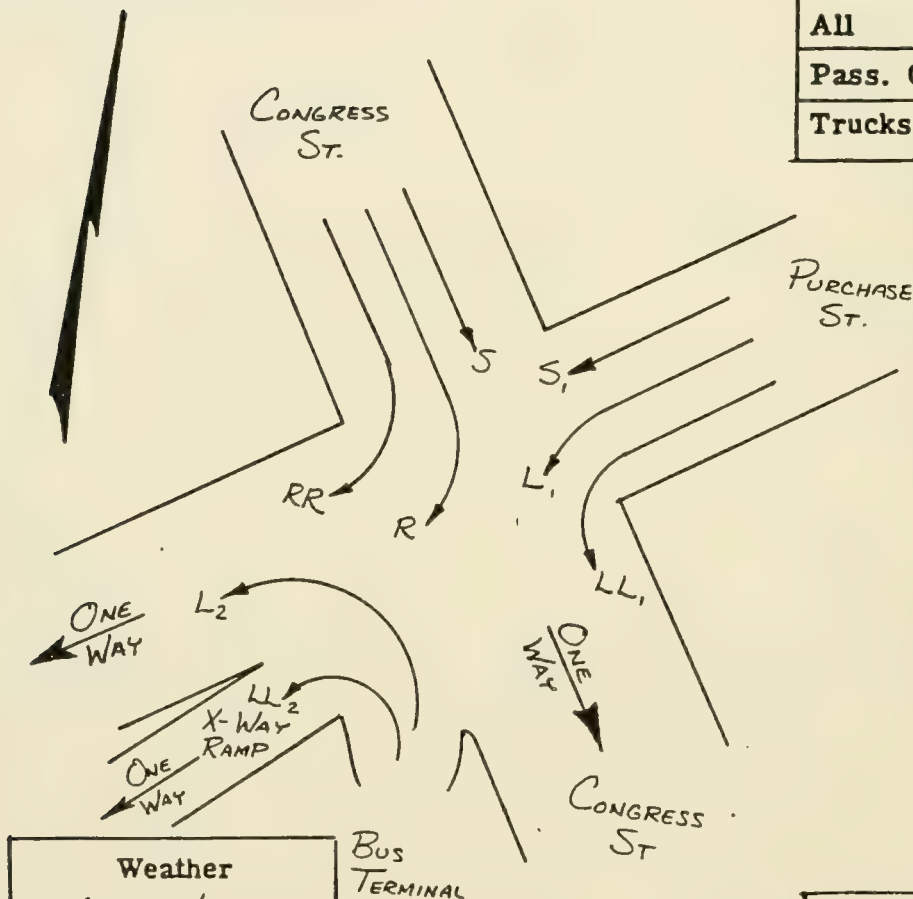
City Boston - Proper  
Intersection CONGRESS ST. & PURCHASE

INT. NO. 73 (BTPD# 3055) Date 6/10/83 Day of Week FRIDAY

INTERSECTION TURNING MOVEMENT COUNT

3055

Vehicles Counted	
All	X
Pass. Cars	
Trucks	



Weather <u>CLOUDY/DRY</u>
Count Taken By <u>C.D. SCHUBERT</u>

BUS  
TERMINAL

Length of Count	
Time	Number of Hours
<u>7AM-6PM</u>	<u>11 HRS</u>

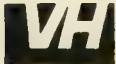
Street	Entering Volume	Flow Percent	Comments
<u>CONGRESS ST. (SB)</u>	<u>9172</u>	<u>47%</u>	
<u>PURCHASE ST. (WB)</u>	<u>10064</u>	<u>52%</u>	
<u>BUS TERMINAL</u>	<u>178</u>	<u>1%</u>	
<b>Total</b>	<u>19,414</u>	<u>100%</u>	

## TRAFFIC MOVEMENT SUMMARY TABLE

**3055**Location CONGRESS ST & PURCHASE ST. City or Town BOSTON - PROPER.Date 6/10/83 Day of Week FRIDAY Weather CLOY Recorder CDS

Time Starts 7:00AM	CONGRESS ST. (SB)			PURCHASE ST. (WB)			BUS TERM						Total Half Hour Tally
	S	R	RR	LL <sub>1</sub>	L <sub>1</sub>	S <sub>1</sub>	LL <sub>2</sub>	L <sub>2</sub>					
7:00-7:30	229	91	22	462	8	39	4	1					856
7:30-8:00	278	111	32	505	18	28	4	4					980
8:00-8:30	254	108	29	454	16	64	9	3					937
8:30-9:00	181	102	24	354	23	74	5	1					764
9:00-9:30	163	105	43	327	9	52	4	2					705
9:30-10:00	135	126	26	285	23	51	5	7					658
10:00-10:30	167	108	35	263	24	63	6	6					672
10:30-11:00	161	112	28	274	13	69	0	2					659
11:00-11:30	157	140	36	299	18	71	5	0					726
11:30-12:00	212	135	48	313	19	60	5	5					797
12:00-12:30	215	142	37	324	10	81	7	8					824
12:30-1:00	171	115	16	222	10	71	4	3					612
1:00-1:30	228	176	29	273	22	83	1	2					814
1:30-2:00	172	151	28	253	18	86	2	4					714
2:00-2:30	187	180	37	251	14	79	1	0					749
2:30-3:00	183	168	45	289	28	66	2	6					787
3:00-3:30	223	247	29	243	89	119	8	1					959
3:30-4:00	195	258	40	337	186	150	3	3					1172
4:00-4:30	282	301	41	324	166	145	3	8					1270
4:30-5:00	258	289	26	326	165	105	2	8					1179
5:00-5:30	313	322	36	338	237	122	6	9					1383
5:30-6:00	241	354	39	274	142	138	2	7					1197
6:00-6:30													
6:30-7:00													
7:00-7:30													
7:30-8:00													
8:00-8:30													
8:30-9:00													
9:00-9:30													
9:30-10:00													
10:00-10:30													
10:30-11:00													
TOTAL	4607	3841	726	6990	1258	1816	88	90					GRAND TOTAL
Total of L S & R	9172			10,064			178						19,414

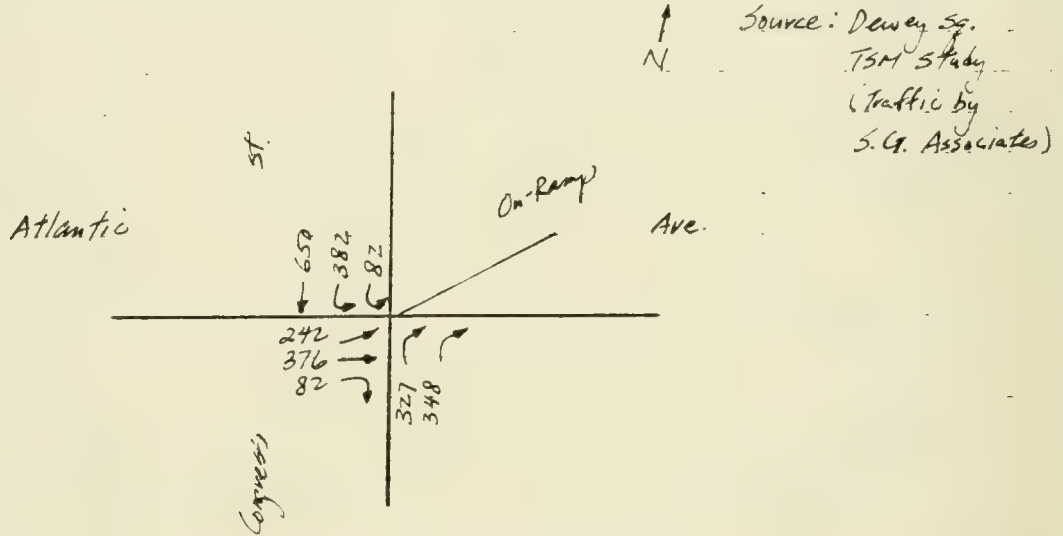




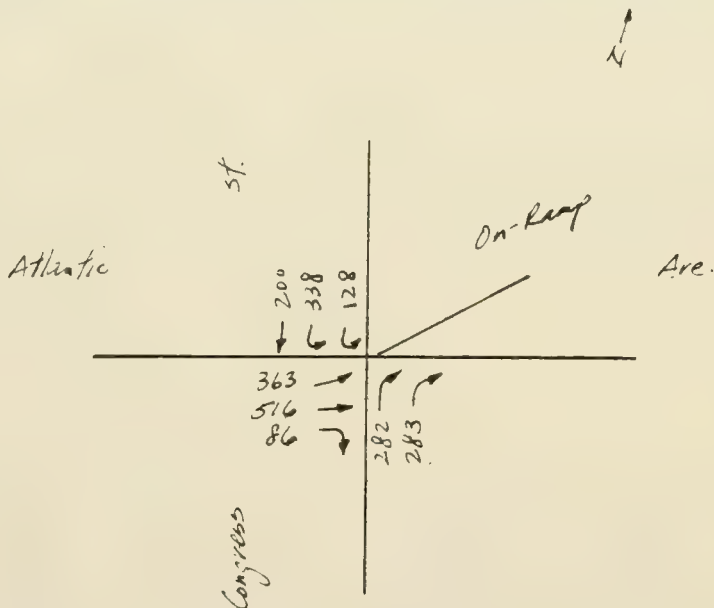
**Vanasse / Hangen Engineering, Inc.**  
Consulting Engineers & Planners  
184 High Street, Boston, Massachusetts 02110  
617 / 482-1870

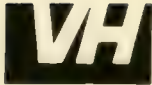
JOB International Place JOB No. 0923  
LOCATION \_\_\_\_\_ SHEET \_\_\_\_\_ OF \_\_\_\_\_  
CALCULATED BY: BG DATE \_\_\_\_\_  
CHECKED BY: \_\_\_\_\_ DATE \_\_\_\_\_  
TITLE Turning Movement Counts

AM



PM



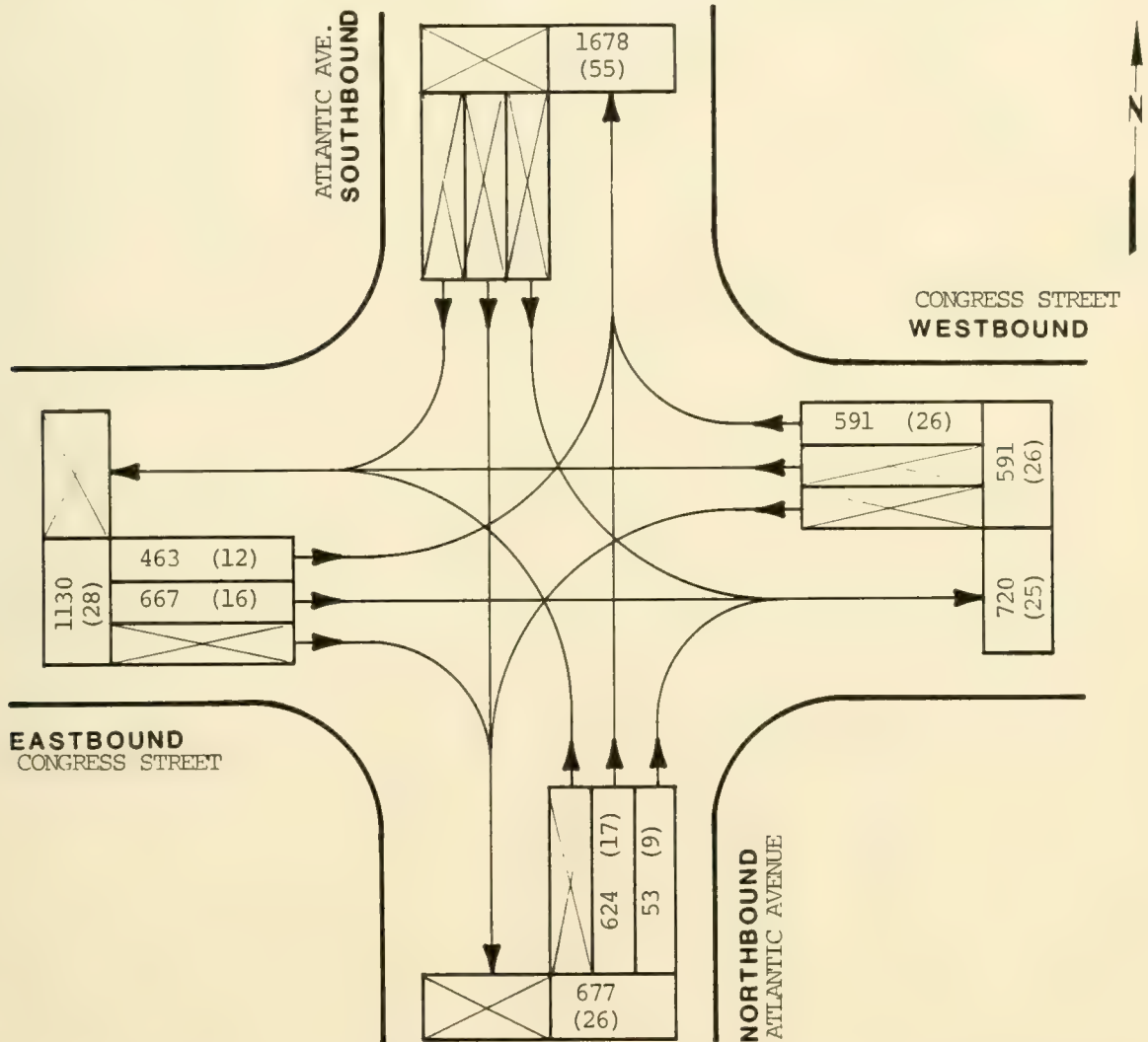


**Vanasse / Hangen Associates, Inc.**  
 Transportation Engineers & Planners  
 184 High Street, Boston, Massachusetts 02110  
 617 / 482-0749

BOSTON REDDEVELOPMENT AUTHORITY  
 LIBRARY

# INTERSECTION TURNING MOVEMENT COUNT

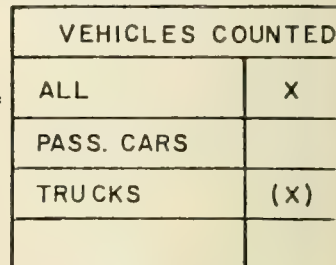
CITY Boston, MA DATE 11/17/81 DAY of WEEK Tuesday  
 INTERSECTION Atlantic Avenue @ Congress Street JOB No. 0121-10



STREET	ENTERING VOLUME	PERCENT OF FLOW	TIME of COUNT
ATLANTIC AVENUE N.B.	677 (26)	28%	4:30PM - 5:30PM
CONGRESS STREET E.B.	1130 (28)	47%	
CONGRESS STREET W.B.	591 (26)	25%	
			PM Peak Hour
			VEHICLES COUNTED
			ALL VEHICLES XXX
			TRUCKS (XX)
TOTAL	2398 (80)	100%	PERCENT TRUCKS 3.3 %

CITY Boston Proper  
INTERSECTION Atlantic Avenue &  
Congress Street  
DATE 6/22/81 DAY OF WEEK Monday

## INTERSECTION TURNING MOVEMENT COUNT 305



Painy

COUNT TAKEN  
BY  
J.T. & G.W.

TIME

NUMBER  
OF HOURS

7am-6pm

11 Hours

STREET		ENTERING	FLOW	COMMENTS			
		VOLUME	PERCENT				
Atlantic Avenue	NB	7911	30.6				
Congress Street	EB	11834	45.6				
Congress Street	WB	6099	23.6				
TOTAL		25844	100%				

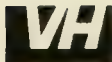
# TRAFFIC MOVEMENT SUMMARY TABLE

LOCATION Atlantic Avenue & Congress Street CITY OR TOWN Boston Proper

DATE 6/22/81 DAY OF WEEK Monday WEATHER Rainy RECORDER J.T. & G

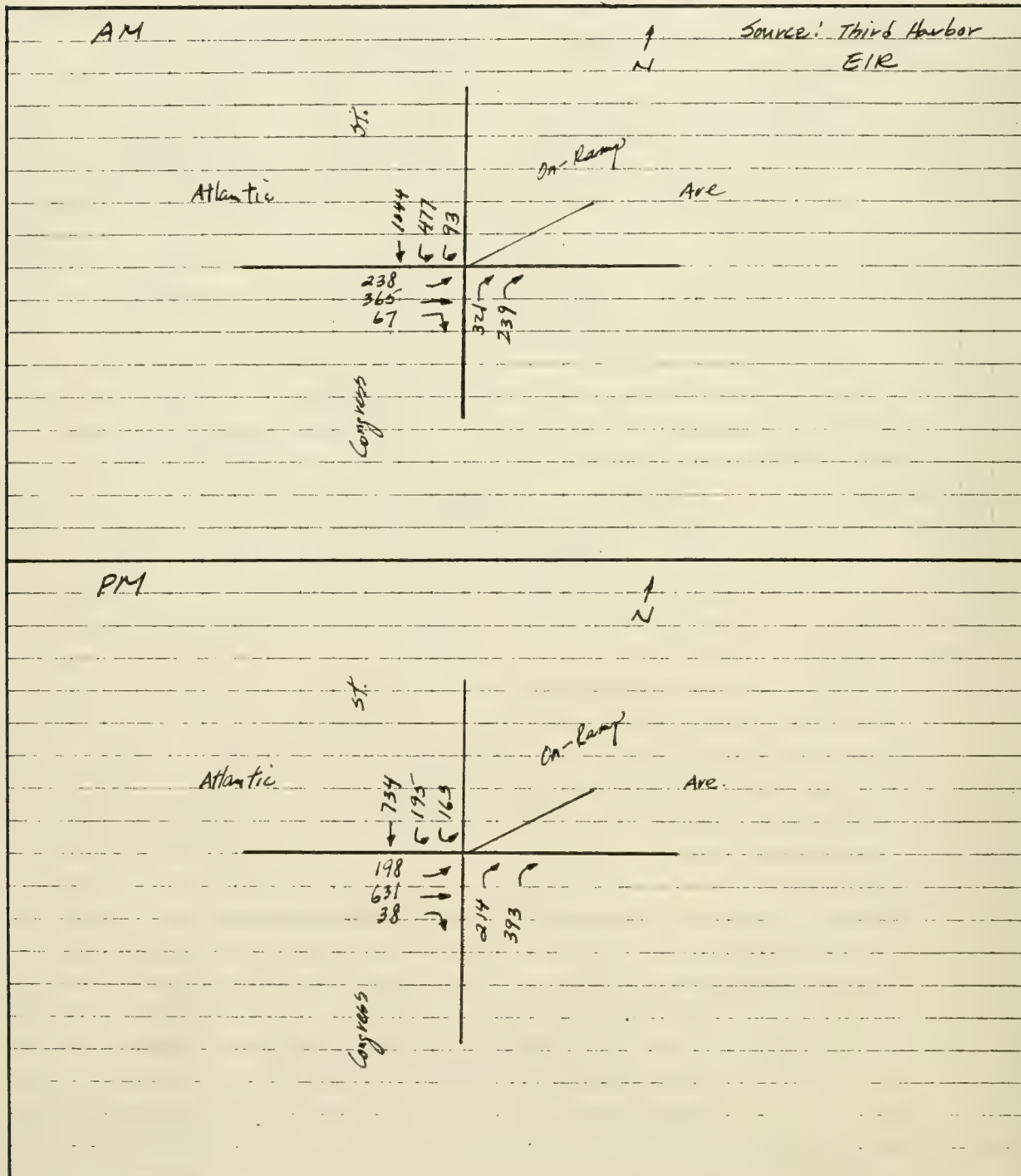
TIME STARTS -- M	Atlantic Avenue			Congress Street			Congress Street						TOT
	Northbound			Eastbound			Westbound						HALF
	L	S	R	LR1	L1	S1	RR2	R2					TAL
7:00-7:30	143	149	30	29	212	406	215	165					134
7:30-8:00	129	168	51	39	236	459	159	145					138
8:00-8:30	135	157	49	37	234	450	165	151					137
8:30-9:00	120	240	38	59	212	309	162	197					133
9:00-9:30	124	184	28	46	201	290	150	171					119
9:30-10:00	115	165	40	57	152	246	118	100					99
10:00-10:30	126	159	27	50	146	239	106	95					94
10:30-11:00	106	171	43	55	136	233	104	87					93
11:00-11:30	132	184	40	58	130	210	138	136					107
11:30-12:00	121	169	29	53	139	229	126	109					97
12:00-12:30	132	172	34	77	112	252	129	97					100
12:30-1:00	127	177	39	78	120	237	132	121					103
1:00-1:30	132	162	33	80	109	278	113	87					99
1:30-2:00	168	171	39	92	96	342	114	113					113
2:00-2:30	142	149	26	75	89	336	167	145					112
2:30-3:00	139	150	18	89	114	273	133	120					103
3:00-3:30	124	201	33	79	93	286	144	101					106
3:30-4:00	105	317	20	53	87	355	138	196					127
4:00-4:30	71	353	18	49	109	445	91	228					136
4:30-5:00	110	319	23	91	153	470	141	237					154
5:00-5:30	73	311	22	79	138	475	124	225					144
5:30-6:00	69	335	20	69	150	402	75	129					124
6:00-6:30													
6:30-7:00													
7:00-7:30													
7:30-8:00													
8:00-8:30													
8:30-9:00													
9:00-9:30													
9:30-10:00													
10:00-10:30													
10:30-11:00													
TOTAL	2643	4568	700	1394	3168	7272	2944	3155					GRAND TOTAL
TOTAL OF LS & R	7911			11834			6099						25844





**Vanasse / Hangen Engineering, Inc.**  
Consulting Engineers & Planners  
184 High Street, Boston, Massachusetts 02110  
617 / 482-1870

JOB: International Place JOB No. 0923  
LOCATION: \_\_\_\_\_ SHEET \_\_\_\_\_ OF \_\_\_\_\_  
CALCULATED BY: RG DATE: \_\_\_\_\_  
CHECKED BY: \_\_\_\_\_ DATE: \_\_\_\_\_  
TITLE: Turning Movement Counts



# PLANNING ENGINEERING & DEVELOPMENT

CITY Boston Proper  
 INTERSECTION Congress Street &  
Dorchester Avenue  
 DATE        \*        DAY OF WEEK Thur-Fri

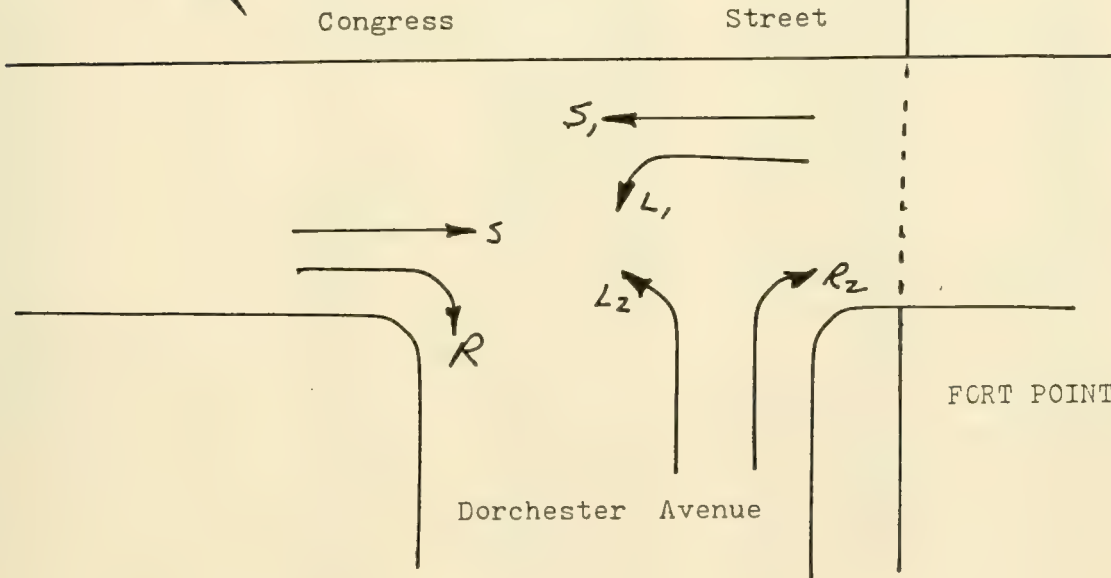
NT. NO.

\* 12/23/76 & 1/7/77  
 PM AM

INTERSECTION TURNING MOVEMENT COUNT #2085 **361**

VEHICLES COUNTED	
ALL	X
PASS. CARS	
TRUCKS	(X)

\*



## WEATHER

snow-am

fair-pm

COUNT TAKEN  
 BY

J.M.

## LENGTH OF COUNT

TIME

NUMBER  
 OF HOURS

7am-6pm

11 hours

\*

STREET		ENTERING VOLUME	FLOW PERCENT	COMMENTS			
Congress St.	EB	5332	45.5				
Congress St.	WB	2476	21.1				
Dorchester Ave.	NB	3920	33.4				
TOTAL		11733	100.0%				

# AFFIC MOVEMENT SUMMARY TABLE

ION Congress St. \* Dorchester Ave.

CITY OR TOWN Boston Proper

Snow-pm

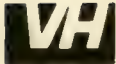
E \* DAY OF WEEK \*

WEATHER

Fair-am

RECORDER J.M

TIME STARTS -- M	Congress			Street			Dorchester Av.						TOTAL HALF HOUR TALLY
	Eastbound			Westbound			Northbound						
	5		R	L1		51	L2		R2				
7:00-7:30	121		111	13		25	86		14				370
7:30-8:00	201		141	13		52	138		22				567
8:00-8:30	182		121	20		65	157		46				591
8:30-9:00	170		98	26		57	158		40				549
9:00-9:30	88		62	35		50	111		23				369
9:30-10:00	90		65	27		40	111		20				353
10:00-10:30	83		71	27		46	88		22				337
10:30-11:00	74		66	25		36	103		22				326
11:00-11:30	78		62	22		60	106		20				348
11:30-12:00	80		66	20		81	110		22				379
12:00-12:30	152		143	61		106	198		37				697
12:30-1:00	126		102	37		73	175		36				549
1:00-1:30	110		114	52		75	204		30				583
1:30-2:00	128		136	39		78	185		26				596
2:00-2:30	148		118	69		123	222		18				698
2:30-3:00	112		113	47		101	171		20				564
3:00-3:30	117		133	62		87	209		24				636
3:30-4:00	132		193	64		100	230		24				743
4:00-4:30	131		211	74		75	188		16				693
4:30-5:00	103		234	54		119	163		9				686
5:00-5:30	90		192	46		80	154		12				574
5:30-6:00	85		184	40		74	141		9				533
6:00-6:30													
6:30-7:00													
7:00-7:30													
7:30-8:00													
8:00-8:30													
8:30-9:00													
9:00-9:30													
9:30-10:00													
10:00-10:30													
10:30-11:00													
TOTAL	2601		2436	873		1603	3408		512				GRAND TOTAL
TOTAL OF L.S & R	5337			2476			3920						11,733



**Vanasse / Hangen Engineering, Inc.**

Consulting Engineers & Planners  
184 High Street, Boston, Massachusetts 02110  
617 / 482-1870

JOB International Place JOB No. 0923

LOCATION \_\_\_\_\_ SHEET \_\_\_\_\_ OF \_\_\_\_\_

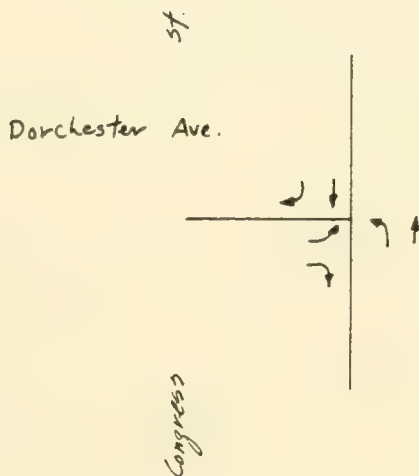
CALCULATED BY BG DATE \_\_\_\_\_

CHECKED BY \_\_\_\_\_ DATE \_\_\_\_\_

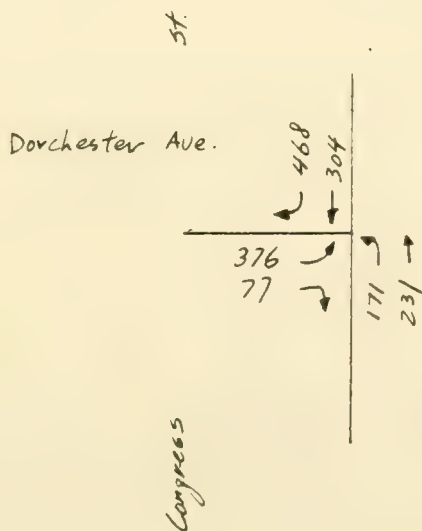
TITLE Turning Movement Counts

A M

Source: Third Harbor EIR



P M



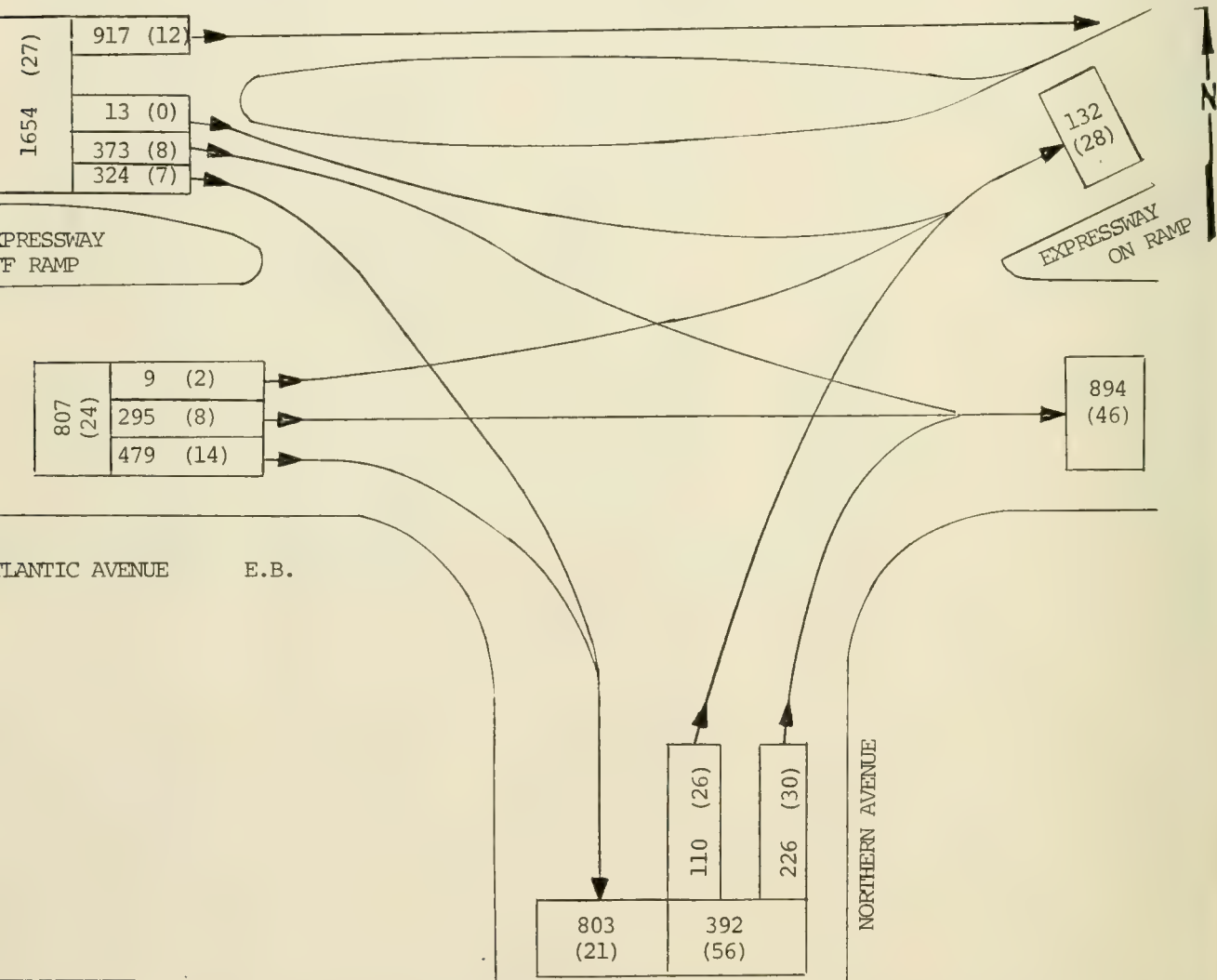




Vanasse / Hangen Associates, Inc.  
Transportation Engineers & Planners  
184 High Street, Boston, Massachusetts 02110  
617 / 482-0749

## INTERSECTION TURNING MOVEMENT COUNT

CITY Boston, MA DATE 11/24/81 DAY of WEEK Tuesday  
INTERSECTION Atlantic Ave., Northern Ave. & Expressway Ramps JOB No. 0121-10



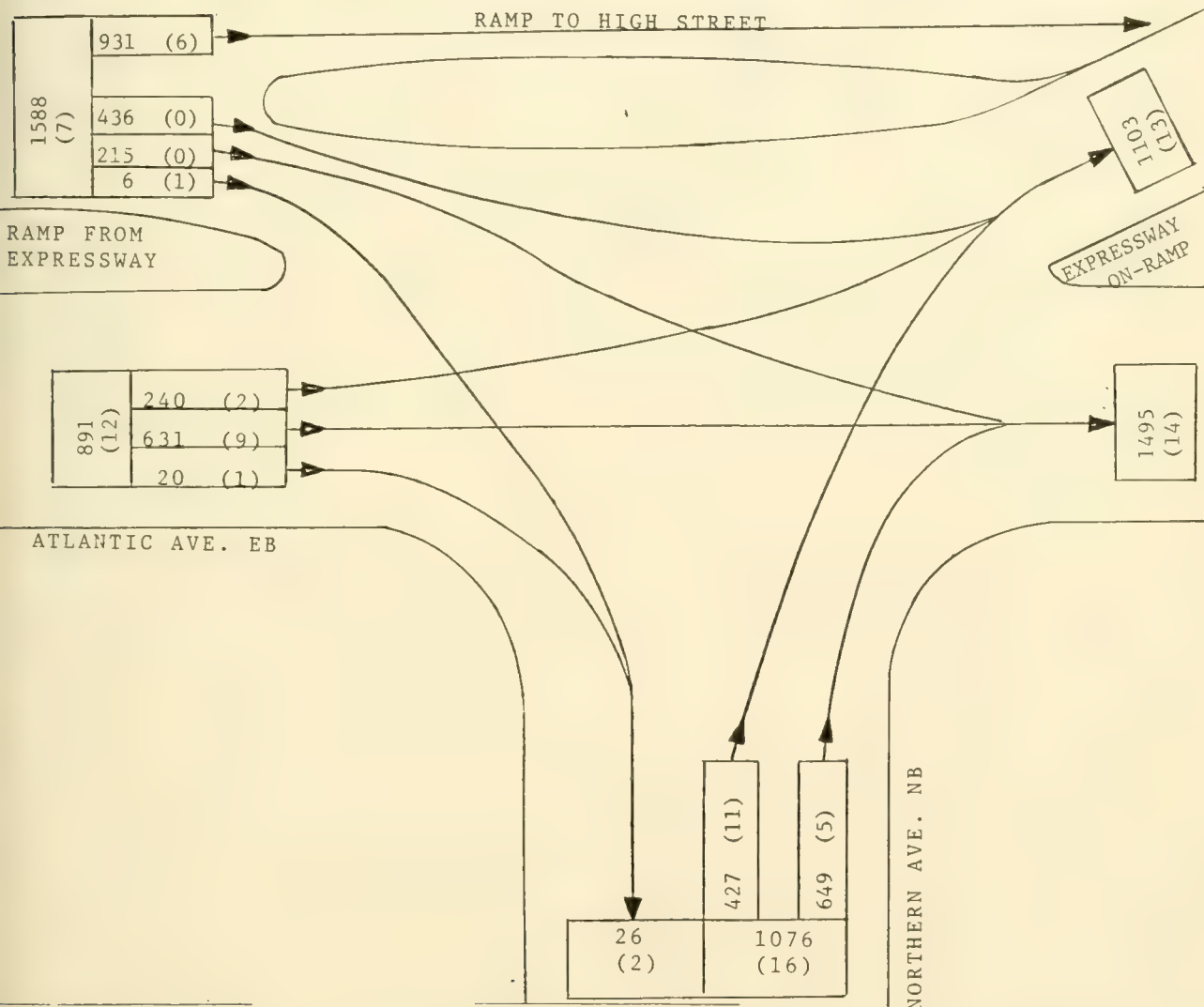
STREET	ENTERING VOLUME	PERCENT OF FLOW	TIME of COUNT
ATLANTIC AVENUE E.B.	807 (24)	28.3%	7:30AM - 8:30AM
NORTHERN AVENUE N.B.	392 (56)	13.7%	
OFF RAMP FROM EXPRESSWAY RAMP TO HIGH STREET	737 (15)	25.8%	
	917 (12)	32.2%	AM Peak Hour
			VEHICLES COUNTED
			ALL VEHICLES XXX
			TRUCKS (XX)
TOTAL	2853 (107)	100%	PERCENT TRUCKS 3.7%



Vanasse / Hangen Associates, Inc.  
 Transportation Engineers & Planners  
 184 High Street, Boston, Massachusetts 02110  
 617 / 482-0749

# INTERSECTION TURNING MOVEMENT COUNT

CITY BOSTON DATE 11-24-81 and 12-09-81 DAY of WEEK Tuesday and Wednesday  
 INTERSECTION Northern Ave. @ Atlantic Ave. JOB No. 0121-10



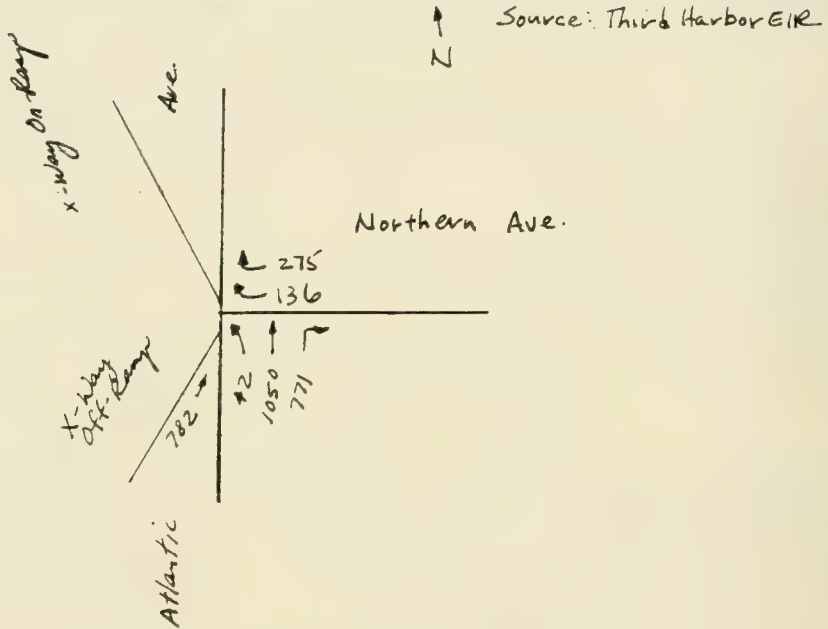
STREET		ENTERING VOLUME	PERCENT OF FLOW	TIME of COUNT
Northern Ave.	NB	1076 (16)	30.3%	4:15 PM to 5:15 PM
Atlantic Ave.	EB	891 (12)	25.1%	
Ramp from Expressway	EB	1588 (7)	44.6%	
				PM Peak Hour
				VEHICLES COUNTED
				ALL VEHICLES XXX
				TRUCKS (XX)
TOTAL		3555 (35)	100%	PERCENT TRUCKS 1.0 %



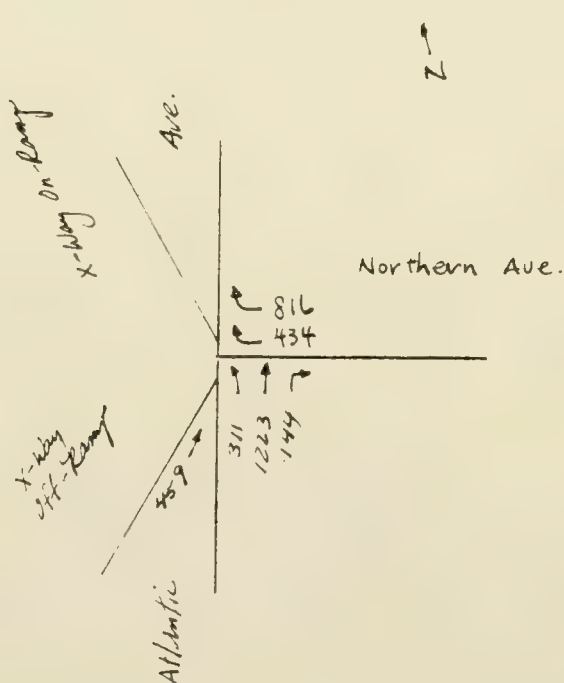
**Vanasse / Hangen Engineering, Inc.**  
Consulting Engineers & Planners  
184 High Street, Boston, Massachusetts 02110  
617 / 482-1870

JOB Interpretation of JOB No. 0923  
LOCATION \_\_\_\_\_ SHEET \_\_\_\_\_ OF \_\_\_\_\_  
CALCULATED BY BL DATE \_\_\_\_\_  
CHECKED BY \_\_\_\_\_ DATE \_\_\_\_\_  
TITLE Turning Movement Counts

AM



PM



INT. NO. 74

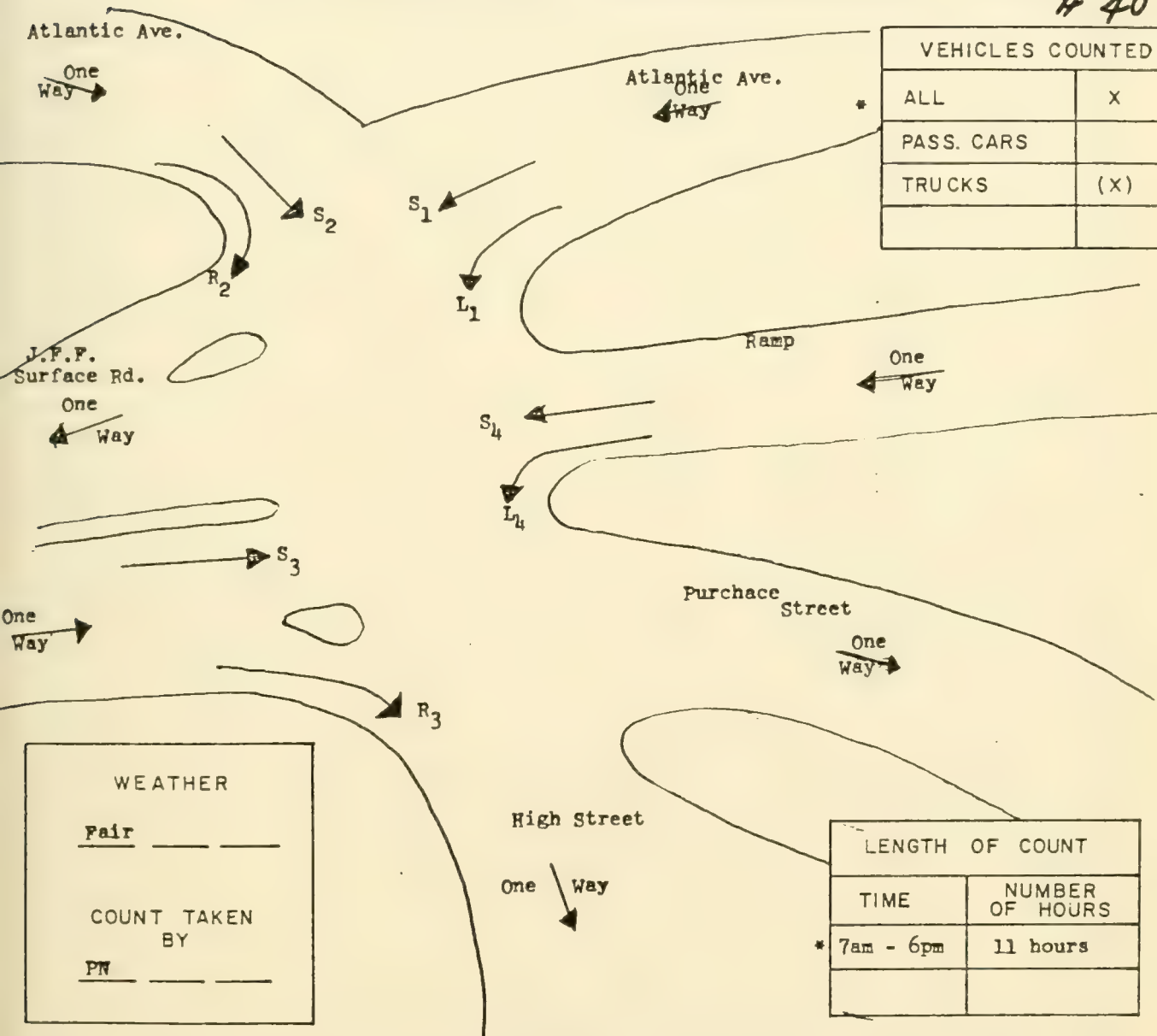
CITY Boston Proper

INTERSECTION Atlantic Ave., High Street &  
 J.F.F. Surface Road

DATE 10/30 & 31/79 DAY OF WEEK Tue & Wed

# INTERSECTION TURNING MOVEMENT COUNT

# 40



STREET	ENTERING	FLOW	COMMENTS
	VOLUME	PERCENT	
Atlantic Ave. NB	6204	26.6	
Atlantic Ave. WB	3145	13.5	
Surface Rd. SR	6109	26.3	
Ramp NB	7827	33.6	
TOTAL	23285	100.0	



# TRAFFIC MOVEMENT SUMMARY TABLE

LOCATION Atlantic Ave. - High St. & I.E.E. Surface Rd. CITY OR TOWN Boston Proper

DATE 10/30 & 31/79 DAY OF WEEK Tue. & Wed WEATHER Fair RECORDER PN #40

TIME STARTS -- M	Atlantic Ave.			Atlantic Ave.			Surface Rd.			Ramp			TOT
	Northbound			Westbound			Southbound			Northbound			HALF
	L <sub>1</sub>	S <sub>1</sub>			S <sub>2</sub>	R <sub>2</sub>		S <sub>3</sub>	R <sub>3</sub>	L <sub>4</sub>	S <sub>4</sub>		TAL
7:00-7:30	52	83			184	0		218	21	100	192		85
7:30-8:00	82	106			190	1		196	23	154	248		100
8:00-8:30	123	182			210	1		271	16	218	296		131
8:30-9:00	123	159			145	1		233	22	261	339		128
9:00-9:30	144	166			139	1		183	20	215	272		114
9:30-10:00	130	102			109	0		174	36	148	224		90
10:00-10:30	142	142			100	2		184	44	144	244		100
10:30-11:00	128	101			91	2		192	38	91	216		80
11:00-11:30	127	93			91	1		185	25	90	149		70
11:30-12:00	115	93			102	0		250	28	121	181		80
12:00-12:30	116	81			118	1		263	32	95	170		80
12:30-1:00	147	94			106	0		225	31	83	127		80
1:00-1:30	155	72			91	1		239	26	72	153		80
1:30-2:00	167	80			117	0		235	34	85	140		80
2:00-2:30	180	114			122	0		300	22	86	168		90
2:30-3:00	171	130			126	1		285	16	74	212		100
3:00-3:30	163	196			170	1		308	15	46	315		120
3:30-4:00	152	237			215	0		401	9	99	395		150
4:00-4:30	165	206			142	1		317	11	35	340		120
4:30-5:00	208	205			198	0		351	23	62	394		140
5:00-5:30	255	191			203	0		345	2	39	393		140
5:30-6:00	181	145			162	0		253	7	33	308		100
6:00-6:30													
6:30-7:00													
7:00-7:30													
7:30-8:00													
8:00-8:30													
8:30-9:00													
9:00-9:30													
9:30-10:00													
10:00-10:30													
10:30-11:00													
TOTAL	3226	2978			3131	14		5608	501	2351	5476		GRA TOT
TOTAL OF	6204				3145			6109		7827			230

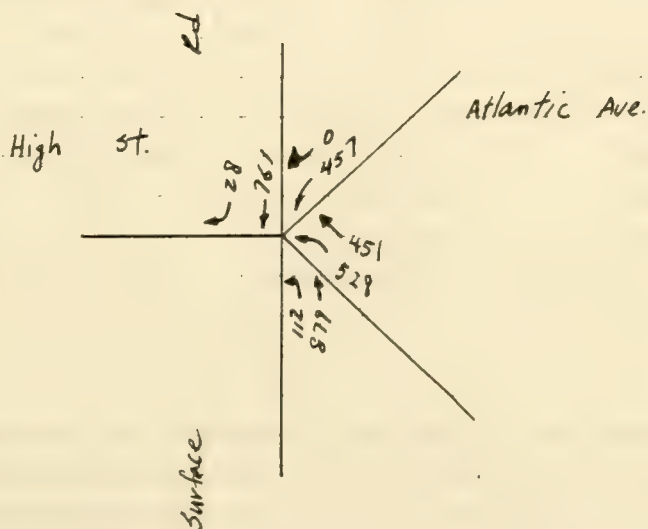
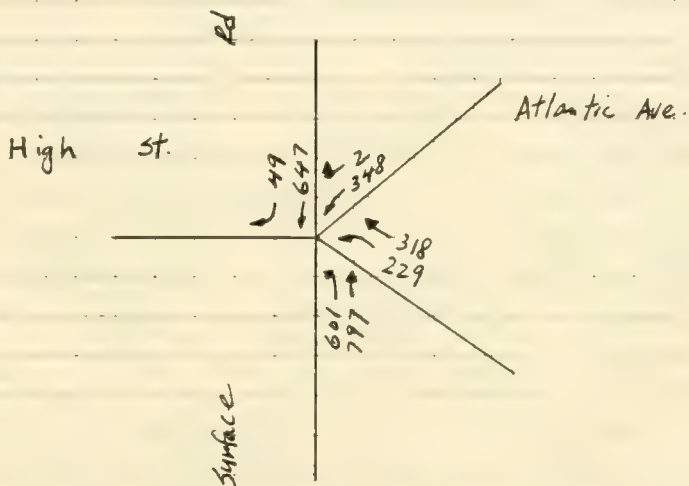


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Consulting Engineers & Planners  
184 High Street, Boston, Massachusetts 02110  
617 / 482-1870

JOB: International Place JOB No. 0923  
LOCATION: \_\_\_\_\_ SHEET \_\_\_\_\_ OF \_\_\_\_\_  
CALCULATED BY: BG DATE \_\_\_\_\_  
CHECKED BY: \_\_\_\_\_ DATE \_\_\_\_\_  
TITLE Turning Movement Counts

AM

Source: Third Harbor EIR



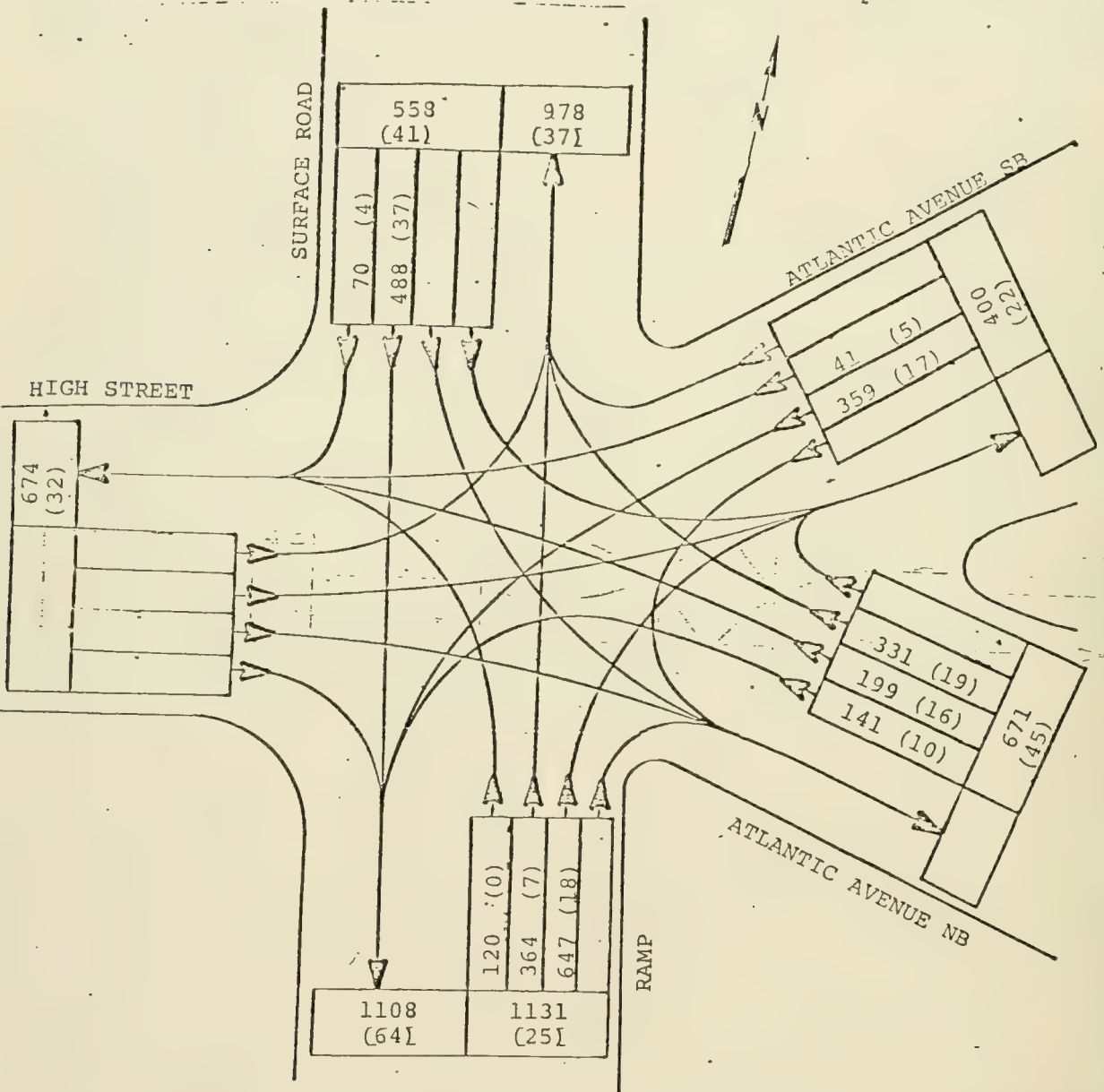
V110

3000, 11/10/80

11/10/80-191

# INTERSECTION TURNING MOVEMENT COUNT

CITY BOSTON, MA DATE 11/10/80 DAY of WEEK Mon.  
INTERSECTION High St. & Surface Rd. & Atlantic Ave. & Ramp



STREET		ENTERING VOLUME	PERCENT of FLOW	LENGTH of COUNT	
				Time	Number of Hours
Ramp	(NB)	1131 (25)	41.0	8:00-9:00AM	AM
Atlantic Ave.	(NB)	671 (45)	24.3		PEAK HOUR
Atlantic Ave.	(SB)	400 (22)	14.5		
Surface Rd.	(SB)	558 (41)	20.2	5% Trucks	
				VEHICLES COUNTED	
				ALL	XXX
TOTAL				133 TRUCKS	(XX)

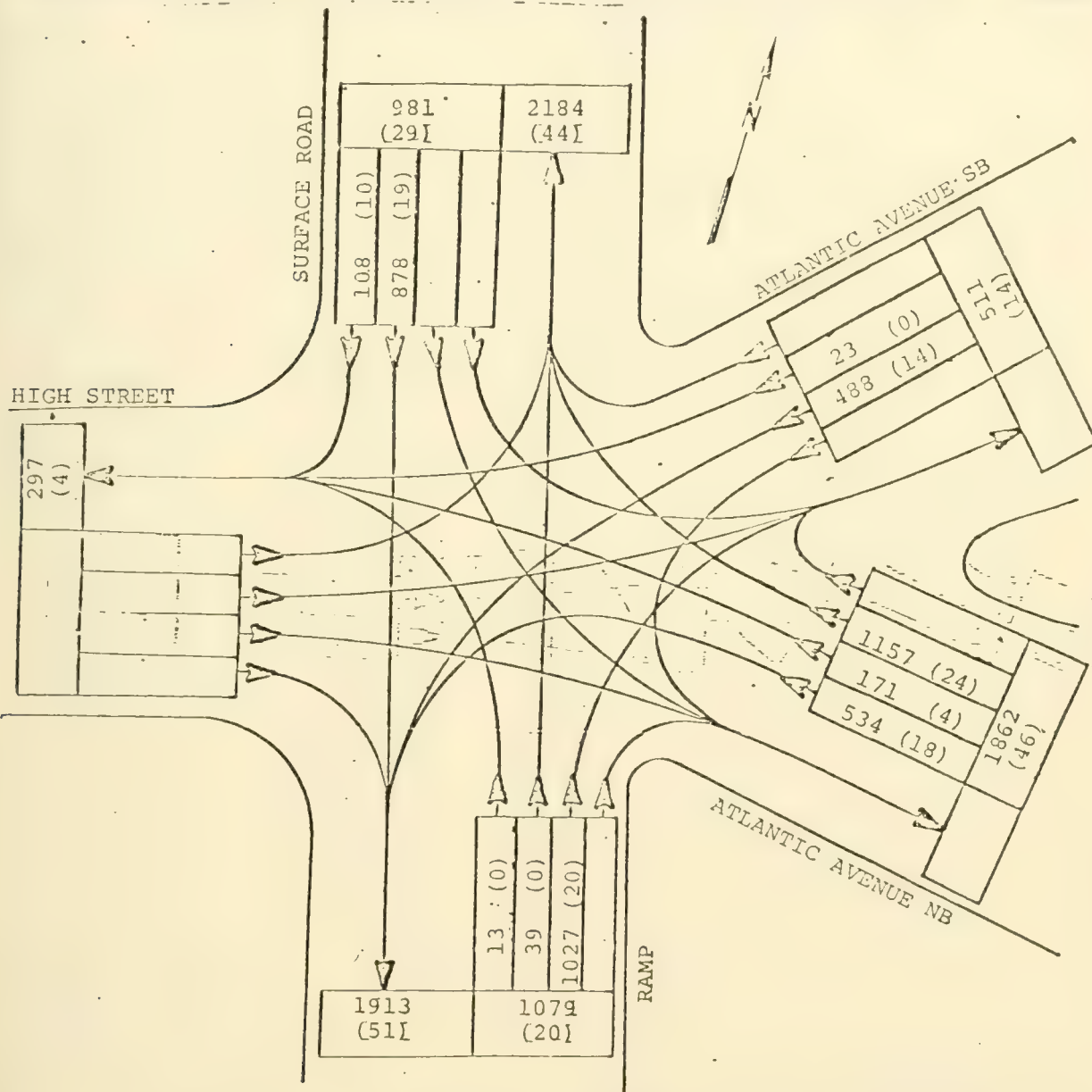
# INTERSECTION TURNING MOVEMENT COUNT

VH #80-101

CITY BOSTON, MA

DATE 11/10/80 DAY of WEEK Monday

INTERSECTION High St. & Surface Rd. & Atlantic Ave. & Purchase St. & Ramp



STREET		ENTERING VOLUME	PERCENT of FLOW	LENGTH of COUNT	
				Time	Number of Hours
Ramp	(NB)	1079 (20)	24.4	4:45-5:45PM	PM
Atlantic	(NB)	1862 (46)	42.0		PEAK HOUR
Atlantic	(SB)	511 (14)	11.5		
Surface Rd.	(SB)	981 (29)	22.1		
				2% Trucks	
				VEHICLES COUNTED	
				ALL	XXX
				TRUCKS	(XX)
TOTAL		4433 (22)	100.0%		

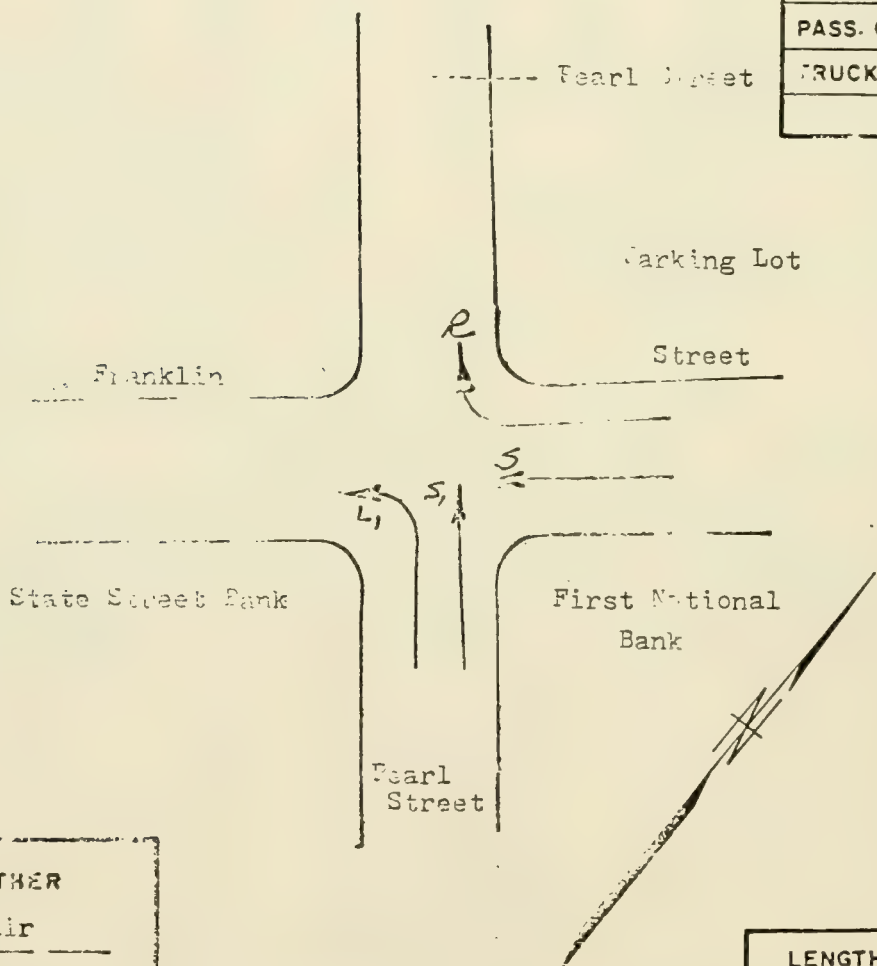


INTERSECTION TURNING MOVEMENT COUNT

CITY Boston Proper  
 INTERSECTION Franklin Street &  
Pearl Street  
 DATE 8/10/79 DAY OF WEEK Friday

INTERSECTION TURNING MOVEMENT COUNT # 57 BRA

VEHICLES COUNTED	
ALL	X
PASS. CARS	
TRUCKS	(X)



WEATHER  
Fair

COUNT TAKEN  
 BY  
E.H.

LENGTH OF COUNT	
TIME	NUMBER OF HOURS
* 7am-6pm	11 hours

STREET	ENTERING VOLUME	FLOW PERCENT	COMMENTS
Franklin St.	2014	51	
Pearl St.	1150	29	



# PLANNING ENGINEERING & DEVELOPMENT

STA. NO. 57

BRA

## TRAFFIC MOVEMENT SUMMARY TABLE

LOCATION Franklin Street & Pearl Street CITY OR TOWN Boston Proper

DATE 8/10/79 DAY OF WEEK Friday WEATHER Fair RECORDER E.H.

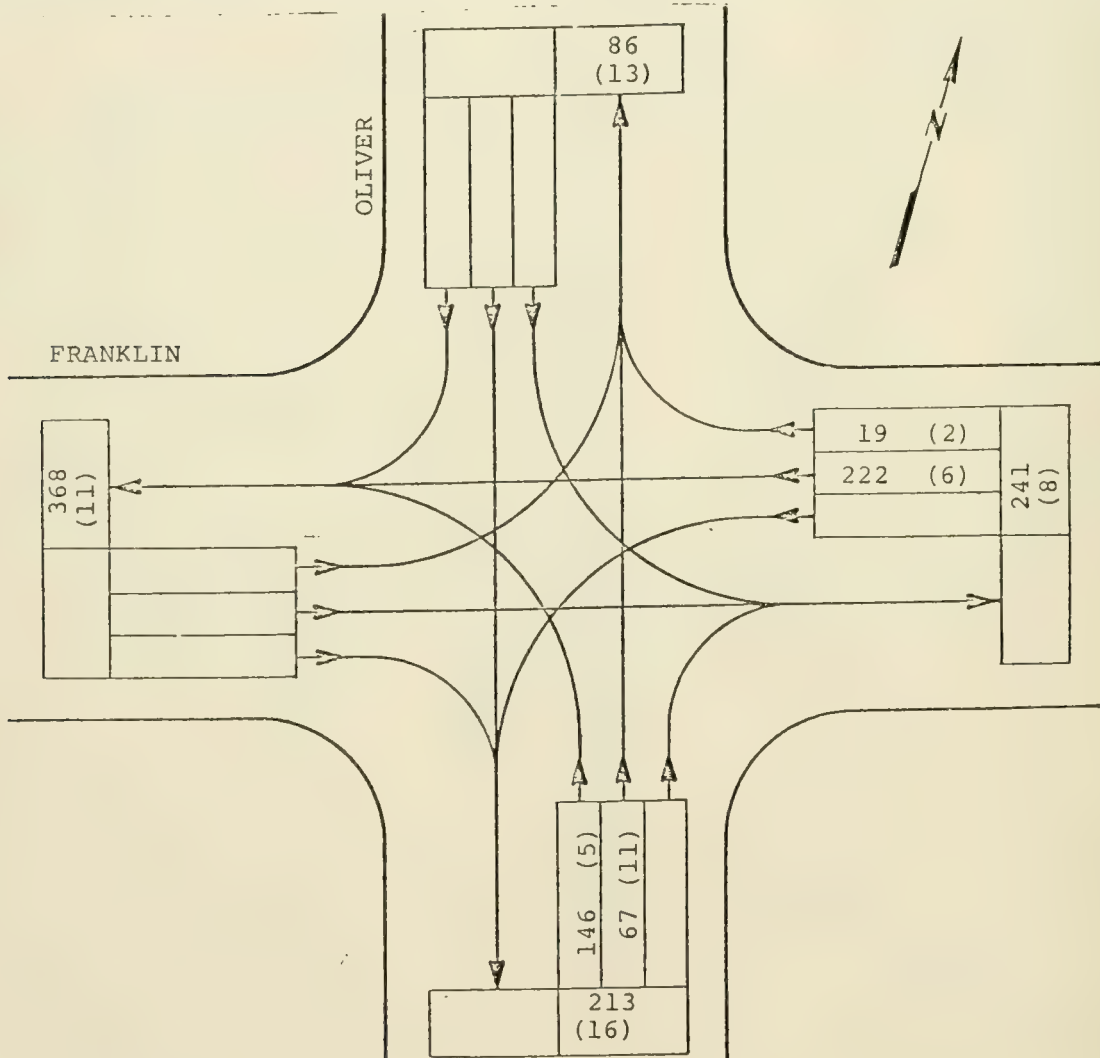
TIME	Franklin St.		Pearl St.								TOTAL
STARTS	Westbound		Northbound								HALF HOURLY
-- M	5	2	4	5							TALLY
7:00-7:30	31	36	21	28							116
7:30-8:00	58	61	43	71							233
8:00-8:30	120	98	76	119							413
8:30-9:00	106	58	63	114							341
9:00-9:30	48	86	45	88							317
9:30-10:00	111	48	34	82							275
10:00-10:30	123	53	38	71							265
10:30-11:00	119	36	42	101							298
11:00-11:30	117	32	56	83							288
11:30-12:00	114	45	44	91							294
12:00-12:30	98	51	32	73							254
12:30-1:00	108	43	64	61							276
1:00-1:30	95	49	64	61							269
1:30-2:00	83	61	73	55							272
2:00-2:30	81	69	69	62							281
2:30-3:00	66	39	72	69							246
3:00-3:30	73	42	39	98							252
3:30-4:00	59	49	48	87							243
4:00-4:30	73	56	55	93							277
4:30-5:00	71	78	64	121							340
5:00-5:30	53	74	79	132							338
5:30-6:00	39	58	53	94							244
6:00-6:30											
6:30-7:00											
7:00-7:30											
7:30-8:00											
8:00-8:30											
8:30-9:00											
9:00-9:30											
9:30-10:00											
10:00-10:30											
10:30-11:00											
TOTAL	1882	1232	1169	1849							GRAND TOTAL
TOTAL OF L.S. & R.	3114		3018								6132



Vanasse/Hangen Design, Inc.  
Boston, Massachusetts

# INTERSECTION TURNING MOVEMENT COUNT

CITY BOSTON, MA DATE 11/13/80 DAY of WEEK Thur.  
INTERSECTION Franklin St. & Oliver St.



STREET		ENTERING VOLUME	PERCENT of FLOW	LENGTH of COUNT	
				Time	Number of Hours
Franklin St.	(WB)	241 (8)	53.1	8:00-9:00AM	AM
Oliver St.	(NB)	213 (16)	46.9		PEAK HOUR
				5% Trucks	
				VEHICLES COUNTED	
				ALL	XXX
				TRUCKS	(XX)
TOTAL		454 (24)	100%		

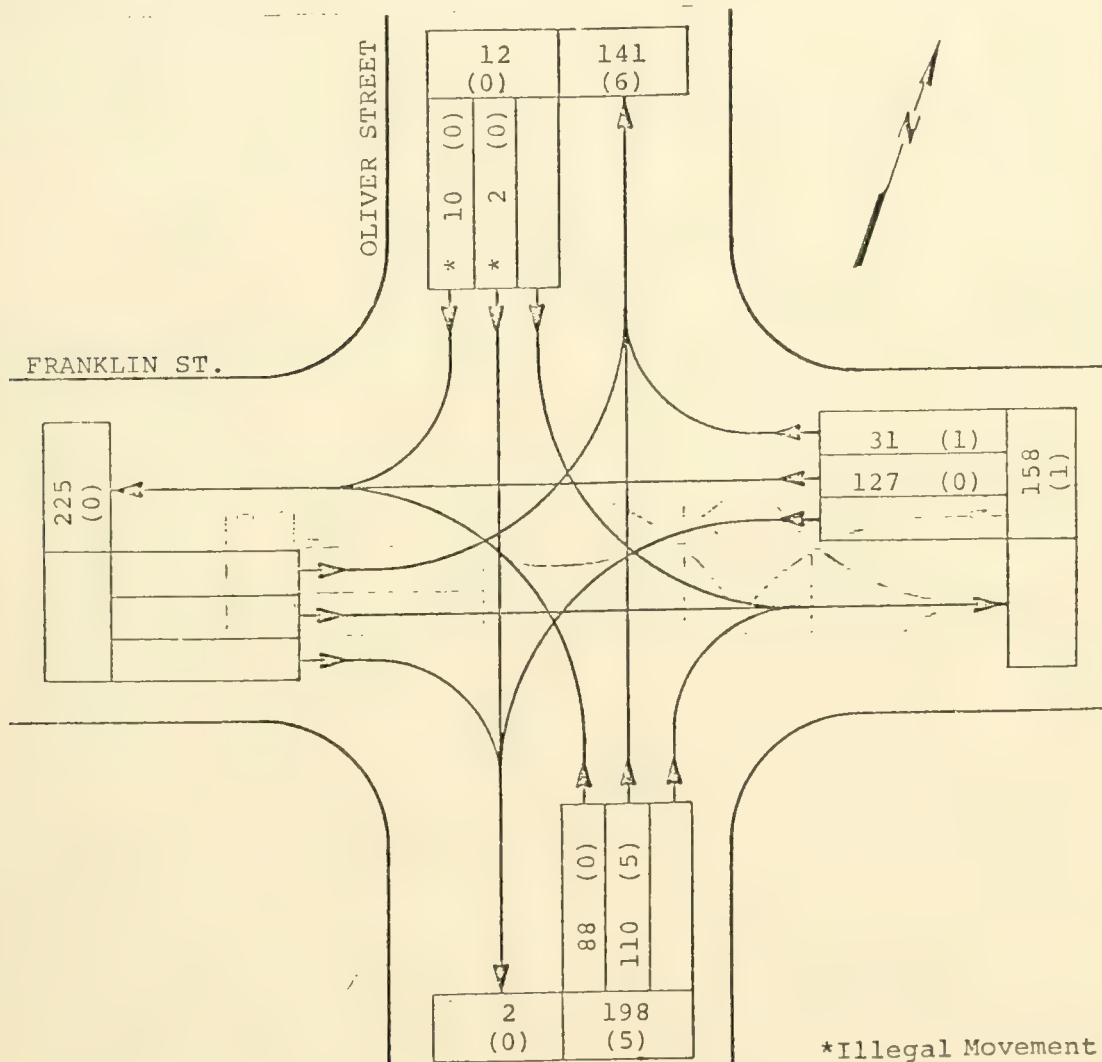


Vanasse/Hangen Design, Inc.  
Boston, Massachusetts

VH #30-101

## INTERSECTION TURNING MOVEMENT COUNT

CITY BOSTON, MA DATE 11/13/80 DAY of WEEK Thur.  
INTERSECTION Franklin St. & Oliver St.



STREET		ENTERING VOLUME	PERCENT of FLOW	LENGTH of COUNT	
				Time	Number of Hours
Franklin St.	(WB)	158 (1)	42.9	4:15-5:15PM	PM
Oliver St.	(NB)	198 (5)	53.8		PEAK HOUR
Oliver St. *	(SB)	12 (0)	* 3.3		
				2% Trucks	
				VEHICLES COUNTED	
				ALL	XXX
TOTAL				TRUCKS	(XX)

City BOSTON - PROPER  
Intersection FRANKLIN ST & OLIVER ST

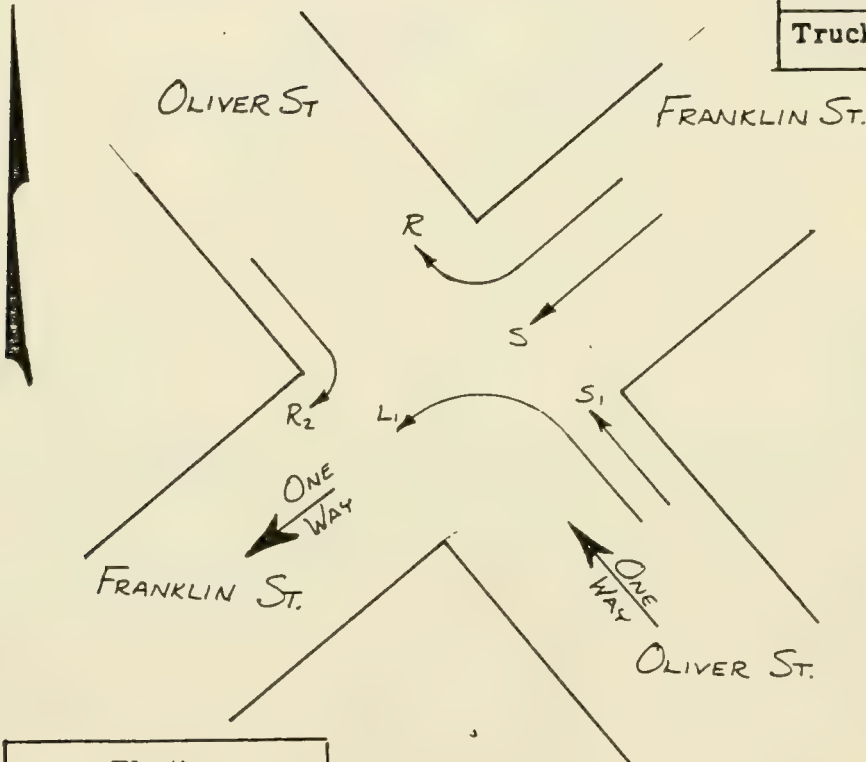
INT. NO. 100 (BTPD # 553) Date 5/20/83 Day of Week FRIDAY

INTERSECTION TURNING MOVEMENT COUNT

**553**

OK

Vehicles Counted	
All	X
Pass. Cars	
Trucks	



Weather <u>CLOUDY/FOG</u>
Count Taken By <u>JOAN SCHUBERT</u>

Length of Count	
Time	Number of Hours
<u>7AM - 6PM</u>	<u>11 HRS.</u>

Street	Entering Volume	Flow Percent	Comments
FRANKLIN ST. (WB)	2307	45 %	
OLIVER ST. (NB)	2247	43 %	
OLIVER ST. (SB)	628	12 %	
Total	5182	100%	



## TRAFFIC MOVEMENT SUMMARY TABLE

553

Location FRANKLIN ST & OLIVER ST. City or Town BOSTON - PROPERDate 5/20/83 Day of Week FRIDAY Weather CLD Recorder JS

Time Starts 7:00AM	FRANKLIN ST. (WB)		OLIVER ST. (NB) (SB)									Total Half Hour Tally
	S	R	L <sub>1</sub>	S <sub>1</sub>	R <sub>2</sub>							
7:00-7:30	39	7	40	35	4							125
7:30-8:00	60	10	51	51	10							182
8:00-8:30	111	41	99	84	14							349
8:30-9:00	82	44	56	75	12							269
9:00-9:30	95	37	60	85	20							297
9:30-10:00	85	32	34	84	24							259
10:00-10:30	80	29	30	67	27							233
10:30-11:00	73	29	49	60	35							246
11:00-11:30	95	38	56	97	17							303
11:30-12:00	102	33	38	51	22							246
12:00-12:30	99	31	48	68	27							273
12:30-1:00	81	39	31	65	18							234
1:00-1:30	117	22	35	50	30							254
1:30-2:00	91	34	32	43	38							238
2:00-2:30	83	16	17	43	27							186
2:30-3:00	66	13	24	34	52							189
3:00-3:30	74	21	41	34	55							225
3:30-4:00	69	20	27	31	24							171
4:00-4:30	66	18	26	66	24							200
4:30-5:00	52	21	35	81	40							229
5:00-5:30	64	17	34	86	52							253
5:30-6:00	55	16	32	62	56							221
6:00-6:30												
6:30-7:00												
7:00-7:30												
7:30-8:00												
8:00-8:30												
8:30-9:00												
9:00-9:30												
9:30-10:00												
10:00-10:30												
10:30-11:00												
TOTAL	1739	568	895	1352	628							GRAND TOTAL
Total of L S & R	2307		2247		628							5182



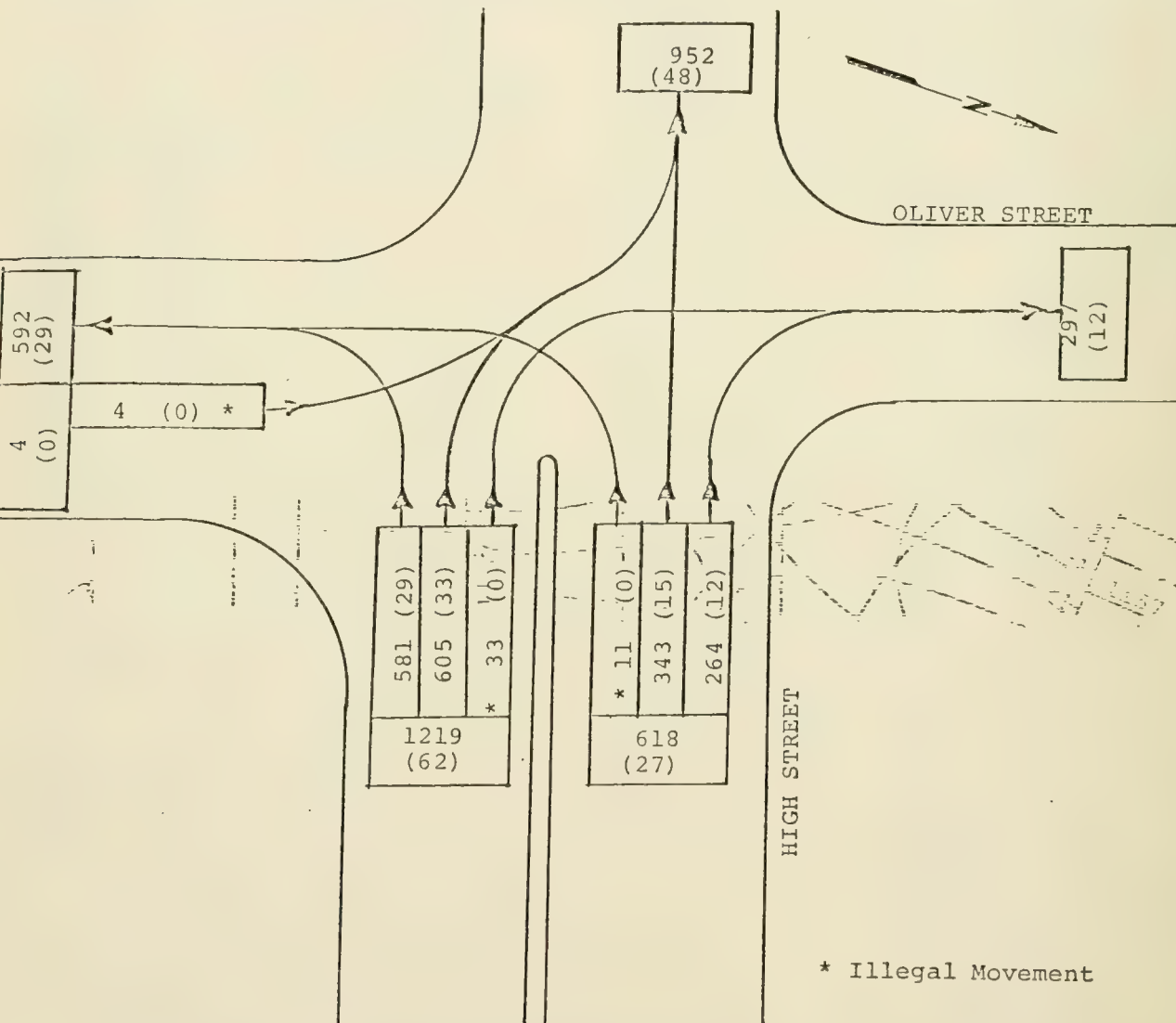


Vanasse/Hangen Design, Inc.  
Boston, Massachusetts

VH 30-101

## INTERSECTION TURNING MOVEMENT COUNT

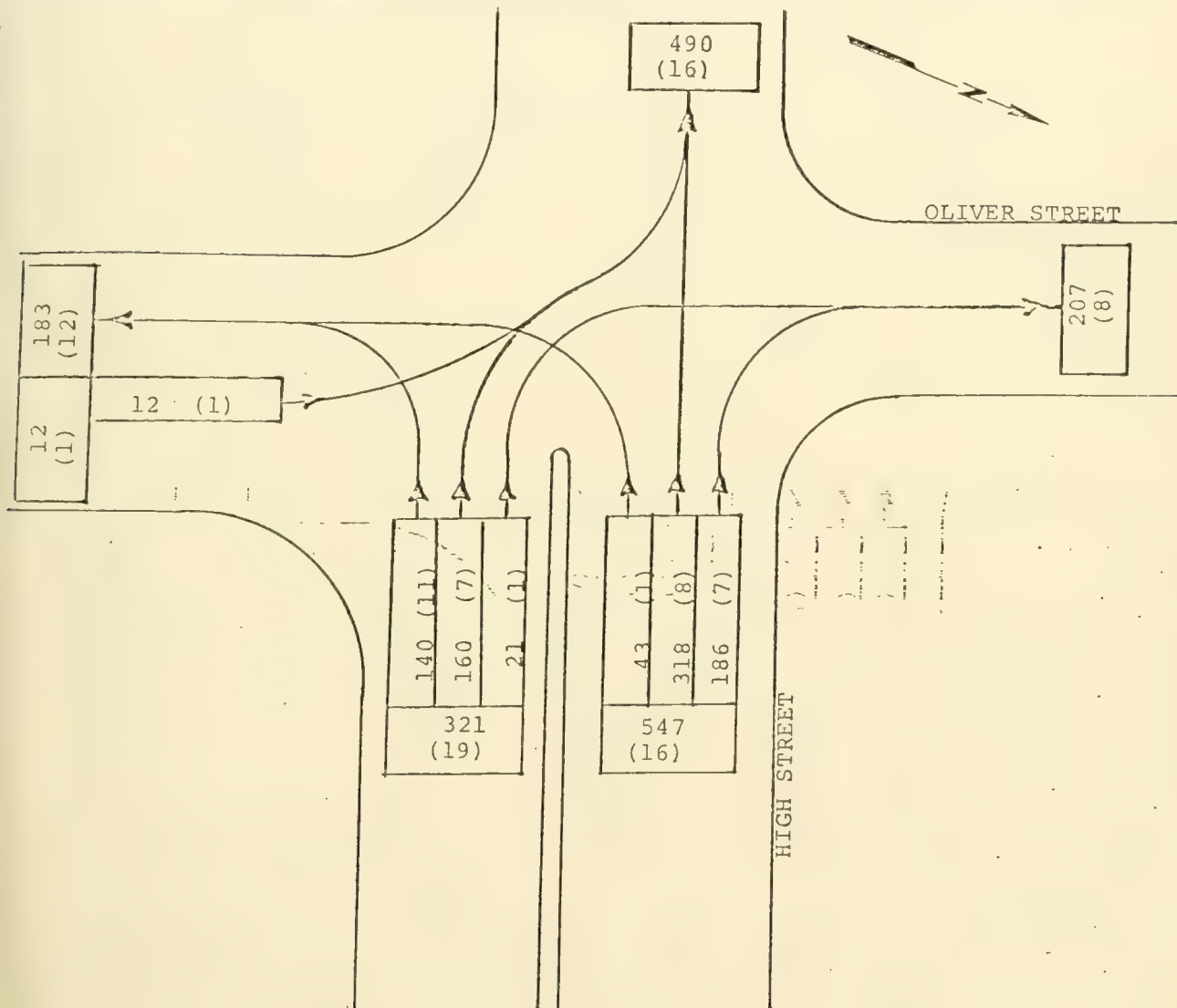
CITY BOSTON, MA DATE 11/12/80 DAY of WEEK Wed.  
INTERSECTION High St. & Oliver St.



STREET		DIRECTIONAL DISTRIBUTION		PERCENT of A.D.T.	TIME of COUNT
Ramp	WB	1219	(62)	66.2	AM PEAK HOUR 8:00A-9:00A
High St.	WB	618	(27)	33.6	
Oliver St.	NB	4	(0)	.2	
					VEHICLES COUNTED
					ALL VEHICLES XXX
					TRUCKS (XX)
TOTAL					PERCENT TRUCKS 4.8 %

## INTERSECTION TURNING MOVEMENT COUNT

CITY BOSTON, MA DATE 11/12/80 DAY of WEEK Wed.  
INTERSECTION High St. & Oliver St.



STREET		DIRECTIONAL DISTRIBUTION	PERCENT of A.D.T.	TIME of COUNT
Ramp	WB	321 (19)	36.5	PM PEAK HOUR 4:30-5:30 PM
High St.	WB	547 (16)	62.2	
Oliver St.	NB	12 (1)	1.3	
				VEHICLES COUNTED
				ALL VEHICLES XXX
				TRUCKS (XX)
TOTAL				PERCENT TRUCKS 4.1 %

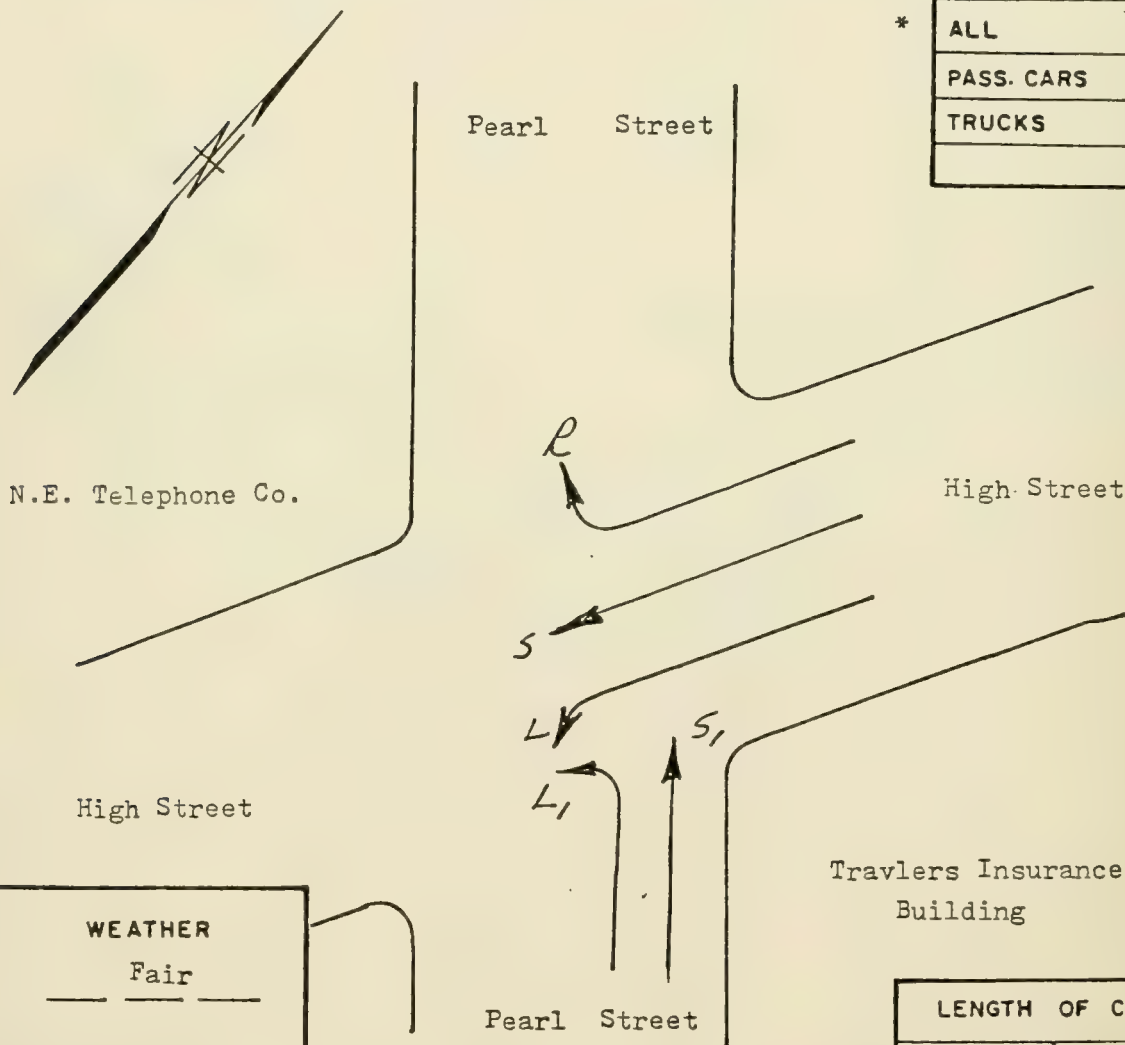
# PLANNING ENGINEERING & DEVELOPMENT

INT. NO.

CITY	Boston Proper
INTERSECTION	High Street & Pearl Street
DATE	9/3/79 DAY OF WEEK Friday

## INTERSECTION TURNING MOVEMENT COUNT #58 BRA

VEHICLES COUNTED	
* ALL	X
PASS. CARS	
TRUCKS	(X)



WEATHER
Fair
COUNT TAKEN BY
E.B.

LENGTH OF COUNT	
TIME	NUMBER OF HOURS
* 7am-6pm	11 hours

STREET		ENTERING VOLUME	FLOW PERCENT	COMMENTS			
High St.	SB	7083	95				
Pearl St.	WB	405	5				
TOTAL		7488	100%				

# PLANNING ENGINEERING & DEVELOPMENT

STA. NO. 58

BRA

## TRAFFIC MOVEMENT SUMMARY TABLE

LOCATION High Street & Pearl Street CITY OR TOWN Boston Proper

DATE 9/3/79 DAY OF WEEK Friday WEATHER Fair RECORDER E.B.

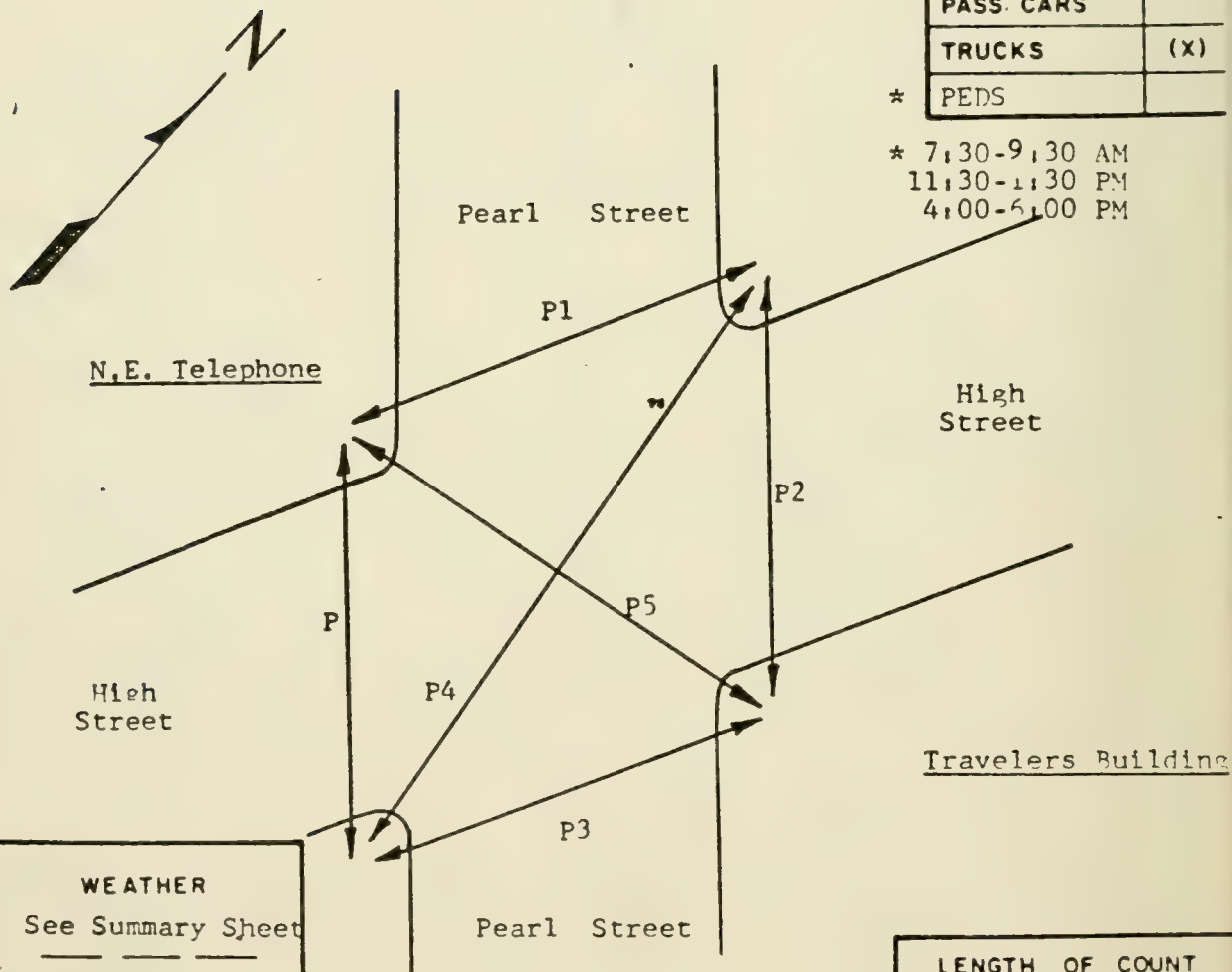
TIME STARTS -- M	High Street			Pearl Street								TOTAL HALF HOURLY TALLY
	Southbound			Westbound								
	L	S	R	L		S						
7:00-7:30	0	191	45	7		5						248
7:30-8:00		247	96	12		6						361
8:00-8:30		368	141	15		4						528
8:30-9:00		329	207	11		13						560
9:00-9:30		303	130	4		7						444
9:30-10:00		202	83	9		8						302
10:00-10:30		207	79	8		8						302
10:30-11:00		246	89	9		9						353
11:00-11:30		254	127	14		9						404
11:30-12:00		301	164	19		12						496
12:00-12:30		266	188	21		14						489
12:30-1:00		233	144	14		15						406
1:00-1:30		209	63	3		10						285
1:30-2:00		187	84	6		6						283
2:00-2:30		198	58	9		7						272
2:30-3:00		205	55	6		9						275
3:00-3:30		173	72	3		8						256
3:30-4:00		163	65	10		14						252
4:00-4:30	Y	160	51	6		7						224
4:30-5:00	Y	216	82	10		9						317
5:00-5:30		191	43	9		11						259
5:30-6:00	0	140	28	4		5						177
6:00-6:30												
6:30-7:00												
7:00-7:30												
7:30-8:00												
8:00-8:30												
8:30-9:00												
9:00-9:30												
9:30-10:00												
10:00-10:30												
10:30-11:00												
TOTAL	0	4983	2094	209		196						GRAND TOTAL
TOTAL OF L.S. & R.		7083		405								7488

CITY \_\_\_\_\_  
 INTERSECTION High Street &  
Pearl Street  
 DATE 2/13/70 DAY OF WEEK Friday

## INTERSECTION TURNING MOVEMENT COUNT # 495

VEHICLES COUNTED	
ALL	X
PASS. CARS	
TRUCKS	(X)
* PEDS	

\* 7:30-9:30 AM  
 11:30-1:30 PM  
 4:00-6:00 PM



WEATHER  
 See Summary Sheet

COUNT TAKEN  
 BY  
W.C.

LENGTH OF COUNT	
TIME	NUMBER OF HOURS
*	6 Hours

STREET	ENTERING VOLUME	FLOW PERCENT	COMMENTS
TOTAL			



# TRAFFIC MOVEMENT SUMMARY TABL

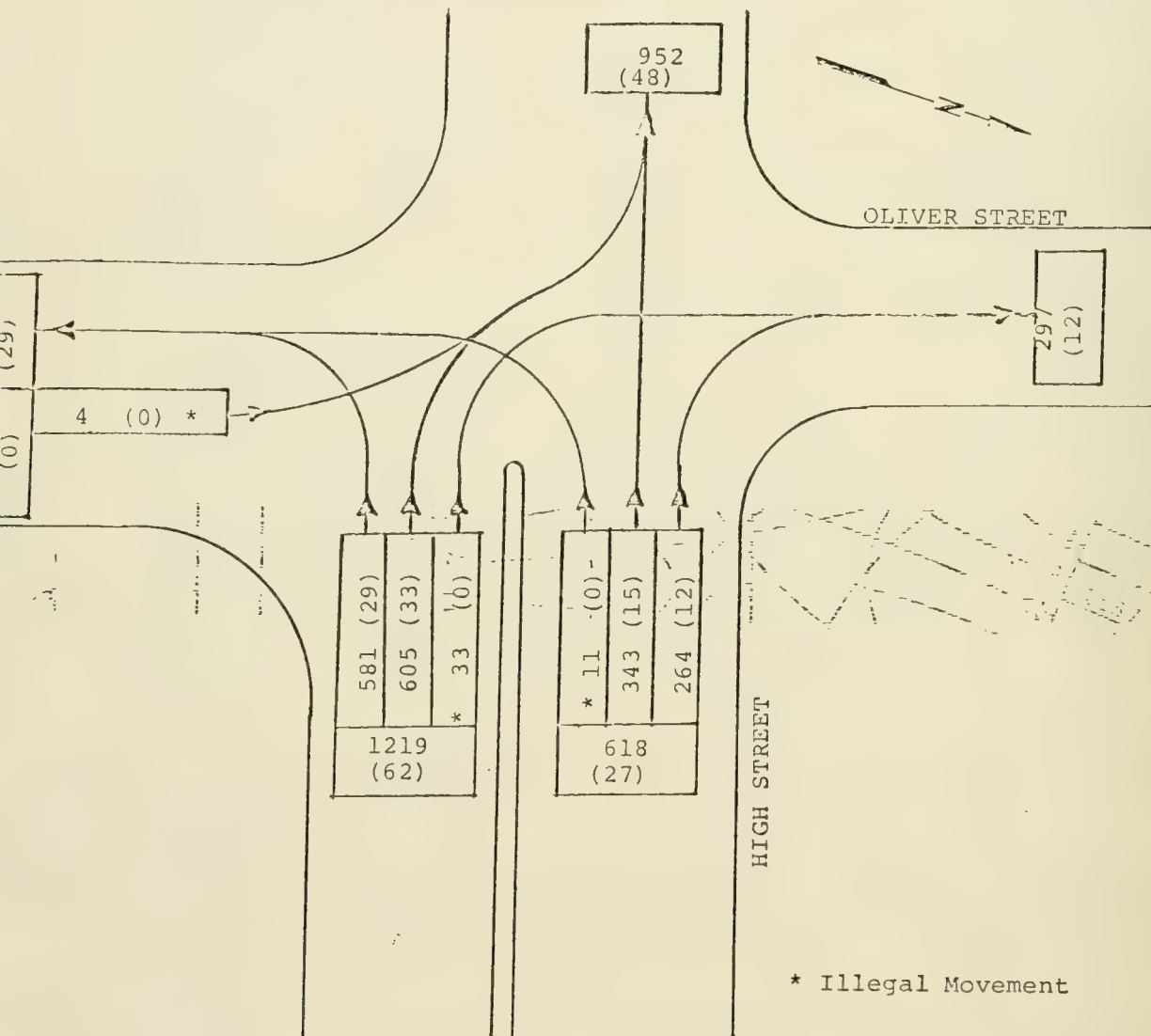
DATE 2/13/70 DAY OF WEEK Friday WEATHER Below RECORDER W.C.

DATE 2/13/70 DAY OF WEEK Friday WEATHER Below RECORDER W.C.

TIME STARTS	See Sketch Plan										TOTAL
	P	P1	P2	P3	P4	P5	.				HALF HOUR TALL
7:00-7:30											
7:30-8:00	34	92	48	26	3	7					210
8:00-8:30	67	411	173	88	9	12					760
8:30-9:00	76	310	139	119	12	21					677
9:00-9:30	35	90	70	42	5	7					249
9:30-10:00											
10:00-10:30											
10:30-11:00											
11:00-11:30											
11:30-12:00	54	129	101	79	14	4					381
12:00-12:30	130	213	185	134	28	22					712
12:30-1:00	122	244	198	121	38	19					742
1:00-1:30	157	356	268	198	18	18					1015
1:30-2:00											
2:00-2:30											
2:30-3:00											
3:00-3:30											
3:30-4:00											
4:00-4:30	35	85	63	25	5	7					220
4:30-5:00	100	190	225	78	14	22					629
5:00-5:30	108	315	180	67	24	18					712
5:30-6:00	45	53	42	33	0	0					173
6:00-6:30											
6:30-7:00											
7:00-7:30											
7:30-8:00											
8:00-8:30											
8:30-9:00											
9:00-9:30											
9:30-10:00											
10:00-10:30											
10:30-11:00											
TOTAL	963	2488	1692	1010	170	157					GRAND TOTAL
TOTAL OF L S & R	6480										6480

# INTERSECTION TURNING MOVEMENT COUNT

CITY BOSTON, MA DATE 11/12/80 DAY of WEEK Wed.  
INTERSECTION High St. & Oliver St.



STREET		DIRECTIONAL DISTRIBUTION	PERCENT of A.D.T.	TIME of COUNT
Ramp	WB	1219 (62)	66.2	AM PEAK HOUR 8:00A-9:00A
High St.	WB	618 (27)	33.6	
Oliver St.	NB	4 (0)	.2	
				VEHICLES COUNTED
				ALL VEHICLES XXX
				TRUCKS (XX)
TOTAL		1841 (89)	100.0	PERCENT TRUCKS 4.8 %



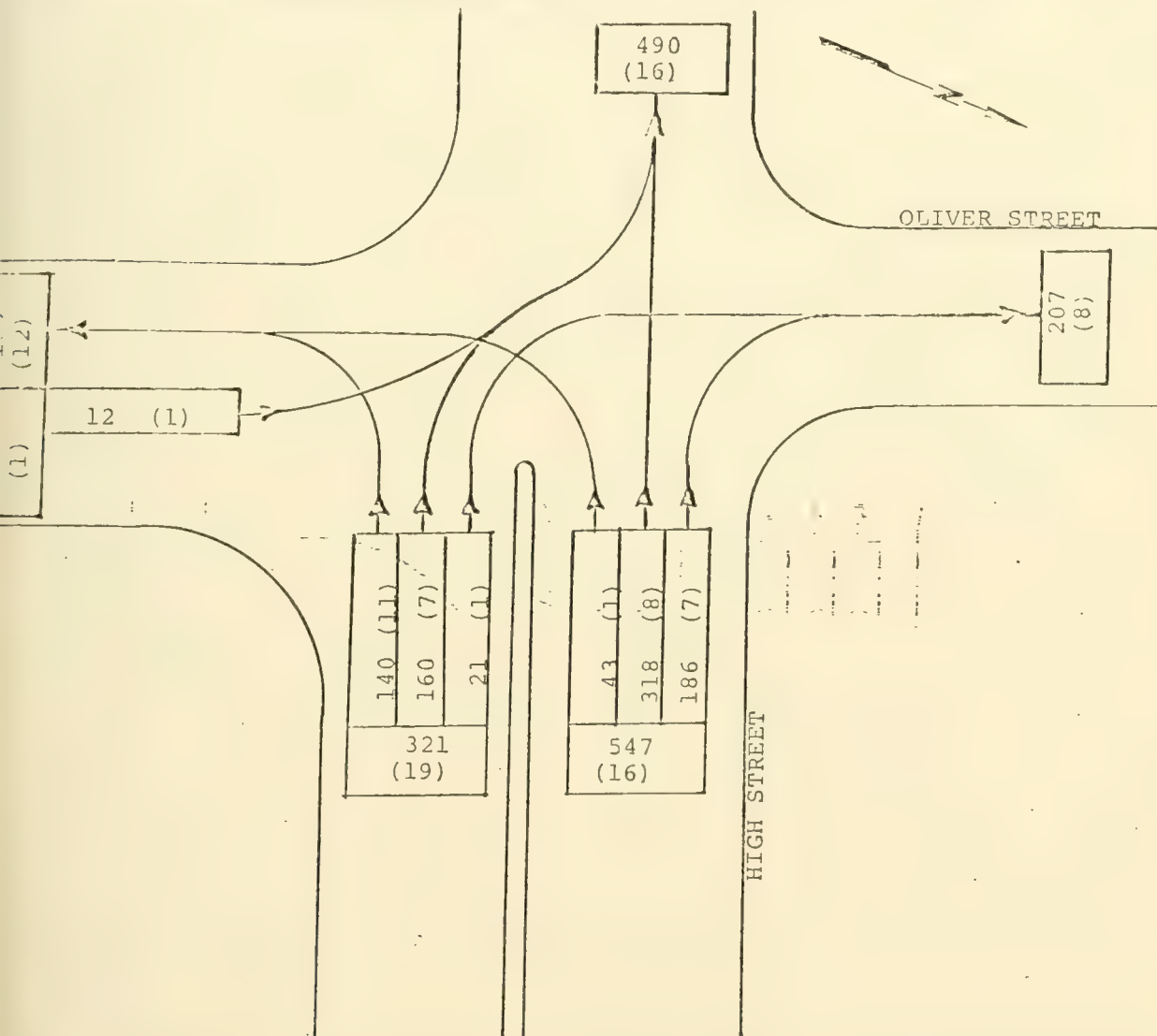
Vanasse/Hangen Design, Inc.  
Boston, Massachusetts

VH 430-101

## INTERSECTION TURNING MOVEMENT COUNT

CITY BOSTON, MA DATE 11/12/80 DAY of WEEK Wed.

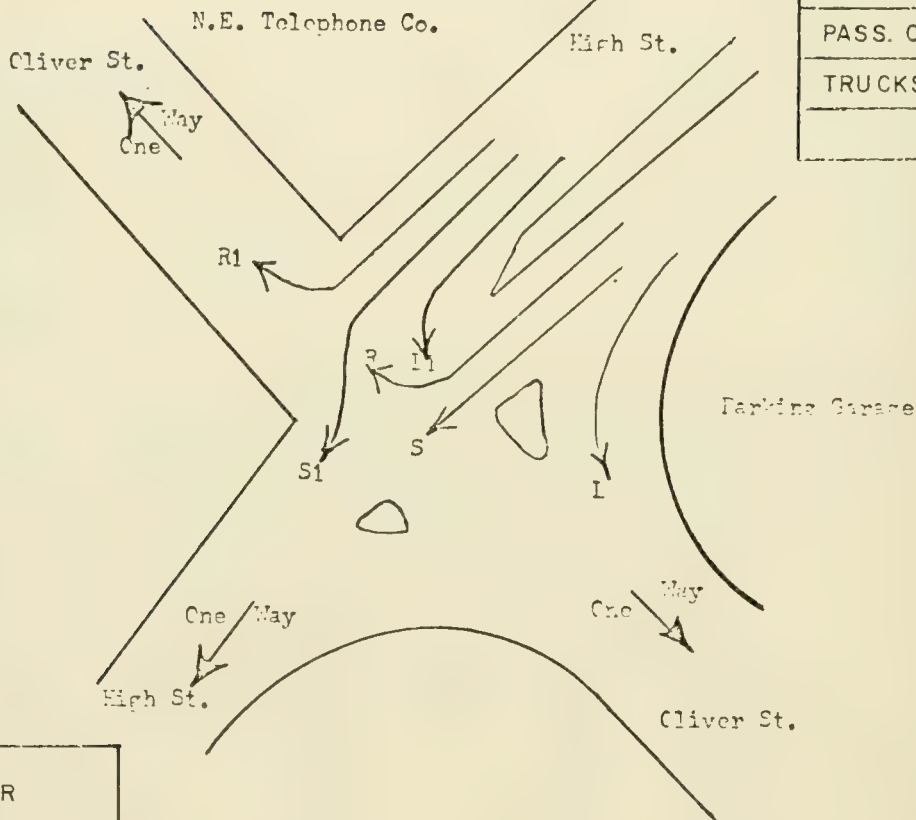
INTERSECTION High St. & Oliver St.



STREET		DIRECTIONAL DISTRIBUTION	PERCENT of A.D.T.	TIME of COUNT
Ramp	WB	321 (19)	36.5	PM PEAK HOUR 4:30-5:30 PM
High St.	WB	547 (16)	62.2	
Oliver St.	NB	12 (1)	1.3	
				VEHICLES COUNTED
				ALL VEHICLES XXX
				TRUCKS (XX)
TOTAL				PERCENT TRUCKS 4.1 %

CITY Boston Proper  
INTERSECTION High Street Off Ramp, &  
Oliver Street  
DATE 3/19/81 DAY OF WEEK Thurs

N



VEHICLES COUNTED	
ALL	X
PASS. CARS	
TRUCKS	(X)

Sunny

D. S., & G. W.

LENGTH OF COUNT	
TIME	NUMBER OF HOURS
7:00-8:00	11 Hours

STREET		ENTERING VOLUME	FLOW PERCENT	COMMENTS			
Artery Off Ramp	SE	8408	63.5				
High Street	SE	4638	36.5				
TOTAL		13046	100%				



# TRAFFIC MOVEMENT SUMMARY TABLE

LOCATION High Street, Off Ramp, & Oliver Street CITY OR TOWN Boston, France

DATE 3/19/81 DAY OF WEEK Thursday WEATHER Sunny RECORDER D.P. & G.

TIME STARTS __ M	Artery Off Ramp			High Street									TOTAL
	Southbound			Southbound									HALF HOUR TALL
	L	S	R	L1	S1	R1							
7:00-7:30	374	226	16	4	114	72							806
7:30-8:00	410	263	6	7	149	93							918
8:00-8:30	384	350	4	6	180	141							1071
8:30-9:00	248	271	19	11	168	113							831
9:00-9:30	229	257	22	3	149	120							781
9:30-10:00	185	203	11	12	131	92							631
10:00-10:30	207	172	28	8	95	83							591
10:30-11:00	170	159	15	12	102	77							531
11:00-11:30	178	181	30	11	116	74							591
11:30-12:00	182	208	21	18	118	98							641
12:00-12:30	180	174	21	13	98	95							581
12:30-1:00	167	169	27	17	89	74							541
1:00-1:30	163	125	15	19	95	69							481
1:30-2:00	196	134	20	19	125	68							511
2:00-2:30	173	133	18	21	94	56							491
2:30-3:00	159	127	17	17	119	64							501
3:00-3:30	130	139	28	24	96	54							471
3:30-4:00	90	83	10	13	100	71							361
4:00-4:30	94	84	10	26	119	71							401
4:30-5:00	107	104	18	18	158	90							491
5:00-5:30	126	111	16	21	129	95							491
5:30-6:00	107	75	29	19	102	103							431
6:00-6:30													
6:30-7:00													
7:00-7:30													
7:30-8:00													
8:00-8:30													
8:30-9:00													
9:00-9:30													
9:30-10:00													
10:00-10:30													
10:30-11:00													
TOTAL	4259	3748	401	319	2646	1873							GRAND TOTAL
TOTAL OF P.P.	8408			4838									1324



# PLANNING ENGINEERING & DEVELOPMENT

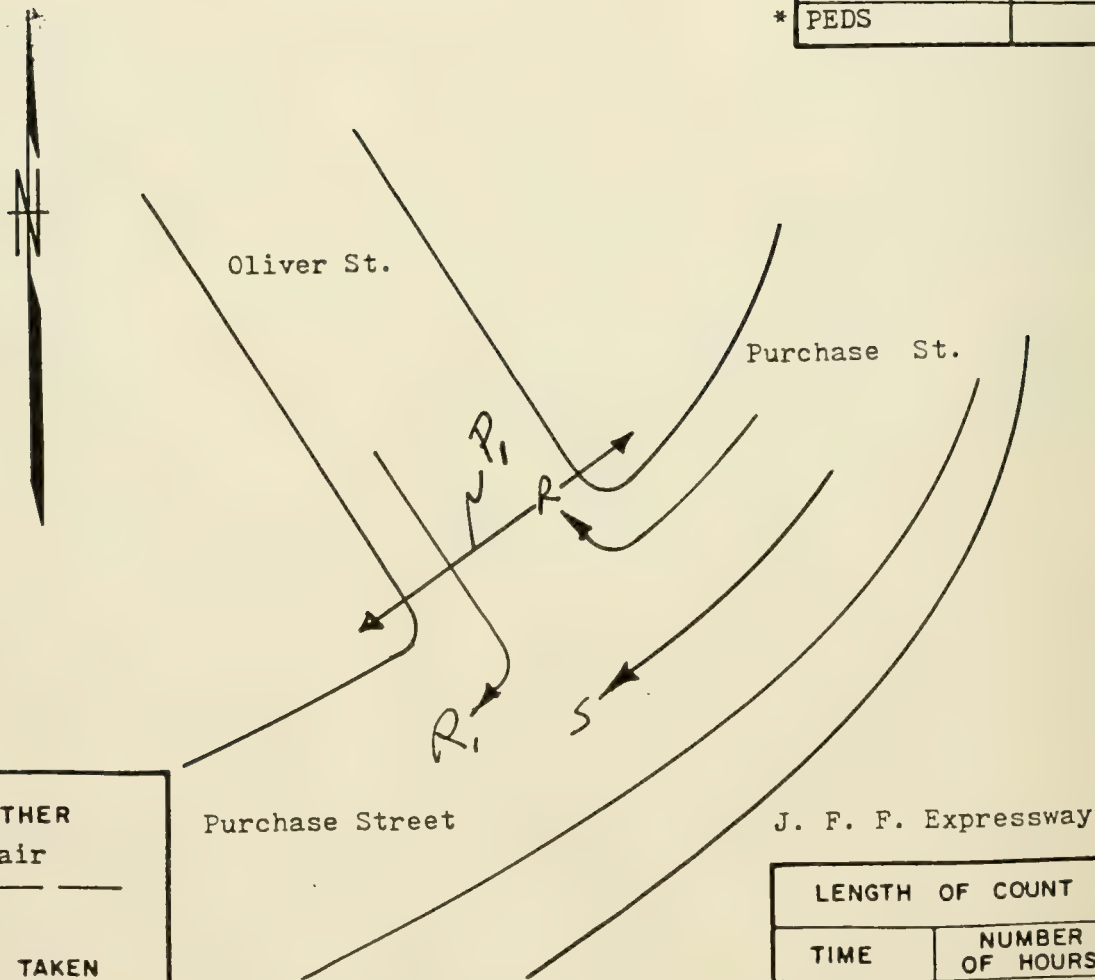
NT. NO.

\* 9/22&23/76

CITY	Boston Proper
INTERSECTION	Oliver Street & Purchase Street
DATE	* DAY OF WEEK Wed-Thur

INTERSECTION TURNING MOVEMENT COUNT #2022 **558**

VEHICLES COUNTED	
* ALL	X
PASS. CARS	
TRUCKS	(X)
* PEDS	



WEATHER

Fair

COUNT TAKEN

BY

J.M.

LENGTH OF COUNT

TIME

NUMBER OF HOURS

7am-6pm

11 hours

STREET		ENTERING VOLUME	FLOW PERCENT	COMMENTS			
Purchase St.	WB	4531	59				
Oliver St.	SB	3178	41				
TOTAL		7709	100%				

# TRAFFIC MOVEMENT SUMMARY TABLE

 LOCATION Oliver St. & Purchase St. CITY OR TOWN Boston Proper

 DATE 9/22&23/76 DAY OF WEEK Wed-Thur WEATHER Fair RECORDER J.M.

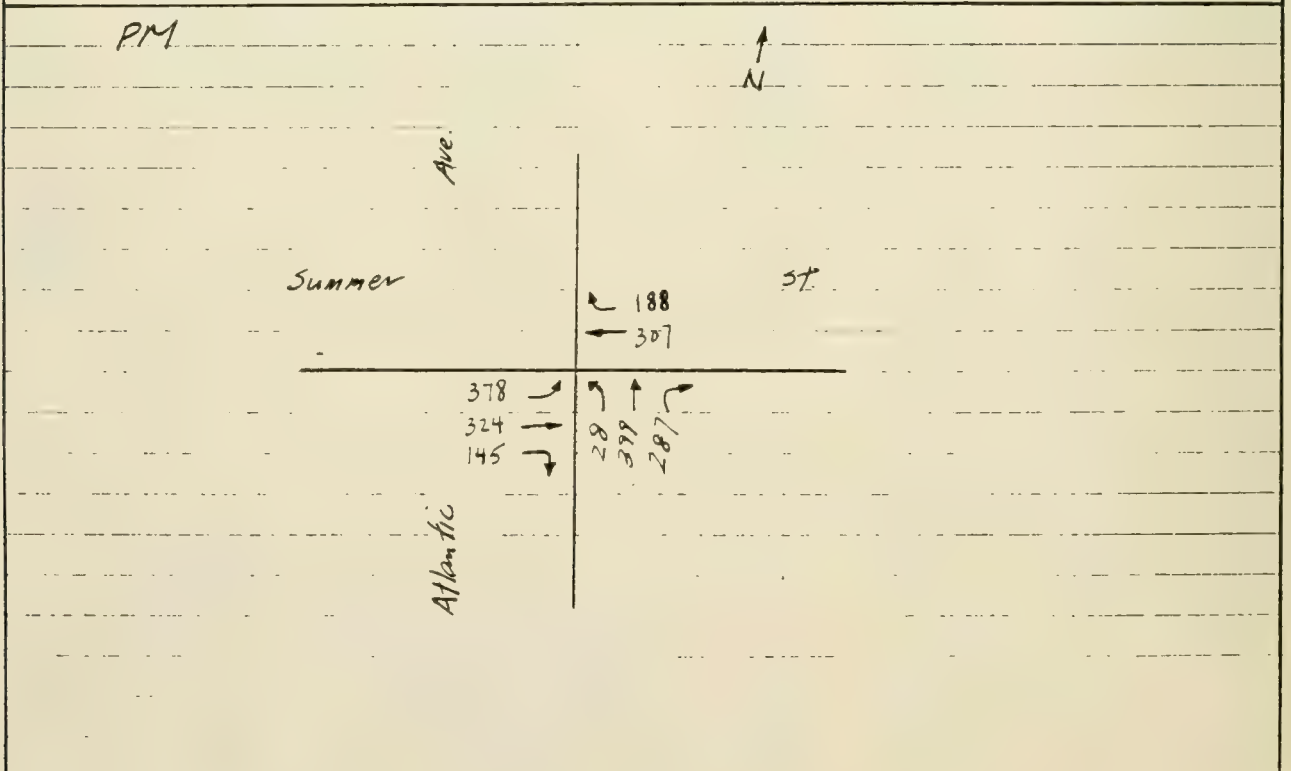
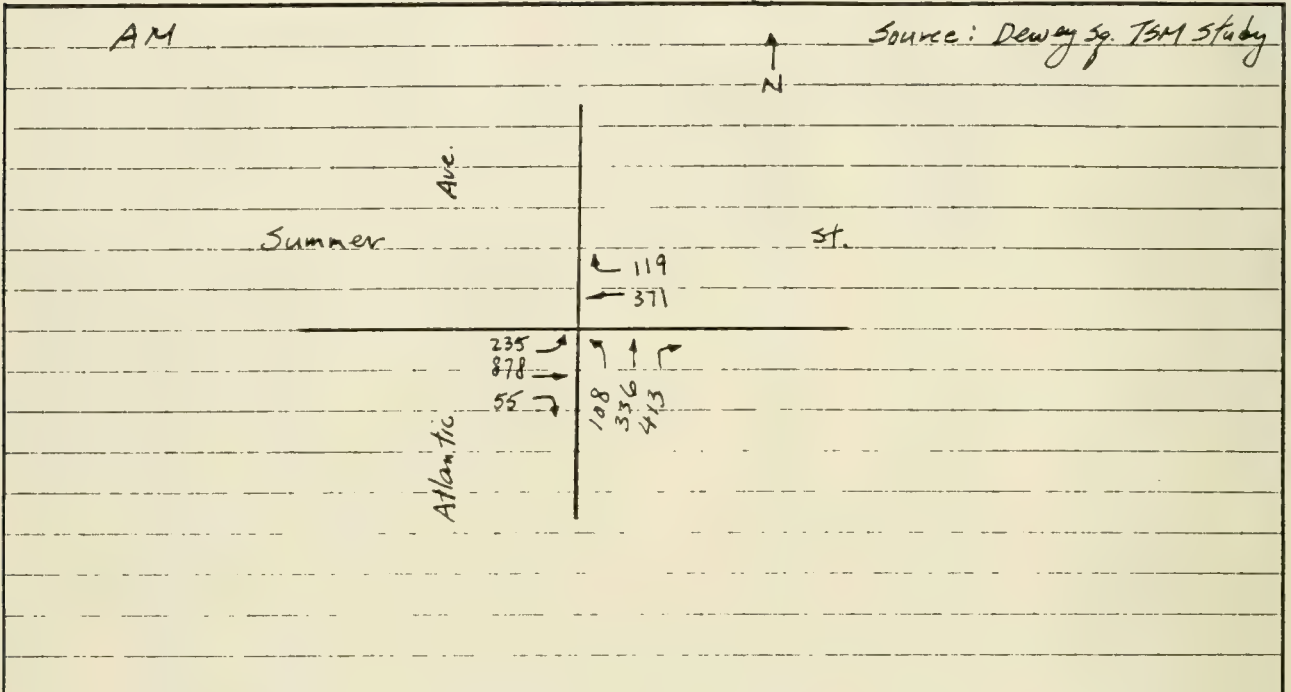
558

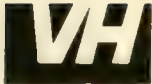
TIME STARTS -- M	Purchase St. Westbound		Oliver St. Southbound								TOTAL HALF HOURLY TALLY
	5	R	R	R	P						
7:00-7:30	99	3	229	2							331
7:30-8:00	194	13	270	15							477
8:00-8:30	276	23	311	26							600
8:30-9:00	294	23	260	35							577
9:00-9:30	165	27	152	27							344
9:30-10:00	156	16	140	15							312
10:00-10:30	148	13	133	13							294
10:30-11:00	126	23	136	7							285
11:00-11:30	132	20	143	9							295
11:30-12:00	150	22	144	16							316
12:00-12:30	176	9	133	20							318
12:30-1:00	195	12	147	21							354
1:00-1:30	188	6	136	32							330
1:30-2:00	195	10	112	26							317
2:00-2:30	238	19	154	22							411
2:30-3:00	188	12	125	22							325
3:00-3:30	205	12	99	7							316
3:30-4:00	196	6	73	17							278
4:00-4:30	240	8	88	26							336
4:30-5:00	252	11	77	32							340
5:00-5:30	269	8	70	53							347
5:30-6:00	146	4	46	18							196
6:00-6:30											
6:30-7:00											
7:00-7:30											
7:30-8:00											
8:00-8:30											
8:30-9:00											
9:00-9:30											
9:30-10:00											
10:00-10:30											
10:30-11:00											
TOTAL	4228	303	3178	460							GRAND TOTAL
TOTAL OF L.S. & R.	4531		3178		<div></div>		<div></div>		<div></div>		7709



**Vanasse / Hangen Engineering, Inc.**  
Consulting Engineers & Planners  
184 High Street, Boston, Massachusetts 02110  
617 / 482-1870

JOB: International Place JOB No. 0923  
LOCATION: \_\_\_\_\_ SHEET \_\_\_\_\_ OF \_\_\_\_\_  
CALCULATED BY: BGT DATE: \_\_\_\_\_  
CHECKED BY: \_\_\_\_\_ DATE: \_\_\_\_\_  
TITLE: Turning Movement Counts

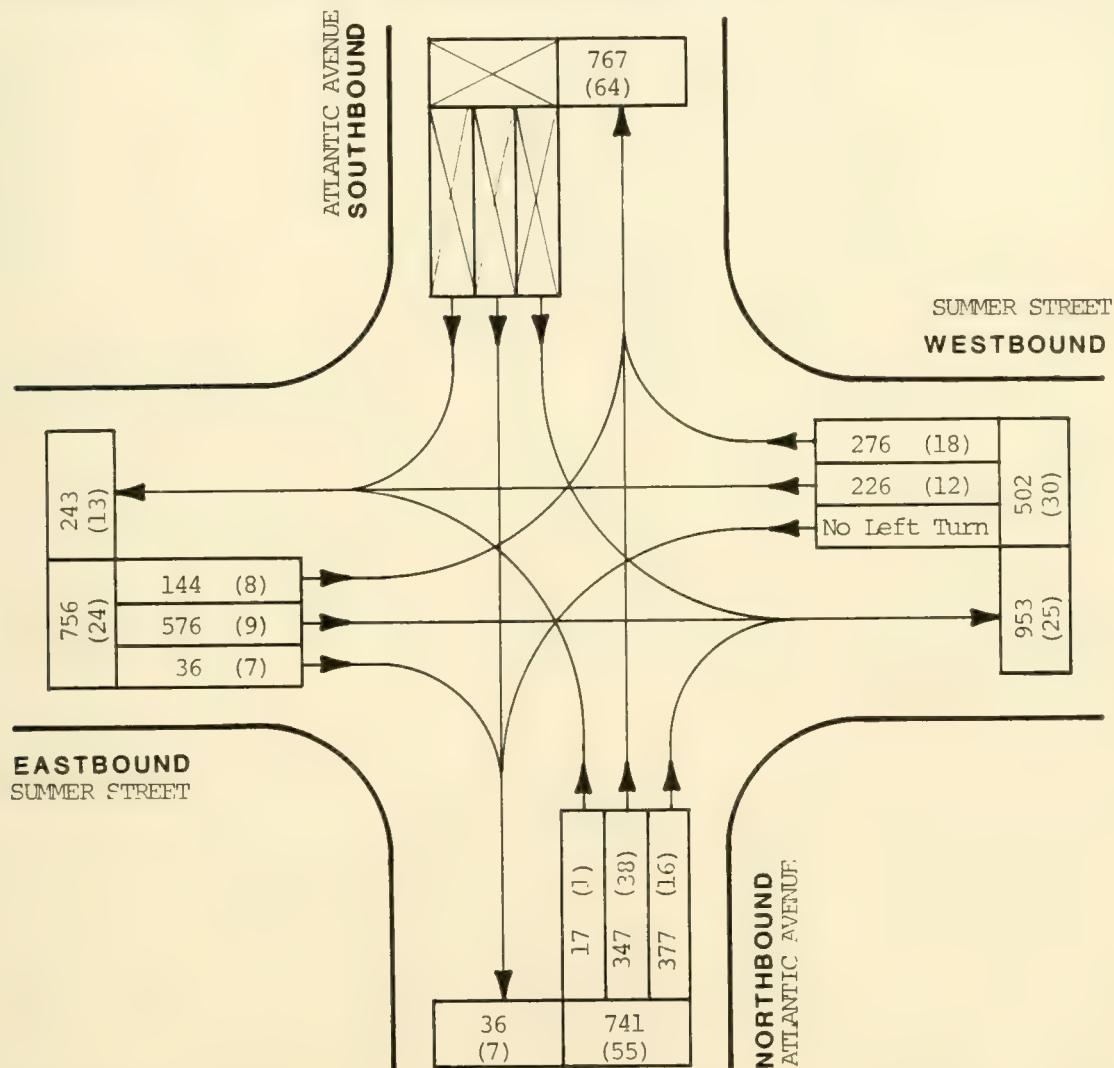




**Vanasse / Hangen Associates, Inc.**  
 Transportation Engineers & Planners  
 184 High Street, Boston, Massachusetts 02110  
 617 / 482-0749

# INTERSECTION TURNING MOVEMENT COUNT

CITY Boston, MA DATE 12/4/81 DAY of WEEK Friday  
 INTERSECTION Atlantic Avenue @ Summer Street JOB No. 0121-10



STREET		ENTERING VOLUME	PERCENT OF FLOW	TIME of COUNT
ATLANTIC AVENUE	N.B.	741 (55)	37%	7:15AM - 8:15AM
SUMMER STREET	E.B.	756 (24)	38%	
SUMMER STREET	W.B.	502 (30)	25%	
				AM Peak Hour
				VEHICLES COUNTED
				ALL VEHICLES XXX
				TRUCKS (XX)
TOTAL		1999 (109)	100%	PERCENT TRUCKS 5.4 %

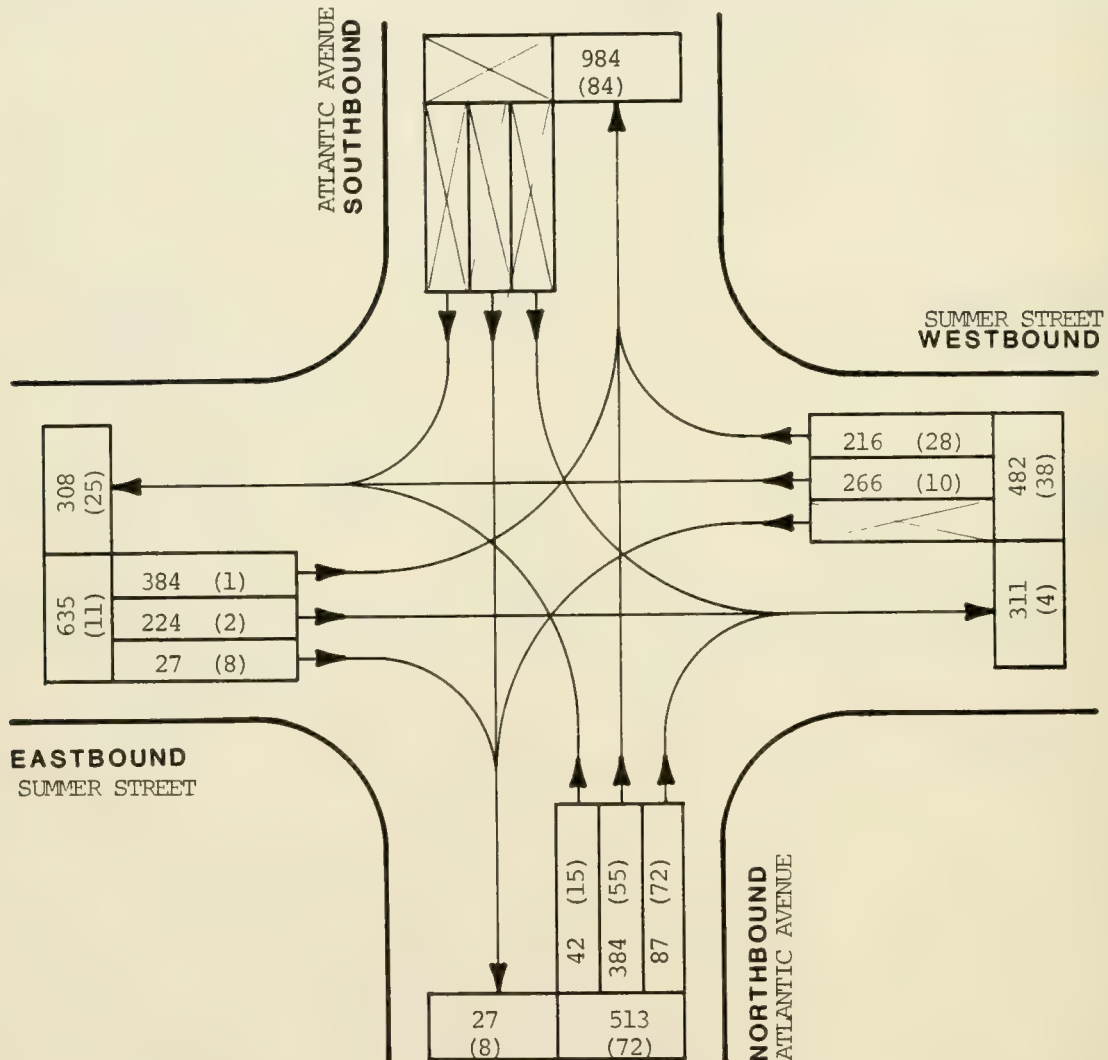




**Vanasse / Hangen Associates, Inc.**  
 Transportation Engineers & Planners  
 184 High Street, Boston, Massachusetts 02110  
 617 / 482-0749

## INTERSECTION TURNING MOVEMENT COUNT

CITY Boston, MA DATE 11/20/81 DAY of WEEK Friday  
 INTERSECTION Atlantic Avenue @ Summer Street JOB No. 0121-10



STREET	ENTERING VOLUME	PERCENT OF FLOW	TIME of COUNT
SUMMER STREET W.B.	482 (38)	30%	4:45PM - 5:45PM
SUMMER STREET E.B.	635 (11)	39%	
ATLANTIC AVENUE N.B.	513 (72)	31%	
			PM Peak Hour
			VEHICLES COUNTED
			ALL VEHICLES XXX
			TRUCKS (XX)
TOTAL	1630 (121)	100%	PERCENT TRUCKS 7.4 %





**Vanasse / Hangen Engineering, Inc.**

Consulting Engineers & Planners  
184 High Street, Boston, Massachusetts 02110  
617 / 482-1870

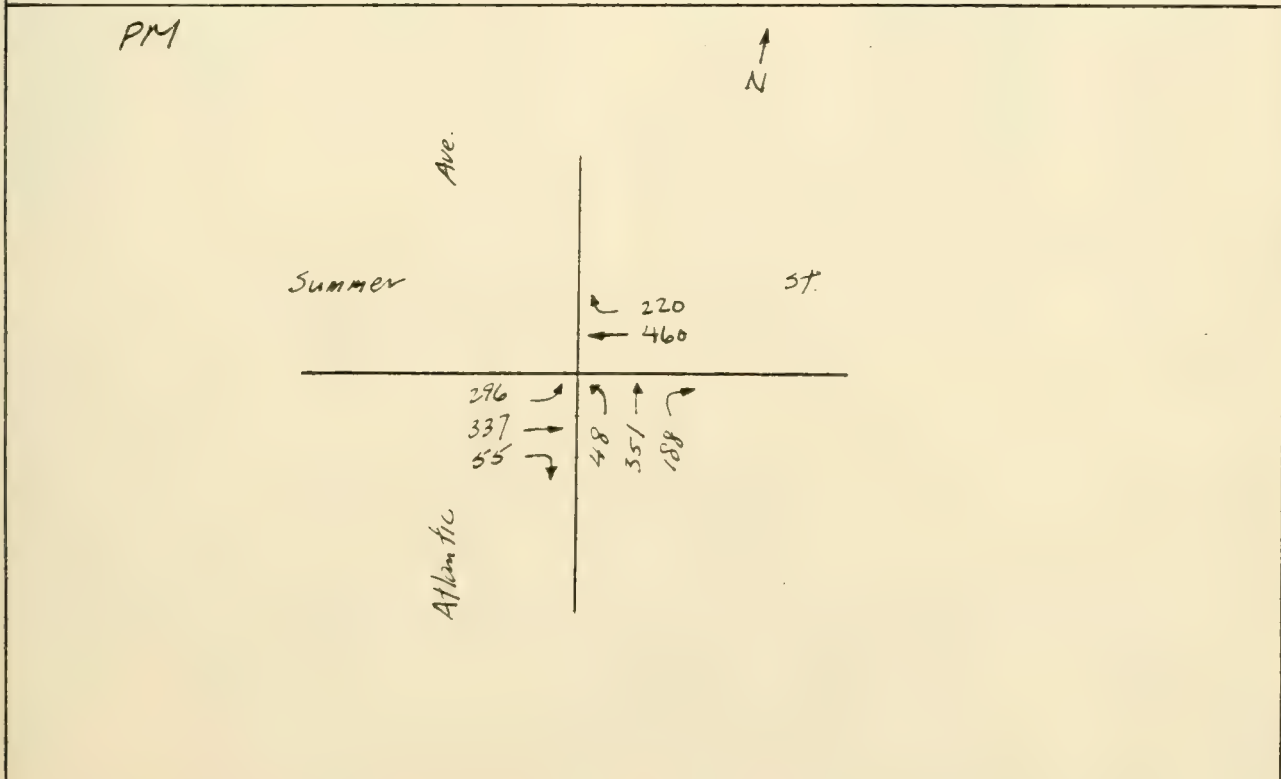
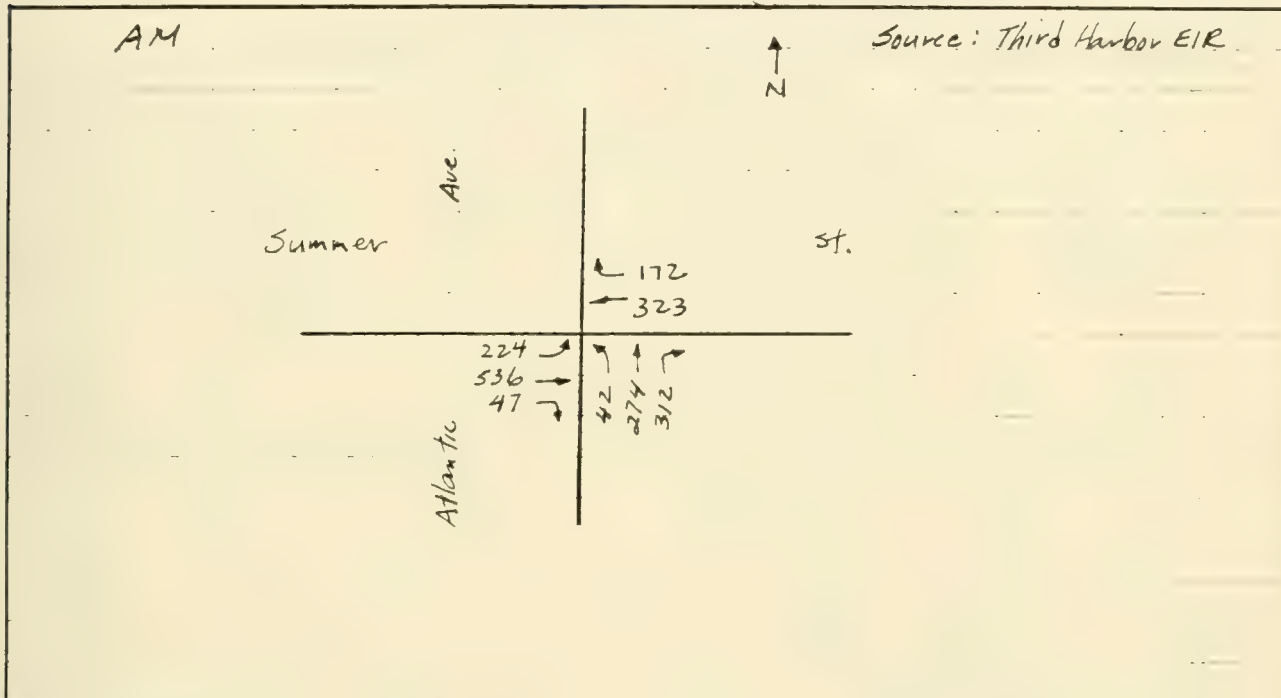
JOB: International Place JOB No. 0923

LOCATION: \_\_\_\_\_ SHEET \_\_\_\_\_ OF \_\_\_\_\_

CALCULATED BY: BG DATE \_\_\_\_\_

CHECKED BY: \_\_\_\_\_ DATE \_\_\_\_\_

TITLE Turning Movement Counts



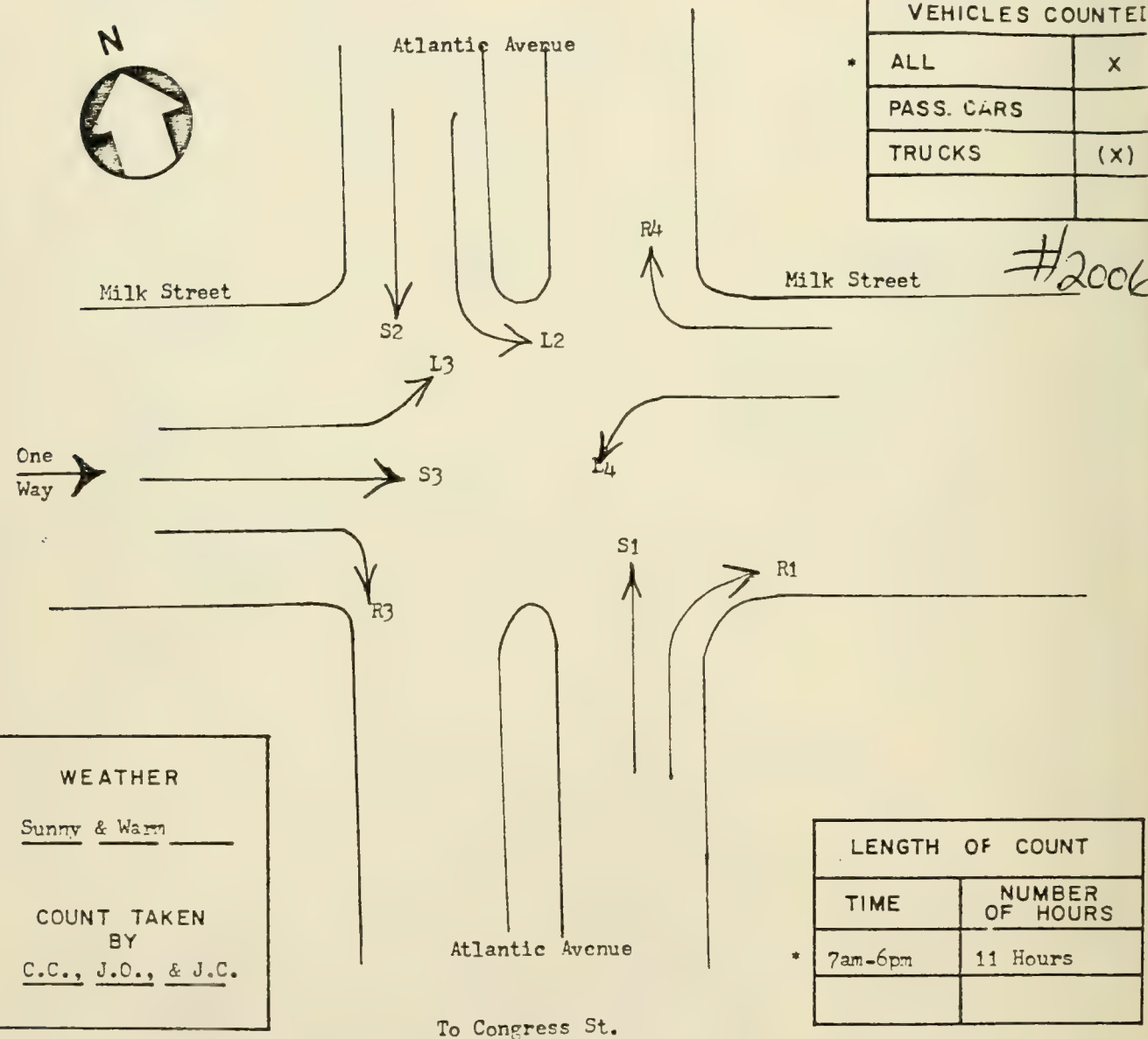
INT. NO. 242

CITY Boston Proper

INTERSECTION Atlantic Ave. & Milk Street

DATE 7/10/80 DAY OF WEEK Thursd

INTERSECTION TURNING MOVEMENT COUNT #2



STREET		ENTERING	FLOW	COMMENTS
		VOLUME	PERCENT	
Atlantic Avenue	WB	7015	52.3	
Atlantic Avenue	SB	3320	23.3	
Milk Street	EB	2119	14.8	
Milk Street	WB	1219	8.6	
TOTAL		14244	100 %	

# TRAFFIC MOVEMENT SUMMARY TABLE

ON Atlantic Avenue & Milk Street

CITY OR TOWN Boston Proper

DATE 7/10/80

DAY OF WEEK Thursday

WEATHER Sunny & Warm

RECORDER C.C., J.C. & J.C.

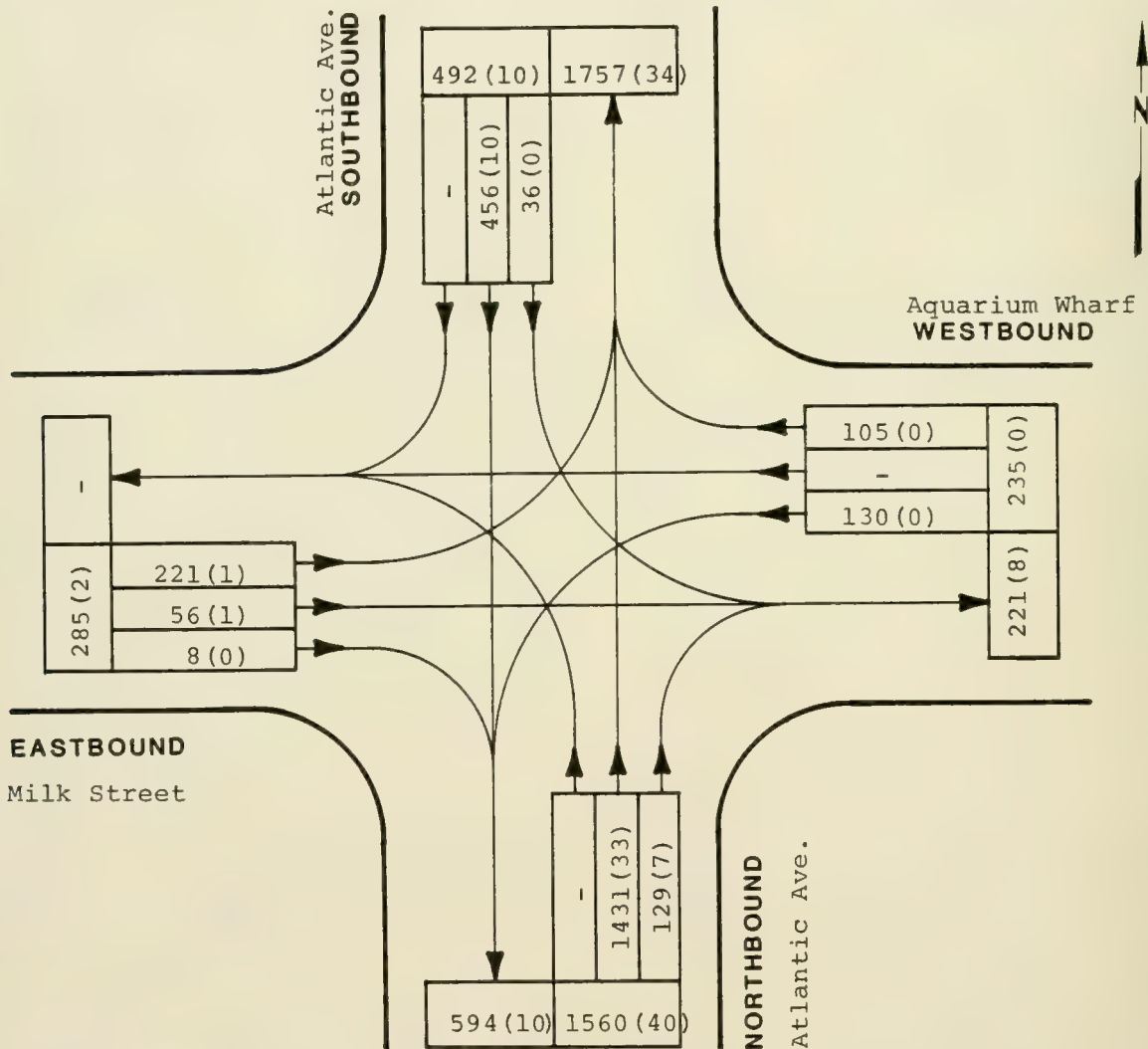
TIME STARTS -- M	Atlantic Avenue Northbound			Atlantic Avenue Southbound			Milk Street East Bound			Milk Street Westbound			TOTAL HALF H TAL
		S1	R1	L2	S2		L3	S3	R3	L4		R4	
7:00-7:30		175	20	6	158		13	23	1	7		3	406
7:30-8:00		206	33	8	219		14	37	4	5		6	530
8:00-8:30		191	66	19	199		28	56	0	16		12	581
8:30-9:00		249	80	20	159		20	68	2	5		11	614
9:00-9:30		228	69	15	104		15	79	0	8		9	52
9:30-10:00		205	58	13	119		19	59	1	16		17	50
10:00-10:30		192	57	5	82		21	34	1	7		8	40
10:30-11:00		227	59	11	136		25	54	2	13		9	53
11:00-11:30		237	68	13	122		40	68	1	12		12	57
11:30-12:00		276	71	21	118		41	65	3	19		27	64
12:00-12:30		224	82	24	130		55	55	4	20		38	63
12:30-1:00		223	50	20	87		29	46	1	29		29	514
1:00-1:30		229	71	13	134		30	50	4	48		45	62
1:30-2:00		210	60	15	124		32	41	2	41		22	54
2:00-2:30		161	33	11	99		26	21	6	35		26	41
2:30-3:00		232	58	14	142		34	37	3	40		16	57
3:00-3:30		308	69	9	193		47	26	4	46		30	73
3:30-4:00		461	35	3	185		104	20	3	52		48	91
4:00-4:30		526	32	4	141		119	12	3	55		43	93
4:30-5:00		524	41	10	159		158	23	2	63		46	102
5:00-5:30		668	27	14	129		137	29	5	88		29	112
5:30-6:00		479	48	8	113		120	36	1	73		35	91
6:00-6:30													
6:30-7:00													
7:00-7:30		440	146	39	358		48	124	2	21		23	120
7:30-8:00													
8:00-8:30													
8:30-9:00		1172	68	24	281		295	52	7	151		75	2150
9:00-9:30													
9:30-10:00													
10:00-10:30													
10:30-11:00													
TOTAL		6431	1187	276	3052		1127	935	53	698		521	GRA TOT
TOTAL OF		7618			3328		2117			1219			1420



Vanasse / Hangen Associates, Inc.  
Transportation Engineers & Planners  
184 High Street, Boston, Massachusetts 02110  
617 / 482-0749

## INTERSECTION TURNING MOVEMENT COUNT

CITY Boston, MA DATE 7/26/84 DAY of WEEK Thursday  
INTERSECTION Milk St./Atlantic Ave. JOB No. 0923



STREET	ENTERING VOLUME	PERCENT OF FLOW	TIME of COUNT
Atlantic Ave. (NB)	1560 (40)	61.0%	5:00 - 6:00 PM PM Peak Hour
Atlantic Ave. (SB)	492 (10)	19.0%	
Milk St. (EB)	285 (2)	11.0%	
Aquarium Wharf (WB)	235 (0)	9.0%	
			VEHICLES COUNTED
			ALL VEHICLES XXX 2572
			TRUCKS (XX) 52
TOTAL	2572 (52)	100.0%	PERCENT TRUCKS 2.0%

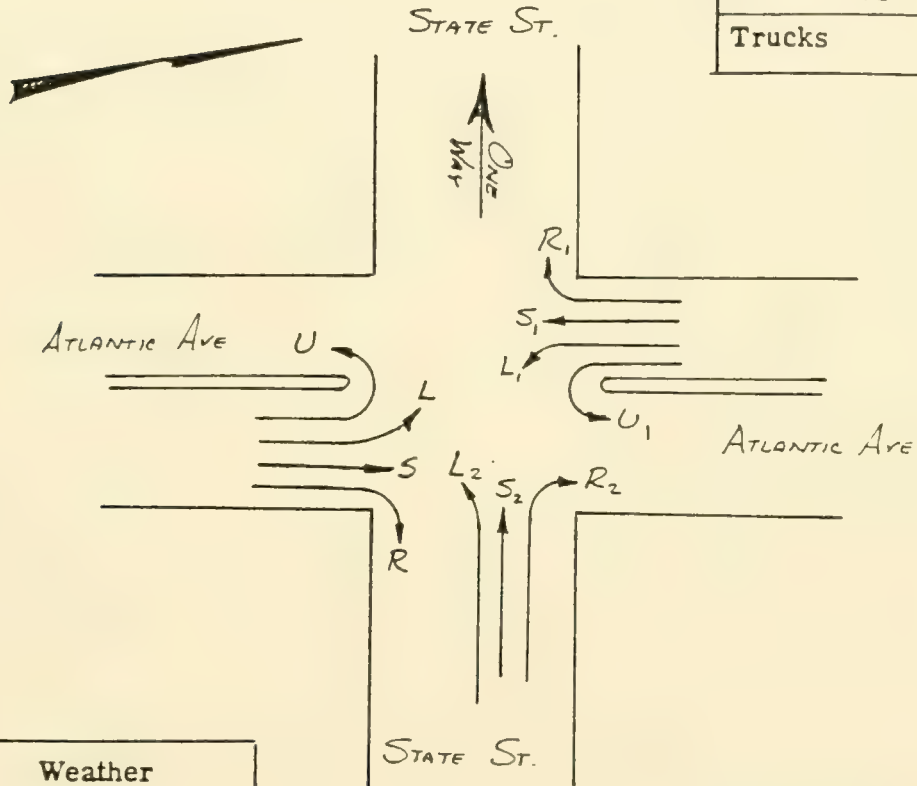
City BOSTON - MA 02116  
Intersection ATLANTIC AVE & STATE ST.

INT. NO. 54 (BTPD # 2023) Date 3/24/83 Day of Week THURSDAY

INTERSECTION TURNING MOVEMENT COUNT

**2023**

Vehicles Counted	
All	X
Pass. Cars	
Trucks	



Weather <u>CLEAR-TEEN'S</u>
Count Taken By <u>KEVIN GABRIEL</u>

Length of Count	
Time	Number of Hours
<u>7am-6pm</u>	<u>11 HRS</u>

Street	Entering Volume	Flow Percent	Comments
ATLANTIC AVE (NB)	10,555	58%	
ATLANTIC AVE (SB)	5843	32%	
STATE ST. (WB)	1729	10%	
Total	18127	100%	



## TRAFFIC MOVEMENT SUMMARY TABLE

Location ATLANTIC AVE & STATE ST. City or Town BOSTON - PROPERDate 3/24/83 Day of Week THURSDAY Weather CLR Recorder KC

2023

Time Starts 7:00AM	ATLANTIC AVENUE								STATE ST.			Total Half Hour Tally
	(NB)				(SB)				(WB)			
	L	S	R	U	L <sub>1</sub>	S <sub>1</sub>	R <sub>1</sub>	U <sub>1</sub>	L <sub>2</sub>	S <sub>2</sub>	R <sub>2</sub>	
7:00-7:30	53	192	33	1	26	169	31	0	6	21	17	549
7:30-8:00	74	263	36	3	31	291	52	1	12	42	38	843
8:00-8:30	99	327	52	6	41	417	63	3	19	36	57	1120
8:30-9:00	93	285	43	2	46	374	74	0	12	24	52	1005
9:00-9:30	84	264	47	3	39	149	66	2	11	54	47	766
9:30-10:00	77	246	31	2	22	138	56	0	11	43	34	660
10:00-10:30	69	213	25	3	16	127	45	1	8	37	24	568
10:30-11:00	68	209	28	2	20	119	54	1	13	40	23	577
11:00-11:30	70	206	26	1	19	116	49	1	11	39	24	562
11:30-12:00	65	282	42	1	21	138	50	0	19	42	20	680
12:00-12:30	68	280	46	1	22	147	59	1	21	43	22	710
12:30-1:00	73	257	37	2	16	143	59	1	3	39	20	650
1:00-1:30	75	231	25	2	21	119	58	0	4	42	22	599
1:30-2:00	77	241	33	2	25	123	64	2	6	47	26	646
2:00-2:30	65	254	23	0	14	113	43	4	5	53	17	591
2:30-3:00	79	271	34	1	27	121	57	0	4	67	24	685
3:00-3:30	73	550	18	2	16	175	50	3	8	39	18	952
3:30-4:00	85	670	19	1	10	200	61	1	5	32	13	1097
4:00-4:30	97	730	18	1	12	241	69	2	8	36	18	1232
4:30-5:00	103	766	21	3	16	269	84	1	14	43	24	1344
5:00-5:30	92	751	36	0	23	185	62	0	7	50	36	1242
5:30-6:00	96	585	34	1	28	176	52	0	4	52	21	1049
6:00-6:30												
6:30-7:00												
7:00-7:30	172	612	95	8	87	791	137	3	31	60	109	2125
7:30-8:00												
8:00-8:30	175	1517	57	3	39	454	146	1	21	93	60	2586
8:30-9:00												
9:00-9:30												
9:30-10:00												
10:00-10:30												
10:30-11:00												
TOTAL	1735	8073	707	40	511	4050	1258	24	211	921	597	GRAND TOTAL
Total of L S & R	10555				5843				1729			18127

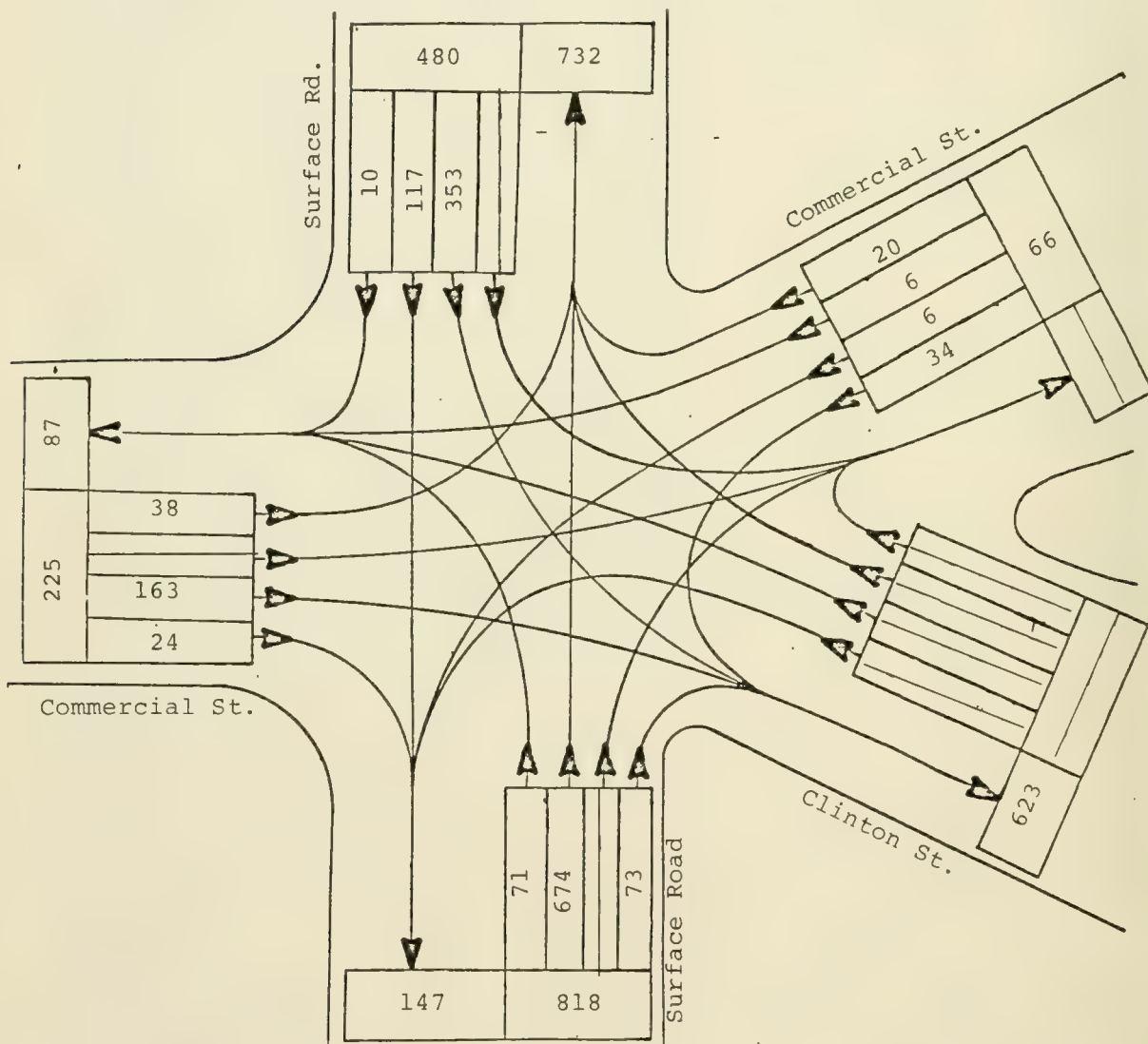




Vanasse/Hangen Associates, Inc.  
 Transportation Engineers & Planners  
 184 High Street, Boston, Massachusetts 02110  
 617 / 482-0749

# INTERSECTION TURNING MOVEMENT COUNT

CITY BOSTON, MA DATE 7-26-84 DAY of WEEK Thursday  
 INTERSECTION Clinton St./Surface Rd. JOB No. 0923



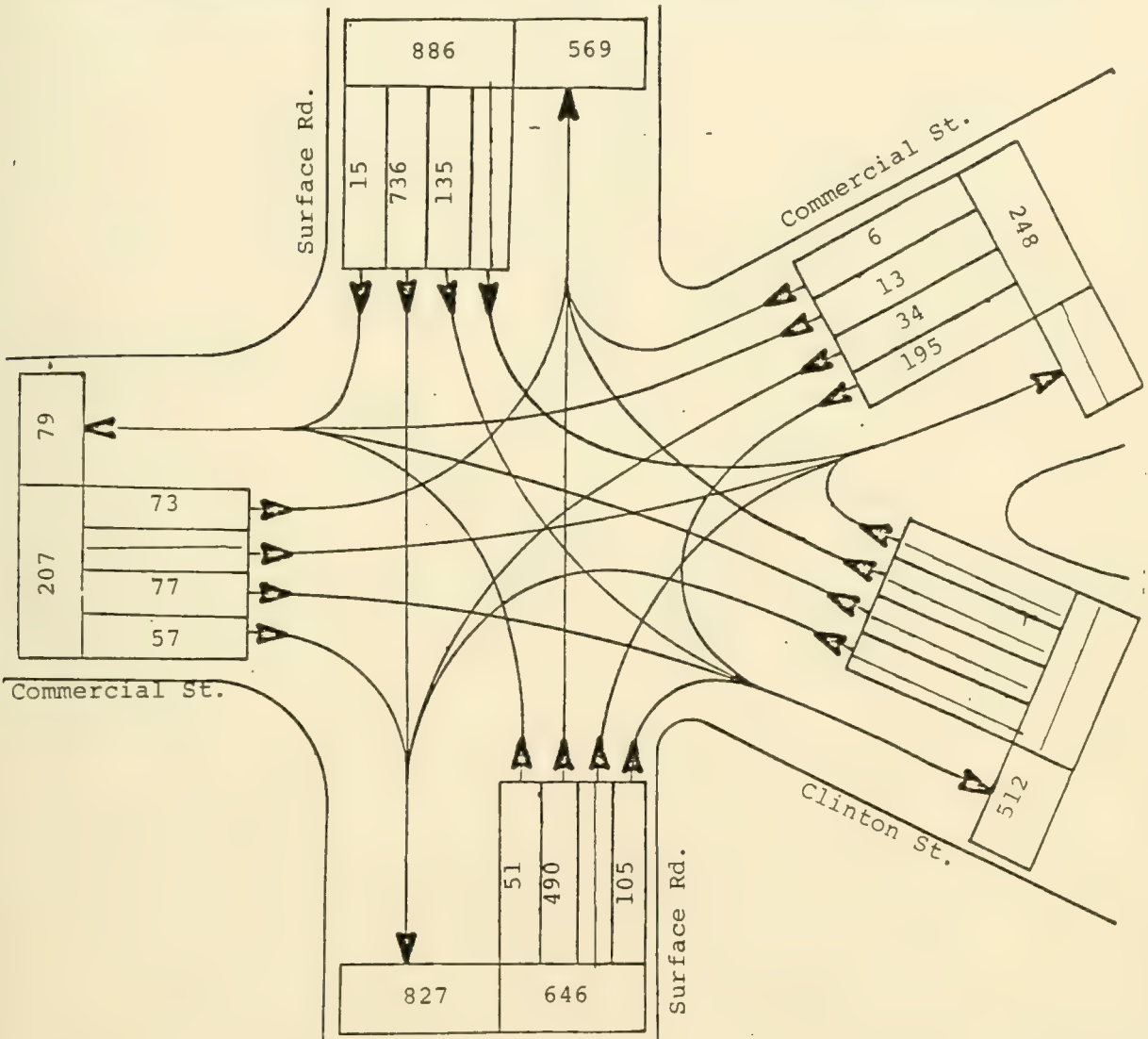
STREET	ENTERING VOLUME	PERCENT OF FLOW	TIME of COUNT
Surface Rd. (NB)	480	30.2%	8:00 - 9:00 AM AM Peak Hour
Surface Rd. (SB)	818	51.5%	
Commercial St. (EB)	66	4.1%	
Commercial St. (NB)	225	14.2%	
			VEHICLES COUNTED
			ALL VEHICLES XXX 1589
			TRUCKS (XX) --
TOTAL	1589	100.0%	PERCENT TRUCKS -- %



Vanasse/Hanger & Associates, Inc.  
Transportation Engineers & Planners  
184 High Street, Boston, Massachusetts 02110  
617/482-0749

## INTERSECTION TURNING MOVEMENT COUNT

CITY BOSTON, MA DATE 7-26-84 DAY of WEEK Thursday  
INTERSECTION Clinton St./Surface Rd. JOB No. 0923



STREET	ENTERING VOLUME	PERCENT OF FLOW	TIME of COUNT
Surface Rd. (NB)	886	44.6%	4:15 - 5:15 PM PM Peak Hour
Surface Rd. (SB)	646	32.5%	
Commercial St. (EB)	248	12.5%	
Commercial St. (WB)	207	10.4%	
			VEHICLES COUNTED
			ALL VEHICLES XXX 1987
			TRUCKS (XX) --
TOTAL	1987	100.0%	PERCENT TRUCKS -- %



**Vanasse / Hangen Engineering, Inc.**

Consulting Engineers & Planners  
184 High Street, Boston, Massachusetts 02110  
617 / 482-1870

JOB: International Place JOB No. 0923

LOCATION: \_\_\_\_\_ SHEET \_\_\_\_\_ OF \_\_\_\_\_

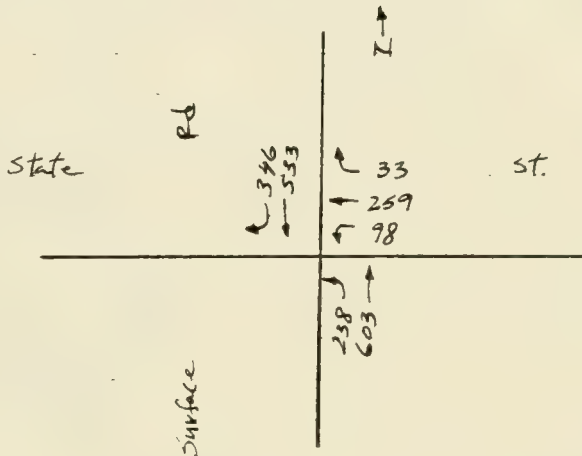
CALCULATED BY BG DATE \_\_\_\_\_

CHECKED BY: \_\_\_\_\_ DATE \_\_\_\_\_

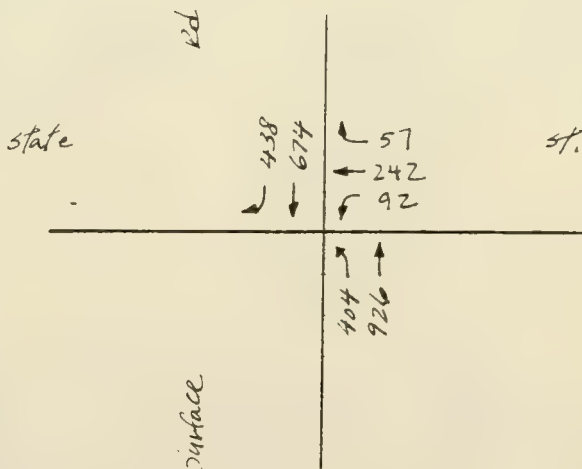
TITLE Turning Movement Counts

AM

Source: Third Harbor EIR  
dated Dec. 82



PM





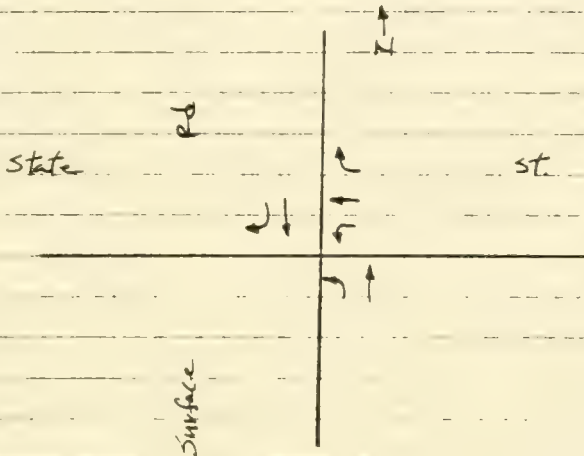


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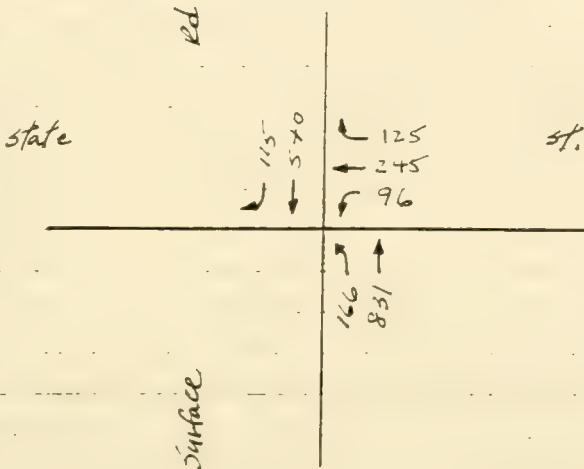
JOB Interpretational Place JOB No. 0923  
LOCATION \_\_\_\_\_ SHEET \_\_\_\_\_ OF \_\_\_\_\_  
CALCULATED BY: BG DATE \_\_\_\_\_  
CHECKED BY: \_\_\_\_\_ DATE: \_\_\_\_\_  
TITLE Turning Movement Counts

AM

Source: Marketplace Center  
EIR dated April, 83.



PM

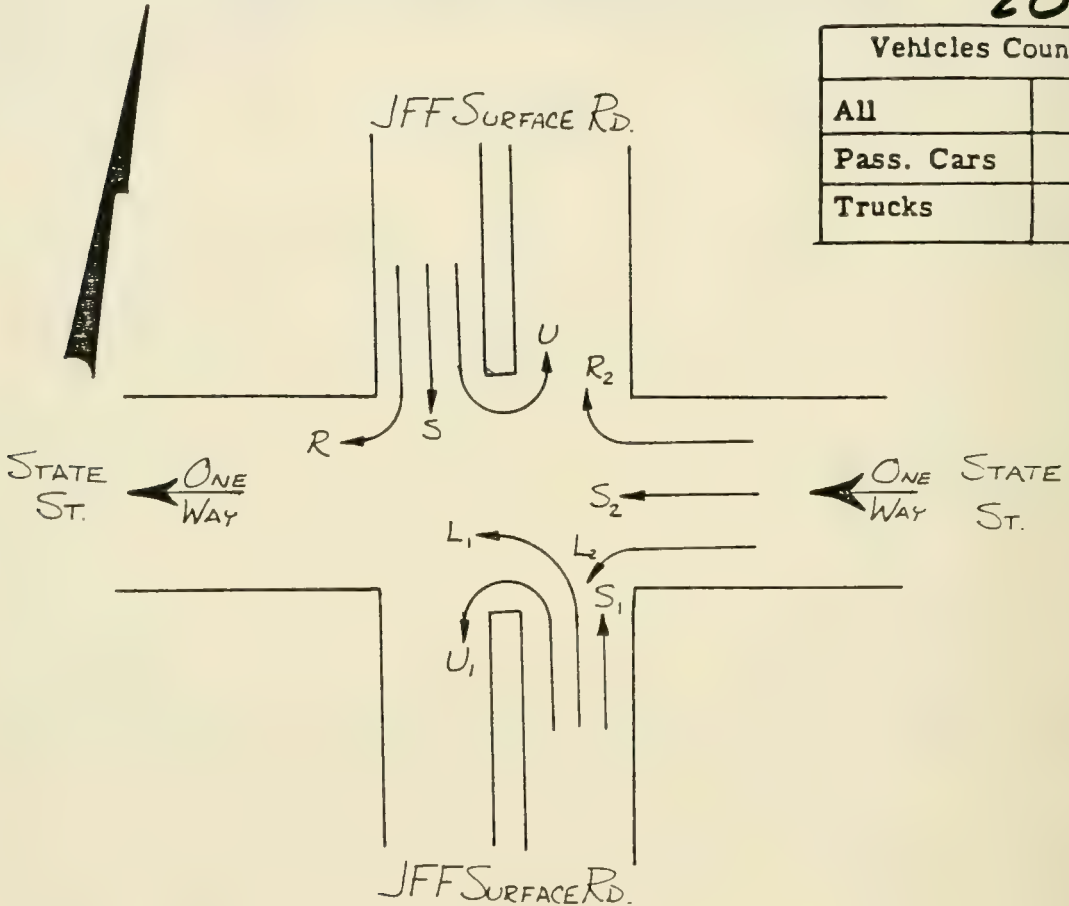


City BOSTON - PROPER  
Intersection JFF SURFACE RD & STATE ST

INT. NO. 55 (BTPD #2024) Date 6/27/83 Day of Week MONDAY

INTERSECTION TURNING MOVEMENT COUNT

**2024**



Vehicles Counted	
ALL	X
Pass. Cars	
Trucks	

Weather <u>CLEAR &amp; DRY</u>
Count Taken By <u>CD SCHUBERT</u>

Length of Count	
Time	Number of Hours
<u>7AM-6PM</u>	<u>11 HRS.</u>

Street	Entering Volume	Flow Percent	Comments
JFF SURFACE RD (SB)	8704	46%	
JFF SURFACE RD (NB)	7148	38%	
STATE ST (WB)	3194	17%	
<b>Total</b>	<b>19,046</b>	<b>100%</b>	

TRAFFIC MOVEMENT SUMMARY TABLE

Location JFF SURFACE RD & STATE ST. City or Town BOSTON - PROPER

Date 6/27/83 Day of Week MONDAY Weather CLR Recorder CDS

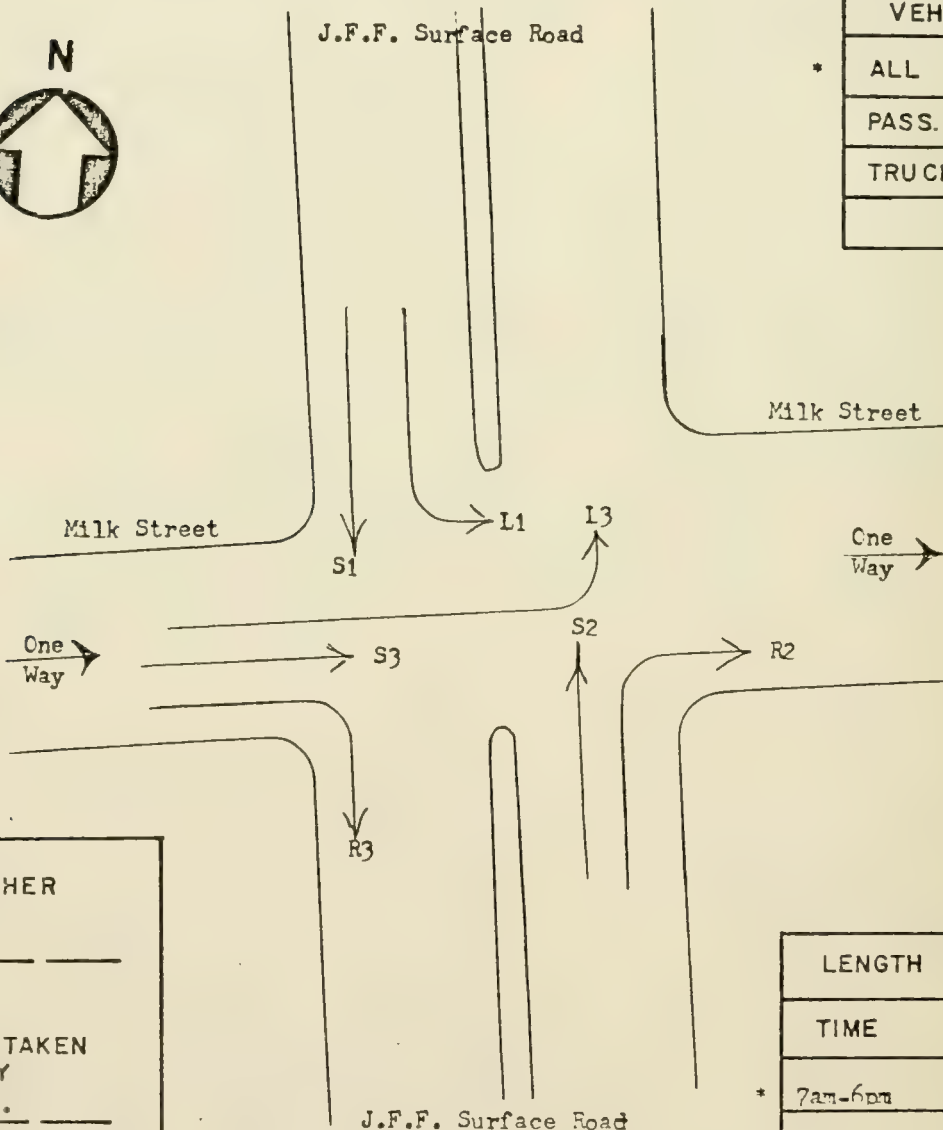
Time Starts 7:00 AM	JFF SURFACE RD						STATE ST.						Total Half Hour Tally
	(SB)			(NB)			WB						
	S	R	U	L <sub>1</sub>	S <sub>1</sub>	U <sub>1</sub>	L <sub>2</sub>	S <sub>2</sub>	R <sub>2</sub>				
7:00-7:30	279	81	0	110	91	1	20	61	12				655
7:30-8:00	268	116	1	134	143	0	35	57	28				782
<del>8:00-8:30</del>	295	130	2	133	142	4	53	89	41				889
8:30-9:00	189	169	0	152	164	1	37	82	35				829
9:00-9:30	204	155	0	140	136	0	32	92	23				782
9:30-10:00	297	174	1	129	134	1	31	81	20				868
10:00-10:30	216	167	5	155	117	2	38	88	16				804
10:30-11:00	170	80	1	98	92	0	21	52	13				527
11:00-11:30	231	134	1	96	161	2	30	82	16				753
11:30-12:00	283	133	0	120	163	3	37	103	23				865
12:00-12:30	224	82	3	128	182	0	36	67	35				757
12:30-1:00	204	85	4	127	176	0	32	94	27				749
1:00-1:30	198	87	1	136	194	0	28	100	22				766
1:30-2:00	262	90	0	114	149	0	52	82	11				760
2:00-2:30	203	113	3	109	153	2	30	91	15				719
2:30-3:00	281	95	2	102	167	0	44	90	24				805
3:00-3:30	319	89	0	103	297	2	48	75	19				952
3:30-4:00	383	69	0	76	348	1	44	96	21				1038
4:00-4:30	499	49	0	58	453	1	39	82	13				1194
4:30-5:00	518	43	0	91	404	0	43	94	43				1236
5:00-5:30	563	29	0	87	438	0	61	104	48				1330
5:30-6:00	400	24	0	77	349	0	34	72	30				986
6:00-6:30													
6:30-7:00													
<del>7:00-7:30</del>	484	299	2	285	306	5	90	171	76				1718
7:30-8:00													
8:00-8:30													
<del>8:30-9:00</del>	1081	72	0	178	842	0	104	198	91				2566
9:00-9:30													
9:30-10:00													
10:00-10:30													
10:30-11:00													
TOTAL	6486	2194	24	2475	4653	20	825	1834	735				GRAND TOTAL
Total of 2 S E R	8704			7148			3194						19,046

INT. NO. 319

CITY Boston Proper  
 INTERSECTION J.F.F. Surface Road & Milk Street  
 DATE 11/24 & 25/80 DAY OF WEEK Mo

# INTERSECTION TURNING MOVEMENT COUNT

# 1052



VEHICLES COUNT	
ALL	
PASS. CARS	
TRUCKS	

## WEATHER

Rain

COUNT TAKEN  
 BY  
E.C.

## LENGTH OF COUNT

TIME	NUMBER OF HOURS
<u>7am-6pm</u>	<u>11 Hours</u>

STREET		ENTERING	FLOW
		VOLUME	PERCENT
J.F.F. Surface Rd.	SB	6544	43.6
J.F.F. Surface Rd.	NR	2028	46.9
Milk Street	ER	1424	9.5
		14006	100%

## COMMENTS




# TRAFFIC MOVEMENT SUMMARY TABLE

STATION J.F.F. Surface Road & Milk Street CITY OR TOWN Boston Proper  
DATE 11/24 & 25/80 DAY OF WEEK Tues. WEATHER Rain RECORDER E.C.

TIME STARTS -- M	Surface Road			Surface Road			Milk Street						TOTAL
	Southbound			Northbound			Eastbound						HALF HOUR
	L1	S1			S2	R2	L3	S3	R3				TALLY
00-7:30	5	172			156	2	2	8	1				346
30-8:00	21	258			304	6	5	19	1				614
00-8:30	24	220			331	4	8	23	3				613
30-9:00	43	203			395	9	11	30	3				694
00-9:30	39	187			323	14	16	32	4				615
30-10:00	24	168			339	11	37	30	6				615
00-10:30	39	317			213	6	22	15	7				619
30-11:00	31	284			204	9	27	23	11				589
00-11:30	24	155			186	12	23	18	8				426
30-12:00	22	163			223	14	29	28	7				488
00-12:30	31	221			345	13	37	41	6				694
30-1:00	14	224			301	9	36	19	10				613
00-1:30	22	252			268	15	33	21	12				623
30-2:00	38	283			245	13	28	20	13				640
00-2:30	28	288			262	11	31	22	11				653
30-3:00	21	303			279	13	33	27	12				688
00-3:30	24	420			319	8	38	46	8				863
30-4:00	23	433			362	14	34	41	10				917
00-4:30	21	440			478	25	37	33	2				1036
30-5:00	26	392			515	23	43	39	11				1049
00-5:30	12	330			381	12	73	46	10				864
30-6:00	15	284			343	13	36	37	9				737
00-6:30													
30-7:00	67	423			726	13	19	53	6				1307
00-7:30													
30-8:00													
00-8:30	47	832			993	48	80	72	13				2085
30-9:00													
00-9:30													
30-10:00													
00-10:30													
30-11:00													
TOTAL	547	4177			3256	639	639	618	167				GRAND TOTAL
TOTAL OF	544				28		1424						14996

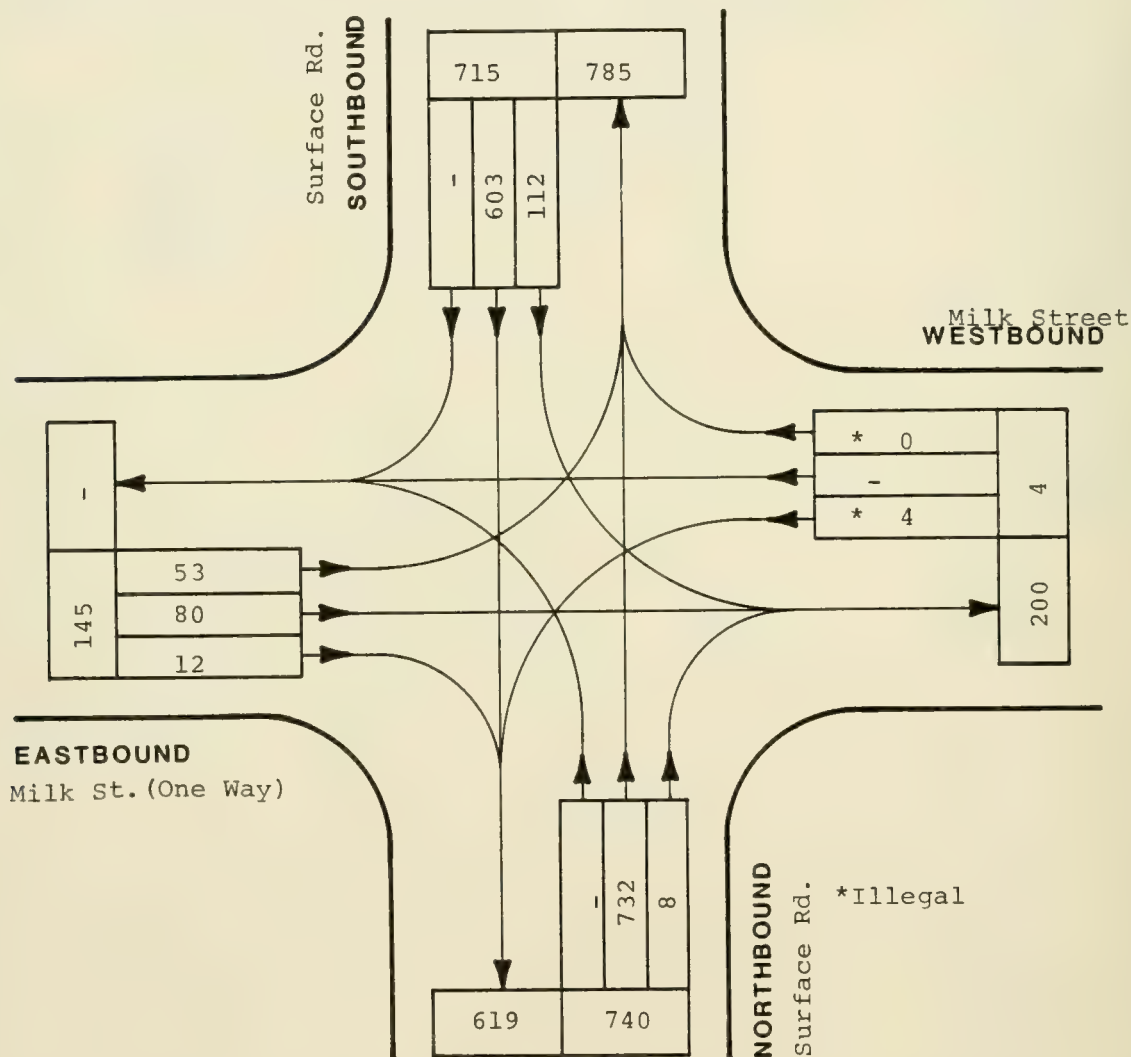




**Vanasse / Hangen Associates, Inc.**  
Transportation Engineers & Planners  
184 High Street, Boston, Massachusetts 02110  
617 / 482-0749

## INTERSECTION TURNING MOVEMENT COUNT

CITY Boston, MA DATE 7/26/84 DAY of WEEK Thursday  
INTERSECTION Milk St./Surface Road JOB No. 0923

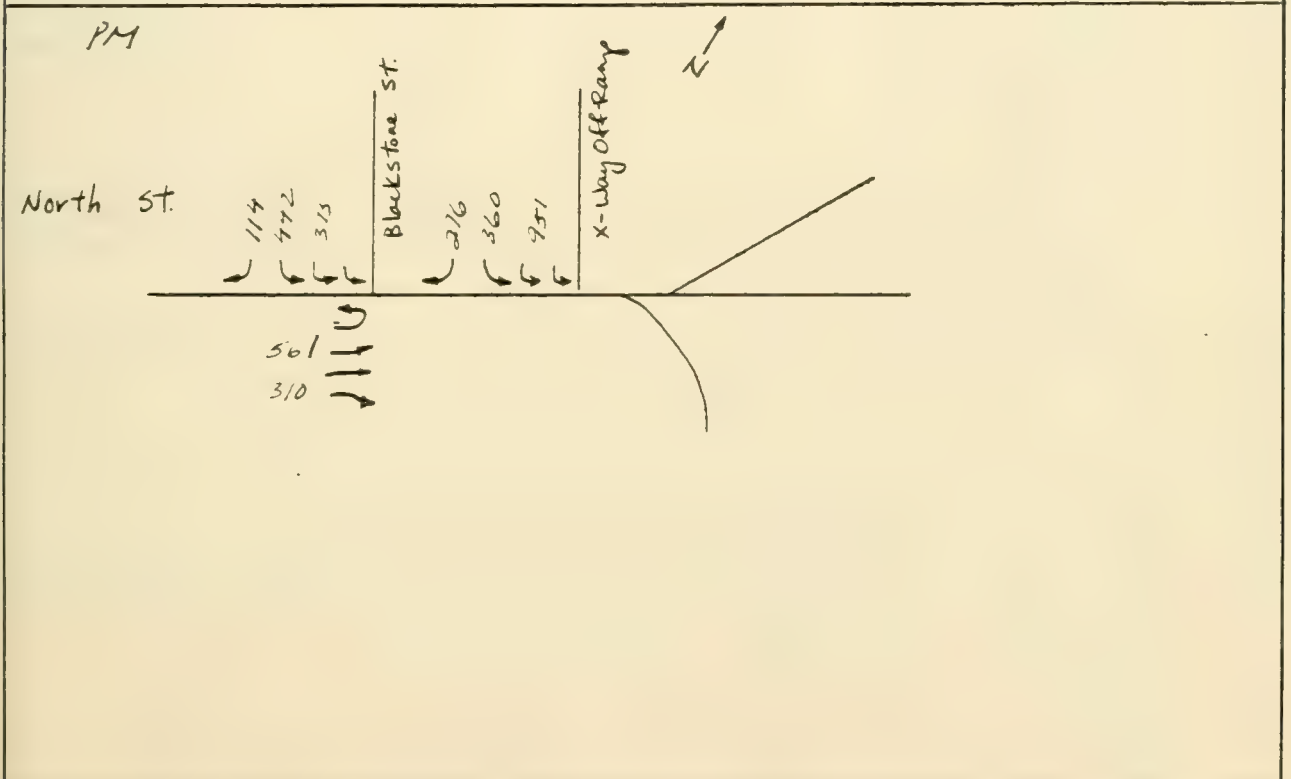
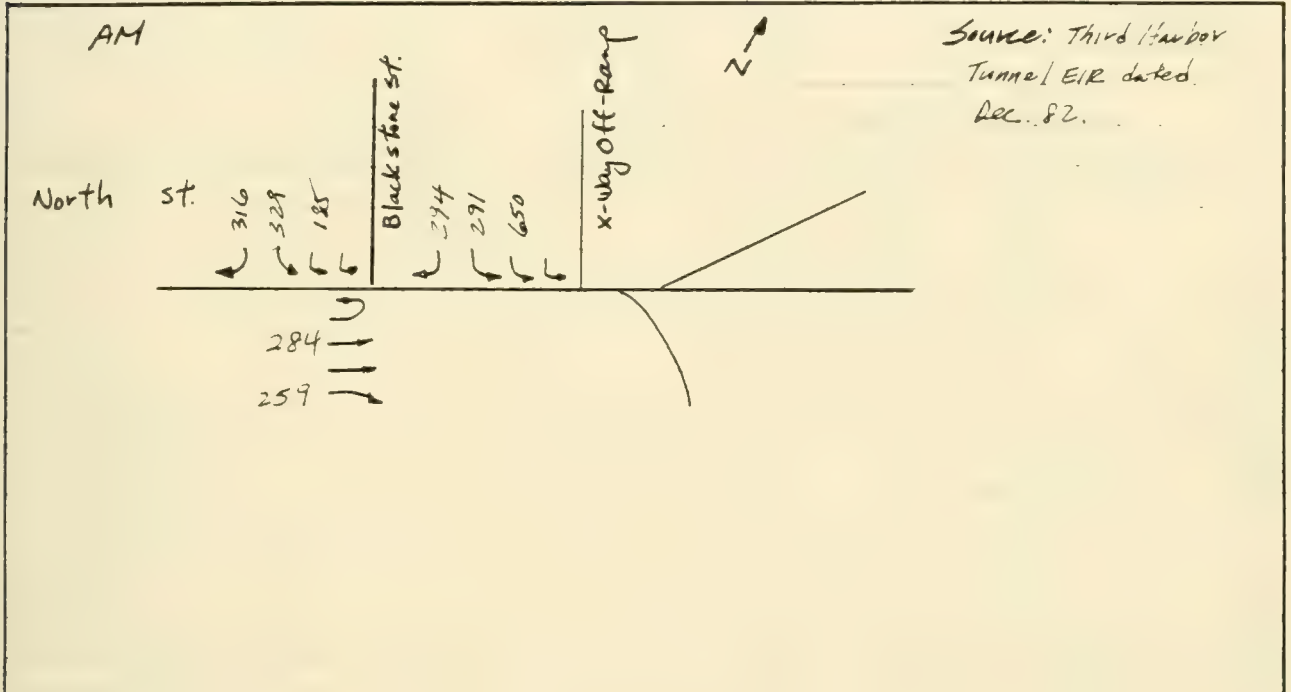


STREET	ENTERING VOLUME	PERCENT OF FLOW	TIME of COUNT
Surface Rd. (NB)	740	46.1%	8:00 - 9:00 AM
Surface Rd. (SB)	715	44.6%	
Milk St. (EB)	145	9.0%	AM Peak Hour
Milk St. (WB)	4	0.3%	
			VEHICLES COUNTED
			ALL VEHICLES XXX1604
			TRUCKS (XX)
TOTAL	1604	100.0%	PERCENT TRUCKS %



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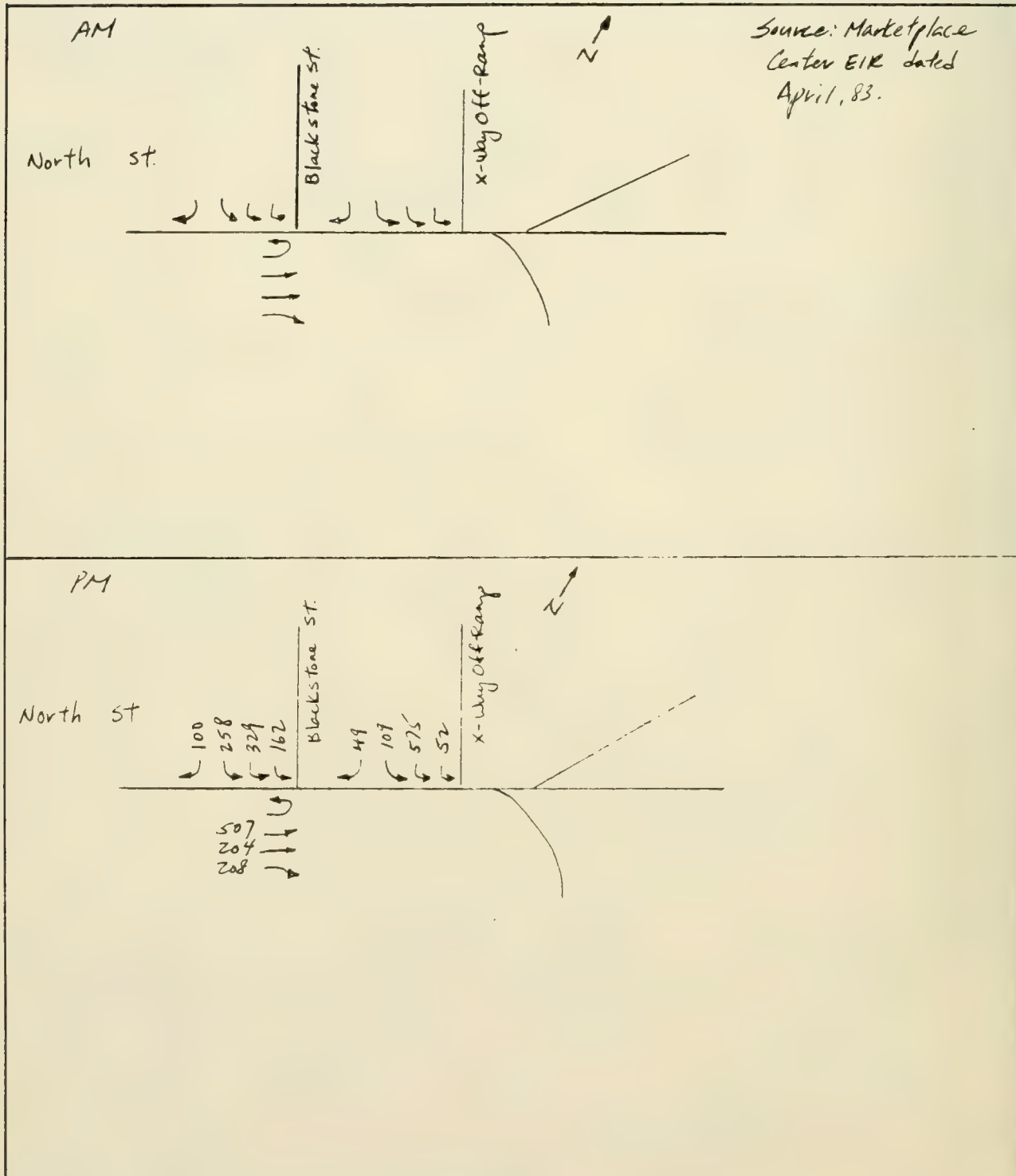
JOB International Place JOB No. 0923  
LOCATION \_\_\_\_\_ SHEET \_\_\_\_\_ OF \_\_\_\_\_  
CALCULATED BY: BG DATE \_\_\_\_\_  
CHECKED BY \_\_\_\_\_ DATE \_\_\_\_\_  
TITLE \_\_\_\_\_





**Vanasse / Hangen Engineering, Inc.**  
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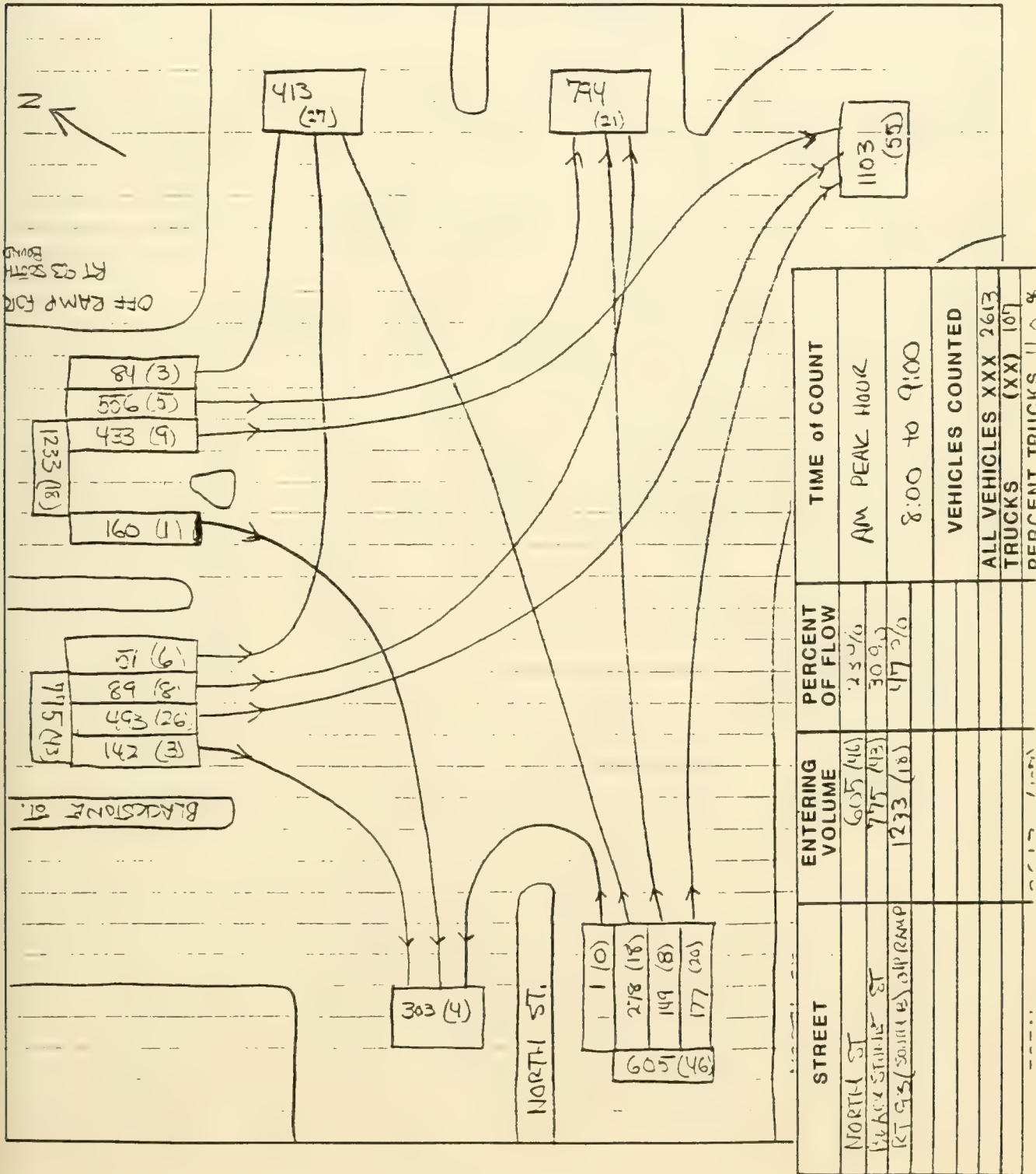
JOB International Place JOB No. 0823  
LOCATION \_\_\_\_\_ SHEET \_\_\_\_\_ OF \_\_\_\_\_  
CALCULATED BY BG DATE \_\_\_\_\_  
CHECKED BY \_\_\_\_\_ DATE \_\_\_\_\_  
TITLE \_\_\_\_\_





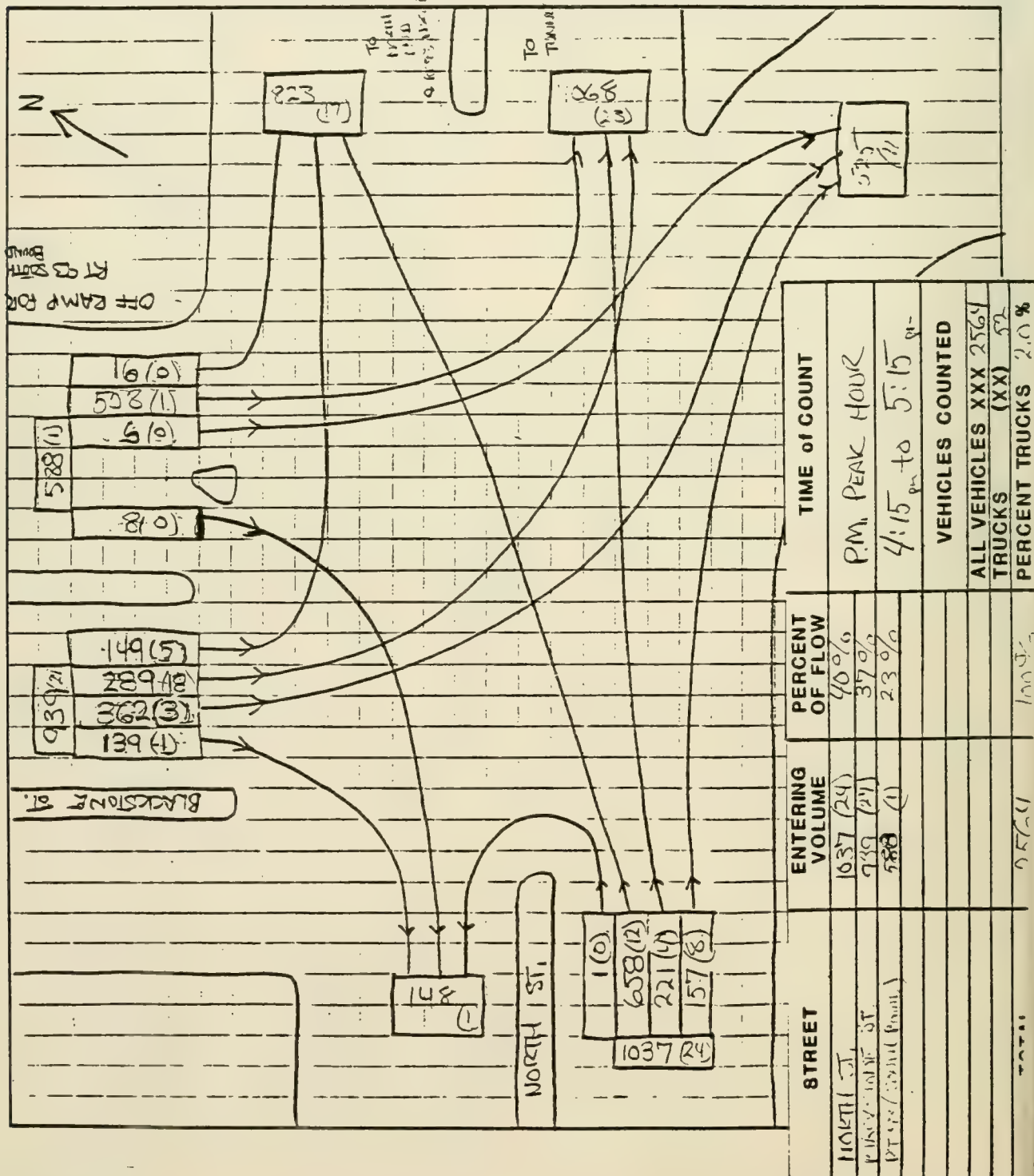
**Vanasse / Hangen Engineering, Inc.**  
Consulting Engineers & Planners  
184 High Street, Boston, Massachusetts 02110  
617 / 482-1870

JOB HOLIDAY INN JOB No. 276  
LOCATION NORTH / BLACKSTONE SHEET 1 OF 5  
CALCULATED BY AND R. OF RAMP DATE PRIDY  
CHECKED BY GJO DATE 7/13/84  
TITLE AM COUNT

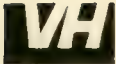




JOB: HOWARD INN JOB No. 296  
LOCATION: 1041 BIRCHMOUNT AVE. S.W. SHEET 1 OF 5  
CALCULATED BY: \_\_\_\_\_ DATE: PR. DDU  
CHECKED BY: GB DATE: 7/13/84  
TITLE: PM COUNT



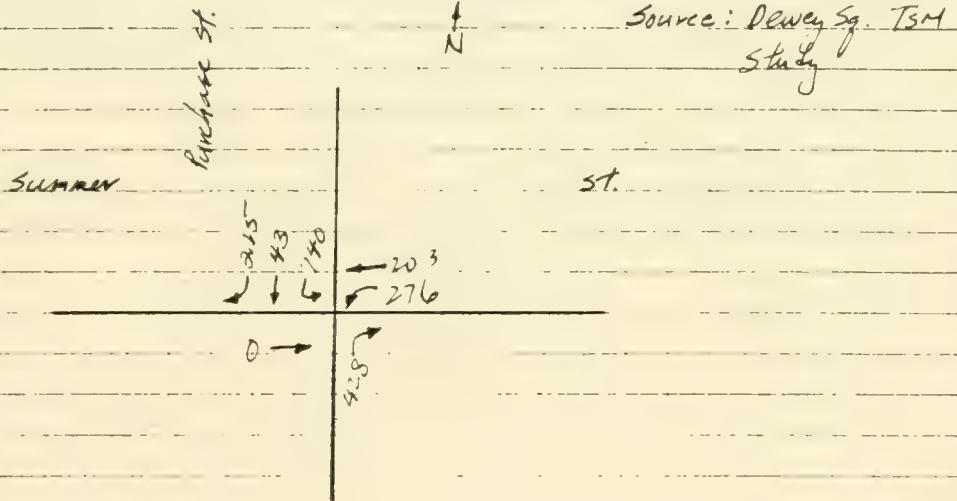




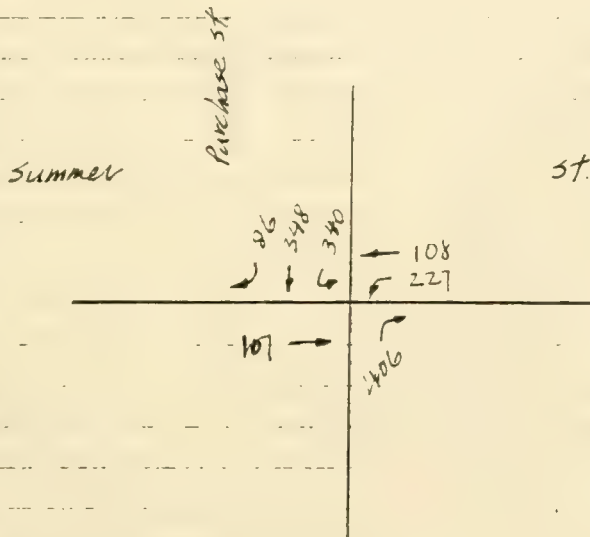
**Vanasse / Hangen Engineering, Inc.**  
Consulting Engineers & Planners  
184 High Street, Boston, Massachusetts 02110  
617 / 482-1870

JOB International Place JOB No. 0923  
LOCATION: \_\_\_\_\_ SHEET \_\_\_\_\_ OF \_\_\_\_\_  
CALCULATED BY: BG DATE: \_\_\_\_\_  
CHECKED BY: \_\_\_\_\_ DATE: \_\_\_\_\_  
TITLE: Turning Movement Counts

AM



PM





**Vanasse / Hangen Engineering, Inc.**

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617 / 482-1870

JOB International Place JOB No. 0923

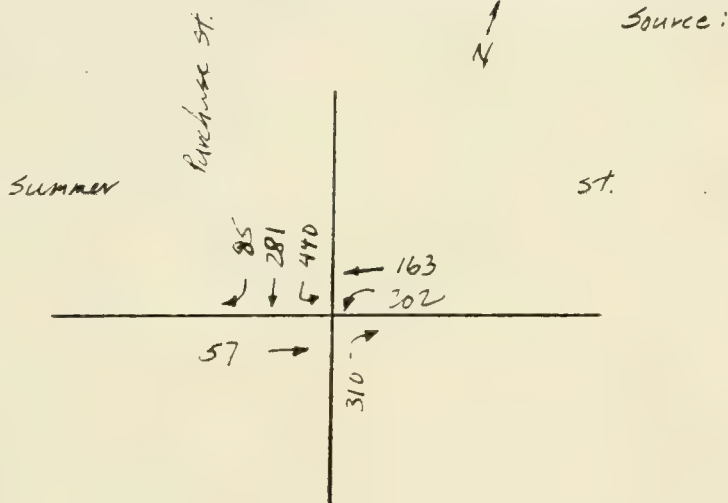
LOCATION \_\_\_\_\_ SHEET \_\_\_\_\_ OF \_\_\_\_\_

CALCULATED BY BG DATE \_\_\_\_\_

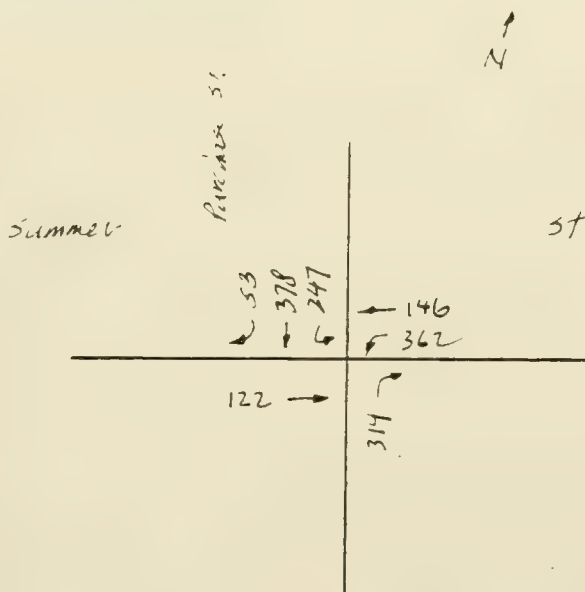
CHECKED BY \_\_\_\_\_ DATE \_\_\_\_\_

TITLE Turning Movement Counts

AM



PM



# Traffic Control Systems

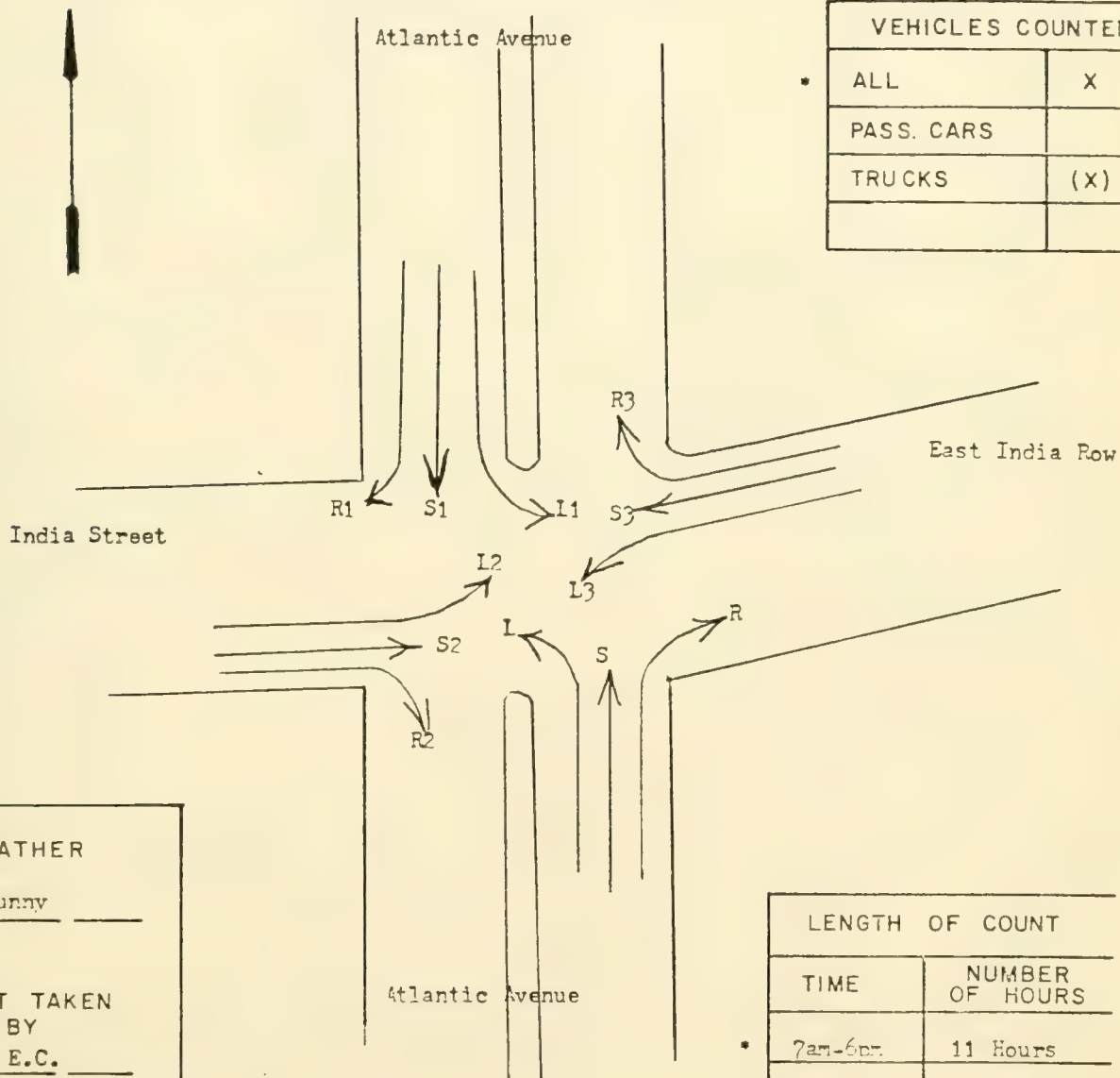
Planning, Engineering, Construction & Maintenance  
Brighton, Ma. Tel. (617) 782-9757

INT. NO. 387

CITY Boston Proper  
INTERSECTION Atlantic Ave., East India Row  
& India Street  
DATE 4/8/81 DAY OF WEEK Wednesday

## N INTERSECTION TURNING MOVEMENT COUNT

200



VEHICLES COUNTED	
ALL	X
PASS. CARS	
TRUCKS	(X)

### WEATHER

Sunny

### COUNT TAKEN BY

D.B. & E.C.

### LENGTH OF COUNT

TIME

NUMBER OF HOURS

7am-6pm

11 Hours

STREET		ENTERING VOLUME	FLOW PERCENT
Atlantic Avenue	NB	6577	55.4
Atlantic Avenue	SB	3695	32.3
India Street	EB	490	4.3
East India Street	WB	525	5.0
TOTAL		11428	100%

### COMMENTS


# TRAFFIC MOVEMENT SUMMARY TABLE

LOCATION Atlantic Ave., East India Row, & India St. CITY OR TOWN Boston Proper

DATE 4/8/81 DAY OF WEEK Wednesday WEATHER Sunny RECORDER D.B. & E.

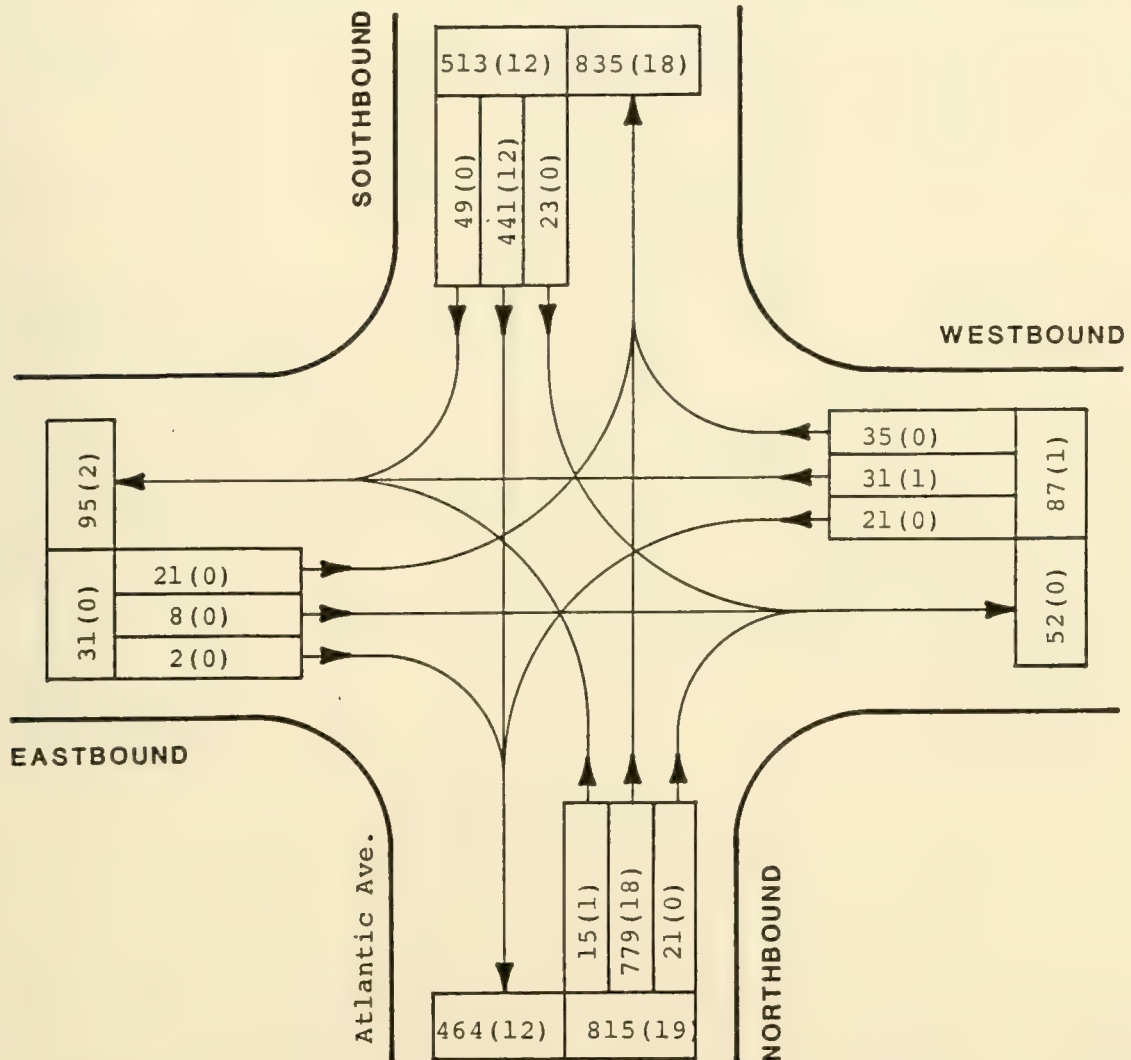
TIME STARTS -- M	Atlantic Avenue			Atlantic Avenue			India Street			East India Street			TOTAL
	Northbound			Southbound			Eastbound			Westbound			HALF HC
	I	S	R	L1	S1	R1	L2	S2	R2	L3	S3	R3	TALL
7:00-7:30	2	221	5	8	147	8	1	5	1	3	11	7	419
7:30-8:00	3	263	12	6	220	23	4	8	1	8	14	14	571
8:00-8:30	10	343	12	10	192	16	9	14	0	8	26	16	651
8:30-9:00	11	426	10	11	159	27	2	4	3	10	17	7	681
9:00-9:30	13	370	13	7	171	19	11	10	2	10	15	12	651
9:30-10:00	8	237	11	5	104	8	6	8	1	5	9	9	411
10:00-10:30	9	320	12	6	123	11	12	5	2	2	14	7	521
10:30-11:00	11	235	11	9	131	12	7	8	1	8	14	10	451
11:00-11:30	9	230	10	3	122	8	15	7	2	3	8	15	431
11:30-12:00	19	256	8	2	128	11	15	9	4	2	8	9	471
12:00-12:30	9	270	4	9	127	12	13	8	1	3	6	6	468
12:30-1:00	16	246	3	19	105	13	10	7	4	5	12	11	451
1:00-1:30	20	209	8	3	115	22	15	9	1	2	9	7	421
1:30-2:00	12	196	5	4	102	12	11	8	2	2	8	4	361
2:00-2:30	17	256	9	5	133	16	15	11	1	6	9	10	481
2:30-3:00	15	243	11	7	129	19	12	7	2	3	11	13	471
3:00-3:30	13	254	9	6	136	12	9	8	3	5	12	9	471
3:30-4:00	7	329	6	4	173	3	1	2	14	0	3	8	551
4:00-4:30	18	436	14	11	268	11	34	8	13	0	4	11	821
4:30-5:00	11	401	8	5	212	7	29	6	7	8	9	14	711
5:00-5:30	5	289	9	3	161	6	12	4	2	3	10	17	521
5:30-6:00	6	201	11	4	107	8	16	5	3	5	7	12	381
6:00-6:30													
6:30-7:00													
AM 7:30	21	769	22	21	351	43	11	18	3	18	43	23	1344
7:30-8:00													
8:00-8:30													
PM 8:30	21	837	22	16	480	18	63	14	20	8	13	25	1545
9:00-9:30													
9:30-10:00													
10:00-10:30													
10:30-11:00													
TOTAL	504	6231	202	147	3265	284	259	161	70	101	236	228	GRAN TOTAL
TOTAL OF	6677			3696			490			565			1142



Vanasse / Hangen Associates, Inc.  
Transportation Engineers & Planners  
184 High Street, Boston, Massachusetts 02110  
617 / 482-0749

## INTERSECTION TURNING MOVEMENT COUNT

CITY Boston, MA DATE 3/2/84 DAY of WEEK Friday  
INTERSECTION Atlantic Ave. & E. India Row JOB No. 0751



STREET	ENTERING VOLUME	PERCENT OF FLOW	TIME of COUNT
Atlantic Ave. (NB)	815 (19)	56.4%	8:00 - 9:00 AM AM Peak Hour
Atlantic Ave. (SB)	513 (12)	35.5%	
E. India Row (EB)	31 (0)	2.1%	
E. India Row (WB)	87 (1)	6.0%	
			VEHICLES COUNTED
			ALL VEHICLES XXX 1446
			TRUCKS (XX) 32
TOTAL	1446 (32)	100.0%	PERCENT TRUCKS 2.2%

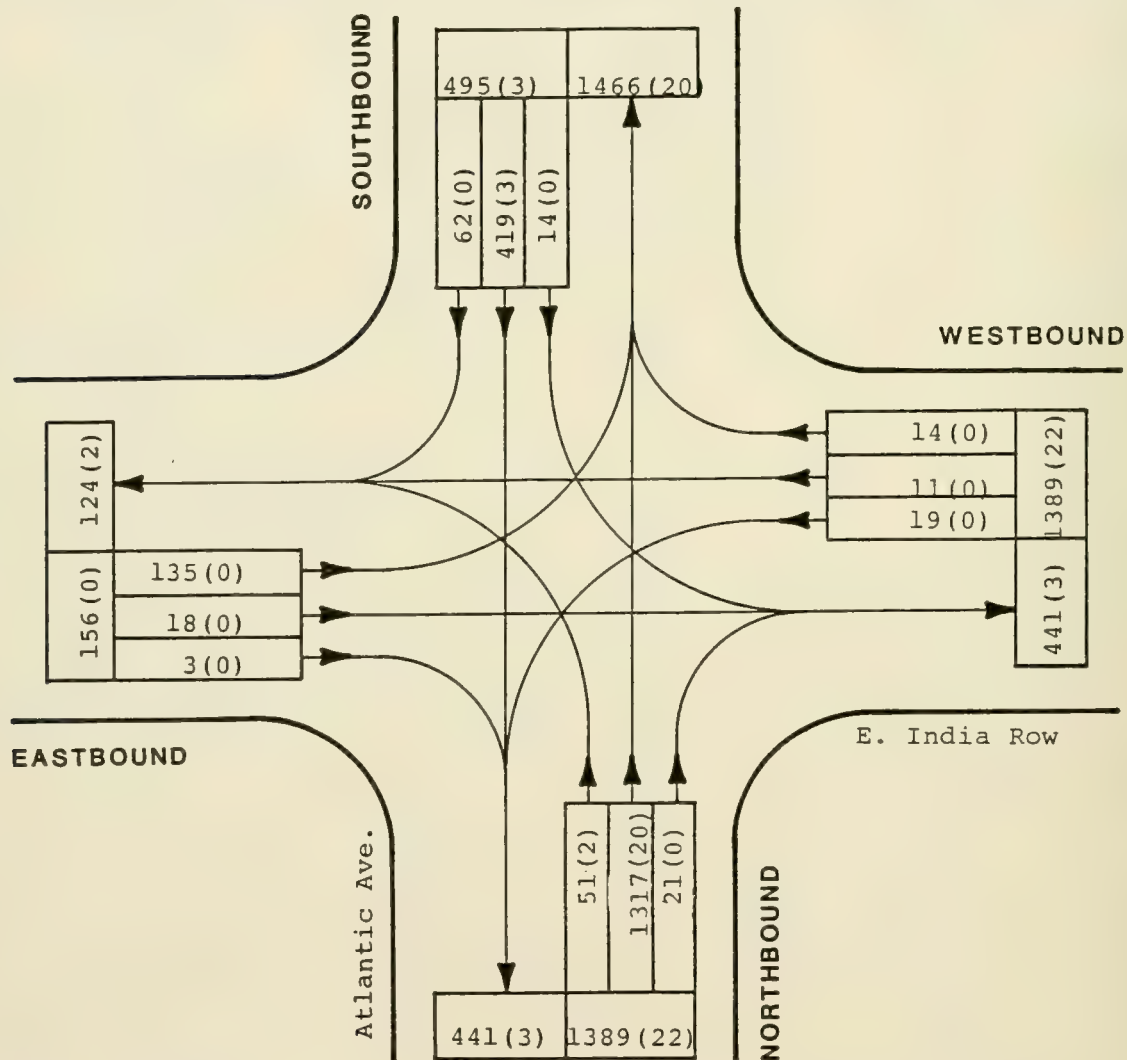




Vanasse / Hangen Associates, Inc.  
Transportation Engineers & Planners  
184 High Street, Boston, Massachusetts 02110  
617 / 482-0749

## INTERSECTION TURNING MOVEMENT COUNT

CITY Boston, MA DATE 3/1/84 DAY of WEEK Thursday  
INTERSECTION Atlantic Ave. & E. India Row JOB No. 0751



STREET	ENTERING VOLUME	PERCENT OF FLOW	TIME of COUNT
Atlantic Ave. (NB)	1389 (22)	66.7%	4:30 - 5:30 PM
Atlantic Ave. (SB)	495 (3)	23.8%	
E. India Row (EB)	156 (0)	7.5%	PM Peak Hour
E. India Row (WB)	44 (0)	2.0%	
			VEHICLES COUNTED
			ALL VEHICLES XXX 2084
			TRUCKS (XX) 25
TOTAL	2084 (25)	100.0%	PERCENT TRUCKS 1.2 %

INT. NO. 86

CITY Boston From                       
INTERSECTION India Street & J. F. F. Surface  
Rd.  
DATE 11/16 & 19/79 DAY OF WEEK Fri & M

# INTERSECTION TURNING MOVEMENT COUNT # 1053

J. F. F. Surface Rd.

VEHICLES COUNTED

* ALL	X
PASS. CARS	
TRUCKS	(X)

India Street

India Street

J. F. F. Surface Rd.

WEATHER

Clear & Cold

COUNT TAKEN  
BY

TP & JT

LENGTH OF COUNT

TIME NUMBER  
OF HOURS

\* 7am - 6pm 11 hours

STREET	ENTERING VOLUME	FLOW PERCENT	COMMENTS			
Surface Rd. SB	5755	53.65				
Surface Rd. NB	8848	51.75				
India Street WB	1101	6.06				
India Street EB	1500	7.45				
TOTAL	17604	100				

# TRAFFIC MOVEMENT SUMMARY TABLE

LOCATION India Street & J. F. F. Surface Rd. CITY OR TOWN Boston Proper

DATE 11/16 & 19/79 DAY OF WEEK Fri & Mon WEATHER Clear & Cold RECORDER TP & JT  
# 1053

TIME STARTS -- M	Surface Rd. Southbound			Surface Rd. Northbound			India Street Westbound			India Street Eastbound			TOTAL HALF H TAL
	L <sub>1</sub>	S <sub>1</sub>			S <sub>2</sub>	R <sub>2</sub>	L <sub>3</sub>		R <sub>3</sub>	L <sub>4</sub>	S <sub>4</sub>	R <sub>4</sub>	
7:00-7:30	7	182			309	9	31		19	6	6	28	59
7:30-8:00	13	176			347	10	35		22	5	11	36	146
8:00-8:30	11	216			411	15	41		24	8	12	41	269
8:30-9:00	14	189			389	12	38		13	6	9	26	169
9:00-9:30	10	163			384	4	40		21	5	6	24	55
9:30-10:00	12	184			314	7	36		21	6	10	27	127
10:00-10:30	11	190			286	15	35		23	4	5	25	113
10:30-11:00	11	144			362	12	42		21	9	11	25	642
11:00-11:30	10	200			314	12	27		22	6	12	20	166
11:30-12:00	14	204			319	14	30		15	13	10	51	67
12:00-12:30	17	203			219	13	52		21	9	8	56	169
12:30-1:00	10	244			322	11	40		14	11	7	49	212
1:00-1:30	7	216			308	8	30		12	6	5	45	63
1:30-2:00	5	252			253	8	41		15	9	5	63	65
2:00-2:30	8	209			296	9	29		18	12	11	39	63
2:30-3:00	6	268			292	7	24		12	5	9	22	115
3:00-3:30	17	211			302	8	36		15	10	12	44	155
3:30-4:00	40	253			465	12	37		27	2	7	38	98
4:00-4:30	20	436			697	25	32		13	7	5	63	129
4:30-5:00	14	440			692	14	46		13	6	4	21	136
5:00-5:30	6	428			678	15	40		11	5	6	20	126
5:30-6:00	10	359			540	11	31		16	8	6	59	104
6:00-6:30													
6:30-7:00													
7:00-7:30	25	405			798	27	79		37	14	21	57	
7:30-8:00													
8:00-8:30													
8:30-9:00	34	876			1384	39	78		210	8	9	84	
9:00-9:30													
9:30-10:00													
10:00-10:30													
10:30-11:00													
TOTAL	372	5412			1500	351	802						GRA TOT
TOTAL OF		57250			33485		100						171

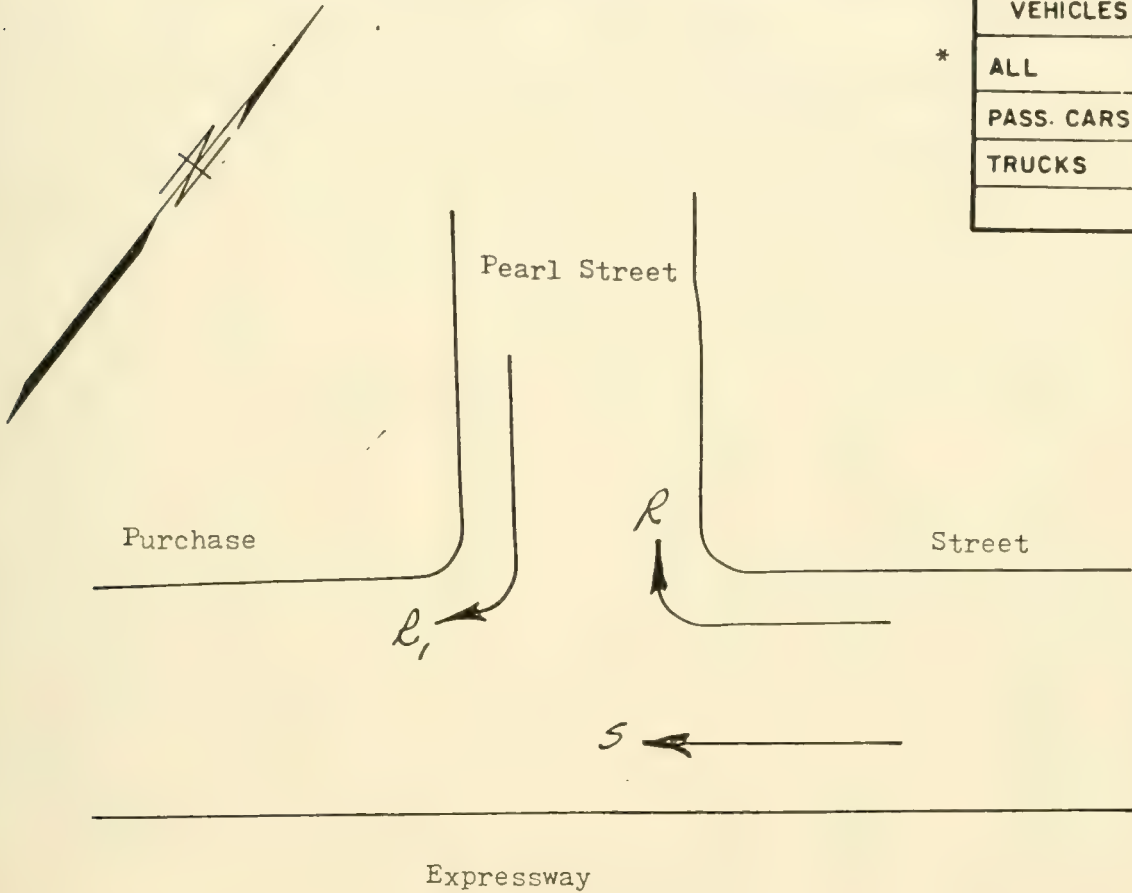
# PLANNING ENGINEERING & DEVELOPMENT

INT. NO.

\* 7/30&31/79

CITY Boston Proper  
 INTERSECTION Pearl Street &  
Purchase Street  
 DATE \* DAY OF WEEK Thur-Fri

INTERSECTION TURNING MOVEMENT COUNT #59 BRA #602



VEHICLES COUNTED	
ALL	X
PASS. CARS	
TRUCKS	(X)

## WEATHER

Fair

## COUNT TAKEN BY

W.C.

## LENGTH OF COUNT

TIME NUMBER OF HOURS

\* 7am-6pm 11 hours

STREET		ENTERING VOLUME	FLOW PERCENT	COMMENTS			
Purchase St.	SB	8593	99.8				
Pearl St.	EB	16	0.2				
TOTAL		9609	100.0%				



STA.NQ 5'

BR.

# TRAFFIC MOVEMENT SUMMARY TABLE

LOCATION Pearl Street & Purchase Street CITY OR TOWN Boston Proper

DATE 7/30&31/79 DAY OF WEEK Thur-Fri WEATHER Fair RECORDER W.C.

#602

TIME STARTS -- M	Purchase St.		Pearl Street								TOTAL HALF HOUR TALLY
	Southbound		Eastbound								
	5	R		R <sub>1</sub>							
7:00-7:30	385	9		1							39
7:30-8:00	445	20		1							46
8:00-8:30	502	28		2							53
8:30-9:00	402	23		0							42
9:00-9:30	402	14		0							41
9:30-10:00	315	7		1							32
10:00-10:30	329	22		0							35
10:30-11:00	276	12		0							28
11:00-11:30	278	22		0							30
11:30-12:00	318	12		0							33
12:00-12:30	387	18		0							40
12:30-1:00	340	18		0							35
1:00-1:30	366	23		0							38
1:30-2:00	318	24		1							34
2:00-2:30	370	18		0							38
2:30-3:00	357	22		0							37
3:00-3:30	362	26		3							39
3:30-4:00	400	21		3							42
4:00-4:30	425	14		1							44
4:30-5:00	440	14		2							45
5:00-5:30	413	11		0							42
5:30-6:00	368	17		1							38
6:00-6:30											
6:30-7:00											
7:00-7:30											
7:30-8:00											
8:00-8:30											
8:30-9:00											
9:00-9:30											
9:30-10:00											
10:00-10:30											
10:30-11:00											
TOTAL	8198	395		16							GRAND TOTAL
TOTAL OF LS BR	8593			16							860



# MECHANICAL RECORDER COUNT RECORD



**Vanasse / Hangen Associates, Inc.**  
 Transportation Engineers & Planners  
 184 High Street, Boston, Massachusetts 02110  
 617 / 482-0749

CALCULATED BY: PD/SS DATE 19 December 81

CITY / TOWN: Boston STATE MA

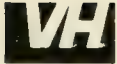
LOCATION: Central Artery Off Ramp at Atlantic Ave/

Northbound JOB No. 0121-10 Northern Ave.  
 DIR. SHEET 1 OF 1

TIME \ MONTH 11/81	Sun. 16	Mon. 16	Tue. 17	Wed. 18	Thu. 19	Fri. 20	Sat.	TOTAL
12 - 1 A.M.			53	46				99
1 - 2 A.M.			21	28				49
2 - 3 A.M.			28	38				66
3 - 4 A.M.			21	16				37
4 - 5 A.M.			35	24				59
5 - 6 A.M.			125	114				239
6 - 7 A.M.			336	328				664
7 - 8 A.M.			575	632				1207
8 - 9 A.M.			1110	1004				2114
9 - 10 A.M.			767	687				1454
10 - 11 A.M.			430	412				842
11 - 12 NOON		386	445	497				1328
12 - 1 P.M.		401	419	435				1255
1 - 2 P.M.		315	318	336				969
2 - 3 P.M.		331	326	344				1001
3 - 4 P.M.		468	583	625				1676
4 - 5 P.M.		459	729	829				2017
5 - 6 P.M.		694	714	485				1893
6 - 7 P.M.		330	308	679				1317
7 - 8 P.M.		212	279	389				880
8 - 9 P.M.		126	162	106				394
9 - 10 P.M.		100	142	80				322
10 - 11 P.M.		111	103	61				275
11 - 12 MID.		62	96	39				197
TOTAL		3995	8125	8234				20354

Avg. Sat. \_\_\_\_\_ Avg. Sun. \_\_\_\_\_ Avg. Weekday 8,234

# MECHANICAL RECORDER COUNT RECORD



**Vanasse / Hangen Associates, Inc.**  
 Transportation Engineers & Planners  
 184 High Street, Boston, Massachusetts 02110  
 617 / 482-0749

CALCULATED BY: GT DATE 10 December 81  
 CITY / TOWN: Boston STATE MA  
 LOCATION: Northern Avenue Bridge  
 DIR. Total JOB No. 0121-10 SHEET 1 OF 1

TIME \ MONTH 11/81	Sun. 15	Mon. 16	Tue. 17	Wed. 18/11	Thu. 12	Fri. 13	Sat. 14	TOTAL
12 - 1 A.M.	399	98	90	107	76	137	243	1150
1 - 2 A.M.	169	29	43	32	42	76	132	523
2 - 3 A.M.	220	31	17	36	18	84	137	543
3 - 4 A.M.	35	21	12	19	20	35	34	176
4 - 5 A.M.	17	42	39	42	39	37	27	243
5 - 6 A.M.	26	192	149	143	180	169	46	905
6 - 7 A.M.	40	489	427	416	502	529	104	2507
7 - 8 A.M.	76	989	1044	998	1125	1114	227	5573
8 - 9 A.M.	92	1359	1416	1237	1470	1373	312	7268
9 - 10 A.M.	129	1143	1025	1084	1249	1124	330	6084
10 - 11 A.M.	194	799	811	738	726	926	504	4688
11 - 12 NOON	356	754	905	862 ↑ 11/18	1076	1085	614	5652
12 - 1 P.M.	662	916	1029	↓ 11/11 897	1147	1321	745	6607
1 - 2 P.M.	676	831	1932	945	1163	1062	826	6535
2 - 3 P.M.	784	888	991	972	1183	1368	889	7075
3 - 4 P.M.	746	1179	1211	1055	1343	1448	985	7967
4 - 5 P.M.	799	1481	1308	1076	1639	1744	972	9019
5 - 6 P.M.	759	1563	1568	1107	1793	1591	907	9288
6 - 7 P.M.	548	999	1022	826	1175	1218	1040	6828
7 - 8 P.M.	523	668	703	757	772	1044	1069	5536
8 - 9 P.M.	378	524	605	582	673	867	1032	4661
9 - 10 P.M.	231	529	460	529	607	824	909	3985
10 - 11 P.M.	198	369	406	484	473	719	784	3433
11 - 12 MID.	138	225	323	269	392	668	750	2765
TOTAL	8075	16018	16636	15213	18892	20563	13614	109011

Avg. Sat. 13,614 Avg. Sun. 8,075 Avg. Weekday 20,563

# MECHANICAL RECORDER COUNT SUMMARY

VANASSE HANGEN ASSOCIATES, INC.  
 TRANSPORTATION ENGINEERS & PLANNERS  
 184 HIGH STREET, BOSTON MA 02110  
 617-482-1870  
 CALCULATOR: WPA JOB NO: 0923  
 DATE: 7/25 YEAR: 1984 (WEDNESDAY)

LOCATION: SURFACE RD 20' S STATE ST  
 BOSTON, MA.  
 DIRECTION: TOTAL  
 COUNT INTERVAL: 60 minutes  
 START TIME: 4:00 P.M.  
 END TIME: 4:00 A.M. WKDY

TIME	SUN	MON	TUES	WED	THUR	FRI	SAT	TOTAL	HRLY AVG
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AM									
12-01	0	0	0	0	473	485	0	958	479
01-02	0	0	0	0	313	371	0	684	342
02-03	0	0	0	0	164	235	0	399	200
03-04	0	0	0	0	90	75	0	165	83
04-05	0	0	0	0	28	0	0	28	28
05-06	0	0	0	0	79	0	0	79	79
06-07	0	0	0	0	418	0	0	418	418
07-08	0	0	0	0	848	0	0	848	848
08-09	0	0	0	0	733	0	0	733	733
09-10	0	0	0	0	804	0	0	804	804
10-11	0	0	0	0	1219	0	0	1219	1219
11-12N	0	0	0	0	1360	0	0	1360	1360

PM									
12-01	0	0	0	0	1148	0	0	1148	1148
01-02	0	0	0	0	1190	0	0	1190	1190
02-03	0	0	0	0	1177	0	0	1177	1177
03-04	0	0	0	0	1579	0	0	1579	1579
04-05	0	0	0	1788	1953	0	0	3741	1871
05-06	0	0	0	2002	1760	0	0	3762	1881
06-07	0	0	0	1539	1300	0	0	2839	1420
07-08	0	0	0	1172	1014	0	0	2186	1093
08-09	0	0	0	957	881	0	0	1838	919
09-10	0	0	0	870	850	0	0	1720	860
10-11	0	0	0	757	892	0	0	1649	825
11-12M	0	0	0	583	675	0	0	1258	629

TOTAL	0	0	0	9668	21165	1166	0	31999	21589
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AVERAGE WEEKDAY DAILY TRAFFIC: 21589 VEHICLES PER DAY (VPD)

AM	%	PEAK	MIDDAY	%	PEAK	PM	%	PEAK
PEAK	OF	HOUR	PEAK	OF	HOUR	PEAK	OF	HOUR
HOUR	ADT	FACTOR	HOUR	ADT	FACTOR	HOUR	ADT	FACTOR
(VPH)	(%)	(PHF)	(VPH)	(%)	(PHF)	(VPH)	(%)	(PHF)

848	4 %	0	2170	10 %	0	2002	9 %	0
AM PEAK HOUR: 7:00- 8:00		M'DAY PEAK HR: 15:00- 16:00PM		PEAK HOUR: 17:00- 18:00				

AVERAGE SATURDAY: 0 VPD

PEAK	%	PEAK
HOUR	OF	HOUR
HOUR	ADT	FACTOR
(VPH)	(%)	(PHF)

0 0 % 0  
 SATURDAY PEAK HOUR: 11:00-12:00

AVERAGE SUNDAY: 0 VPD

PEAK	%	PEAK
HOUR	OF	HOUR
HOUR	ADT	FACTOR
(VPH)	(%)	(PHF)

0 0 % 0  
 SUNDAY PEAK HOUR: 11:00-12:00

# MECHANICAL RECORDER COUNT RECORD



**Vanasse / Hangen Associates, Inc.**  
 Transportation Engineers & Planners  
 184 High Street, Boston, Massachusetts 02110  
 617 / 482-0749

CALCULATED BY: PD/SS DATE 19 November 81  
 CITY/TOWN: Boston STATE MA  
 LOCATION: Atlantic Ave. South Of Ramp/Northern Ave.  
 DIR. Northbound JOB No. 0121-10 SHEET 1 OF 1

TIME \ MONTH 11/81	Sun. 16	Mon. 16	Tue. 17	Wed. 18	Thu. 19	Fri. 20	Sat.	TOTAL
12 - 1 A.M.			112	133				245
1 - 2 A.M.			47	90				137
2 - 3 A.M.			62	65				127
3 - 4 A.M.			44	51				95
4 - 5 A.M.			76	83				159
5 - 6 A.M.			234	194				428
6 - 7 A.M.			505	616				1121
7 - 8 A.M.			1114	1203				2317
8 - 9 A.M.			1204	1245				2339
9 - 10 A.M.			989	1111				2093
10 - 11 A.M.			823	920				1743
11 - 12 NOON		911	951	1020				2882
12 - 1 P.M.		922	849	926				2697
1 - 2 P.M.		820	888	933				2641
2 - 3 P.M.		946	851	907				2704
3 - 4 P.M.		1032	1044	1277				3353
4 - 5 P.M.		1215	1307	1451				3973
5 - 6 P.M.		1354	1244	1441				4039
6 - 7 P.M.		868	788	1511				3167
7 - 8 P.M.		499	539	692				1730
8 - 9 P.M.		300	446	401				1147
9 - 10 P.M.		249	301	327				877
10 - 11 P.M.		183	201	260				644
11 - 12 MID.		137	189	180				506
TOTAL		9436	14801	17037				41274

Avg. Sat. \_\_\_\_\_ Avg. Sun. \_\_\_\_\_ Avg. Weekday 17,037



# MECHANICAL RECORDER COUNT SUMMARY

VANASSE HANGEN ASSOCIATES, INC.  
TRANSPORTATION ENGINEERS & PLANNERS  
184 HIGH STREET, BOSTON MA 02110  
617-482-1870  
CALCULATOR: WPA JOB NO: 0923  
DATE: 7/25 YEAR: 1984 (WEDNESDAY)

LOCATION: SURFACE RD 20' S STATE ST.  
BOSTON, MA.  
DIRECTION: NORTHBOUND  
COUNT INTERVAL: 60 minutes  
START TIME: 4:00 P.M.  
END TIME: 4:00 A.M. WKDY  
HRLY  
AVG

TIME	SUN	MON	TUES	WED	THUR	FRI	SAT	TOTAL	WKDY HRLY AVG
AM									
12-01	0	0	0	0	171	176	0	347	174
01-02	0	0	0	0	74	116	0	190	95
02-03	0	0	0	0	55	85	0	140	70
03-04	0	0	0	0	22	30	0	52	26
04-05	0	0	0	0	0	0	0	0	0
05-06	0	0	0	0	0	0	0	0	0
06-07	0	0	0	0	0	0	0	0	0
07-08	0	0	0	0	0	0	0	0	0
08-09	0	0	0	0	0	0	0	0	0
09-10	0	0	0	0	0	0	0	0	0
10-11	0	0	0	0	575	0	0	575	575
11-12N	0	0	0	0	612	0	0	612	612
PM									
12-01	0	0	0	0	448	0	0	448	448
01-02	0	0	0	0	474	0	0	474	474
02-03	0	0	0	0	500	0	0	500	500
03-04	0	0	0	0	831	0	0	831	831
04-05	0	0	0	1091	1053	0	0	2144	1072
05-06	0	0	0	1275	1047	0	0	2322	1161
06-07	0	0	0	759	668	0	0	1427	714
07-08	0	0	0	441	375	0	0	816	408
08-09	0	0	0	371	372	0	0	743	372
09-10	0	0	0	315	329	0	0	644	322
10-11	0	0	0	270	308	0	0	578	289
11-12M	0	0	0	225	256	0	0	481	241
TOTAL	0	0	0	4747	8170	407	0	13324	8495

AVERAGE WEEKDAY DAILY TRAFFIC: 8495				VEHICLES PER DAY (VPD)				
AM	%	PEAK	MIDDAY	%	PEAK	PM	%	PEAK
PEAK	OF	HOUR	PEAK	OF	HOUR	PEAK	OF	HOUR
HOUR	ADT	FACTOR	HOUR	ADT	FACTOR	HOUR	ADT	FACTOR
(VPH)	(%)	(PHF)	(VPH)	(%)	(PHF)	(VPH)	(%)	(PHF)
0	0 %	0	1053	12 %	0	1275	15 %	0
AM PEAK HOUR: -1:00- 0:00 M'DAY PEAK HR: 15:00- 16:00 PM PEAK HOUR: 17:00- 18:00								

AVERAGE SATURDAY: 0			VPD			AVERAGE SUNDAY: 0			VPD		
PEAK	%	PEAK	PEAK	%	PEAK	PEAK	%	PEAK	PEAK	%	PEAK
HOUR	OF	HOUR	HOUR	OF	HOUR	HOUR	OF	HOUR	HOUR	OF	HOUR
HOUR	ADT	FACTOR	HOUR	ADT	FACTOR	HOUR	ADT	HOUR	HOUR	ADT	FACTOR
(VPH)	(%)	(PHF)	(VPH)	(%)	(PHF)	(VPH)	(%)	(VPH)	(VPH)	(%)	(PHF)

0 0 % 0  
SATURDAY PEAK HOUR: 11:00-12:00  
0 0 % 0  
SUNDAY PEAK HOUR: 11:00-12:00



# MECHANICAL RECORDER COUNT SUMMARY

VANASSE HANGEN ASSOCIATES, INC.  
 TRANSPORTATION ENGINEERS & PLANNERS  
 184 HIGH STREET, BOSTON MA 02110  
 617-482-1870  
 CALCULATOR: WPA JOB NO: 0923  
 DATE: 7/25 YEAR: 1984 (WEDNESDAY)

LOCATION: SURFACE RD. 20' S STATE ST.  
 BOSTON MA.  
 DIRECTION: SOUTHBOUND  
 COUNT INTERVAL: 60 minutes  
 START TIME: 4:00 P.M.  
 END TIME: 4:00 A.M. WKDY  
 HRLY  
 AVG

TIME	SUN	MON	TUES	WED	THUR	FRI	SAT	TOTAL	WKDY HRLY AVG
AM									
12-01	0	0	0	0	302	309	0	611	306
01-02	0	0	0	0	239	255	0	494	247
02-03	0	0	0	0	109	150	0	259	130
03-04	0	0	0	0	68	45	0	113	57
04-05	0	0	0	0	28	0	0	28	28
05-06	0	0	0	0	79	0	0	79	79
06-07	0	0	0	0	418	0	0	418	418
07-08	0	0	0	0	848	0	0	848	848
08-09	0	0	0	0	733	0	0	733	733
09-10	0	0	0	0	804	0	0	804	804
10-11	0	0	0	0	644	0	0	644	644
11-12N	0	0	0	0	748	0	0	748	748
PM									
12-01	0	0	0	0	700	0	0	700	700
01-02	0	0	0	0	716	0	0	716	716
02-03	0	0	0	0	677	0	0	677	677
03-04	0	0	0	0	748	0	0	748	748
04-05	0	0	0	697	900	0	0	1597	798
05-06	0	0	0	727	930	0	0	1657	829
06-07	0	0	0	780	632	0	0	1412	706
07-08	0	0	0	731	639	0	0	1370	685
08-09	0	0	0	586	509	0	0	1095	548
09-10	0	0	0	555	521	0	0	1076	538
10-11	0	0	0	487	584	0	0	1071	536
11-12M	0	0	0	358	419	0	0	777	389
TOTAL	0	0	0	4921	12995	759	0	18675	13097

AVERAGE WEEKDAY DAILY TRAFFIC: 13097 VEHICLES PER DAY (VPD)									
AM	%	PEAK	MIDDAY	%	PEAK	PM	%	PEAK	
PEAK	OF	HOUR	PEAK	OF	HOUR	PEAK	OF	HOUR	
HOUR	ADT	FACTOR	HOUR	ADT	FACTOR	HOUR	ADT	FACTOR	
(VPH)	(%)	(PHF)	(VPH)	(%)	(PHF)	(VPH)	(%)	(PHF)	
848	6 %	0	1117	9 %	0	748	6 %	0	
AM PEAK HOUR: 7:00- 8:00 M'DAY PEAK HR: 15:00- 16:00PM PEAK HOUR: 16:00- 17:00									

AVERAGE SATURDAY: 0 VPD					AVERAGE SUNDAY: 0 VPD				
PEAK	%	PEAK			PEAK	%	PEAK		
HOUR	OF	HOUR			HOUR	OF	HOUR		
(VPH)	ADT	FACTOR			(VPH)	ADT	FACTOR		
	(%)	(PHF)				(%)	(PHF)		

0 0 % 0 0 0  
 SATURDAY PEAK HOUR: 11:00-12:00 SUNDAY PEAK HOUR: 11:00-12:00

## MECHANICAL RECORDER COUNT SUMMARY

VANASSE HANGEN ASSOCIATES, INC.  
 TRANSPORTATION ENGINEERS & PLANNERS  
 184 HIGH STREET, BOSTON MA 02110  
 617-482-1870  
 CALCULATOR: PES JOB NO: 896

LOCATION: BLACKSTONE 200' E. SUDBURY  
 BOSTON, MASS.  
 DIRECTION: SOUTHBOUND ON SURFACE  
 COUNT INTERVAL: 60 minutes  
 START TIME: 12:00

DATE: 07/12 YEAR: 1964 (THURSDAY) END TIME: 1:00 A.M. P.M. WKDY

TIME SUN MON TUES WED THUR FRI SAT TOTAL HRLY AVG

AM  
 12-01 349 134 0 0 0 259 388 1130 197  
 01-02 251 100 0 0 0 177 324 852 139  
 02-03 210 80 0 0 0 124 261 675 102  
 03-04 65 82 0 0 0 62 88 297 72  
 04-05 27 43 0 0 0 49 59 178 46  
 05-06 43 66 0 0 0 100 71 280 83  
 06-07 58 285 0 0 0 334 141 818 310  
 07-08 90 534 0 0 0 451 206 1281 493  
 08-09 142 618 0 0 0 411 326 1497 515  
 09-10 220 521 0 0 0 468 367 1576 495  
 10-11 283 509 0 0 0 528 352 1672 519  
 11-12M 417 579 0 0 0 657 377 2030 618

PM  
 12-01 420 637 0 0 619 554 397 2627 603  
 01-02 399 0 0 0 596 569 393 1957 583  
 02-03 329 0 0 0 653 639 363 1984 646  
 03-04 0 0 0 0 724 771 350 1845 748  
 04-05 418 0 0 0 709 756 292 2175 733  
 05-06 628 0 0 0 680 563 238 2109 622  
 06-07 586 0 0 0 722 593 272 2173 658  
 07-08 519 0 0 0 668 557 315 2059 613  
 08-09 516 0 0 0 598 615 300 2029 607  
 09-10 400 0 0 0 559 547 549 2055 553  
 10-11 273 0 0 0 496 535 695 1999 516  
 11-12M 0 0 0 0 377 515 480 1372 446

TOTAL 6643 4188 0 0 7401 10834 7604 36670 10917

AVERAGE WEEKDAY DAILY TRAFFIC: 10917 VEHICLES PER DAY (VPD)

AM	%	PEAK	MIDDAY	%	PEAK	PM	%	PEAK
PEAK	OF	HOUR	PEAK	OF	HOUR	PEAK	OF	HOUR
HOUR	ADT	FACTOR	HOUR	ADT	FACTOR	HOUR	ADT	FACTOR
(VPH)	(%)	(PHF)	(VPH)	(%)	(PHF)	(VPH)	(%)	(PHF)

618 6 % 0 771 7 % 0 756 7 % 0  
 AM PEAK HOUR: 8:00- 9:00 M'DAY PEAK HR: 15:00- 16:00PM PEAK HOUR: 16:00- 17:00

AVERAGE SATURDAY: 317 VPD

PEAK	%	PEAK
HOUR	OF	HOUR
HOUR	ADT	FACTOR
(VPH)	(%)	(PHF)

AVERAGE SUNDAY: 277 VPD

PEAK	%	PEAK
HOUR	OF	HOUR
HOUR	ADT	FACTOR
(VPH)	(%)	(PHF)

695 6 % 0  
 SATURDAY PEAK HOUR: 10:00-11:00

628 6 % 0  
 SUNDAY PEAK HOUR: 5:00-6:00

# MECHANICAL RECORDER COUNT SUMMARY

VANASSE HANGEN ASSOCIATES, INC.  
TRANSPORTATION ENGINEERS & PLANNERS  
184 HIGH STREET, BOSTON MA 02110  
617-482-1870  
CALCULATOR: PES JOB NO: 896  
DATE: 07/12 YEAR: 1984 (THURSDAY)

LOCATION: BLACKSTONE 200' E. SUDBURY  
BOSTON, MASS.  
DIRECTION: SOUTHBOUND ON RAMP  
COUNT INTERVAL: 60 minutes  
START TIME: 12:00 A.M.  
END TIME: 1:00 P.M.

TIME	SUN	MON	TUES	WED	THUR	FRI	SAT	TOTAL	WKDY HRLY AVG
AM									
12-01	209	103	0	0	0	138	293	743	121
01-02	174	66	0	0	0	96	226	562	81
02-03	159	63	0	0	0	89	162	473	76
03-04	63	26	0	0	0	39	92	220	33
04-05	31	16	0	0	0	28	58	133	22
05-06	38	51	0	0	0	98	71	258	75
06-07	68	380	0	0	0	478	144	1070	429
07-08	116	674	0	0	0	552	176	1518	613
08-09	147	624	0	0	0	304	229	1304	464
09-10	231	450	0	0	0	406	315	1402	428
10-11	248	444	0	0	0	398	339	1429	421
11-12N	319	529	0	0	0	434	242	1524	482
PM									
12-01	325	482	0	0	414	415	262	1898	437
01-02	295	40	0	0	493	400	268	1456	447
02-03	208	0	0	0	456	381	282	1327	419
03-04	0	0	0	0	671	433	228	1332	552
04-05	250	0	0	0	459	428	223	1360	444
05-06	250	0	0	0	269	307	234	1060	288
06-07	249	0	0	0	418	347	235	1249	383
07-08	282	0	0	0	439	394	190	1305	417
08-09	290	0	0	0	312	409	211	1222	361
09-10	251	0	0	0	450	376	301	1378	413
10-11	202	0	0	0	409	446	456	1513	428
11-12M	0	0	0	0	301	440	331	1072	371
TOTAL	4405	3908	0	0	5091	7836	5568	26808	8205

AVERAGE WEEKDAY DAILY TRAFFIC: 8205

VEHICLES PER DAY (VPD)

AM	%	PEAK	MIDDAY	%	PEAK	PM	%	PEAK
PEAK	OF	HOUR	PEAK	OF	HOUR	PEAK	OF	HOUR
HOUR	ADT	FACTOR	HOUR	ADT	FACTOR	HOUR	ADT	FACTOR
(VPH)	(%)	(PHF)	(VPH)	(%)	(PHF)	(VPH)	(%)	(PHF)

674 8 % 0 671 8 % 0 459 6 % 0  
AM PEAK HOUR: 7:00- 8:00 M'DAY PEAK HR: 15:00- 16:00PM PEAK HOUR: 16:00- 17:00

AVERAGE SATURDAY: 232 VPD

AVERAGE SUNDAY: 184 VPD

PEAK	%	PEAK	PEAK	%	PEAK
HOUR	OF	HOUR	HOUR	OF	HOUR
(VPH)	ADT	FACTOR	(VPH)	ADT	FACTOR
(VPH)	(%)	(PHF)	(VPH)	(%)	(PHF)

456 6 % 0  
SATURDAY PEAK HOUR: 10:00-11:00

325 4 % 0  
SUNDAY PEAK HOUR: 12:00-1:00

Town: BOSTON, MA

Location: High Street (30' East of Batterymarch St.)

Direction: Westbound

Month Hour 1980	11	Sun.	Mon.	Tues.	Wed.	Thu.	Fri.	Sat.	Total
		16	17			13	14	15	
12 - 1A.M.		45	17				29	50	
1 - 2A.M.		34	9				20	29	
2 - 3A.M.		18	9				22	28	
3 - 4A.M.		4	8				14	16	
4 - 5A.M.		3	11				10	21	
5 - 6A.M.		9	49				43	15	
6 - 7A.M.		23	165				163	64	
7 - 8A.M.		38	397				380	162	
8 - 9A.M.		42	578				620	169	
9 - 10A.M.		45	474				473	174	
10 - 11A.M.		50	376				366	184	
11 - 12P.M.		99					389	192	
12 - 1P.M.		71					348	184	
1 - 2P.M.		89					339	173	
2 - 3P.M.		88				389	394	152	
3 - 4P.M.		108				306	311	163	
4 - 5P.M.		95				376	371	122	
5 - 6P.M.		55				305	281	91	
6 - 7P.M.		52				228	191	63	
7 - 8P.M.		42				120	147	76	
8 - 9P.M.		22				97	140	77	
9 - 10P.M.		28				69	137	73	
10 - 11P.M.		32				95	102	68	
11 - 12MID.		39				63	81	71	
TOTAL		1131	2093			2048	5371	2417	

Avg. Sat. 2417 Avg. Sun. 1131 Avg. Weekday 5371



# NATIONAL RECORDER COUNT RECORD

VH #80-101

Town: BOSTON, MA

Location: Franklin St. (East of Oliver St.)

Direction: Westbound

Month 11	Sun.	Mon.	Tues.	Wed.	Thu.	Fri.	Sat.	Total
Hour 1980		10	11*	12	13			
12 - 1A.M.			37	19	25			
1 - 2A.M.			43	30	18			
2 - 3A.M.			8	7				
3 - 4A.M.			6	2				
4 - 5A.M.			9	17				
5 - 6A.M.			9	23				
6 - 7A.M.			35	70				
7 - 8A.M.			116	237				
8 - 9A.M.			253	367				
9 - 10A.M.			217	354				
10 - 11A.M.			146	259	73	93		571
11 - 12P.M.			174	223	82	142		621
12 - 1P.M.			155	218				
1 - 2P.M.			201	210				
2 - 3P.M.			169	260				
3 - 4P.M.			142	246				
4 - 5P.M.		250	140	261				
5 - 6P.M.		124	81	187				
6 - 7P.M.		102	34	131				
7 - 8P.M.		92	54	95				
8 - 9P.M.		38	40	73				
9 - 10P.M.		47	31	62				
10 - 11P.M.		53	47	64				
11 - 12MID.		47	36	63				
TOTAL		753	2183	3478	43			

Avg. Sat. \_\_\_\_\_ Avg. Sun. \_\_\_\_\_ Avg. Weekday 3478

\* VETERAN'S DAY

## MECHANICAL RECORDER COUNT RECORD VII 480-101

Town: BOSTONLocation: Oliver St. (South of Franklin St.)Direction: Northbound

Month Hour 1980	Sun. 11	Mon. 10	Tues. 11*	Wed. 12	Thu. 13	Fri.	Sat.	Total
12 - 1A.M.			40	19	34			
1 - 2A.M.			14	11	15			
2 - 3A.M.			18	1				
3 - 4A.M.			12	10				
4 - 5A.M.			12	17				
5 - 6A.M.			17	74				
6 - 7A.M.			104	187				
7 - 8A.M.			235	275				
8 - 9A.M.			368	575				
9 - 10A.M.			199	411				
10 - 11A.M.			155	296	146	259		
11 - 12P.M.			175	279	174	223		
12 - 1P.M.			207	215				
1 - 2P.M.			197	239				
2 - 3P.M.			163	319				
3 - 4P.M.			139	301				
4 - 5P.M.		207	130	328				
5 - 6P.M.		201	102	204				
6 - 7P.M.		137	79	170				
7 - 8P.M.		99	44	138				
8 - 9P.M.		76	31	76				
9 - 10P.M.		101	22	80				
10 - 11P.M.		67	44	64				
11 - 12MID.		45	50	53				
TOTAL		933	2557	4342	49			

Avg. Sat. \_\_\_\_\_ Avg. Sun. \_\_\_\_\_ Avg. Weekday 4342

\* VETERAN'S DAY

# MECHANICAL RECORDER COUNT RECORD



**Vanasse / Hangen Associates, Inc.**  
 Transportation Engineers & Planners  
 184 High Street, Boston, Massachusetts 02110  
 617 / 482-0749

CALCULATED BY: GHA DATE: 4/24/82

CITY/TOWN: Boston STATE MA

LOCATION: Oliver St. North of the Parking Garage

DIR. Total JOB No. 0266-10 SHEET OF Entrance

TIME \ MONTH	April 1982	Sun.	Mon.	Tue. 20	Wed. 21	Thu. 22	Fri. 23	Sat.	TOTAL
12 - 1 A.M.					35	46	69		150
1 - 2 A.M.					12	15	52		79
2 - 3 A.M.					14	18	37		69
3 - 4 A.M.					6	9	11		25
4 - 5 A.M.					6	6	7		19
5 - 6 A.M.					28	39	39		106
6 - 7 A.M.					56	69	65		190
7 - 8 A.M.					89	75	94		258
8 - 9 A.M.					124	131	117		372
9 - 10 A.M.					153	179	169		501
10 - 11 A.M.					147	173	135		455
11 - 12 NOON					211	156	166		533
12 - 1 P.M.					153	168	201		522
1 - 2 P.M.					190	187			377
2 - 3 P.M.					219	171			390
3 - 4 P.M.				204	189	173			566
4 - 5 P.M.				256	219	232			707
5 - 6 P.M.				196	213	289			698
6 - 7 P.M.				154	144	156			454
7 - 8 P.M.				93	96	108			297
8 - 9 P.M.				82	75	93			250
9 - 10 P.M.				54	64	85			203
10 - 11 P.M.				48	67	129			244
11 - 12 MID.				43	46	82			171
TOTAL				1130	2556	2789	1162		7637

Avg. Sat. \_\_\_\_\_ Avg. Sun. \_\_\_\_\_ Avg. Weekday 2672

✓

MASSACHUSETTS DEPARTMENT OF PUBLIC WORKS  
BUREAU OF TRANSPORTATION PLANNING & DEVELOPMENT  
VOLUME SUMMARY  
CONDUCTED IN COOPERATION WITH FEDERAL HIGHWAY ADMINISTRATION

Year 1979

Station No. 8222 - 2 Way Traffic

Month December

Route No. \_\_\_\_\_

Town Boston

or  
Street Northern Avenue Bridge; Over  
Fort Point Channel

Day	Sunday	Monday	Tuesday	Wednesday	Thursday	Friday	Saturday	Total
Date				12-5-79	12-6-79	12-7-79		
12 - 1 A.M.					204	156		
2 - 2					94	86		
3 - 3					62	58		
4 - 4					52	68		
5 - 5					74	82		
6 - 6					239	226		
7 - 7					516	527		
8 - 8					1,217	1,223		
9 - 9				77	1,336	1,348		
10 - 10				926	1,004	1,016		
11 - 11				911	911	910		
12 - 12				934	967			
1 - 1 P.M.				1,123	1,144	1,169		
2 - 2				1,181	1,151	1,217		
3 - 3				1,237	1,189			
4 - 4				1,339	1,296			
5 - 5				1,806	1,782			
6 - 6				1,446	1,515			
7 - 7				1,126	1,161			
8 - 8				967	1,123			
9 - 9				821	782			
10 - 10				638	557			
11 - 11				536	510			
12 - 12				511	424			
Total				5,642*	10,465*	9,112*		43,000*
				10,477				
Average Per Day								38825

Day	Weather	Road Conditions	Temperature
Monday			
Tuesday			
Wednesday			
Thursday			
Friday			
Saturday			
Sunday			

19413  
100  
19410



# DIVERSIFIED ENGINEERING SERVICES

19 WINTHROP ROAD • BROOKLINE, MASSACHUSETTS 02148

## AUTOMATIC TRAFFIC COUNTER SUMMARY

LOCATION: SUMMER STREET BRIDGE (FORT POINT CH.) OUTBOUND

LOCATION 18

BOSTON CORDON COUNT

YEAR 1982

MONTH SEPT.

DAYS

Hour Month Beginning	Sun.	Mon.	Tue.	Wed.	Thu.	Fri.	Sat.	Total
		9/20	9/21	9/22				
12 - 1 A.M.			89	122				
1 - 2 A.M.			60	107				
2 - 3 A.M.			50	72				
3 - 4 A.M.			76	49				
4 - 5 A.M.			161	191				
5 - 6 A.M.			816	835				
6 - 7 A.M.		1002	1418	1423				
7 - 8 A.M.		1028		1286				
8 - 9 A.M.		880	995	990				
9 - 10 A.M.		877	1393	910				
10 - 11 A.M.		823	1014	841				
11 - 12 Noon		728	894	852				
12 - 1 P.M.		793	976	875				
1 - 2 P.M.		836	1009	879				
2 - 3 P.M.		1014	1022	1297				
3 - 4 P.M.		1066	998	1131				
4 - 5 P.M.		1103	965	1288				
5 - 6 P.M.		716	743	750				
6 - 7 P.M.		428	482	422				
7 - 8 P.M.		358	403	349				
8 - 9 P.M.		336	389	361				
9 - 10 P.M.		360	344	388				
10 - 11 P.M.		194	251	287				
11 - 12 Mid.		184	174	200				
TOTALS			(15,677)	15,922				

Avg Day = 16,008

**DIVERSIFIED ENGINEERING SERVICES**  
18 WINTHROP ROAD • BROOKLINE, MASSACHUSETTS 02108

**AUTOMATIC TRAFFIC COUNTER SUMMARY**

**LOCATION:** SUMMER STREET BRIDGE (FORT POINT CH.) INBOUND  
BOSTON CORDON COUNT

**LOCATION 19**

**YEAR** 1982 **MONTH** SEPT **DAYS**     

Hour Month Beginning	Sun.	Mon.	Tue.	Wed.	Thu.	Fri.	Sat.	Total
		9/20	9/21	9/22				
12 - 1 A.M.			57	209				
1 - 2 A.M.			74	115				
2 - 3 A.M.			47	124				
3 - 4 A.M.			57	89				
4 - 5 A.M.			64	105				
5 - 6 A.M.			54	64				
6 - 7 A.M.		616	516	552				
7 - 8 A.M.		927	999	1186				
8 - 9 A.M.		1153	986	1313				
9 - 10 A.M.		786	748	1293				
10 - 11 A.M.		768	761	914				
11 - 12 Noon		771	1001	719				
12 - 1 P.M.		873	948	522				
1 - 2 P.M.		890	1025	735				
2 - 3 P.M.		769	933	879				
3 - 4 P.M.		983	1148	1015				
4 - 5 P.M.			1118	1192				
5 - 6 P.M.			830					
6 - 7 P.M.			733					
7 - 8 P.M.			511					
8 - 9 P.M.		375	419					
9 - 10 P.M.		342	318					
10 - 11 P.M.		323	323					
11 - 12 MID.		312	352					
TOTALS			(14,000)	(14,500)				

*Avg. Day = 14,132*

TOTAL: 16,008  
14,132  
28,140



**Vanasse / Hangen Engineering, Inc.**  
Consulting Engineers & Planners  
184 High Street, Boston, Massachusetts 02110  
617 / 482-1870

JOB: International Place JOB No. 0923  
LOCATION: \_\_\_\_\_ SHEET \_\_\_\_\_ OF \_\_\_\_\_  
CALCULATED BY: 89 DATE: \_\_\_\_\_  
CHECKED BY: \_\_\_\_\_ DATE: \_\_\_\_\_  
TITLE: Mechanical Recorder Counts

<u>Location</u>	<u>Year</u>	<u>ADT</u>
<u>Atlantic Ave.</u>		
at Northern Ave.	1981	17,040 <sup>2)</sup>
at Northern Ave.	1982	14,650 <sup>4)</sup>
South of Congress St.	1982	10,600 <sup>4)</sup>
NORTH OF NORTHERN AVE.	1982	21,500 <sup>4)</sup>
<u>BLACKSTONE ST.</u>		
EAST OF SUDBURY ST.	1982	3750 <sup>4)</sup>
EAST OF NEW CHARDON ST.	1982	7250 <sup>4)</sup>
<u>CLINTON ST.</u>		
<u>CONGRESS ST.</u>		
EAST OF MILK ST.	1980	9460 <sup>4)</sup>
EAST OF FRANKLIN ST.	1980	12,050 <sup>4)</sup>
EAST OF ATLANTIC AVE.	1981	10,090 <sup>2)</sup>
EAST OF ATLANTIC AVE. (EB)	1982	8800 <sup>4)</sup>
EAST OF ATLANTIC AVE. (WB)	1982	8500 <sup>4)</sup>
 <sup>1)</sup> Traffic Study for a proposed Multi-Office Building by VHA dated Jan., 81. <sup>2)</sup> Comm Pier Five EIR by VHA dated July, 82. <sup>3)</sup> Building 114 Renovation EIR by VHA dated Dec., 82. <sup>4)</sup> Third Harbor Tunnel EIR dated Dec., 82.		



**Vanasse / Hangen Engineering, Inc.**  
Consulting Engineers & Planners  
184 High Street, Boston, Massachusetts 02110  
617 / 482-1870

JOB International Place JOB No. 0923  
LOCATION: \_\_\_\_\_ SHEET \_\_\_\_\_ OF \_\_\_\_\_  
CALCULATED BY: BG DATE \_\_\_\_\_  
CHECKED BY: \_\_\_\_\_ DATE \_\_\_\_\_  
TITLE Mechanical Recorder Counts

<u>Location</u>	<u>Year</u>	<u>ADT</u>
<u>DORCHESTER AVE.</u>		

FRANKLIN ST.

East of OLIVER ST.	1980	3430 <sup>4</sup>
East of PEARL ST.	1980	4390 <sup>4</sup>
At PEARL ST.	1930	3690 <sup>4</sup>

HIGH ST.

East of PEARL ST.	1980	11,120 <sup>4</sup>
East of CONGRESS ST.	1980	7,250 <sup>4</sup>
East of BATTERYMARCH ST.	1930	5370 <sup>4</sup>

MILL ST.

East of BROAD ST.	1980	3420 <sup>4</sup>
East of CONGRESS ST.	1980	1700 <sup>4</sup>

NORTH ST.

EAST OF UNION ST. (EB)	1932	9200 <sup>4</sup>
EAST OF UNION ST. (WB)	1932	7300 <sup>4</sup>

- <sup>1</sup> Traffic Study for a proposed Multi-Office Building by VHA dated Jan., 81.
- <sup>2</sup> Comm Pier Five EIR by VHA dated July, 82.
- <sup>3</sup> Building 114 Renovation EIR by VHA dated Dec., 82.
- <sup>4</sup> Third Harbor Tunnel EIR dated Dec., 82.





**Vanasse / Hangen Engineering, Inc.**  
Consulting Engineers & Planners  
184 High Street, Boston, Massachusetts 02110  
617 / 482-1870

JOB: International Place JOB No. 0923  
LOCATION: \_\_\_\_\_ SHEET \_\_\_\_\_ OF \_\_\_\_\_  
CALCULATED BY: 89 DATE: \_\_\_\_\_  
CHECKED BY: \_\_\_\_\_ DATE: \_\_\_\_\_  
TITLE: Mechanical Recorder Counts

<u>Location</u>	<u>Year</u>	<u>ADT</u>
-----------------	-------------	------------

NORTHERN AVE.

NORTHERN AVE. BRIDGE	1981	20,560 <sup>L2</sup>
EAST OF ATLANTIC AVE. (EB)	1982	8250 <sup>L4</sup>
EAST OF ATLANTIC AVE. (WB)	1982	9800 <sup>L4</sup>

OLIVER ST.

SOUTH OF FRANKLIN ST.	1980	4340 <sup>L4</sup>
-----------------------	------	--------------------

PEARL ST.

SOUTH OF M <sup>R</sup> ST.	1980	5660 <sup>L4</sup>
SOUTH OF FRANKLIN ST.	1980	4740 <sup>L4</sup>

PURCHASE ST.

STATE ST.

EAST OF NEW CONGRESS ST.	1982	16,000 <sup>L4</sup>
EAST OF CENTRAL ARTERY	1982	5100 <sup>L4</sup>

- <sup>11</sup> Traffic study for a proposed Multi-Office Building by VHA dated Jan., 81.
- <sup>31</sup> Comm Pier Five EIR by VHA dated July, 82.
- <sup>31</sup> Building 114 Renovation EIR by VHA dated Dec., 82.
- <sup>41</sup> Third Harbor Tunnel EIR dated Dec., 82.



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JOB: International Place JOB No. 0923  
LOCATION: \_\_\_\_\_ SHEET \_\_\_\_\_ OF \_\_\_\_\_  
CALCULATED BY: 89 DATE: \_\_\_\_\_  
CHECKED BY: \_\_\_\_\_ DATE: \_\_\_\_\_  
TITLE: Mechanical Recorder Counts

Location

Year

ADT

SUMMER ST.

AT FORT POINT CHANNEL	1981	28,290 <sup>12</sup>
AT FORT POINT CHANNEL	1982	28,140 <sup>13</sup>
EAST OF ATLANTIC AVE. (EB)	1982	10,300 <sup>14</sup>
EAST OF ATLANTIC AVE. (WB)	1982	10,000 <sup>14</sup>

SURFACE ARTERY

NORTH OF STATE ST. (SB)	1982	15,750 <sup>14</sup>
SOUTH OF STATE ST. (WB)	1982	14,550 <sup>14</sup>

OFF-RAMP AT HIGH ST

1981	10,020 <sup>14</sup>
1982	12,000 <sup>14</sup>

OFF-RAMP AT NORTHERN AVE  
AND ATLANTIC

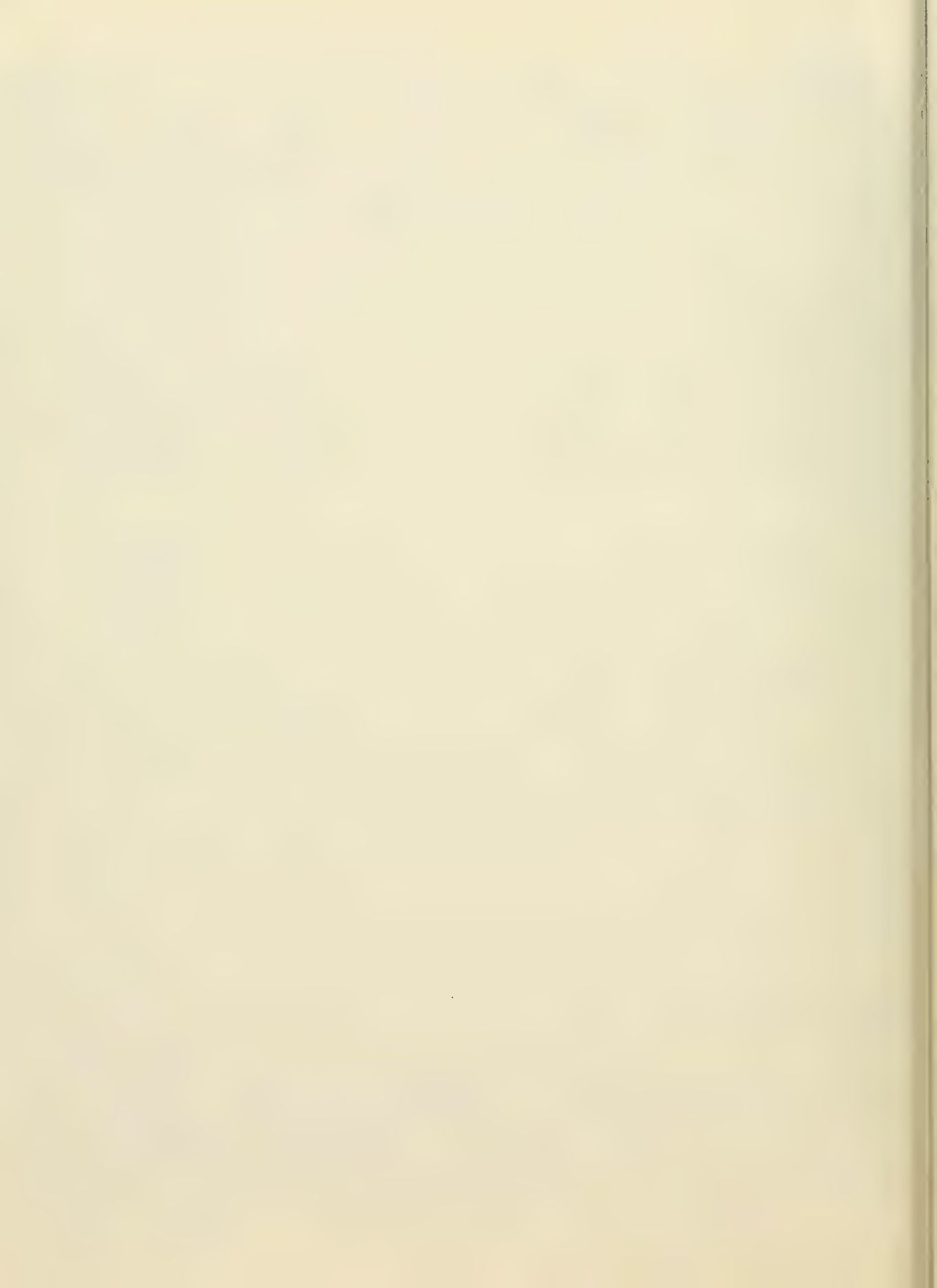
1981	8,230 <sup>13</sup>
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<sup>11</sup> Traffic study for a proposed Multi-Office Building by VHA dated Jan., 81.

<sup>12</sup> Comm Pier Five EIR by VHA dated July, 82.

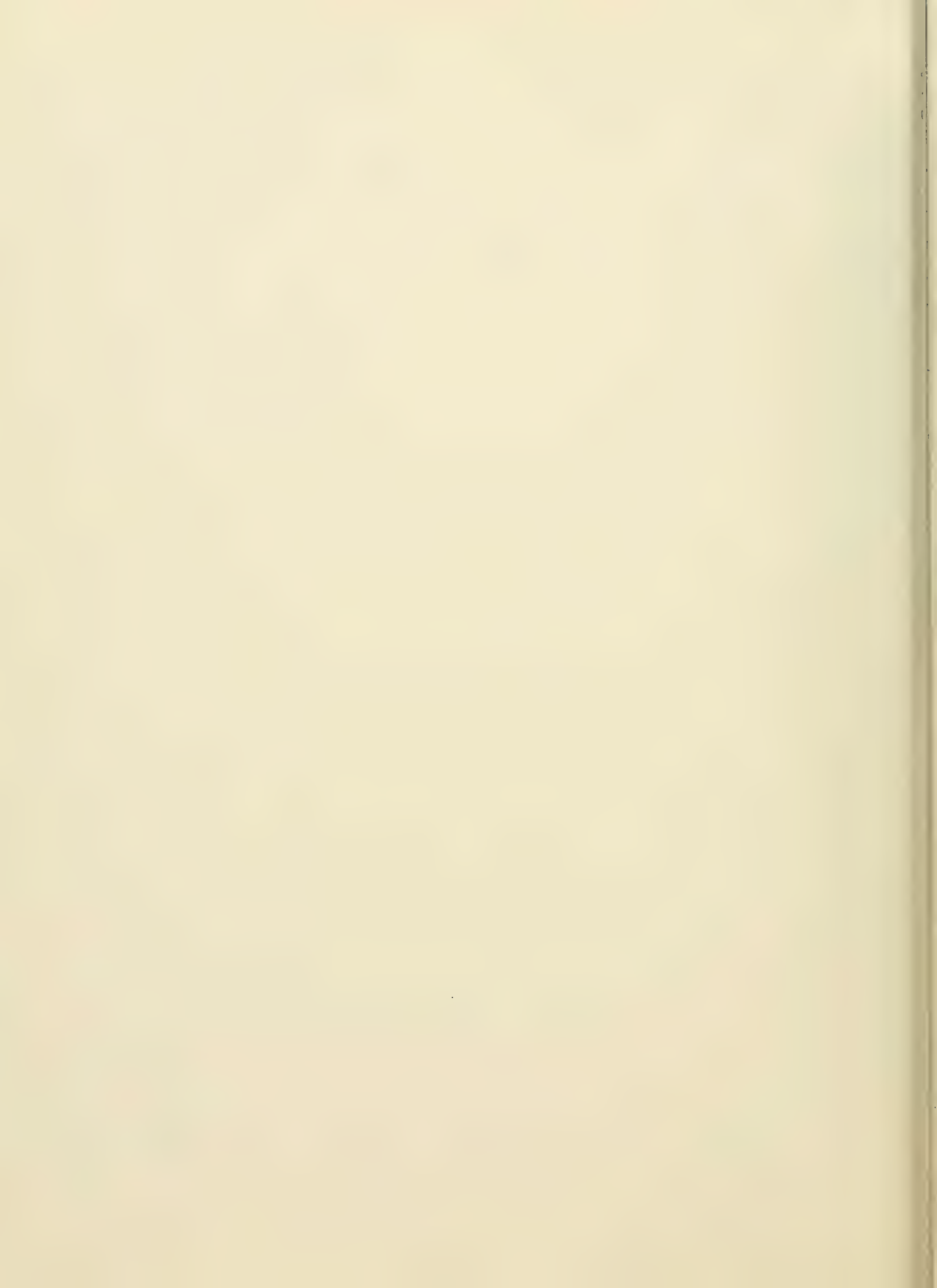
<sup>13</sup> Building 114 Renovation EIR by VHA dated Dec., 82.

<sup>14</sup> Third Harbor Tunnel EIR dated Dec., 82.



## LEVEL OF SERVICE ANALYSES



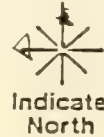
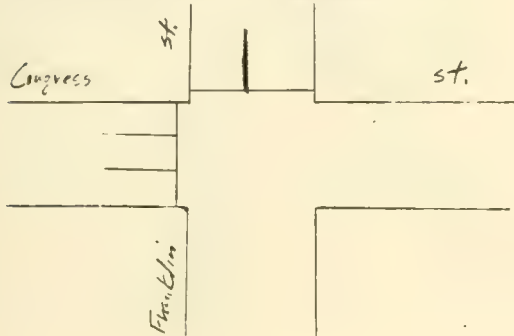




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INTERSECTION CONGRESS ST. / FRANKLIN ST.  
 ALT. EXISTING YEAR \_\_\_\_\_ PERIOD AM  
 CALCULATED BY EG DATE 4-11-84 SHEET \_\_\_\_\_ OF \_\_\_\_\_  
 CHECKED BY WJS DATE \_\_\_\_\_ JOB NO. 0782

## INTERSECTION GEOMETRY



## Left Turn Check

	Approach			
	1	2	3	4
a. Number of change intervals per hour				
b. Left turn capacity on change interval, in vph				
c. G/C Ratio				
d. Opposing volume in vph				
e. Left turn capacity on green, in vph				
f. Left turn capacity in vph (b * e)				
g. Left turn volume in vph				
h. Is volume > capacity (g > f)?				

## PHASING (2φ)

(A)	(B)	(C)	(D)	(E)
316 212 103	185 137			
CLV = 316	CLV = 185	CLV =	CLV =	CLV =

Σ CLV 501 AD = 626  
 V/C 0.42  
 LOS A  
 20% Reduction for Peds

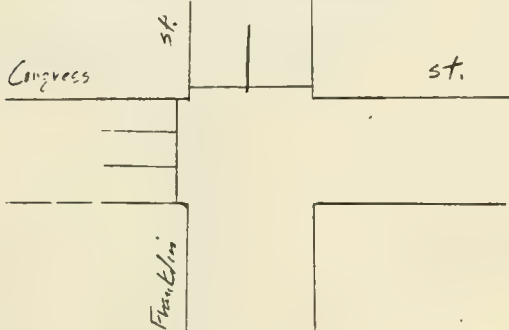
CRITERIA (vph)		AD	2 B	3 B	4 B
LOS	A	750	900	855	825
	B	840	1050	1000	965
	C	960	1200	1140	1100
	D	1050	1350	1275	1225
	E	1200	1500	1425	1375



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INTERSECTION CONGRESS ST. / FRANKLIN ST.  
 ALT. EXISTING YEAR \_\_\_\_\_ PERIOD PM  
 CALCULATED BY BO DATE 4-11-84 SHEET OF  
 CHECKED BY WJS DATE \_\_\_\_\_ JOB NO. 0788

## INTERSECTION GEOMETRY



## Left Turn Check

	Approach			
	1	2	3	4
a. Number of change intervals per hour				
b. Left turn capacity on change interval, in vph				
c. G/C Ratio				
d. Opposing volume in vph				
e. Left turn capacity on green, in vph				
f. Left turn capacity in vph (b + e)				
g. Left turn volume in vph				
h. Is volume > capacity (g > 0)?				

## PHASING

(A)	(B)	(C)	(D)	(E)
→ →	↖ ↗			
→ 563 ↖ 421 ↗ 142	↓ 124 ↓ 123 ↘ 109			
CLV = 563	CLV = 124	CLV =	CLV =	CLV =

Σ CLV 687

V/C 0.57

LOS A

20% Reduction for Peds

Adj ✓

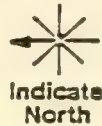
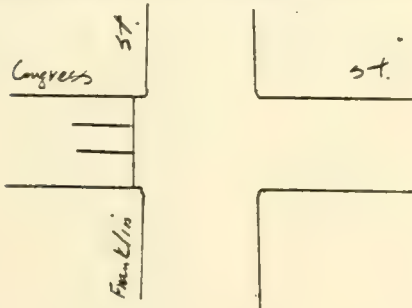
CRITERIA (vph)		ADP	2 B	3 B	4 B
LOS	A	720	900	855	825
	B	840	1050	1000	965
	C	960	1200	1140	1100
	D	1080	1350	1275	1225
	E	1200	1500	1425	1375



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INTERSECTION CONGRESS ST. / FRANKLIN ST.  
 ALT. No-Build YEAR 1990 PERIOD AM  
 CALCULATED BY BG DATE \_\_\_\_\_ SHEET OF  
 CHECKED BY RB DATE 7/13 JOB NO. 0423

## INTERSECTION GEOMETRY



## Left Turn Check

	Approach			
	1	2	3	4
a. Number of change intervals per hour				
b. Left turn capacity on change interval, in vph				
c. G/C Ratio				
d. Opposing volume in vph				
e. Left turn capacity on green, in vph				
f. Left turn capacity in vph (b * e)				
g. Left turn volume in vph				
h. Is volume > capacity (g > f)?				

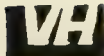
## PHASING 2b

(A)	(B)	(C)	(D)	(E)
427 → 427 ↘ 111	240 224 224			
CLV = 427	CLV = 240	CLV =	CLV =	CLV =

$\Sigma$  CLV 667 ADJ  
(834)  
 V/C 0.56  
 LOS A

20% Reduction for Peds

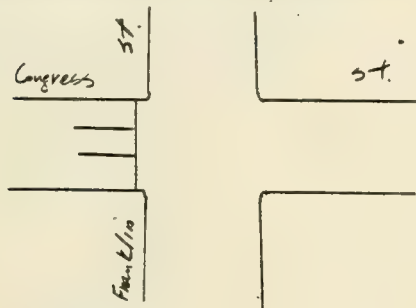
CRITERIA (vph)		ADJ	2 B	3 B	4 B
LOS	A	720	900	888	825
	B	840	1050	1000	968
	C	960	1200	1140	1100
	D	1080	1350	1275	1225
	E	1200	1500	1425	1375



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INTERSECTION CONGRESS ST. / FRANKLIN ST.  
 ALT. No Build YEAR 1990 PERIOD PM  
 CALCULATED BY BY DATE 8/13 SHEET OF  
 CHECKED BY KB DATE 8/13 JOB NO. 0423

## INTERSECTION GEOMETRY



1390 →  
 149 ↘  
 152 ↙  
 167 ↘

## Left Turn Check

	Approach			
	1	2	3	4
a. Number of change intervals per hour				
b. Left turn capacity on change interval, in vph				
c. G/C Ratio				
d. Opposing volume in vph				
e. Left turn capacity on green, in vph				
f. Left turn capacity in vph (b + e)				
g. Left turn volume in vph				
h. Is volume > capacity (g > f)?				

## PHASING 2p

(A)	(B)	(C)	(D)	(E)
↑ → ↙	↓ →			
→ 770 → 620 ↘ 149	159 ↓ 160 ↘			
CLV = 770	CLV = 160	CLV =	CLV =	CLV =

$\Sigma$  CLV 930 (<sup>ADT</sup> 1163)  
 V/C 0.78  
 LOS C

20% Reduction for Peds

CRITERIA (vph)		ADT	2 B	3 B	4 B
LOS	A	750	900	855	825
	B	840	1050	1000	965
	C	960	1200	1140	1100
	D	1080	1350	1275	1225
	E	1200	1500	1425	1375

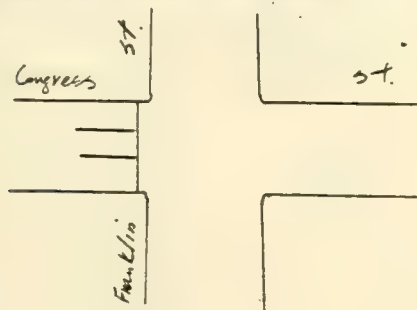




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INTERSECTION CONGRESS ST. / FRANKLIN ST.  
 ALT. BUILD YEAR 1990 PERIOD AM  
 CALCULATED BY EG/OD DATE 8/13/94 SHEET OF  
 CHECKED BY R.R. DATE 8/13/94 JOB NO. 0723

## INTERSECTION GEOMETRY



## Left Turn Check

	Approach			
	1	2	3	4
a. Number of change intervals per hour				
b. Left turn capacity on change interval, in vph				
c. G/C Ratio				
d. Opposing volume in vph				
e. Left turn capacity on green, in vph				
f. Left turn capacity in vph (b * c)				
g. Left turn volume in vph				
h. Is volume > capacity (g > f)?				

## PHASING 20

(A)	(B)	(C)	(D)	(E)
↓	↓			
→	→			
427 →	240 240 ↓ bump			
427 111				
CLV= 427	CLV= 240	CLV=	CLV=	CLV=

Σ CLV 667

V/C 0.56

LOS A

20% Reduction for Peds

AOS  
(8.33)

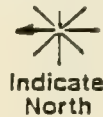
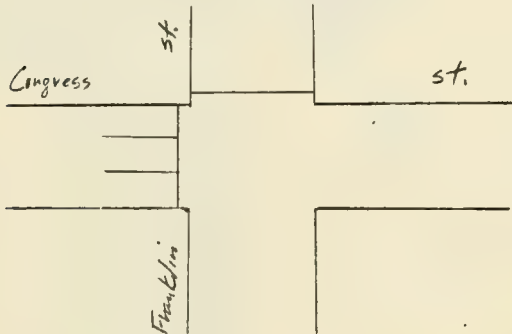
CRITERIA (vph)		1	2	3	4
LOS	A	730	900	888	825
	B	840	1050	1000	965
	C	960	1200	1140	1100
	D	1080	1350	1275	1225
	E	1200	1500	1425	1375



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INTERSECTION CONGRESS ST. / FRANKLIN ST.  
ALT. BUILD YEAR 1990 PERIOD PM  
CALCULATED BY DSD DATE 4/30/94 SHEET OF  
CHECKED BY RW DATE 5/13 JOB NO. 0788/923

## INTERSECTION GEOMETRY



152  
167  
↓

1439 →  
149 ↓

## Left Turn Check

	Approach			
	1	2	3	4
a. Number of change intervals per hour				
b. Left turn capacity on change interval, in vph				
c. G/C Ratio				
d. Opposing volume in vph				
e. Left turn capacity on green, in vph				
f. Left turn capacity in vph (b + e)				
g. Left turn volume in vph				
h. Is volume > capacity (g > f)?				

## PHASING 2φ

(A)	(B)	(C)	(D)	(E)
↓	↓			
794 → 794 → 149 ↘	160 ↓ 157 ↓			
CLV = 794	CLV = 160	CLV =	CLV =	CLV =

$\Sigma$  CLV 954 <sup>AOS</sup> (1193)  
VIC 0.79  
LOS C  
20% Reduction for Ped

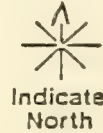
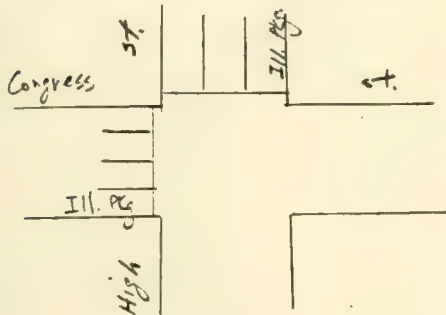
CRITERIA (vph)		ASD	2 φ	3 φ	4 φ
LOS	A	720	900	955	925
	B	840	1050	1000	965
	C	960	1200	1140	1100
	D	1080	1350	1275	1225
	E	1200	1500	1425	1375



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INTERSECTION CONGRESS ST / HIGH ST  
ALT. EXISTING YEAR 1984 PERIOD AM  
CALCULATED BY BG DATE 4-10-84 SHEET OF  
CHECKED BY RB DATE 8/10/84 JOB NO. 0789

## INTERSECTION GEOMETRY



389  
301  
511  
154

## Left Turn Check

	Approach			
	1	2	3	4
a. Number of change intervals per hour				
b. Left turn capacity on change interval, in vph				
c. G/C Ratio				
d. Opposing volume in vph				
e. Left turn capacity on green, in vph				
f. Left turn capacity in vph (b + e)				
g. Left turn volume in vph				
h. Is volume > capacity (g > f)?				

## PHASING 2Ø

(A)	(B)	(C)	(D)	(E)
CLV = 222	CLV = 389	CLV =	CLV =	CLV =

$\Sigma$  CLV 611 (719)

VIC 0.48

LOS A

15% Reduction for Ped

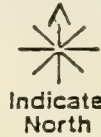
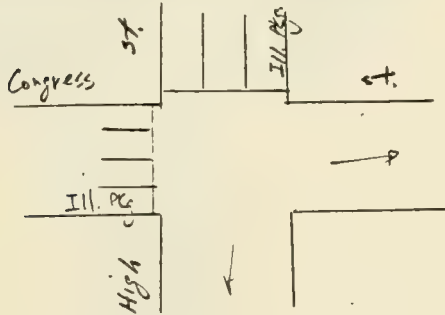
CRITERIA (vph)	AC	2 Ø	3 Ø	4 Ø
LOS A	765	900	855	825
B	843	1050	1000	965
C	1020	1200	1140	1100
D	1145	1350	1275	1225
E	1275	1500	1425	1375



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INTERSECTION CONGRESS ST / HIGH ST  
 ALT. EXISTING YEAR 1984 PERIOD AM  
 CALCULATED BY BC DATE 4-16-84 SHEET OF  
 CHECKED BY WJS DATE        JOB NO. 0788

## INTERSECTION GEOMETRY



258  
219

963  
130

## Left Turn Check

	Approach			
	1	2	3	4
a. Number of change intervals per hour				
b. Left turn capacity on change interval, in vph				
c. G/C Ratio				
d. Opposing volume in vph				
e. Left turn capacity on green, in vph				
f. Left turn capacity in vph (b + e)				
g. Left turn volume in vph				
h. Is volume > capacity (g > f)?				

## PHASING 2Ø

(A)	(B)	(C)	(D)	(E)
→ →	↓ ↓			
364 → 365 → 364 ↘ 130	258 ↓ 219 ↓	↓ ↓ OPTIONAL	↓ ↓ Conservative	
CLV = 365	CLV = 258	CLV =	CLV =	CLV =

$\Sigma$  CLV 623 (AOS) (733)  
 VIC 0.49  
 LOS A  
 15% Reduction for Peds

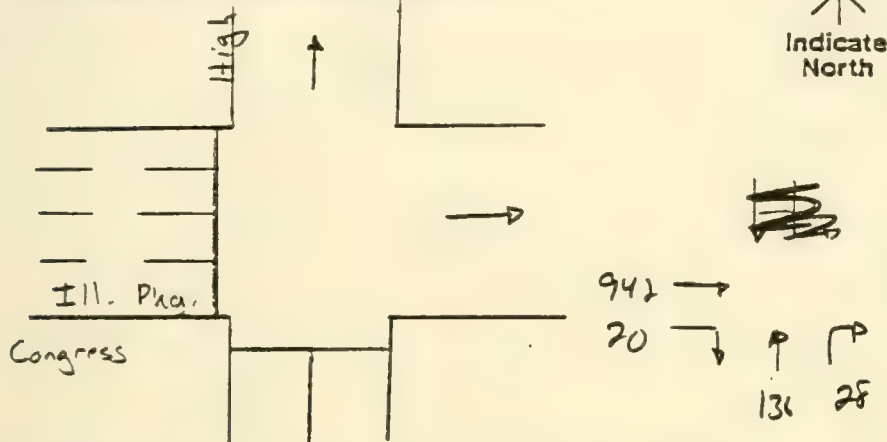
CRITERIA (vph)	4 Ø	2 Ø	3 Ø	4 Ø
LOS A	765	900	855	825
B	843	1050	1000	965
C	1020	1200	1140	1100
D	1145	1350	1275	1225
E	1275	1500	1425	1375



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INTERSECTION Congress St / High St  
 ALT. No Build YEAR 1990 PERIOD AM  
 CALCULATED BY \_\_\_\_\_ DATE \_\_\_\_\_ SHEET OF  
 CHECKED BY RB DATE 10/29 JOB NO. 728

## INTERSECTION GEOMETRY



## Left Turn Check

	Approach		
	1	2	3
a. Number of change intervals per hour			
b. Left turn capacity on change interval, in vph			
c. G/C Ratio			
d. Opposing volume in vph			
e. Left turn capacity on green, in vph			
f. Left turn capacity in vph (b * e)			
g. Left turn volume in vph			
h. Is volume > capacity (g > f)?			

## PHASING

2  $\phi$

(A)	(B)	(C)	(D)	(E)
321 → 321 → 320 → 20 ↓	82 ↑ 82 ↑			
CLV= 321	CLV= 82	CLV=	CLV=	CLV=

$\Sigma$  CLV 403

V/C 0.32

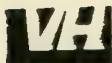
LOS A

ADJ.  
CLV

CRITERIA (vph)	ADJ.	2 $\phi$	3 $\phi$	4 $\phi$
LOS A	765	800	855	825
B	793	1050	1000	965
C	1020	1200	1140	1100
D	1145	1350	1275	1225
E	1275	1500	1425	1375

15% Reduction for P.D.s

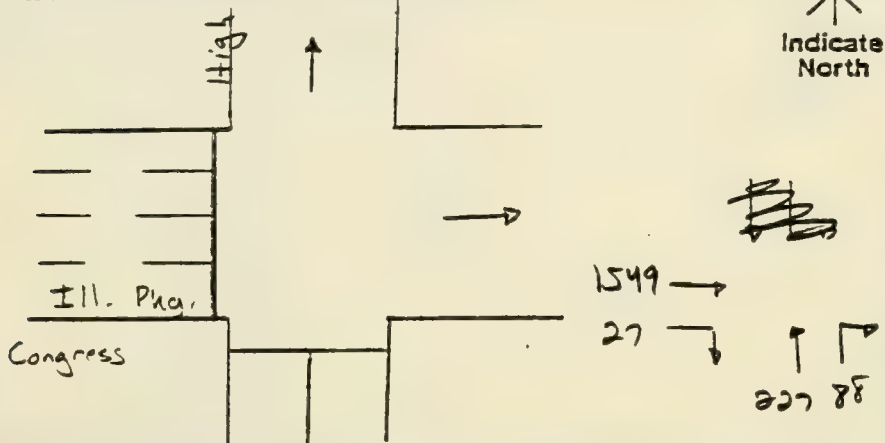




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INTERSECTION Congress St / High St  
 ALT. No Build YEAR 1990 PERIOD PM  
 CALCULATED BY \_\_\_\_\_ DATE \_\_\_\_\_ SHEET OF \_\_\_\_\_  
 CHECKED BY RR DATE 10/29 JOB NO. 778

## INTERSECTION GEOMETRY



## Left Turn Check

	Approach		
	1	2	3
a. Number of change intervals per hour			
b. Left turn capacity on change interval, in vph			
c. G/C Ratio			
d. Opposing volume in vph			
e. Left turn capacity on green, in vph			
f. Left turn capacity in vph (b - e)			
g. Left turn volume in vph			
h. Is volume > capacity (g > f)?			

## PHASING

2  $\phi$

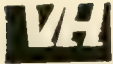
(A)	(B)	(C)	(D)	(E)
→ ↘	↑ ↗			
S25 → S26 → S25 → 27	↑ ↗ 158 157			
CLV = 526	CLV = 158	CLV =	CLV =	CLV =

$\Sigma$  CLV 684  
 VIC .54  
 LOS A

ADJ.  
CLV.

CRITERIA (vph)		ADJ	2 $\phi$	3 $\phi$	4 $\phi$
LOS	A	765	900	855	825
	B	893	1050	1000	965
	C	1020	1200	1140	1100
	D	1145	1350	1275	1225
	E	1275	1500	1425	1375

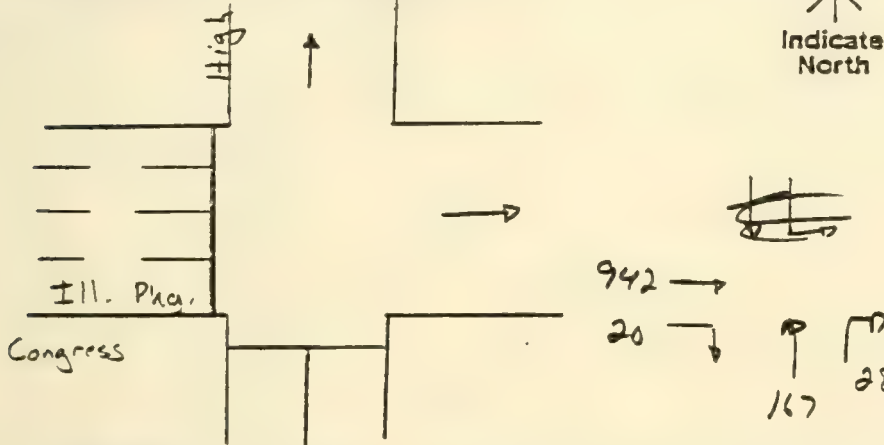
15% Reduction for Peds.



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INTERSECTION Congress St / High St  
 ALT. Build YEAR 1990 PERIOD AM  
 CALCULATED BY \_\_\_\_\_ DATE \_\_\_\_\_ SHEET OF  
 CHECKED BY RR DATE 10/29 JOB NO. 788

## INTERSECTION GEOMETRY



## Left Turn Check

	Approach		
	1	2	3
a. Number of change intervals per hour			
b. Left turn capacity on change interval, in vph			
c. G/C Ratio			
d. Opposing volume in vph			
e. Left turn capacity on green, in vph			
f. Left turn capacity in vph (b * e)			
g. Left turn volume in vph			
h. Is volume > capacity (g > f)?			

## PHASING

2  $\phi$

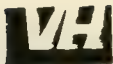
(A)	(B)	(C)	(D)	(E)
321 → 321 → 321 ↘ 20	98 ↑ 97 ↘ 25			
CLV= 321	CLV= 98	CLV=	CLV=	CLV=

$\Sigma$  CLV 419  
 V/C .33  
 LOS A

ADJ.  
CLV.

CRITERIA (vph)		ADJ.	2 $\phi$	3 $\phi$	4 $\phi$
LCS	A	765	800	868	925
	B	893	1050	1090	968
	C	1020	1200	1140	1100
	D	1149	1380	1275	1225
	E	1275	1500	1425	1375

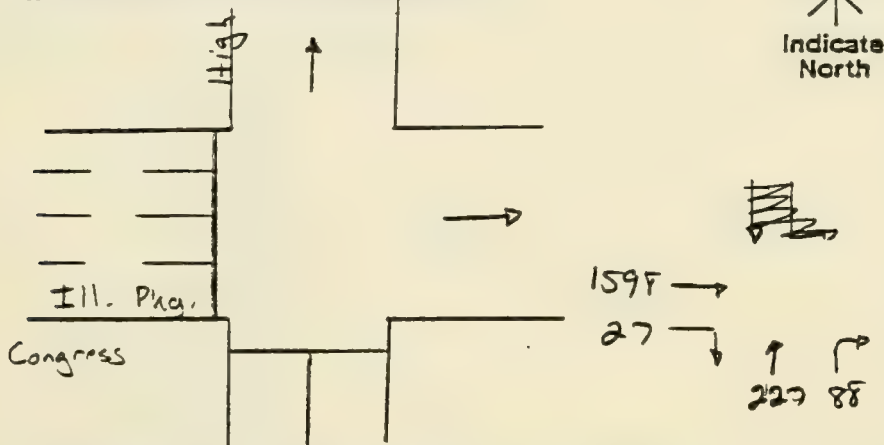
15% Reduction for Peds.



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INTERSECTION Congress St / High St  
 ALT. Bu 116 YEAR 1990 PERIOD PM  
 CALCULATED BY \_\_\_\_\_ DATE \_\_\_\_\_ SHEET OF  
 CHECKED BY RB DATE 10/29 JOB NO. 728

## INTERSECTION GEOMETRY



## Left Turn Check

	Approach		
	1	2	3
a. Number of change intervals per hour			
b. Left turn capacity on change interval, in vph			
c. G/C Ratio			
d. Opposing volume in vph			
e. Left turn capacity on green, in vph			
f. Left turn capacity in vph (b * e)			
g. Left turn volume in vph			
h. Is volume > capacity (g > 0?)			

## PHASING

2  $\phi$

(A)	(B)	(C)	(D)	(E)
→ ↘	↑ ↗			
541 → 542 → 542 ↘ 27	↑ ↗ 158 157			
CLV = 542	CLV = 158	CLV =	CLV =	CLV =

$\Sigma$  CLV 700  
 V/C .55  
 LOS A

ADJ.  
CLV.

CRITERIA (vph)		ADJ	2 B	3 B	4 B
LOS	A	765	900	855	825
	B	893	1050	1000	965
	C	1020	1200	1140	1100
	D	1145	1350	1275	1225
	E	1275	1500	1425	1375

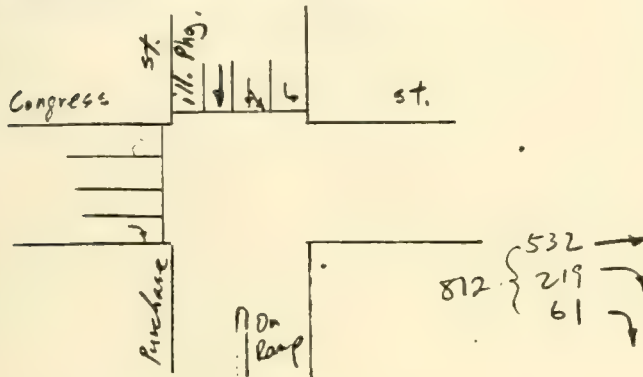
15% Reduction for P.D.s.



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INTERSECTION CONGRESS ST. / PURCHASE ST.  
 ALT. EXISTING YEAR        PERIOD AM  
 CALCULATED BY EL DATE 4-10-84 SHEET OF  
 CHECKED BY RB DATE 8/12/84 JOB NO. 0788

## INTERSECTION GEOMETRY



## Left Turn Check

	Approach			
	1	2	3	4
a. Number of change intervals per hour				
b. Left turn capacity on change interval, in vph				
c. G/C Ratio				
d. Opposing volume in vph				
e. Left turn capacity on green, in vph				
f. Left turn capacity in vph (b + e)				
g. Left turn volume in vph				
h. Is volume > capacity (g > f)?				

## PHASING ~~2nd~~ w/ Advance

(A)	(B)	(C)	(D)	(E)
 45' L L 538	 ↓ L	 →		LT ADV = 16 sec / 90 sec cycle ≈ 18%
 L L 213 260	 ↓ L L 92 34 268	 → 270 → 271 → 271		Assume 3 sec start-up and 2 sec / veh = 13 sec or 6.5 veh / veh 40 cycles / L = 260 vph
CLV = 260	CLV = 268	CLV = 271	CLV =	CLV =

Use 2nd criteria

Σ CLV 791 ADJ. 1130  
 V/C .75  
 LOS C  
 30% Reduction for Peds

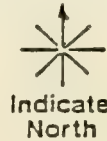
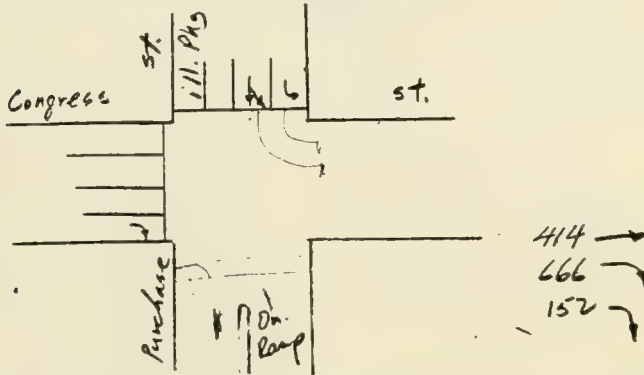
CRITERIA (vph)	ADJ	2nd	3rd	4th
LOS A	630	900	855	825
B	735	1050	1000	965
C	840	1200	1140	1100
D	945	1350	1275	1225
E	1050	1500	1425	1375



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INTERSECTION CONGRESS ST. / PURCHASE ST.  
 ALT. EXISTING YEAR            PERIOD PM  
 CALCULATED BY BC DATE 4-10-84 SHEET        OF         
 CHECKED BY RO DATE 7/10 JOB NO. 0788

## INTERSECTION GEOMETRY



## Left Turn Check

- Number of change intervals per hour
- Left turn capacity on change interval, in vph
- G/C Ratio
- Opposing volume in vph
- Left turn capacity on green, in vph
- Left turn capacity in vph (b + c)
- Left turn volume in vph
- Is volume > capacity (g > n)?

Approach

1 2 3 4

## PHASING

2  $\phi$  Advance

(A)	(B)	(C)	(D)	(E)
 260 vph MAX based on timing				
 130 260 CARRY OVER = 664 - 390 = 274	 315 315 274 227 88	 410 411 407 411 259 152		
CLV = 260	CLV = 315	CLV = 411	CLV =	CLV =

MIXED FLOW in LT Lane - comp only 1/2 of inside lane

PFO

ADJ.

$\Sigma$  CLV 986

VIC 0.94

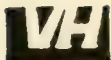
LOS E

30% Reduction for Peds

1409

CRITERIA (vph)	ADJ	2 B	3 B	4 B
LOS A	630	900	855	825
B	735	1050	1000	965
C	840	1200	1140	1100
D	945	1350	1275	1225
E	1050	1500	1425	1375

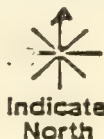
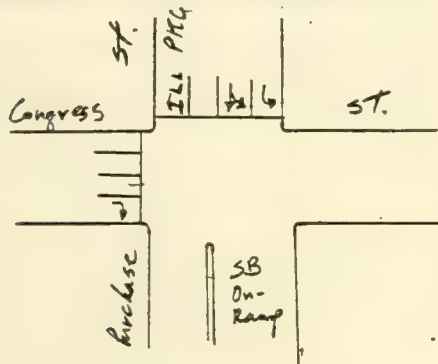




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INTERSECTION CONGRESS ST. / PURCHASE ST.  
 ALT. No-Build YEAR 1990 PERIOD AM  
 CALCULATED BY BS DATE 7/13 SHEET OF  
 CHECKED BY RB DATE 7/13 JOB NO. 0733

## INTERSECTION GEOMETRY



## Left Turn Check

- Number of change intervals per hour
- Left turn capacity on change interval, in vph
- G/C Ratio
- Opposing volume in vph
- Left turn capacity on green, in vph
- Left turn capacity in vph ( $b + c$ )
- Left turn volume in vph
- Is volume > capacity ( $g > 1$ )?

	Approach		
	1	2	3

## PHASING 2 φ w ADV

(A)	(B)	(C)	(D)	(E)
ADV ↓ 260 msa based on timing	↓ (786 + 189 + 692) ÷ 3	→ ↓		
↓ 213 260  1259 - 473 = 786	SSS ↓ SSS SSS	314 → 314 ↓ 314 170		
CLV = 260	CLV = 550	CLV = 314	CLV =	CLV =

Use 2 φ criteria

Σ CLV 1130  
 V/C 0.94  
 LOS E  
 20% Reduction for PEs

PED  
 ADD  
 (1413)

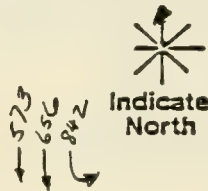
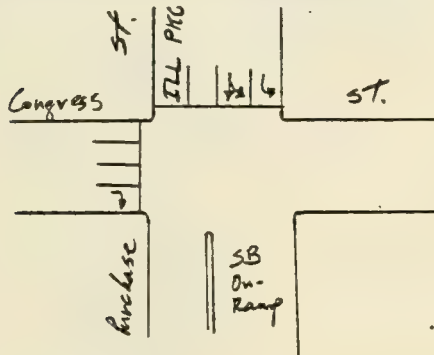
CRITERIA (vph)		ACT	2 φ	3 φ	4 φ
LOS	A	720	900	858	825
	B	540	1080	1000	968
	C	760	1200	1140	1100
	D	1050	1350	1275	1225
	E	200	1500	1425	1375



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 ALT. No Build YEAR 1990 PERIOD PM  
 CALCULATED BY BG DATE \_\_\_\_\_ SHEET OF  
 CHECKED BY PR DATE 4/13 JOB NO. 0733

## INTERSECTION GEOMETRY



395  
 740  
 324

## Left Turn Check

- Number of change intervals per hour
- Left turn capacity on change interval, in vph
- G/C Ratio
- Opposing volume in vph
- Left turn capacity on green, in vph
- Left turn capacity in vph ( $b = c$ )
- Left turn volume in vph
- Is volume > capacity ( $g > 0?$ )

Approach

1 2 3

## PHASING 2d w/ Adv.

(A)	(B)	(C)	(D)	(E)
↓	↓ $1681/3 =$	→		
$  \begin{array}{c}  \downarrow \downarrow \\  130 \quad 260 \\  842 - 390 = \\  452  \end{array}  $	$  \begin{array}{c}  \downarrow \downarrow \downarrow \\  614 \quad 615 \quad 452  \end{array}  $	$  \begin{array}{c}  \rightarrow \\  395 \\  532 \\  532  \end{array}  $		
CLV = 260	CLV = 615	CLV = 532	CLV =	CLV =

Use 2d criteria

$\Sigma$  CLV 1407

V/C 1.17

LOS E

20% Reduction for Rds

ADJ

1259

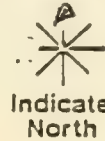
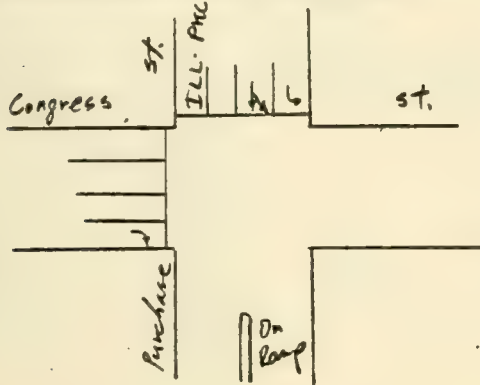
CRITERIA (vph)		ADJ	2d	3d	4d
LOS	A	720	900	868	825
	B	840	1080	1000	965
	C	960	1200	1140	1100
	D	1080	1380	1275	1225
	E	1200	1500	1425	1375



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 ALT. BUILD YEAR 1990 PERIOD AM  
 CALCULATED BY DJD DATE 4/24/84 SHEET OF  
 CHECKED BY AB DATE 7/13 JOB NO. 0788/923

## INTERSECTION GEOMETRY



692  
189  
1267

458  
234  
250

## Left Turn Check

	Approach			
	1	2	3	4
a. Number of change intervals per hour				
b. Left turn capacity on change interval, in vph				
c. G/C Ratio				
d. Opposing volume in vph				
e. Left turn capacity on green, in vph				
f. Left turn capacity in vph (b * c)				
g. Left turn volume in vph				
h. Is volume > capacity (g > f)?				

## PHASING

2Ø W/LEAD

(A)	(B)	(C)	(D)	(E)
	$794 + 189 + 692$ $= 1675 / 3$			
<p>213 260</p> $1267 - 473$ $= 794$	<p>314 314 314 170</p>			
CLV = 860	CLV = 558	CLV = 314	CLV =	CLV =

Use 2Ø Criteria

ADJ  
 $\Sigma$  CLV 1132 1415  
 V/C .94  
 LOS E  
 20% Reduction for Peds

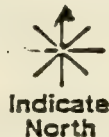
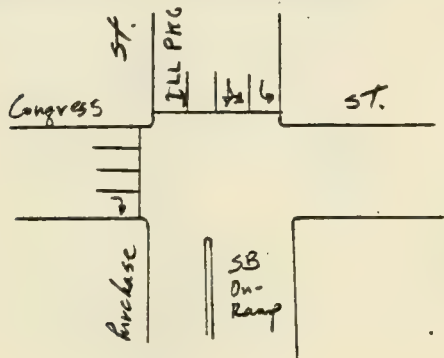
CRITERIA (vph)	ADJ	2 Ø	3 Ø	4 Ø
LOS A	720	900	855	825
B	840	1050	1000	965
C	960	1200	1140	1100
D	1080	1350	1275	1225
E	1200	1500	1425	1375



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INTERSECTION CONGRESS ST. / PURCHASE ST.  
 ALT. Build YEAR 1990 PERIOD PM  
 CALCULATED BY DJD DATE 8/11/84 SHEET OF  
 CHECKED BY AGT DATE 8/11/84 JOB NO. 0723

## INTERSECTION GEOMETRY



## Left Turn Check

- Number of change intervals per hour
- Left turn capacity on change interval, in vph
- G/C Ratio
- Opposing volume in vph
- Left turn capacity on green, in vph
- Left turn capacity in vph ( $b + c$ )
- Left turn volume in vph
- Is volume > capacity ( $g > 0$ )?

Approach

1 2 3

## PHASING 30

(A)	(B)	(C)	(D)	(E)
 130 260 $887 - 390 = 498$	658 658 498 	413 → 562 → 562 →		
CLV = 260	CLV = 658	CLV = 562	CLV =	CLV =

$\Sigma$  CLV 1480 (1850)

V/C 1.23

LOS E

20% reduction for PDS

CRITERIA (vph)		2 B	ADT	3 B	4 B
LOS	A	900	654	888	823
	B	1050	800	1000	965
	C	1200	912	1140	1100
	D	1350	1020	1275	1225
	E	1500	1140	1425	1375



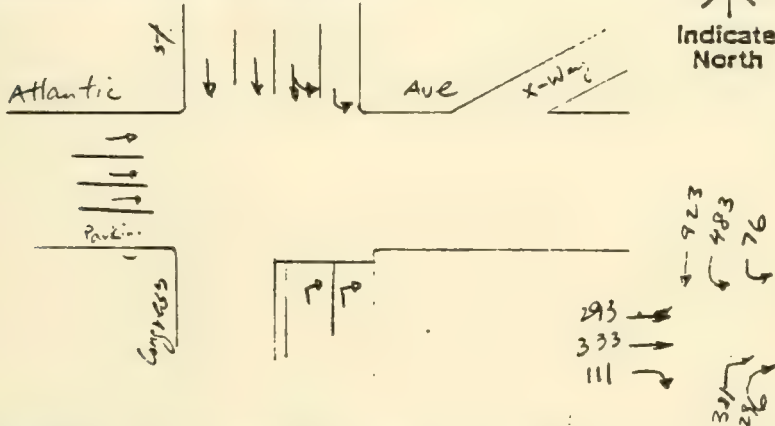


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INTERSECTION ATLANTIC AVE. / CONGRESS ST.

ALT. Existing YEAR            PERIOD AM  
 CALCULATED BY DJC DATE            SHEET        OF         
 CHECKED BY BVT DATE 8/13/84 JOB NO. 0923

## INTERSECTION GEOMETRY



## Left Turn Check

	Approach			
	1	2	3	4
a. Number of change intervals per hour				
b. Left turn capacity on change interval, in vph				
c. G/C Ratio				
d. Opposing volume in vph				
e. Left turn capacity on green, in vph				
f. Left turn capacity in vph (b * e)				
g. Left turn volume in vph				
h. Is volume > capacity (g > f?)				

## PHASING

(A)	(B)	(C)	(D)	(E)
↓ ↓	↓ ↓ ↓	→ →		
338 338 ↓ ↓	123 104 62 297 ↓ ↓ ↓ ↓	246 → 246 → 246 →		
CLV = 338	CLV = 307	CLV = 246	CLV =	CLV =

\* USE 50/50 split since ramp vol. > RT volume

$\sum$  CLV 891  
 V/C 0.74  
 LOS C

ADJ  
 1048

CRITERIA (vph)		2 B	3 B	4 B
LOS	A	900	1177	823
	B	1050	1500	965
	C	1200	1609	1100
	D	1350	1751	1225
	E	1500	1901	1375

15% Reduction for Peds

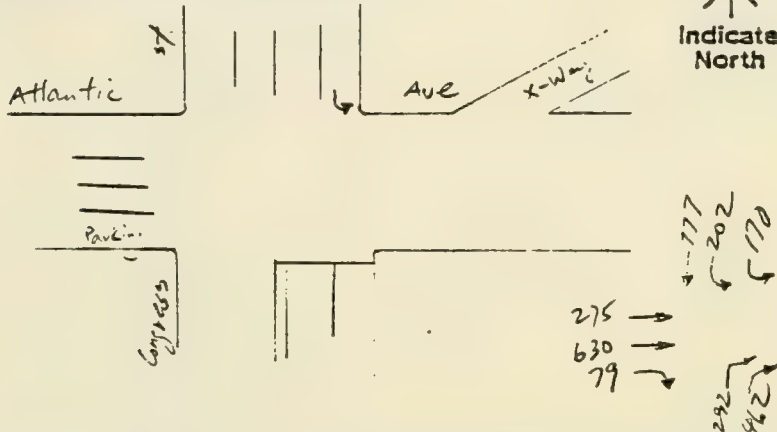




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INTERSECTION ATLANTIC AVE. / CONGRESS ST.  
 ALT. EXISTING YEAR \_\_\_\_\_ PERIOD P.M.  
 CALCULATED BY DJC DATE \_\_\_\_\_ SHEET OF  
 CHECKED BY DET DATE 9/13/84 JOB NO. 0923

## INTERSECTION GEOMETRY



## Left Turn Check

	Approach			
	1	2	3	4
a. Number of change intervals per hour				
b. Left turn capacity on change interval, in vph				
c. G/C Ratio				
d. Opposing volume in vph				
e. Left turn capacity on green, in vph				
f. Left turn capacity in vph (b * e)				
g. Left turn volume in vph				
h. Is volume > capacity (g > f)?				

## PHASING 3P

(A)	(B)	(C)	(D)	(E)
↓ ↓ 379	↓ ↓ ↓ ↓	→ →		
379 380 ↓ ↓ 379 380	379 380 ↓ ↓	379 → 324 → 328 →		
CLV = 415	CLV = 205	CLV = 328	CLV =	CLV =

Σ CLV 998

V/C 0.78

LOS C

15% Reduction for P.C.s

805  
1115

CRITERIA (vph)		2 B	ADT	3 B	4 B
LOS	A	900	727	855	825
	B	1050	850	1000	965
	C	1200	964	1140	1100
	D	1350	1051	1275	1225
	E	1500	1211	1425	1375

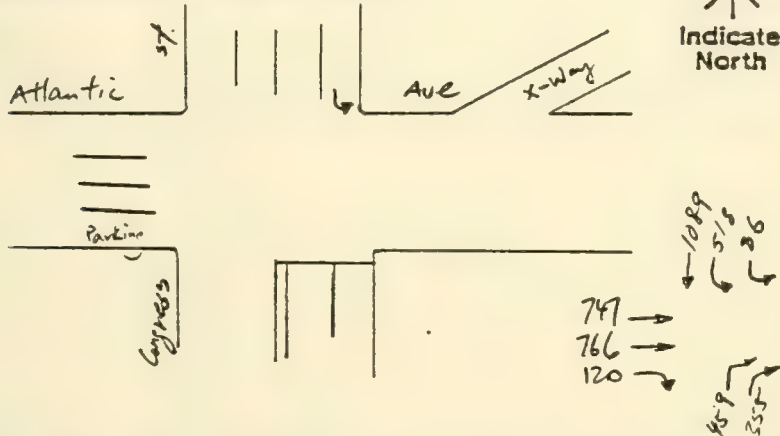


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INTERSECTION ATLANTIC AVE. / CONGRESS ST.

ALT. No-Build YEAR 1990 PERIOD AM  
 CALCULATED BY GB DATE \_\_\_\_\_ SHEET OF  
 CHECKED BY AB DATE 7/13 JOB NO. 0923

## INTERSECTION GEOMETRY



## Left Turn Check

	Approach			
	1	2	3	4
a. Number of change intervals per hour				
b. Left turn capacity on change interval, in vph				
c. G/C Ratio				
d. Opposing volume in vph				
e. Left turn capacity on green, in vph				
f. Left turn capacity in vph (b + e)				
g. Left turn volume in vph				
h. Is volume > capacity (g > f)?				

## PHASING 3

(A)	(B)	(C)	(D)	(E)
$1089 - 814 = 275$ compare 				
CLV = 407	CLV = 332	CLV = 544	CLV =	CLV =

\* S/D/S: split OK as Ramp Vol > RT Vol.

$\Sigma$  CLV 1283  $\frac{AOS}{1509}$   
 V/C 1.06  
 LOS E

15% Reduction for Peds

CRITERIA (vph)		2 B	AOS	3 B	4 B
LOS	A	800	727	855	825
	B	1050	552	1000	965
	C	1200	901	1140	1100
	D	1350	1054	1275	1225
	E	1500	1211	1425	1375

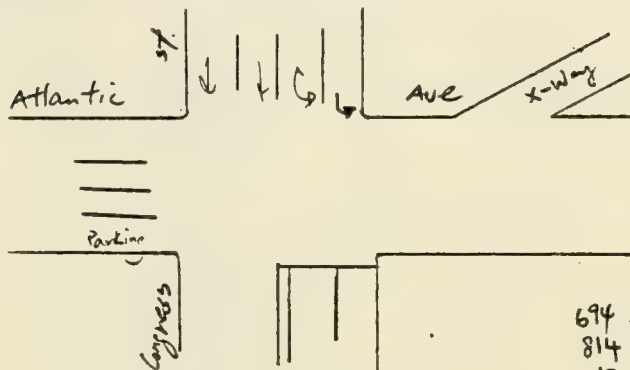


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INTERSECTION ATLANTIC AVE. / CONGRESS ST.

ALT. No Build YEAR 1996 PERIOD PM  
 CALCULATED BY BGT DATE 7/17 SHEET OF  
 CHECKED BY JP DATE 7/17 JOB NO. 0923

## INTERSECTION GEOMETRY



Indicate North

## Left Turn Check

	Approach			
	1	2	3	4
a. Number of change intervals per hour				
b. Left turn capacity on change interval, in vph				
c. G/C Ratio				
d. Opposing volume in vph				
e. Left turn capacity on green, in vph				
f. Left turn capacity in vph (b * e)				
g. Left turn volume in vph				
h. Is volume > capacity (g > f)?				

Handwritten traffic volume data:  
 805  
 261  
 197  
 694  
 814  
 142  
 330  
 597

## PHASING 3

(A)	(B)	(C)	(D)	(E)
↓ ↓	↓ ↓ ↓	→ →		
↓ ↓ 402 403 417 510	206 252	→ 550 → 550 → 550		
CLV = 510	CLV = 252	CLV = 550	CLV =	CLV =

$\Sigma$  CLV 1312

V/C 1.08

LOS E

15% Reduction for Ped's

AOT  
1544

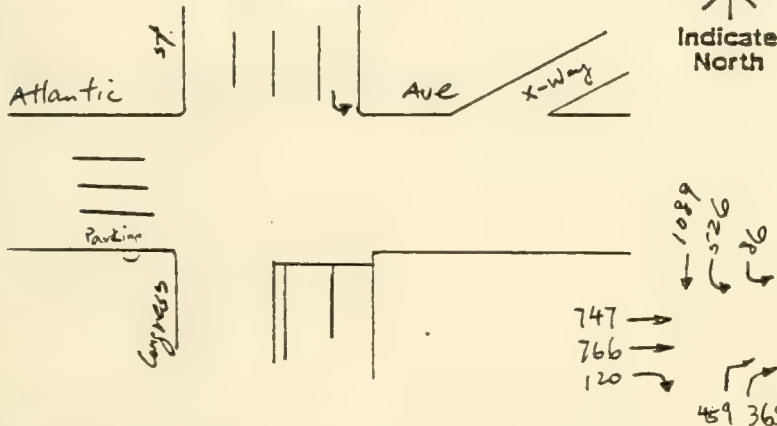
CRITERIA (vph)		2 B	AOT	3 B	4 B
LOS	A	900	727	868	823
	B	1050	850	1000	965
	C	1200	909	1140	1100
	D	1350	1054	1275	1225
	E	1500	1211	1425	1375



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INTERSECTION ATLANTIC AVE. / CONGRESS ST.  
 ALT. Build YEAR 1990 PERIOD AM  
 CALCULATED BY BT DATE 8/11/84 SHEET OF  
 CHECKED BY KE DATE 8/14/84 JOB NO. 0923

## INTERSECTION GEOMETRY



## Left Turn Check

	Approach			
	1	2	3	4
a. Number of change intervals per hour				
b. Left turn capacity on change interval, in vph				
c. G/C Ratio				
d. Opposing volume in vph				
e. Left turn capacity on green, in vph				
f. Left turn capacity in vph (b - e)				
g. Left turn volume in vph				
h. Is volume > capacity (g > f)?				

## PHASING 3/

(A)	(B)	(C)	(D)	(E)
↓ ↓	↓ ↓ ↓	→ →		
412 412 ↓ ↓	132 132 337 337 ↓ ↓ ↓ ↓	544 544 544 120		
CLV = 412	CLV = 337	CLV = 544	CLV =	CLV =

SB/S split OK as Ramp vol > RT vol.

$\Sigma$  CLV 1293 ADT  
1521  
 V/C 1.07  
 LOS E

15% Reduction for Peds

CRITERIA (vph)		2 S	ADT	3 S	4 S
LOS	A	900	777	885	825
	B	1050	850	1000	965
	C	1200	969	1140	1100
	D	1350	1054	1275	1225
	E	1500	1211	1425	1375

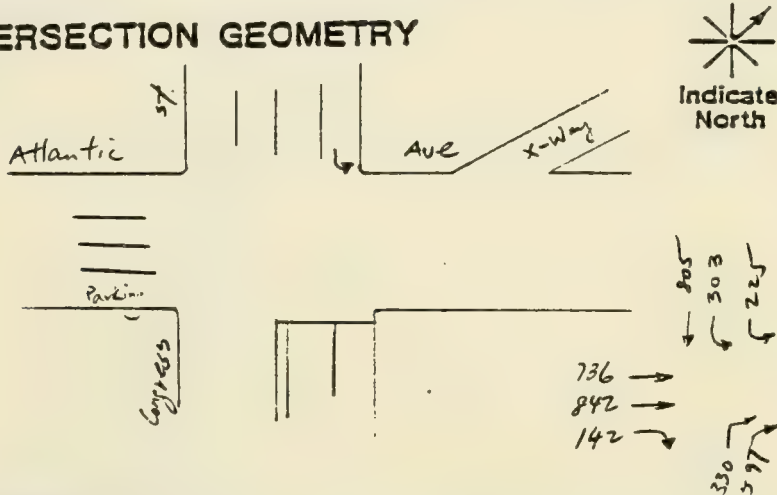




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INTERSECTION ATLANTIC AVE. / CONGRESS ST.  
 ALT. Build YEAR 1990 PERIOD PM  
 CALCULATED BY DJD DATE 8/11/84 SHEET OF  
 CHECKED BY CGT JOB NO. 0523

## INTERSECTION GEOMETRY



## Left Turn Check

	Approach			
	1	2	3	4
a. Number of change intervals per hour				
b. Left turn capacity on change interval, in vph				
c. G/C Ratio				
d. Opposing volume in vph				
e. Left turn capacity on green, in vph				
f. Left turn capacity in vph (b + e)				
g. Left turn volume in vph				
h. Is volume > capacity (g > f)?				

## PHASING 3

(A)	(B)	(C)	(D)	(E)
↓ ↓	↓ ↓ ↓	→ →		
402 403 417 510	235 290	574 573 142		
CLV = 510	CLV = 290	CLV = 574	CLV =	CLV =

$\Sigma$  CLV 1374  
 V/C 1.13  
 LOS E

15% Reduction for Peds

ADT  
1616

CRITERIA (vph)		2 S	4 S	3 S	4 S
LOS	A	900	127	855	825
	B	1050	580	1000	965
	C	1200	707	1140	1100
	D	1350	1057	1275	1225
	E	1500	1211	1425	1375



# TRAFFIC STREAM GAP ANALYSIS PACKAGE

VER 3.5.3 MARCH84

BOSTON, MA  
CONGRESS ST./DORCHESTER AVE.  
EXIST AM - LT OUT FROM DORCHESTER AVE.

## DATA

FIRST VEHICLE CRITICAL GAP, T1, ..... 5 SECONDS  
ADDITIONAL TIME NEEDED FOR SECOND VEHICLE, B1, ... 3 SECONDS  
MOVE UP TIME, B2, ..... 2.5 SECONDS

### OPPOSING TRAFFIC

VOLUME..... 1089 VPH  
ARRIVAL RATE..... .303 VPS

### ANALYSIS MOVEMENT TRAFFIC

VOLUME..... 295 VPH  
ARRIVAL RATE..... .082 VPS

## RESULTS

CAPACITY= 402 VPH

RESERVE CAPACITY= 107 VPH

### ACCEPTABLE GAPS

PERCENT OF ALL GAPS..... 22 PERCENT  
AVERAGE LENGTH..... 8.3 SECONDS

### AVERAGE DELAY TO A VEHICLE AT STOP BAR

TO ALL VEHICLES..... .6 SECONDS  
TO DELAYED VEHICLES ONLY..... 3.9 SECONDS

### AVERAGE WAIT IN A QUEUE

TO ALL VEHICLES..... 24.6 SECONDS  
TO QUEUED VEHICLES ONLY..... 33.5 SECONDS

### AVERAGE DELAY PLUS AVERAGE WAIT

TO ALL VEHICLES..... 25.2 SECONDS  
TO DELAYED AND QUEUED VEHICLES ONLY..... 37.5 SECONDS

### QUEUE LENGTH

AVERAGE..... 2.7 VEHICLES  
95TH PERCENTILE..... 5.4 VEHICLES

LEVEL OF SERVICE --- D ---

# TRAFFIC STREAM GAP ANALYSIS PACKAGE

VER 3.5.3 MARCH84

BOSTON, MA  
CONGRESS ST./DORCHESTER AVE.  
EXISTING PM - LT OUT FROM DORCHESTER AVE.

## DATA

FIRST VEHICLE CRITICAL GAP, T1, ..... 5 SECONDS  
ADDITIONAL TIME NEEDED FOR SECOND VEHICLE, B1, ... 3 SECONDS  
MOVE UP TIME, B2, ..... 2.5 SECONDS

### OPPOSING TRAFFIC

VOLUME..... 958 VPH  
ARRIVAL RATE..... .266 VPS

### ANALYSIS MOVEMENT TRAFFIC

VOLUME..... 459 VPH  
ARRIVAL RATE..... .128 VPS

## RESULTS

CAPACITY= 460 VPH

RESERVE CAPACITY= 1 VPH

### ACCEPTABLE GAPS

PERCENT OF ALL GAPS..... 26.4 PERCENT  
AVERAGE LENGTH..... 8.8 SECONDS

### AVERAGE DELAY TO A VEHICLE AT STOP BAR

TO ALL VEHICLES..... .5 SECONDS  
TO DELAYED VEHICLES ONLY..... 3.8 SECONDS

### AVERAGE WAIT IN A QUEUE

TO ALL VEHICLES..... 2422.7 SECONDS  
TO QUEUED VEHICLES ONLY..... 2430.5 SECONDS

### AVERAGE DELAY PLUS AVERAGE WAIT

TO ALL VEHICLES..... 2423.2 SECONDS  
TO DELAYED AND QUEUED VEHICLES ONLY..... 2434.3 SECONDS

### QUEUE LENGTH

AVERAGE..... 309.9 VEHICLES  
95TH PERCENTILE.....-851.6 VEHICLES

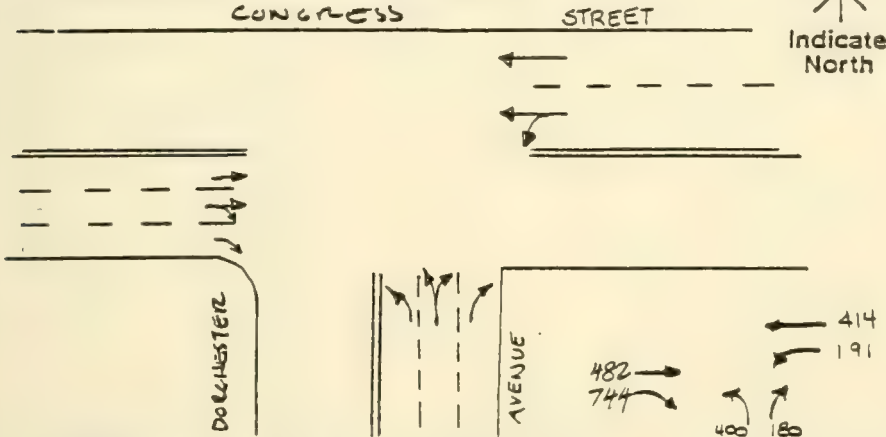
LEVEL OF SERVICE --- E ---



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INTERSECTION CONGRESS ST/DORCHESTER AVE.  
 ALT. No BUILD YEAR 1990 PERIOD AM  
 CALCULATED BY DJD DATE 4/26/84 SHEET OF  
 CHECKED BY FG DATE 8/12/84 JOB NO. 0923

## INTERSECTION GEOMETRY



## Left Turn Check

	Approach			
	1	2	3	4
a. Number of change intervals per hour				
b. Left turn capacity on change interval, in vph				
c. G/C Ratio				
d. Opposing volume in vph				
e. Left turn capacity on green, in vph				
f. Left turn capacity in vph (b * e)				
g. Left turn volume in vph				
h. Is volume > capacity (g > f)?				

## PHASING 30

(A)	(B)	(C)	(D)	(E)
CLV = <del>200</del> 220	CLV = 409	CLV = 191	CLV =	CLV =

ADJ 820  
 $\Sigma$  CLV 1025  
 V/C .72  
 LOS C  
 20% Reduction For Peds

CRITERIA (vph)		2 B	3 B	4 B
LOS	A	900	855	825
	B	1050	1000	965
	C	1200	1140	1100
	D	1350	1275	1225
	E	1500	1425	1375



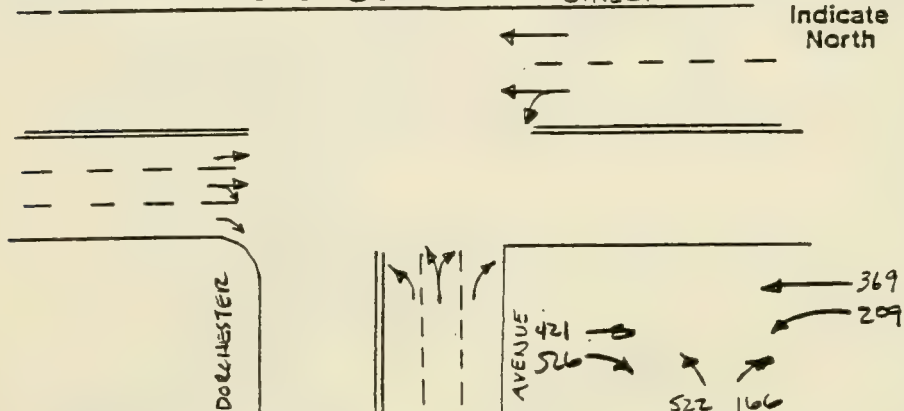
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INTERSECTION CONGRESS ST / DORCHESTER AVE.  
 ALT. NO BUILD YEAR 1990 PERIOD PM  
 CALCULATED BY D.S.D. DATE 4/30/84 SHEET OF  
 CHECKED BY FR DATE 5-1-84 JOB NO. 0788/92

## INTERSECTION GEOMETRY

CONGRESS

STREET



## Left Turn Check

- Number of change intervals per hour
- Left turn capacity on change interval, in vph
- G/C Ratio
- Opposing volume in vph
- Left turn capacity on green, in vph
- Left turn capacity in vph (b - c)
- Left turn volume in vph
- Is volume > capacity (g > 0)?

Approach

1 2 3 4

## PHASING

3 2

(A)	(B)	(C)	(D)	(E)
CLV = <del>287</del> 287	CLV = 316	CLV = 209	CLV =	CLV =

$\Sigma$ CLV	ADT	CRITERIA (vph)	2 B	HCT	3 B	4 B
712	1015	LOS A	900	654	853	825
V/C <del>0.71</del> .71		B	1050	800	1000	965
LOS <del>B</del> C		C	1200	912	1140	1100
		D	1350	1020	1275	1225
		E	1500	1140	1425	1375

20% Reduction For Peds



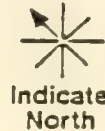
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INTERSECTION CONGRESS ST / DORCHESTER AVE.  
 ALT. BUILD YEAR 1990 PERIOD AM  
 CALCULATED BY DJD DATE 4/26/84 SHEET OF  
 CHECKED BY RB DATE 8/13/84 JOB NO. 0923

## INTERSECTION GEOMETRY

CONGRESS

STREET

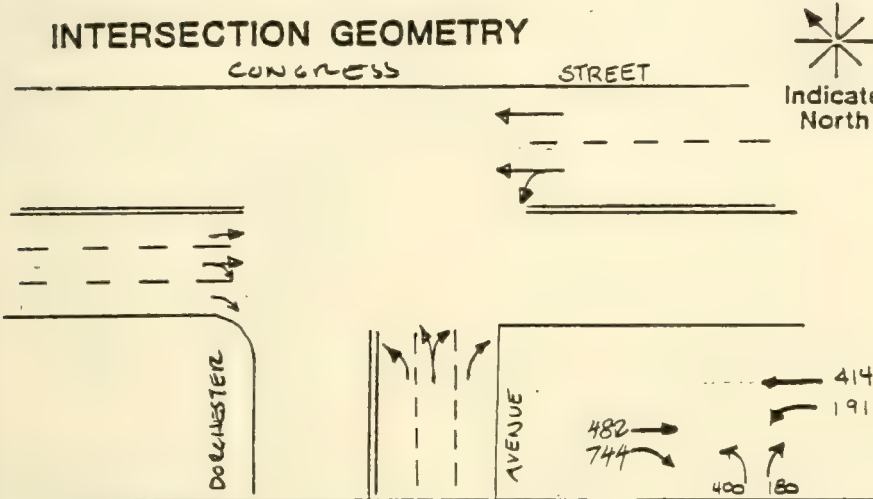


## Left Turn Check

Approach

1 2 3 4

- Number of change intervals per hour
- Left turn capacity on change interval, in vph
- G/C Ratio
- Opposing volume in vph
- Left turn capacity on green, in vph
- Left turn capacity in vph ( $b + e$ )
- Left turn volume in vph
- Is volume > capacity ( $g > 0$ )?



## PHASING 3 Ø

(A)	(B)	(C)	(D)	(E)
CLV = 220	CLV = 409	CLV = 191	CLV =	CLV =

$\Sigma$  CLV 820 <sup>AOT</sup> 1025 800  
 V/C .72 0.807  
 LOS C B  
 20% Reduction For Peds

CRITERIA (vph)	2 Ø	AOT	3 Ø	4 Ø
LOS A	900	659	855	825
B	1050	700	1000	965
C	1200	742	1140	1100
D	1350	782	1275	1225
E	1500	820	1425	1375





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INTERSECTION CONGRESS ST / DORCHESTER AVE.  
 ALT. BUILD YEAR 1990 PERIOD PM  
 CALCULATED BY D.S.D. DATE 4/30/84 SHEET OF  
 CHECKED BY RB DATE 5/1/84 JOB NO. 0788/923

## INTERSECTION GEOMETRY

CONGRESS

STREET

Indicate North

DORCHESTER

AVENUE

## Left Turn Check

Approach

1 2 3 4

- Number of change intervals per hour
- Left turn capacity on change interval, in vph
- G/C Ratio
- Opposing volume in vph
- Left turn capacity on green, in vph
- Left turn capacity in vph (b + c)
- Left turn volume in vph
- Is volume > capacity (g > 0)?

## PHASING

3

(A)	(B)	(C)	(D)	(E)
CLV= 287	CLV= 316	CLV= 209	CLV=	CLV=

$\Sigma$  CLV 812

V/C 0.71

LOS C

20% Reduction For Peds

ADT  
1015

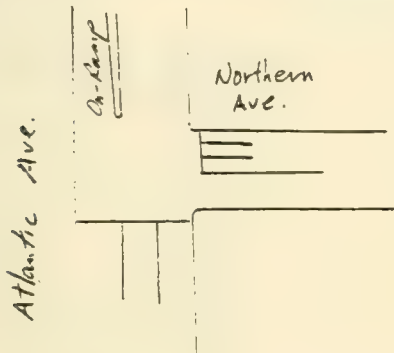
CRITERIA (vph)	2	ADT	3	4
LOS A	900	654	855	825
B	1050	800	1000	965
C	1200	912	1140	1100
D	1350	1020	1275	1225
E	1500	1140	1425	1375



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INTERSECTION Atlantic Ave. / Nor + Leav Ave.  
 ALT. Existing YEAR \_\_\_\_\_ PERIOD AM  
 CALCULATED BY BG DATE \_\_\_\_\_ SHEET OF  
 CHECKED BY CB DATE 8/13/84 JOB NO. 0923

## INTERSECTION GEOMETRY



← 351  
 ← 147

↑ 113  
 ↑ 839  
 ↑ 860

### Left Turn Check

	Approach			
	1	2	3	4
a. Number of change intervals per hour				
b. Left turn capacity on change interval, in vph				
c. G/C Ratio				
d. Opposing volume in vph				
e. Left turn capacity on green, in vph				
f. Left turn capacity in vph (b - e)				
g. Left turn volume in vph				
h. Is volume > capacity (g > f)?				

## PHASING 2Ø

(A)	(B)	(C)	(D)	(E)
↑ ↑	↑ ←			
↑ ↑ ↑ 576 576 860 *	← 274 ← 224			
CLV = 476	CLV = 279	CLV =	CLV =	CLV =

\* OK - RT is free flow

Σ CLV 750

V/C 0.50

LOS A

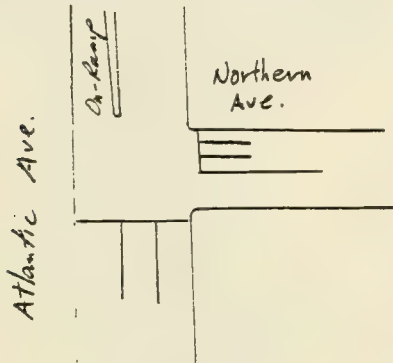
CRITERIA (vph)		2 Ø	3 Ø	4 Ø
LOS	A	900	855	825
	B	1050	1000	965
	C	1200	1140	1100
	D	1350	1275	1225
	E	1500	1425	1375



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INTERSECTION Atlantic Ave. / North Ave.  
 ALT. Existing YEAR          PERIOD PM  
 CALCULATED BY BG DATE          SHEET          OF           
 CHECKED BY RK DATE 1/13/84 JOB NO. 0923

## INTERSECTION GEOMETRY



782  
 696

332  
 1578  
 312

## Left Turn Check

	Approach			
	1	2	3	4
a. Number of change intervals per hour				
b. Left turn capacity on change interval, in vph				
c. G/C Ratio				
d. Opposing volume in vph				
e. Left turn capacity on green, in vph				
f. Left turn capacity in vph (b * e)				
g. Left turn volume in vph				
h. Is volume > capacity (g > 0)?				

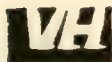
## PHASING 2Ø

(A)	(B)	(C)	(D)	(E)
↑	↑			
↑	↑			
674 674 674	591 591 296*			
CLV= 674	CLV= 591	CLV=	CLV=	CLV=

\* During 1/2 hour of the peak hour, the third lane is utilized based on field observations.

Σ CLV 1265  
 V/C 0.84  
 LOS D

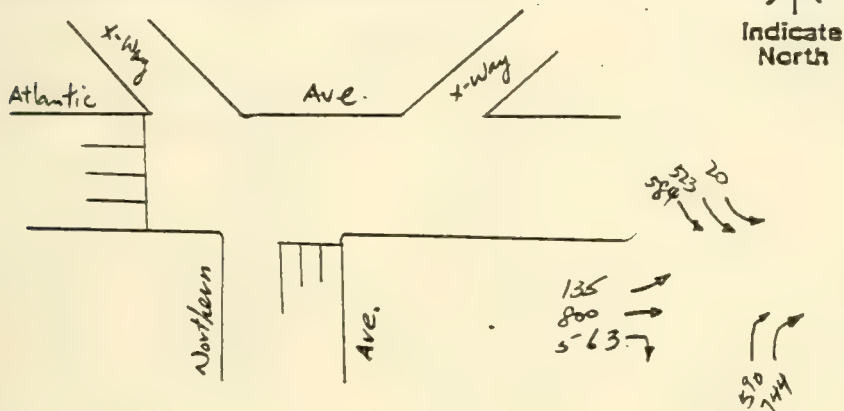
CRITERIA (vph)		2 Ø	3 Ø	4 Ø
LOS	A	900	855	825
	B	1050	1000	965
	C	1200	1140	1100
	D	1350	1275	1225
	E	1500	1425	1375



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INTERSECTION ATLANTIC AVE / NORTHERN AVE  
 ALT. No Build YEAR 1990 PERIOD AM  
 CALCULATED BY BS DATE \_\_\_\_\_ SHEET OF  
 CHECKED BY PR DATE 7/13 JOB NO. 0923

## INTERSECTION GEOMETRY



## Left Turn Check

	Approach			
	1	2	3	4
a. Number of change intervals per hour				
b. Left turn capacity on change interval, in vph				
c. G/C Ratio				
d. Opposing volume in vph				
e. Left turn capacity on green, in vph				
f. Left turn capacity in vph (b * e)				
g. Left turn volume in vph				
h. Is volume > capacity (g > f)?				

## PHASING 3φ

(A)	(B)	(C)	(D)	(E)
→ ↩	↘ ↩	↩ ↘		
311 → 312 → 312 ↩	584 ↘ 543 ↘ 2 ↘	↩ ↘ ↘ ↘		
CLV = 312	CLV = 584	CLV = 445	CLV =	CLV =

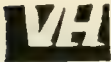
\* FLAT DIST OK due to high ramp volume

Σ CLV 1341  
 V/C 1.11  
 LOS E

15% Reduction for Redo

ADJ  
 1577

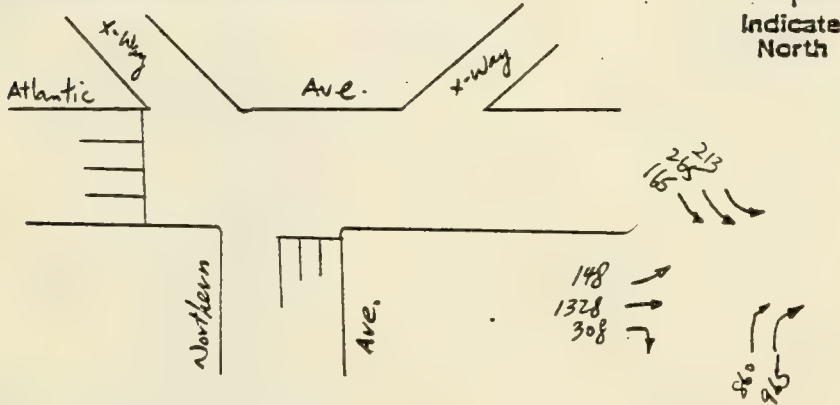
CRITERIA (vph)		2 B	3 B	4 B
LOS	A	900	727	655
	B	1050	850	765
	C	1200	964	860
	D	1350	1079	965
	E	1500	1200	1079



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INTERSECTION ATLANTIC AVE / NORTHERN AVE  
 ALT. No Build YEAR 1990 PERIOD PM  
 CALCULATED BY BG DATE 7/12 SHEET OF  
 CHECKED BY RY DATE 7/12 JOB NO. 0423

## INTERSECTION GEOMETRY



## Left Turn Check

	Approach			
	1	2	3	4
a. Number of change intervals per hour				
b. Left turn capacity on change interval, in vph				
c. G/C Ratio				
d. Opposing volume in vph				
e. Left turn capacity on green, in vph				
f. Left turn capacity in vph (b - e)				
g. Left turn volume in vph				
h. Is volume > capacity (g > f)?				

## PHASING 3φ

(A)	(B)	(C)	(D)	(E)
→ ↩	↙ ↘	↙ ↘		
492 492 492 ↘	322 321 213 ↘	↙ ↘ ↙ ↘		
CLV = 492	CLV = 322	CLV = 609	CLV =	CLV =

Σ CLV 1423

VIC 1.18

LOS E

15% Reduction for Reds

105  
1674

CRITERIA (vph)		2 B	3 B	4 B
LOS	A	900	127	825
	B	1050	1000	1000
	C	1200	1140	1100
	D	1350	1275	1225
	E	1500	1425	1375





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INTERSECTION Atlantic Avenue at Northern Avenue  
 ALT. BUILD YEAR 1990 PERIOD AM  
 CALCULATED BY DSD DATE 4/27/84 SHEET OF  
 CHECKED BY KD DATE 7/1/84 JOB NO. 0788/92

## INTERSECTION GEOMETRY



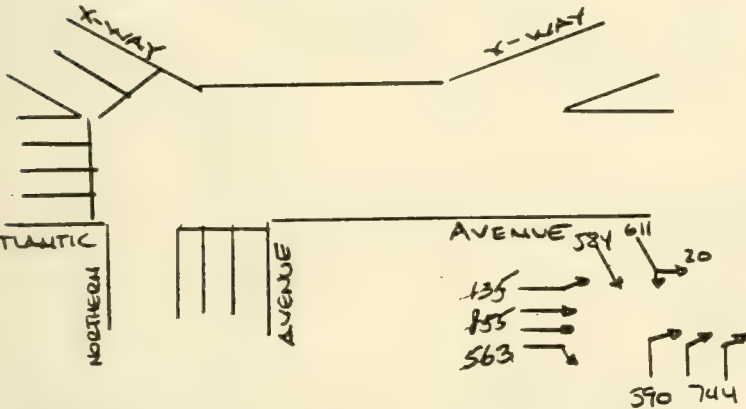
Indicate North

## Left Turn Check

Approach

1 2 3

- Number of change intervals per hour
- Left turn capacity on change interval, in vph
- G/C Ratio
- Opposing volume in vph
- Left turn capacity on green, in vph
- Left turn capacity in vph ( $b \cdot c$ )
- Left turn volume in vph
- Is volume > capacity ( $g > 0$ )?



## PHASING

32

(A)	(B)	(C)	(D)	(E)
325 → 120 325 → 325 → 325 →	584 → 611 219 →	160 → 444 445 445		
CLV = 325	CLV = 611	CLV = 445	CLV =	CLV =

$\Sigma$  CLV 1381

V/C 1.14

LOS E

Adj. for 15% ped

ADJ  
1624

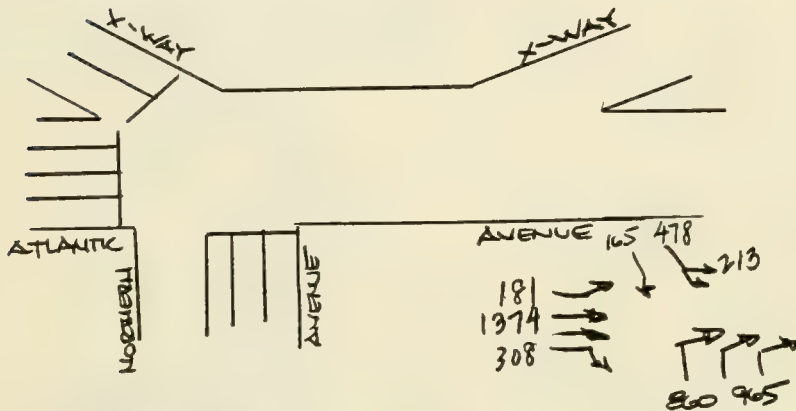
CRITERIA (vph)		2 B	ADJ	3 B	4 B
LOS	A	900	727	855	825
	B	1050	850	1000	965
	C	1200	969	1140	1100
	D	1350	1084	1275	1225
	E	1500	1211	1425	1375



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INTERSECTION Atlantic Avenue at Northern Ave  
 ALT. BUILD YEAR 1990 PERIOD PM  
 CALCULATED BY DSD DATE 4/30/84 SHEET OF  
 CHECKED BY RR DATE 8/1/84 JOB NO. 0738.42

## INTERSECTION GEOMETRY



## Left Turn Check

	Approach		
	1	2	3
a. Number of change intervals per hour			
b. Left turn capacity on change interval, in vph			
c. G/C Ratio			
d. Opposing volume in vph			
e. Left turn capacity on green, in vph			
f. Left turn capacity in vph (b = e)			
g. Left turn volume in vph			
h. Is volume > capacity (g > f)?			

## PHASING

(A)	(B)	(C)	(D)	(E)
518' → 181 519' → 578' →	322' → 321 165' → 213 165' →	608' → 609 609' → 608		
CLV = 519	CLV = 322	CLV = 609	CLV =	CLV =

Σ CLV 1450  
 V/C 1.20  
 LOS E

ADJ  
1706

CRITERIA (vph)		2 B	ADJ	3 B	4 B
LOS	A	900	727	855	925
	B	1050	852	1000	985
	C	1200	909	1140	1100
	D	1350	1054	1275	1225
	E	1500	1211	1425	1375

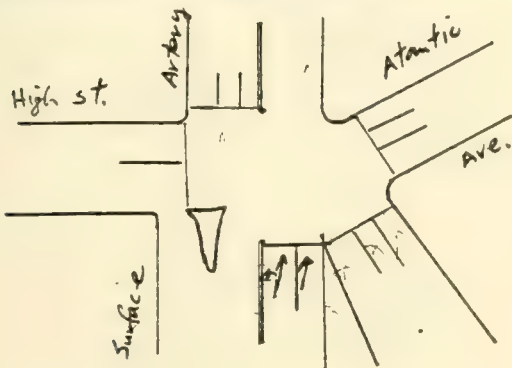
Adj 15% for ADJ



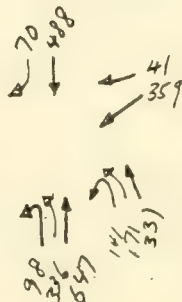
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INTERSECTION ATLANTIC AVE / HIGH ST. / SURFACE ARTERY  
 ALT. EXISTING YEAR 1984 PERIOD AM  
 CALCULATED BY EG DATE \_\_\_\_\_ SHEET OF \_\_\_\_\_  
 CHECKED BY RD DATE 8/11 JOB NO. 0923

## INTERSECTION GEOMETRY



Indicate North



## Left Turn Check

	Approach			
	1	2	3	4
a. Number of change intervals per hour				
b. Left turn capacity on change interval, in vph				
c. G/C Ratio				
d. Opposing volume in vph				
e. Left turn capacity on green, in vph				
f. Left turn capacity in vph (b + e)				
g. Left turn volume in vph				
h. Is volume > capacity (g > f)?				

## PHASING 15% 3 Ø W/ADV

(A)	(B)	(C)	(D)	(E)
50% green time 80% per cycle 99 vph 320	244 vph 114 vph 327	200 vph use two lanes	156 vph 156 vph	
CLV = 320	114 + 244 CLV = 358	CLV = 200	CLV = 156	CLV =

\* 50/50 split OK as outside turn volume > inside volume.

$\Sigma$  CLV 1034

V/C 0.73

LOS C

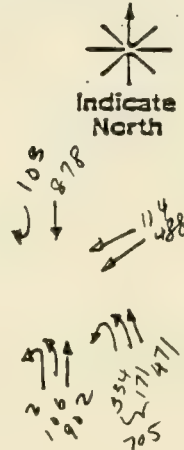
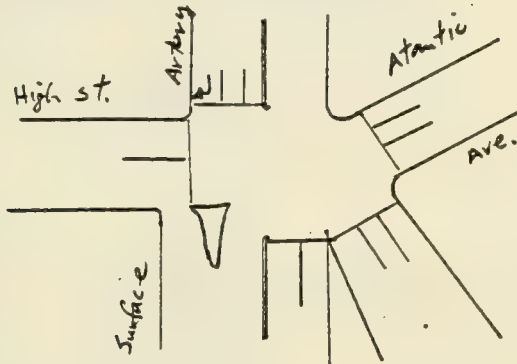
CRITERIA (vph)		2 Ø	3 Ø	4 Ø
LOS	A	900	845	825
	B	1050	1000	965
	C	1200	1140	1100
	D	1350	1275	1225
	E	1500	1425	1375



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INTERSECTION ATLANTIC AVE / HIGH ST. / SURFACE ARTERY  
 ALT. Exist. YEAR 1984 PERIOD PM  
 CALCULATED BY BG DATE 8/10 SHEET OF  
 CHECKED BY RB DATE 8/10 JOB NO. 0923

## INTERSECTION GEOMETRY



## Left Turn Check

	Approach			
	1	2	3	4
a. Number of change intervals per hour				
b. Left turn capacity on change interval, in vph				
c. G/C Ratio				
d. Opposing volume in vph				
e. Left turn capacity on green, in vph				
f. Left turn capacity in vph (b - e)				
g. Left turn volume in vph				
h. Is volume > capacity (g > f)?				

## PHASING use 30

(A)	(B)	(C)	(D)	(E)
77 ↑	77 ↑	301 ↗	77 ↑	3624 = 144
6h Green, 2 carpooling 72 ↑ 72 ↗	457 ↑ 361 ↑ 399 ↗	301 ↗ 301 ↘ use two lanes	77 ↑ 388 317	
CLV = 72	CLV = 487	CLV = 301	CLV = 388	CLV =

Carryover  
 36 ↑ 830 ↑ 399

Σ CLV 1248  
 V/C 0.88  
 LOS D

CRITERIA (vph)		2 B	3 B	4 B
LOS	A	900	955	925
	B	1050	1000	965
	C	1200	1140	1100
	D	1350	1275	1225
	E	1500	1425	1375

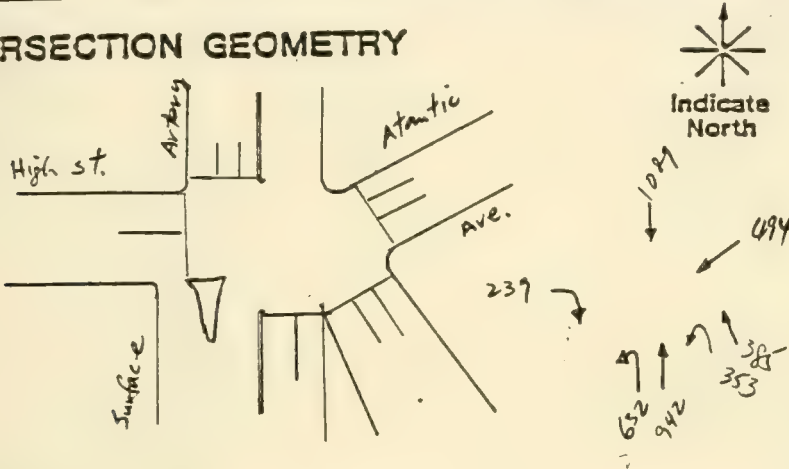




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INTERSECTION ATLANTIC AVE / HIGH ST. / SURFACE ALTERNARY  
 ALT. No-Build YEAR 1990 PERIOD AM  
 CALCULATED BY CS DATE 8/11 SHEET OF  
 CHECKED BY RB DATE 8/11 JOB NO. 0923

## INTERSECTION GEOMETRY



## Left Turn Check

	Approach			
	1	2	3	4
a. Number of change intervals per hour				
b. Left turn capacity on change interval, in vph				
c. G/C Ratio				
d. Opposing volume in vph				
e. Left turn capacity on green, in vph				
f. Left turn capacity in vph (b * e)				
g. Left turn volume in vph				
h. Is volume > capacity (g > f)?				

## PHASING 30

(A)	(B)	(C)	(D)	(E)
25% Assigned Green Time 1000 ↑ 180 58	363 ↓ 363 452 ↑ 452 762	247 ← 247 239	194 ← 194 159 ↑ 159 115	
CLV = 180	CLV = 452 + 363	CLV = 247	CLV = 194	CLV =

CARRY OVER = 452.762 → USE OPP VOL = (363 x 1.5) = 544 LT Factor = 2.0

Σ CLV 1436  
 V/C 1.01  
 LOS E

CRITERIA (vph)		2 B	3 B	4 B
LOS	A	900	1155	1325
	B	1050	1000	965
	C	1200	1140	1100
	D	1350	1275	1225
	E	1500	1425	1375

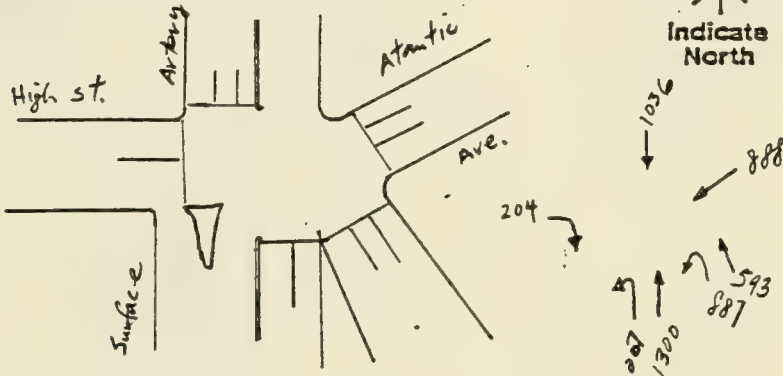




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INTERSECTION ATLANTIC AVE / HIGH ST. / SURFACE AVE  
 ALT. No Build YEAR 1990 PERIOD PM  
 CALCULATED BY DATE SHEET OF  
 CHECKED BY DATE JOB NO. 0923

## INTERSECTION GEOMETRY



## Left Turn Check

	Approach			
	1	2	3	4
a. Number of change intervals per hour				
b. Left turn capacity on change interval, in vph				
c. G/C Ratio				
d. Opposing volume in vph				
e. Left turn capacity on green, in vph				
f. Left turn capacity in vph (b + e)				
g. Left turn volume in vph				
h. Is volume > capacity (g > f)?				

## PHASING 3 φ

(A)	(B)	(C)	(D)	(E)
↑ ↑	↑ ↑	↑	↑ ↑	
↑ ↑ 16 207 207	345 346 348 104 517 495 599	204 444 444	488 399	
CLV = 207	CLV = 599	CLV = 444	CLV = 488	CLV =

Since mixed vehicles on advance

Assume: if 207, 1/2 on LT then: Capacity = 104 990

OPP vol = 346 x 1.5 = 519 LT FAK = 2.0

Σ CLV 1738

VIC 1.22

LOS E

CRITERIA (vph)		2 B	3 B	4 B
LOS	A	900	855	825
	B	1050	1000	965
	C	1200	1140	1100
	D	1350	1275	1225
	E	1500	1425	1375



INTERSECTION ATLANTIC AVE / HIGH ST / SURFACE ARTER  
ALT. BUILD YEAR 1990 PERIOD 2M  
CALCULATED BY D.S.D. DATE 4/26/84 SHEET OF  
CHECKED BY DS DATE 5/1/84 JOB NO. 078P



Indicate  
North

### Left Turn Check

	Approach			
	1	2	3	4
a. Number of change intervals per hour				
b. Left turn capacity on change interval, in vph				
c. G/C Ratio				
d. Opposing volume in vph				
e. Left turn capacity on green, in vph				
f. Left turn capacity in vph ( $b + e$ )				
g. Left turn volume in vph				
h. Is volume > capacity ( $g > f$ )?				

NO LT  
Problem

## PHASING

(A)	(B)	(C)	(D)	(E)
<p>CLV = 180</p>	<p>CLV = 539 + 363</p>	<p>CLV = 245</p>	<p>CLV = 194</p>	<p>CLV =</p>

Carry over

539 762

L1 @ 2.0

Σ CLV 1561  
V/C 1.10  
LOS E

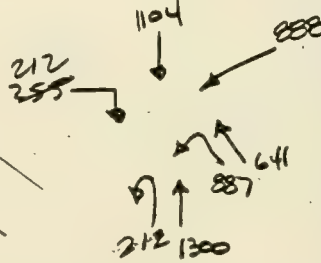
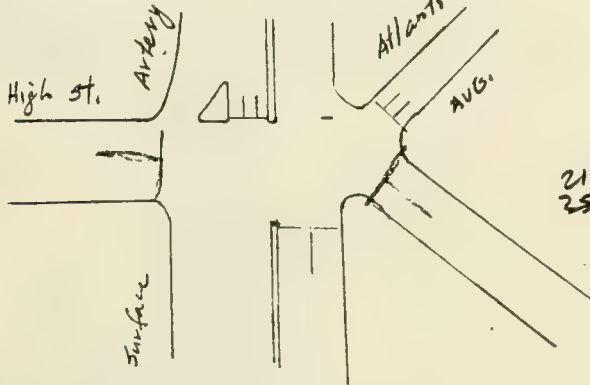
CRITERIA (vph)		2 B	3 B	4 B
LOS	A	900	855	825
	B	1050	1000	965
	C	1200	1140	1100
	D	1350	1275	1225
	E	1500	1425	1375



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INTERSECTION ATLANTIC AVE / HIGH ST. / SURFACE ARTER  
 ALT. Build YEAR 1990 PERIOD PM  
 CALCULATED BY BG DATE 4-13-84 SHEET OF  
 CHECKED BY AB DATE 8-13 JOB NO. 0788

## INTERSECTION GEOMETRY



## Left Turn Check

	Approach			
	1	2	3	4
a. Number of change intervals per hour				
b. Left turn capacity on change interval, in vph				
c. G/C Ratio				
d. Opposing volume in vph				
e. Left turn capacity on green, in vph				
f. Left turn capacity in vph (b * e)				
g. Left turn volume in vph				
h. Is volume > capacity (g > f)?				

## PHASING

3φ

(A)	(B)	(C)	(D)	(E)
* 106 106 212 212 76	368 368 368 106 991 597 329	212 255 444 444	488 397	
CLV= 212	CLV= 597	CLV= 444 ✓	CLV= 488	CLV=

\* Assume only 1/2 LTS  
 as mixed traffic

CARRY OVER 47 106 982

Σ CLV 1741

V/C 1.22

LOS E

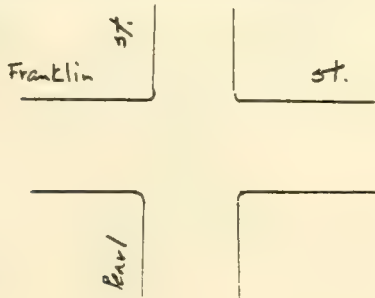
CRITERIA (vph)		2 B	3 B	4 B
LOS	A.	900	855	825
	B	1030	1000	968
	C	1200	1140	1100
	D	1350	1275	1225
	E	1500	1425	1375



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INTERSECTION FRANKLIN ST. / PEARL ST  
 ALT. Existing YEAR      PERIOD Any  
 CALCULATED BY BG DATE      SHEET      OF       
 CHECKED BY RL DATE 8/13/84 JOB NO. 0923

## INTERSECTION GEOMETRY



Indicate  
North

328  
← 664

30  
↑  
20

## Left Turn Check

- Number of change intervals per hour
- Left turn capacity on change interval, in vph
- G/C Ratio
- Opposing volume in vph
- Left turn capacity on green, in vph
- Left turn capacity in vph ( $b = c$ )
- Left turn volume in vph
- Is volume > capacity (g > 0)?

Approach

1 2 3 4

## PHASING 20

(A)	(B)	(C)	(D)	(E)
↑ T	← T			
30 ↑ 50	324 ↑ 496 ← 496			
CLV= 50	CLV= 496	CLV=	CLV=	CLV=

Σ CLV 546

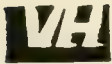
V/C 0.46

LOS A

20% Reduction for Pedestrians

NOT  
682

CRITERIA (vph)	ALL	2 B	3 B	4 B
LOS A	726	900	855	825
B	340	1050	1000	965
C	1000	1200	1140	1100
D	1050	1350	1275	1225
E	1000	1500	1425	1375



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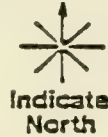
INTERSECTION FRANKLIN ST. / PEAK ST  
 ALT. Existing YEAR \_\_\_\_\_ PERIOD PM  
 CALCULATED BY CG DATE \_\_\_\_\_ SHEET OF  
 CHECKED BY RS DATE 8/13/64 JOB NO. 0923

## INTERSECTION GEOMETRY

Franklin St.

St.

Peak



167  
131

8628

### Left Turn Check

Approach

1 2 3 4

- Number of change intervals per hour
- Left turn capacity on change interval, in vph
- G/C Ratio
- Opposing volume in vph
- Left turn capacity on green, in vph
- Left turn capacity in vph ( $b + c$ )
- Left turn volume in vph
- Is volume > capacity ( $g > 0$ )?

## PHASING

(A)	(B)	(C)	(D)	(E)
↑	↑			
184	167 131			
CLV = 184	CLV = 167	CLV =	CLV =	CLV =

$\Sigma$  CLV 351

V/C 0.29

LOS A

20% Reduction for Peds

ADJ  
439

CRITERIA (vph)	ACT	2 B	3 B	4 B
LOS A	720	900	855	825
B	840	1050	1000	965
C	960	1200	1140	1100
D	1080	1350	1275	1225
E	1200	1500	1425	1375

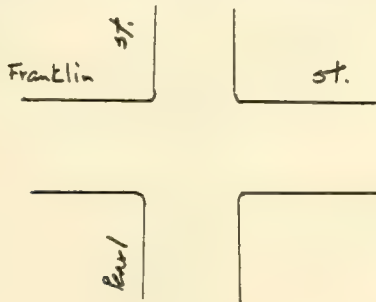




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INTERSECTION FRANKLIN ST. / PEARL ST  
 ALT. No-Build YEAR 1990 PERIOD AM  
 CALCULATED BY SG DATE 8/13 SHEET OF  
 CHECKED BY KB DATE 8/13 JOB NO. 0923

## INTERSECTION GEOMETRY



## Left Turn Check

Approach

1 2 3 4

- Number of change intervals per hour
- Left turn capacity on change interval, in vph
- G/C Ratio
- Opposing volume in vph
- Left turn capacity on green, in vph
- Left turn capacity in vph ( $b + e$ )
- Left turn volume in vph
- Is volume > capacity ( $g > 0$ )?

## PHASING

(A)	(B)	(C)	(D)	(E)
↑	↑			
273 ↑	171 ↑ 198 ← 197			
CLV= 334	CLV= 198	CLV=	CLV=	CLV=

Σ CLV 532

V/C 0.44

LOS A

20% Reduction for Peds

ADL  
645

CRITERIA (vph)	1st	2nd	3rd	4th
LOS A	720	900	885	825
B	840	1050	1000	965
C	960	1200	1140	1100
D	1080	1350	1275	1225
E	1200	1500	1425	1375

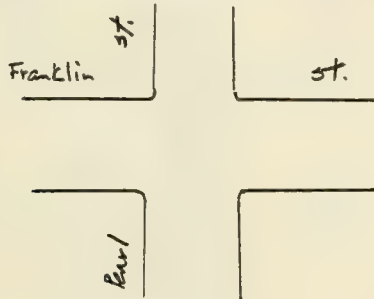


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INTERSECTION FRANKLIN ST. / PEARL ST

ALT. No-Build YEAR 1990 PERIOD PM  
 CALCULATED BY SG DATE 8/30 SHEET OF  
 CHECKED BY RB DATE 8/30 JOB NO. 0923

## INTERSECTION GEOMETRY



179  
101

218 285

## Left Turn Check

Approach

1 2 3 4

- Number of change intervals per hour
- Left turn capacity on change interval, in vph
- G/C Ratio
- Opposing volume in vph
- Left turn capacity on green, in vph
- Left turn capacity in vph ( $b = e$ )
- Left turn volume in vph
- Is volume > capacity ( $g > 0$ )?

## PHASING

(A)	(B)	(C)	(D)	(E)
↑	↑			
218 251	179 101			
CLV = 252	CLV = 179	CLV =	CLV =	CLV =

Σ CLV 431

V/C 0.36

LOS A

20% Reduction for Ped

AOT  
539

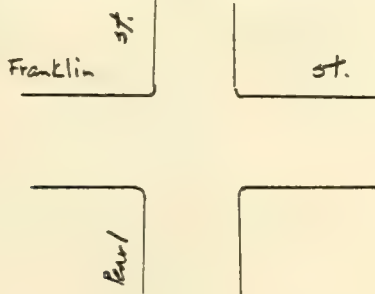
CRITERIA (vph)	1st	2nd	3rd	4th
LOS A	720	900	855	825
B	840	1050	1000	965
C	960	1200	1140	1100
D	1080	1350	1275	1225
E	1200	1500	1425	1375



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INTERSECTION FRANKLIN ST. / PEARL ST  
ALT. Build YEAR 1990 PERIOD AM  
CALCULATED BY GG DATE 8/13/24 SHEET OF  
CHECKED BY RB DATE 8/13/24 JOB NO. 0923

## INTERSECTION GEOMETRY



## Left Turn Check

- a. Number of change intervals per hour  
b. Left turn capacity on change interval, in vph  
c. G/C Ratio  
d. Opposing volume in vph  
e. Left turn capacity on green, in vph  
f. Left turn capacity in vph (b - e)  
g. Left turn volume in vph  
h. Is volume > capacity (g > 0)?

Approach

1 2 3 4

## PHASING 2φ

(A)	(B)	(C)	(D)	(E)
↑	←			
273 ↑ 358 359	198 ← 197			
CLV= 359	CLV= 198	CLV=	CLV=	CLV=

Σ CLV 557

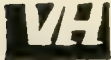
V/C 0.46

LOS A

20% Reduction for Ped

ADJ  
694

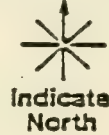
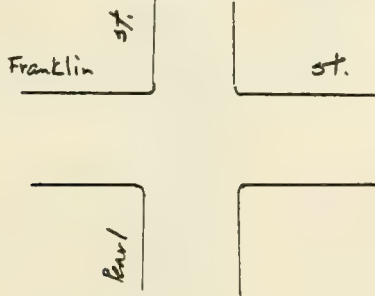
CRITERIA (vph)	1 φ	2 φ	3 φ	4 φ
LOS A	720	900	855	825
B	840	1050	1000	965
C	960	1200	1140	1100
D	1080	1350	1275	1225
E	1200	1500	1425	1375



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INTERSECTION FRANKLIN ST. / PEAK ST  
 ALT. Build YEAR 1990 PERIOD PM  
 CALCULATED BY DJD DATE 4/30/84 SHEET OF  
 CHECKED BY DG DATE        JOB NO. 0923

## INTERSECTION GEOMETRY



179  
101  
218  
285

## Left Turn Check

	Approach			
	1	2	3	4
a. Number of change intervals per hour				
b. Left turn capacity on change interval, in vph				
c. G/C Ratio				
d. Opposing volume in vph				
e. Left turn capacity on green, in vph				
f. Left turn capacity in vph (b * e)				
g. Left turn volume in vph				
h. Is volume > capacity (g > f)?				

## PHASING 2φ

(A)	(B)	(C)	(D)	(E)
↑	↑			
218 ↑ 252 251	179 ↑ 101			
CLV = 252	CLV = 179	CLV =	CLV =	CLV =

Σ CLV 431

V/C 0.36

LOS A

20% Reduction for Peds

AOS  
539

CRITERIA (vph)	1 φ	2 φ	3 φ	4 φ
LOS A	700	900	1100	1300
B	840	1050	1260	1470
C	980	1200	1410	1620
D	1050	1350	1500	1710
E	1200	1500	1800	2100

# TRAFFIC STREAM GAP ANALYSIS PACKAGE

VER 3.5.3 MARCH84

BOSTON, MA.  
FRANKLIN ST./OLIVER ST.  
1984 AM EXISTING - TOTAL OUT FROM OLIVER ST.

## DATA

FIRST VEHICLE CRITICAL GAP, T1, ..... 5 SECONDS  
ADDITIONAL TIME NEEDED FOR SECOND VEHICLE, B1, ... 3 SECONDS  
MOVE UP TIME, B2, ..... 2.5 SECONDS

### OPPOSING TRAFFIC

VOLUME..... 276 VPH  
ARRIVAL RATE..... .077 VPS

### ANALYSIS MOVEMENT TRAFFIC

VOLUME..... 318 VPH  
ARRIVAL RATE..... .088 VPS

## RESULTS

CAPACITY= 916 VPH

RESERVE CAPACITY= 598 VPH

### ACCEPTABLE GAPS

PERCENT OF ALL GAPS..... 68.2 PERCENT  
AVERAGE LENGTH..... 18 SECONDS

### AVERAGE DELAY TO A VEHICLE AT STOP BAR

TO ALL VEHICLES..... .1 SECONDS  
TO DELAYED VEHICLES ONLY..... 3.4 SECONDS

### AVERAGE WAIT IN A QUEUE

TO ALL VEHICLES..... 2.1 SECONDS  
TO QUEUED VEHICLES ONLY..... 6 SECONDS

### AVERAGE DELAY PLUS AVERAGE WAIT

TO ALL VEHICLES..... 2.2 SECONDS  
TO DELAYED AND QUEUED VEHICLES ONLY..... 9.4 SECONDS

### QUEUE LENGTH

AVERAGE..... .5 VEHICLES  
95TH PERCENTILE..... 2.4 VEHICLES

LEVEL OF SERVICE --- A ---



# TRAFFIC STREAM GAP ANALYSIS PACKAGE

VER 3.5.3 MARCH84

BOSTON, MA.

FRANKLIN ST./OLIVER ST.

1984 PM EXISTING - TOTAL OUT FROM OLIVER ST.

## DATA

FIRST VEHICLE CRITICAL GAP, T1, ..... 5 SECONDS  
ADDITIONAL TIME NEEDED FOR SECOND VEHICLE, B1, ... 3 SECONDS  
MOVE UP TIME, B2, ..... 2.5 SECONDS

### OPPOSING TRAFFIC

VOLUME..... 236 VPH  
ARRIVAL RATE..... .066 VPS

### ANALYSIS MOVEMENT TRAFFIC

VOLUME..... 207 VPH  
ARRIVAL RATE..... .058 VPS

## RESULTS

CAPACITY= 952 VPH

RESERVE CAPACITY= 745 VPH

### ACCEPTABLE GAPS

PERCENT OF ALL GAPS..... 72.1 PERCENT  
AVERAGE LENGTH..... 20.3 SECONDS

### AVERAGE DELAY TO A VEHICLE AT STOP BAR

TO ALL VEHICLES..... .1 SECONDS  
TO DELAYED VEHICLES ONLY..... 3.4 SECONDS

### AVERAGE WAIT IN A QUEUE

TO ALL VEHICLES..... 1 SECONDS  
TO QUEUED VEHICLES ONLY..... 4.9 SECONDS

### AVERAGE DELAY PLUS AVERAGE WAIT

TO ALL VEHICLES..... 1.1 SECONDS  
TO DELAYED AND QUEUED VEHICLES ONLY..... 8.2 SECONDS

### QUEUE LENGTH

AVERAGE..... .3 VEHICLES  
95TH PERCENTILE..... 1.8 VEHICLES

LEVEL OF SERVICE --- A ---

TRAFFIC STREAM GAP ANALYSIS PACKAGE  
VER 3.5.3 MARCH84

BOSTON, MA.  
FRANKLIN ST./OLIVER ST.  
1990 NO BUILD AM - TOTAL OUT FROM OLIVER ST.

DATA

FIRST VEHICLE CRITICAL GAP, T1, ..... 5 SECONDS  
ADDITIONAL TIME NEEDED FOR SECOND VEHICLE, B1, ... 3 SECONDS  
MOVE UP TIME, B2, ..... 2.5 SECONDS

OPPOSING TRAFFIC

VOLUME..... 297 VPH  
ARRIVAL RATE..... .083 VPS

ANALYSIS MOVEMENT TRAFFIC

VOLUME..... 200 VPH  
ARRIVAL RATE..... .056 VPS

RESULTS

CAPACITY= 897 VPH

RESERVE CAPACITY= 697 VPH

ACCEPTABLE GAPS

PERCENT OF ALL GAPS..... 66.2 PERCENT  
AVERAGE LENGTH..... 17.1 SECONDS

AVERAGE DELAY TO A VEHICLE AT STOP BAR

TO ALL VEHICLES..... .1 SECONDS  
TO DELAYED VEHICLES ONLY..... 3.4 SECONDS

AVERAGE WAIT IN A QUEUE

TO ALL VEHICLES..... 1.2 SECONDS  
TO QUEUED VEHICLES ONLY..... 5.2 SECONDS

AVERAGE DELAY PLUS AVERAGE WAIT

TO ALL VEHICLES..... 1.3 SECONDS  
TO DELAYED AND QUEUED VEHICLES ONLY..... 8.6 SECONDS

QUEUE LENGTH

AVERAGE..... .3 VEHICLES  
95TH PERCENTILE..... 1.8 VEHICLES

LEVEL OF SERVICE --- A ---

TRAFFIC STREAM GAP ANALYSIS PACKAGE  
VER 3.5.3 MARCH84

BOSTON, MA.  
FRANKLIN ST./OLIVER ST.  
1990 NO BUILD PM - TOTAL OUT FROM OLIVER ST.

DATA

FIRST VEHICLE CRITICAL GAP, T1, ..... 5 SECONDS  
ADDITIONAL TIME NEEDED FOR SECOND VEHICLE, B1, ... 3 SECONDS  
MOVE UP TIME, B2, ..... 2.5 SECONDS

OPPOSING TRAFFIC

VOLUME..... 260 VPH  
ARRIVAL RATE..... .072 VPS

ANALYSIS MOVEMENT TRAFFIC

VOLUME..... 20 VPH  
ARRIVAL RATE..... .006 VPS

RESULTS

CAPACITY= 930 VPH

RESERVE CAPACITY= 910 VPH

ACCEPTABLE GAPS

PERCENT OF ALL GAPS..... 69.7 PERCENT  
AVERAGE LENGTH..... 18.8 SECONDS

AVERAGE DELAY TO A VEHICLE AT STOP BAR

TO ALL VEHICLES..... .1 SECONDS  
TO DELAYED VEHICLES ONLY..... 3.4 SECONDS

AVERAGE WAIT IN A QUEUE

TO ALL VEHICLES..... .1 SECONDS  
TO QUEUED VEHICLES ONLY..... 4 SECONDS

AVERAGE DELAY PLUS AVERAGE WAIT

TO ALL VEHICLES..... .2 SECONDS  
TO DELAYED AND QUEUED VEHICLES ONLY..... 7.4 SECONDS

QUEUE LENGTH

AVERAGE..... 0 VEHICLES  
95TH PERCENTILE..... .8 VEHICLES

LEVEL OF SERVICE --- A ---

# TRAFFIC STREAM GAP ANALYSIS PACKAGE

VER 3.5.2 15AUG83

BOSTON, MA.  
FRANKLIN ST./OLIVER ST.  
1990 BUILD AM - OLIVER ST. EB

## DATA

FIRST VEHICLE CRITICAL GAP, T1, ..... 5 SECONDS  
ADDITIONAL TIME NEEDED FOR SECOND VEHICLE, B1, ... 3 SECONDS  
MOVE UP TIME, B2, ..... 2.5 SECONDS  
MAIN STREET HOURLY TRAFFIC VOLUME: ..... 338 VPH  
MAIN STREET ARRIVAL RATE: ..... .0938889 VPS  
SIDE STREET HOURLY TRAFFIC VOLUME: ..... 200 VPH  
SIDE STREET ARRIVAL RATE: ..... .0555556 VPS

## RESULTS

CAPACITY= 861 VPH

RESERVE CAPACITY= 661 VPH

PERCENT ACCEPTABLE GAPS: ..... 62.535 PERCENT  
AVERAGE ACCEPTABLE GAP LENGTH: ..... 15.6509 SECONDS  
AVERAGE DELAY: ..... .147355 SECONDS  
AVERAGE DELAY TO A DELAYED VEHICLE: ... 3.44512 SECONDS  
AVERAGE WAIT IN QUEUE:..... 1.26491 SECONDS  
AVERAGE WAIT WHEN QUEUED:..... 5.44581 SECONDS  
AVERAGE DELAY :..... 1.41227 SECONDS  
AVERAGE TOTAL DELAY AND WAIT:..... 8.89094 SECONDS  
AVERAGE QUEUE LENGTH:..... .302545 VEHICLES  
NINETY-FIFTH PERCENTILE QUEUE..... 1.87103 VEHICLES

LEVEL OF SERVICE --- A ---

TRAFFIC STREAM GAP ANALYSIS PACKAGE  
VER 3.5.3 MARCH84

BOSTON, MA.  
FRANKLIN ST./OLIVER ST.  
1990 BUILD PM - TOTAL OUT FROM OLIVER ST.

DATA

FIRST VEHICLE CRITICAL GAP, T1, ..... 5 SECONDS  
ADDITIONAL TIME NEEDED FOR SECOND VEHICLE, B1, ... 3 SECONDS  
MOVE UP TIME, B2, ..... 2.5 SECONDS

OPPOSING TRAFFIC

VOLUME..... 260 VPH  
ARRIVAL RATE..... .072 VPS

ANALYSIS MOVEMENT TRAFFIC

VOLUME..... 20 VPH  
ARRIVAL RATE..... .006 VPS

RESULTS

CAPACITY= 930 VPH

RESERVE CAPACITY= 910 VPH

ACCEPTABLE GAPS

PERCENT OF ALL GAPS..... 69.7 PERCENT  
AVERAGE LENGTH..... 18.8 SECONDS

AVERAGE DELAY TO A VEHICLE AT STOP BAR

TO ALL VEHICLES..... .1 SECONDS  
TO DELAYED VEHICLES ONLY..... 3.4 SECONDS

AVERAGE WAIT IN A QUEUE

TO ALL VEHICLES..... .1 SECONDS  
TO QUEUED VEHICLES ONLY..... 4 SECONDS

AVERAGE DELAY PLUS AVERAGE WAIT

TO ALL VEHICLES..... .2 SECONDS  
TO DELAYED AND QUEUED VEHICLES ONLY..... 7.4 SECONDS

QUEUE LENGTH

AVERAGE..... 0 VEHICLES  
95TH PERCENTILE..... .8 VEHICLES

LEVEL OF SERVICE --- A ---



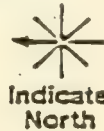
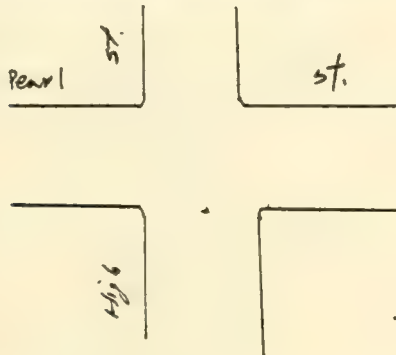


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INTERSECTION HIGH ST / PEARL ST.

ALT. Eastline YEAR 1980 PERIOD AM  
CALCULATED BY BG DATE 8/10 SHEET OF  
CHECKED BY RR DATE 8/10 JOB NO. 0723

## INTERSECTION GEOMETRY



328  
664

20  
30

## Left Turn Check

- Number of change intervals per hour
- Left turn capacity on change interval, in vph
- G/C Ratio
- Opposing volume in vph
- Left turn capacity on green, in vph
- Left turn capacity in vph (b - e)
- Left turn volume in vph
- Is volume > capacity (g > f)?

Approach

1 2 3 4

## PHASING 2p

(A)	(B)	(C)	(D)	(E)
↓	→			
328 664	50			
CLV = 496	CLV = 50	CLV =	CLV =	CLV =

$\Sigma$  CLV 546  
V/C 0.40  
LOS A

20% Reduction for Pedals

ADJ  
683

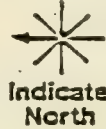
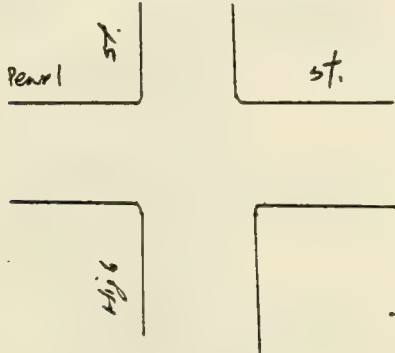
CRITERIA (van)	1 L	2 B	3 B	4 B
LOS A	720	900	855	825
B	840	1050	1000	965
C	960	1200	1140	1100
D	1080	1350	1275	1225
E	1200	1500	1425	1375



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INTERSECTION HIGH ST / PEARL ST.  
 ALT. Existing YEAR 1984 PERIOD PM  
 CALCULATED BY RG DATE \_\_\_\_\_ SHEET OF  
 CHECKED BY RB DATE 8/10 JOB NO. 0723

## INTERSECTION GEOMETRY



## Left Turn Check

	Approach			
	1	2	3	4
a. Number of change intervals per hour				
b. Left turn capacity on change interval, in vph				
c. G/C Ratio				
d. Opposing volume in vph				
e. Left turn capacity on green, in vph				
f. Left turn capacity in vph (b * e)				
g. Left turn volume in vph				
h. Is volume > capacity (g > f)?				

## PHASING 2p

(A)	(B)	(C)	(D)	(E)
↓	→			
167 ↓	98 → 86			
CLV = 167	CLV = 184	CLV =	CLV =	CLV =

$\Sigma$  CLV 351  
 V/C 0.29  
 LOS A

20% Reduction for Pedals

AOT  
439

CRITERIA (von)	A	2 B	3 B	4 B
LOS A	720	900	885	825
B	840	1050	1000	965
C	700	1200	1140	1100
D	1080	1350	1275	1225
E	1200	1500	1425	1375

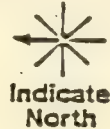
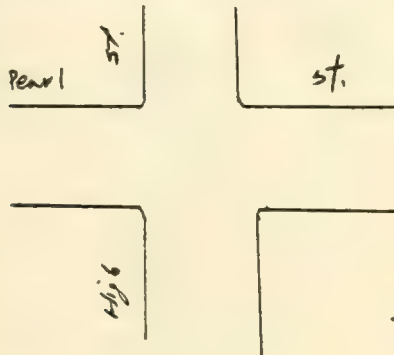


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INTERSECTION HIGH ST / PEARL ST.

ALT. No - Build YEAR 1990 PERIOD AM  
 CALCULATED BY GG DATE \_\_\_\_\_ SHEET OF  
 CHECKED BY RR DATE 5/3 JOB NO. 0723

## INTERSECTION GEOMETRY



26  
130  
321  
672

## Left Turn Check

	Approach			
	1	2	3	4
a. Number of change intervals per hour				
b. Left turn capacity on change interval, in vph				
c. G/C Ratio				
d. Opposing volume in vph				
e. Left turn capacity on green, in vph				
f. Left turn capacity in vph (b + e)				
g. Left turn volume in vph				
h. Is volume > capacity (g > f)?				

## PHASING 2p

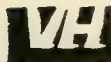
(A)	(B)	(C)	(D)	(E)
↑	←			
26 20 20	321 486 497			
CLV = 78	CLV = 497	CLV =	CLV =	CLV =

$\Sigma$  CLV 575  
 V/C 0.48  
 LOS A

20% Reduction for Ped.

ADJ  
714

CRITERIA (vph)		1 S	2 S	3 S	4 S
LOS	A	720	900	1155	1425
	B	840	1050	1365	1680
	C	960	1200	1540	1920
	D	1080	1350	1725	2160
	E	1200	1500	1920	2400

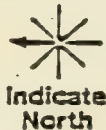
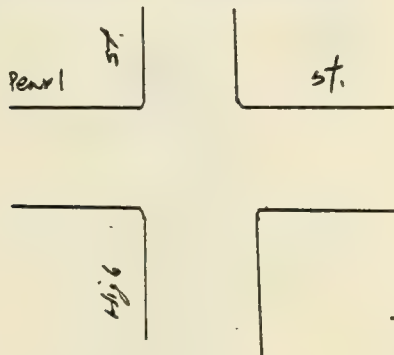


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INTERSECTION HIGH ST / PEARL ST.

ALT. No-Build YEAR 1990 PERIOD PM  
CALCULATED BY RG DATE 8/13 SHEET OF  
CHECKED BY RB DATE 8/13 JOB NO. 0923

## INTERSECTION GEOMETRY



### Left Turn Check

Approach

1 2 3 4

- Number of change intervals per hour
- Left turn capacity on change interval, in vph
- G/C Ratio
- Opposing volume in vph
- Left turn capacity on green, in vph
- Left turn capacity in vph ( $b - e$ )
- Left turn volume in vph
- Is volume > capacity ( $g > 0$ )?

## PHASING 2p

(A)	(B)	(C)	(D)	(E)
↑	←			
26 ↑ 177	18 191 198			
CLV= 177	CLV= 198	CLV=	CLV=	CLV=

$\Sigma$  CLV 325

V/C 0.27

LOS A

20% Reduction for Ped.

ADJ  
406

CRITERIA (vph)	ADJ	2 B	3 B	4 B
LOS A	700	900	1155	1425
B	840	1050	1000	965
C	960	1200	1140	1100
D	1050	1350	1275	1225
E	1200	1500	1425	1375

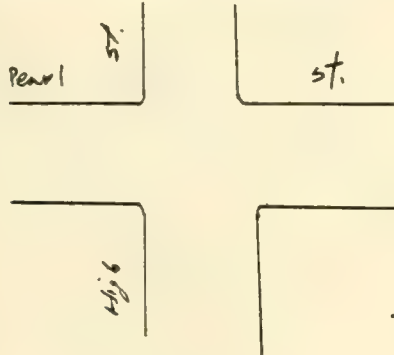


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INTERSECTION HIGH ST / PEARL ST.

ALT. Build YEAR 1990 PERIOD A-7  
 CALCULATED BY DJD DATE 8/11/84 SHEET OF  
 CHECKED BY RGT JOB NO. 0723

## INTERSECTION GEOMETRY



367  
 690  
 57  
 130

## Left Turn Check

	Approach			
	1	2	3	4
a. Number of change intervals per hour				
b. Left turn capacity on change interval, in vph				
c. G/C Ratio				
d. Opposing volume in vph				
e. Left turn capacity on green, in vph				
f. Left turn capacity in vph (b * e)				
g. Left turn volume in vph				
h. Is volume > capacity (g > f)?				

## PHASING 2p

(A)	(B)	(C)	(D)	(E)
↑	→			
57 ↑ 94	367 529 → 529			
CLV= 94	CLV= 529	CLV=	CLV=	CLV=

$\Sigma$  CLV 623

V/C 0.52

LOS A

20% Reduction for Ped.

CRITERIA (vph)	1st	2nd	3rd	4th
LOS A	720	900	855	825
B	840	1050	1000	965
C	100	1200	1140	1100
D	1030	1280	1275	1225
E	1000	1500	1425	1375

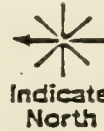
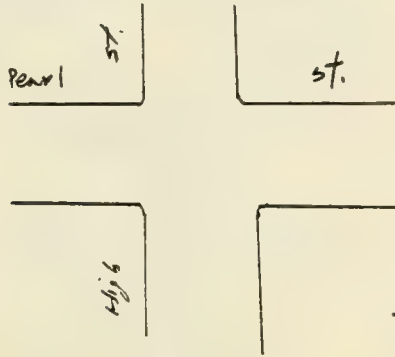




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INTERSECTION HIGH ST / PEARL ST.  
 ALT. Build YEAR 1990 PERIOD PM  
 CALCULATED BY WJS DATE \_\_\_\_\_ SHEET OF  
 CHECKED BY OG DATE 8/11/84 JOB NO. 0923

## INTERSECTION GEOMETRY



26  
378

## Left Turn Check

	Approach			
	1	2	3	4
a. Number of change intervals per hour				
b. Left turn capacity on change interval, in vph				
c. G/C Ratio				
d. Opposing volume in vph				
e. Left turn capacity on green, in vph				
f. Left turn capacity in vph (b * e)				
g. Left turn volume in vph				
h. Is volume > capacity (g > f)?				

## PHASING 2p

(A)	(B)	(C)	(D)	(E)
↑	→			
26 ↑ 137 137	26 → 202 ← 202			
CLV= 137	CLV= 202	CLV=	CLV=	CLV=

Σ CLV 339  
 V/C 0.27  
 LOS A

20% Reduction for Ped.

ADJ  
424

CRITERIA (von)	1st	2nd	3rd	4th
LOS A	720	900	855	825
B	840	1050	1000	965
C	960	1200	1140	1100
D	1080	1350	1275	1225
E	1200	1500	1425	1375

# TRAFFIC STREAM GAP ANALYSIS PACKAGE

VER 3.5.3 MARCH84

BOSTON,MA.  
X-WAY OFF RAMP/HIGH ST.  
EXISTING AM PEAK - HIGH ST. THRU

## DATA

FIRST VEHICLE CRITICAL GAP, T1, ..... 5 SECONDS  
ADDITIONAL TIME NEEDED FOR SECOND VEHICLE, B1, ... 3 SECONDS  
MOVE UP TIME, B2, ..... 2.5 SECONDS

### OPPOSING TRAFFIC

VOLUME..... 637 VPH  
ARRIVAL RATE..... .177 VPS

### ANALYSIS MOVEMENT TRAFFIC

VOLUME..... 354 VPH  
ARRIVAL RATE..... .098 VPS

## RESULTS

CAPACITY= 638 VPH

RESERVE CAPACITY= 284 VPH

### ACCEPTABLE GAPS

PERCENT OF ALL GAPS..... 41.3 PERCENT  
AVERAGE LENGTH..... 10.7 SECONDS

### AVERAGE DELAY TO A VEHICLE AT STOP BAR

TO ALL VEHICLES..... .3 SECONDS  
TO DELAYED VEHICLES ONLY..... 3.6 SECONDS

### AVERAGE WAIT IN A QUEUE

TO ALL VEHICLES..... 7 SECONDS  
TO QUEUED VEHICLES ONLY..... 12.7 SECONDS

### AVERAGE DELAY PLUS AVERAGE WAIT

TO ALL VEHICLES..... 7.3 SECONDS  
TO DELAYED AND QUEUED VEHICLES ONLY..... 16.3 SECONDS

### QUEUE LENGTH

AVERAGE..... 1.2 VEHICLES  
95TH PERCENTILE..... 3.7 VEHICLES

LEVEL OF SERVICE --- C ---

# TRAFFIC STREAM GAP ANALYSIS PACKAGE

VER 3.5.3 MARCH84

BOSTON, MA.  
X-WAY OFF RAMP/HIGH ST.  
EXISTING PM PEAK - HIGH ST. THRU

## DATA

FIRST VEHICLE CRITICAL GAP, T1, ..... 5 SECONDS  
ADDITIONAL TIME NEEDED FOR SECOND VEHICLE, B1, ... 3 SECONDS  
MOVE UP TIME, B2, ..... 2.5 SECONDS

### OPPOSING TRAFFIC

VOLUME..... 181 VPH  
ARRIVAL RATE..... .05 VPS

### ANALYSIS MOVEMENT TRAFFIC

VOLUME..... 361 VPH  
ARRIVAL RATE..... .1 VPS

## RESULTS

CAPACITY= 1005 VPH

RESERVE CAPACITY= 644 VPH

### ACCEPTABLE GAPS

PERCENT OF ALL GAPS..... 77.8 PERCENT  
AVERAGE LENGTH..... 24.9 SECONDS

### AVERAGE DELAY TO A VEHICLE AT STOP BAR

TO ALL VEHICLES..... .1 SECONDS  
TO DELAYED VEHICLES ONLY..... 3.4 SECONDS

### AVERAGE WAIT IN A QUEUE

TO ALL VEHICLES..... 2 SECONDS  
TO QUEUED VEHICLES ONLY..... 5.6 SECONDS

### AVERAGE DELAY PLUS AVERAGE WAIT

TO ALL VEHICLES..... 2.1 SECONDS  
TO DELAYED AND QUEUED VEHICLES ONLY..... 9 SECONDS

### QUEUE LENGTH

AVERAGE..... .6 VEHICLES  
95TH PERCENTILE..... 2.5 VEHICLES

LEVEL OF SERVICE --- A ---

TRAFFIC STREAM GAP ANALYSIS PACKAGE  
VER 3.5.3 MARCH84

BOSTON, MA.  
PURCHASE ST./OLIVER ST.  
EXISTING AM BASE - RT OUT FROM OLIVER ST.

DATA

FIRST VEHICLE CRITICAL GAP, T1, ..... 5 SECONDS  
ADDITIONAL TIME NEEDED FOR SECOND VEHICLE, B1, ... 3 SECONDS  
MOVE UP TIME, B2, ..... 2.5 SECONDS

OPPOSING TRAFFIC

VOLUME..... 298 VPH  
ARRIVAL RATE..... .083 VPS

ANALYSIS MOVEMENT TRAFFIC

VOLUME..... 460 VPH  
ARRIVAL RATE..... .128 VPS

RESULTS

CAPACITY= 896 VPH

RESERVE CAPACITY= 436 VPH

ACCEPTABLE GAPS

PERCENT OF ALL GAPS..... 66.1 PERCENT  
AVERAGE LENGTH..... 17.1 SECONDS

AVERAGE DELAY TO A VEHICLE AT STOP BAR

TO ALL VEHICLES..... .1 SECONDS  
TO DELAYED VEHICLES ONLY..... 3.4 SECONDS

AVERAGE WAIT IN A QUEUE

TO ALL VEHICLES..... 4.2 SECONDS  
TO QUEUED VEHICLES ONLY..... 8.3 SECONDS

AVERAGE DELAY PLUS AVERAGE WAIT

TO ALL VEHICLES..... 4.4 SECONDS  
TO DELAYED AND QUEUED VEHICLES ONLY..... 11.7 SECONDS

QUEUE LENGTH

AVERAGE..... 1.1 VEHICLES  
95TH PERCENTILE..... 3.4 VEHICLES

LEVEL OF SERVICE --- A ---

# TRAFFIC STREAM GAP ANALYSIS PACKAGE

VER 3.5.3 MARCH84

BOSTON,MA  
PURCHASE ST./OLIVER ST.  
EXISTING PM - RT OUT FROM OLIVER ST.

## DATA

FIRST VEHICLE CRITICAL GAP, T1, ..... 5 SECONDS  
ADDITIONAL TIME NEEDED FOR SECOND VEHICLE, B1, ... 3 SECONDS  
MOVE UP TIME, B2, ..... 2.5 SECONDS

### OPPOSING TRAFFIC

VOLUME..... 590 VPH  
ARRIVAL RATE..... .164 VPS

### ANALYSIS MOVEMENT TRAFFIC

VOLUME..... 130 VPH  
ARRIVAL RATE..... .036 VPS

## RESULTS

CAPACITY= 669 VPH

RESERVE CAPACITY= 539 VPH

### ACCEPTABLE GAPS

PERCENT OF ALL GAPS..... 44.1 PERCENT  
AVERAGE LENGTH..... 11.1 SECONDS

### AVERAGE DELAY TO A VEHICLE AT STOP BAR

TO ALL VEHICLES..... .3 SECONDS  
TO DELAYED VEHICLES ONLY..... 3.6 SECONDS

### AVERAGE WAIT IN A QUEUE

TO ALL VEHICLES..... 1.3 SECONDS  
TO QUEUED VEHICLES ONLY..... 6.7 SECONDS

### AVERAGE DELAY PLUS AVERAGE WAIT

TO ALL VEHICLES..... 1.6 SECONDS  
TO DELAYED AND QUEUED VEHICLES ONLY..... 10.2 SECONDS

### QUEUE LENGTH

AVERAGE..... .2 VEHICLES  
95TH PERCENTILE..... 1.7 VEHICLES

LEVEL OF SERVICE --- A ---



TRAFFIC STREAM GAP ANALYSIS PACKAGE  
VER 3.5.3 MARCH84

BOSTON, MA.  
PURCHASE ST./OLIVER ST.  
1990 NO BUILD AM - RT OUT OF OLIVER ST.

DATA

FIRST VEHICLE CRITICAL GAP, T1, ..... 5 SECONDS  
ADDITIONAL TIME NEEDED FOR SECOND VEHICLE, B1, ... 3 SECONDS  
MOVE UP TIME, B2, ..... 2.5 SECONDS

OPPOSING TRAFFIC  
VOLUME..... 1625 VPH  
ARRIVAL RATE..... .451 VFS  
ANALYSIS MOVEMENT TRAFFIC  
VOLUME..... 20 VPH  
ARRIVAL RATE..... .006 VFS

RESULTS

CAPACITY= 229 VPH

RESERVE CAPACITY= 209 VPH

ACCEPTABLE GAPS  
PERCENT OF ALL GAPS..... 10.5 PERCENT  
AVERAGE LENGTH..... 7.2 SECONDS

AVERAGE DELAY TO A VEHICLE AT STOP BAR  
TO ALL VEHICLES..... 1.2 SECONDS  
TO DELAYED VEHICLES ONLY..... 4.4 SECONDS

AVERAGE WAIT IN A QUEUE  
TO ALL VEHICLES..... 1.5 SECONDS  
TO QUEUED VEHICLES ONLY..... 17.2 SECONDS

AVERAGE DELAY PLUS AVERAGE WAIT  
TO ALL VEHICLES..... 2.7 SECONDS  
TO DELAYED AND QUEUED VEHICLES ONLY..... 21.6 SECONDS

QUEUE LENGTH  
AVERAGE..... .1 VEHICLES  
95TH PERCENTILE..... 1.2 VEHICLES

LEVEL OF SERVICE --- C ---

TRAFFIC STREAM GAP ANALYSIS PACKAGE  
VER 3.5.3 MARCH84

BOSTON, MA.  
PURCHASE ST./OLIVER ST.  
1990 NO BUILD PM - RT OUT OF OLIVER ST.

DATA

FIRST VEHICLE CRITICAL GAP, T1, ..... 5 SECONDS  
ADDITIONAL TIME NEEDED FOR SECOND VEHICLE, B1, ... 3 SECONDS  
MOVE UP TIME, B2, ..... 2.5 SECONDS

OPPOSING TRAFFIC

VOLUME..... 1234 VPH  
ARRIVAL RATE..... .343 VPS

ANALYSIS MOVEMENT TRAFFIC

VOLUME..... 20 VPH  
ARRIVAL RATE..... .006 VPS

RESULTS

CAPACITY= 346 VPH

RESERVE CAPACITY= 326 VPH

ACCEPTABLE GAPS

PERCENT OF ALL GAPS..... 18 PERCENT  
AVERAGE LENGTH..... 7.9 SECONDS

AVERAGE DELAY TO A VEHICLE AT STOP BAR

TO ALL VEHICLES..... .8 SECONDS  
TO DELAYED VEHICLES ONLY..... 4 SECONDS

AVERAGE WAIT IN A QUEUE

TO ALL VEHICLES..... .6 SECONDS  
TO QUEUED VEHICLES ONLY..... 11 SECONDS

AVERAGE DELAY PLUS AVERAGE WAIT

TO ALL VEHICLES..... 1.4 SECONDS  
TO DELAYED AND QUEUED VEHICLES ONLY..... 15.1 SECONDS

QUEUE LENGTH

AVERAGE..... .1 VEHICLES  
95TH PERCENTILE..... 1 VEHICLES

LEVEL OF SERVICE --- B ---

# TRAFFIC STREAM GAP ANALYSIS PACKAGE

VER 3.5.3 MARCH84

BOSTON, MA.

PURCHASE ST./OLIVER ST.

1990 BUILD AM - RT OUT OF OLIVER ST.

## DATA

FIRST VEHICLE CRITICAL GAP, T1, ..... 5 SECONDS  
ADDITIONAL TIME NEEDED FOR SECOND VEHICLE, B1, ... 3 SECONDS  
MOVE UP TIME, B2, ..... 2.5 SECONDS

### OPPOSING TRAFFIC

VOLUME..... 1664 VPH

ARRIVAL RATE..... .462 VPS

### ANALYSIS MOVEMENT TRAFFIC

VOLUME..... 20 VPH

ARRIVAL RATE..... .006 VPS

## RESULTS

CAPACITY= 220 VPH

RESERVE CAPACITY= 200 VPH

### ACCEPTABLE GAPS

PERCENT OF ALL GAPS..... 9.9 PERCENT

AVERAGE LENGTH..... 7.2 SECONDS

### AVERAGE DELAY TO A VEHICLE AT STOP BAR

TO ALL VEHICLES..... 1.3 SECONDS

TO DELAYED VEHICLES ONLY..... 4.5 SECONDS

### AVERAGE WAIT IN A QUEUE

TO ALL VEHICLES..... 1.6 SECONDS

TO QUEUED VEHICLES ONLY..... 18 SECONDS

### AVERAGE DELAY PLUS AVERAGE WAIT

TO ALL VEHICLES..... 2.9 SECONDS

TO DELAYED AND QUEUED VEHICLES ONLY..... 22.5 SECONDS

### QUEUE LENGTH

AVERAGE..... .1 VEHICLES

95TH PERCENTILE..... 1.2 VEHICLES

LEVEL OF SERVICE --- C ---

TRAFFIC STREAM GAP ANALYSIS PACKAGE  
VER 3.5.3 MARCH84

BOSTON, MA.  
PURCHASE ST./OLIVER ST.  
1990 BUILD PM - RT OUT OF OLIVER ST.

DATA

FIRST VEHICLE CRITICAL GAP, T1, ..... 5 SECONDS  
ADDITIONAL TIME NEEDED FOR SECOND VEHICLE, B1, ... 3 SECONDS  
MOVE UP TIME, B2, ..... 2.5 SECONDS

OPPOSING TRAFFIC

VOLUME..... 1314 VPH  
ARRIVAL RATE..... .365 VPS

ANALYSIS MOVEMENT TRAFFIC

VOLUME..... 50 VPH  
ARRIVAL RATE..... .014 VPS

RESULTS

CAPACITY= 318 VPH

RESERVE CAPACITY= 268 VPH

ACCEPTABLE GAPS

PERCENT OF ALL GAPS..... 16.1 PERCENT  
AVERAGE LENGTH..... 7.7 SECONDS

AVERAGE DELAY TO A VEHICLE AT STOP BAR

TO ALL VEHICLES..... .9 SECONDS  
TO DELAYED VEHICLES ONLY..... 4.1 SECONDS

AVERAGE WAIT IN A QUEUE

TO ALL VEHICLES..... 2.1 SECONDS  
TO QUEUED VEHICLES ONLY..... 13.4 SECONDS

AVERAGE DELAY PLUS AVERAGE WAIT

TO ALL VEHICLES..... 3 SECONDS  
TO DELAYED AND QUEUED VEHICLES ONLY..... 17.5 SECONDS

QUEUE LENGTH

AVERAGE..... .2 VEHICLES  
95TH PERCENTILE..... 1.5 VEHICLES

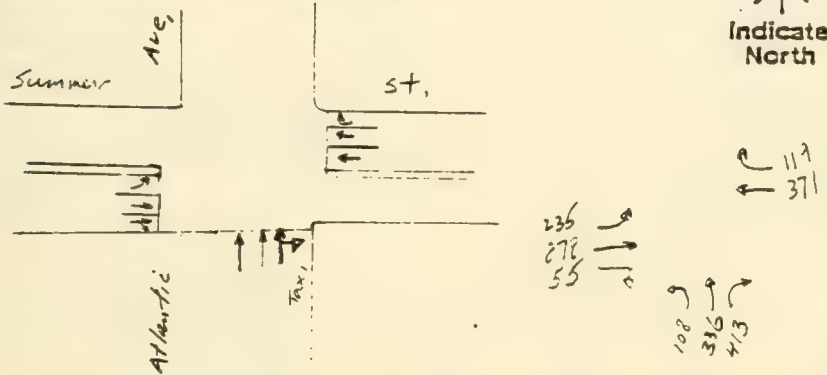
LEVEL OF SERVICE --- C ---



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INTERSECTION Atlantic Ave. / Summer St.  
 ALT. Gustine YEAR \_\_\_\_\_ PERIOD AM  
 CALCULATED BY BG DATE \_\_\_\_\_ SHEET OF  
 CHECKED BY RB DATE 8/13/84 JOB NO. 0423

## INTERSECTION GEOMETRY



## Left Turn Check

- Number of change intervals per hour
- Left turn capacity on change interval, in vph
- G/C Ratio
- Opposing volume in vph
- Left turn capacity on green, in vph
- Left turn capacity in vph (b - e)
- Left turn volume in vph
- Is volume > capacity (g > f)?

Approach				
1	2	3	4	

## PHASING ~~20~~ with Lead

(A)	(B)	(C)	(D)	(E)
↑	↘	→	→	
108 ↘ 222 ↘ 222 ↘ 413		235 ↘ 235 → 235 ↘	119 ↘ 186 → 186 ↘ 222	
CLV = 413	CLV =	CLV = 235	CLV = 232	CLV =

~~Use 30 criteria~~

Carryover =

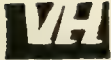
$\Sigma$  CLV 880  
 V/C 0.84  
 LOS D

30% Reduction for Bids

AOS  
12.57

CRITERIA (vph)		2 B	3 B	4 B
LOS	A	620	855	825
	B	1035	1000	965
	C	1240	1140	1100
	D	1345	1275	1225
	E	1500	1425	1375

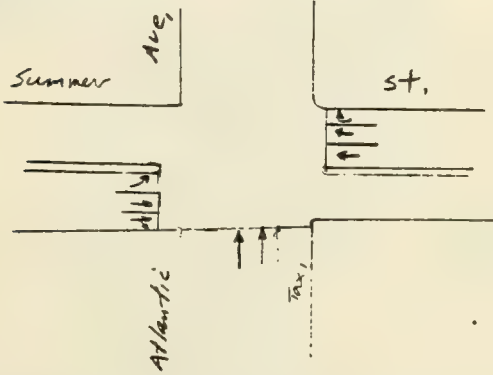




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INTERSECTION Atlantic Ave. / Summer St.  
 ALT. Existing YEAR 1984 PERIOD PM  
 CALCULATED BY BY DATE 8/13/84 SHEET OF  
 CHECKED BY CV DATE 8/13/84 JOB NO. 0923

## INTERSECTION GEOMETRY



## Left Turn Check

- Number of change intervals per hour
- Left turn capacity on change interval, in vph
- G/C Ratio
- Opposing volume in vph
- Left turn capacity on green, in vph
- Left turn capacity in vph (b = e)
- Left turn volume in vph
- Is volume > capacity (g > 0)?

Approach				
1	2	3	4	

## PHASING ~~30~~ with Lead

(A)	(B)	(C)	(D)	(E)
↑	↘	→	←	
2/3 2/4 287	↘	378 234 235	287 154 153	
CLV = 287	CLV =	CLV = 378	CLV = 188	CLV =

Use ~~30~~ criteria

Σ CLV 853

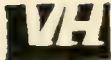
V/C 0.81

LOS D

30 % Reduction for Ped.

AOS  
1219

CRITERIA (vph)		AOS	2 B	3 B	4 B
LOS	A	630	900	1140	1225
	B	735	1050	1275	1375
	C	840	1200	1425	1500
	D	945	1350	1575	1650
	E	1050	1500	1725	1800

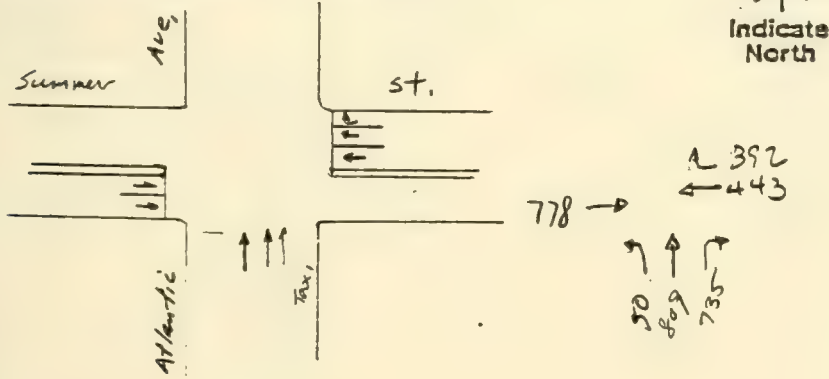


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INTERSECTION Atlantic Ave. / Summer St.

ALT. No Build YEAR 1970 PERIOD AM  
 CALCULATED BY RG DATE \_\_\_\_\_ SHEET OF  
 CHECKED BY RG DATE 8/10 JOB NO. 0423

## INTERSECTION GEOMETRY



## Left Turn Check

	Approach			
	1	2	3	4
a. Number of change intervals per hour				
b. Left turn capacity on change interval, in vph				
c. G/C Ratio				
d. Opposing volume in vph				
e. Left turn capacity on green, in vph				
f. Left turn capacity in vph (b * e)				
g. Left turn volume in vph				
h. Is volume > capacity (g > f)?				

## PHASING 2φ with lead

(A)	(B)	(C)	(D)	(E)
↑	→	→		
↑ ↑ ↑ 531 531 531	→ → → 2 vehicle per cycle = 60 vehicle per hour	→ → → 392 ← 221 ← 222 → 389 → 389		
CLV = 531	CLV =	CLV = 392	CLV =	CLV =

Analyzed as 2φ

Σ CLV 923

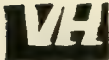
V/C 0.89

LOS D

30 % Reduction for Reds

ADJ  
1314

CRITERIA (vph)		405	2 B	3 B	4 B
LOS	A	630	900	855	825
	B	735	1050	1000	965
	C	840	1200	1140	1100
	D	945	1350	1275	1225
	E	1050	1500	1425	1375

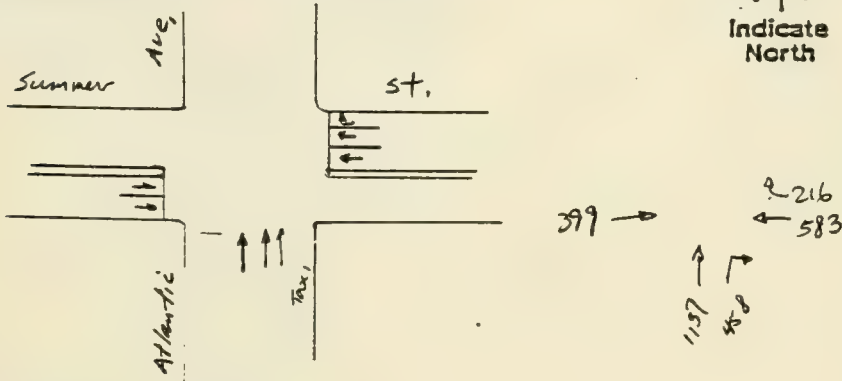


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INTERSECTION Atlantic Ave. / Summer St.

ALT. No Build YEAR 1970 PERIOD PM  
 CALCULATED BY SG DATE \_\_\_\_\_ SHEET OF  
 CHECKED BY RB DATE 8/10 JOB NO. 0923

## INTERSECTION GEOMETRY



## Left Turn Check

- Number of change intervals per hour
- Left turn capacity on change interval, in vph
- G/C Ratio
- Opposing volume in vph
- Left turn capacity on green, in vph
- Left turn capacity in vph ( $b = e$ )
- Left turn volume in vph
- Is volume > capacity ( $g > 0?$ )

Approach

1 2 3 4

## PHASING $2\phi$ with Lead

(A)	(B)	(C)	(D)	(E)
↑	→ →	→ →		
↑↑↑ 855	→ 72 →	→ 128 → 127		
CLV = 532	CLV = 72	CLV = 292	CLV =	CLV =

$\Sigma$  CLV 896

V/C 0.85

LOS D

30 % Reduction for Pedals

ADJ  
1288

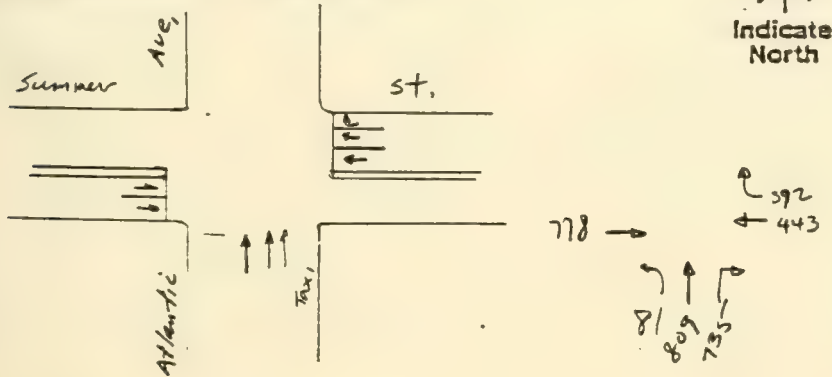
CRITERIA (vph)		1st	2nd	3rd	4th
LOS	A	630	900	865	825
	B	735	1050	1000	965
	C	840	1200	1140	1100
	D	945	1350	1275	1225
	E	1050	1500	1425	1375



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INTERSECTION Atlantic Ave. / Summer St.  
 ALT. Build YEAR 1970 PERIOD AM  
 CALCULATED BY B/G DATE 8/12 SHEET OF  
 CHECKED BY RR DATE 8/12 JOB NO. 0923

## INTERSECTION GEOMETRY



## Left Turn Check

- Number of change intervals per hour
- Left turn capacity on change interval, in vph
- G/C Ratio
- Opposing volume in vph
- Left turn capacity on green, in vph
- Left turn capacity in vph ( $b = e$ )
- Left turn volume in vph
- Is volume > capacity ( $g > 0?$ )

### Approach

1 2 3 4

## PHASING 2φ with Lead

(A)	(B)	(C)	(D)	(E)
↑	→	→		
↑ ↑ ↑ 542 542 544	→ →	↑ 392 → 221 ← 222 389 → 389 →		
CLV= 542	CLV=	CLV= 392	CLV=	CLV=

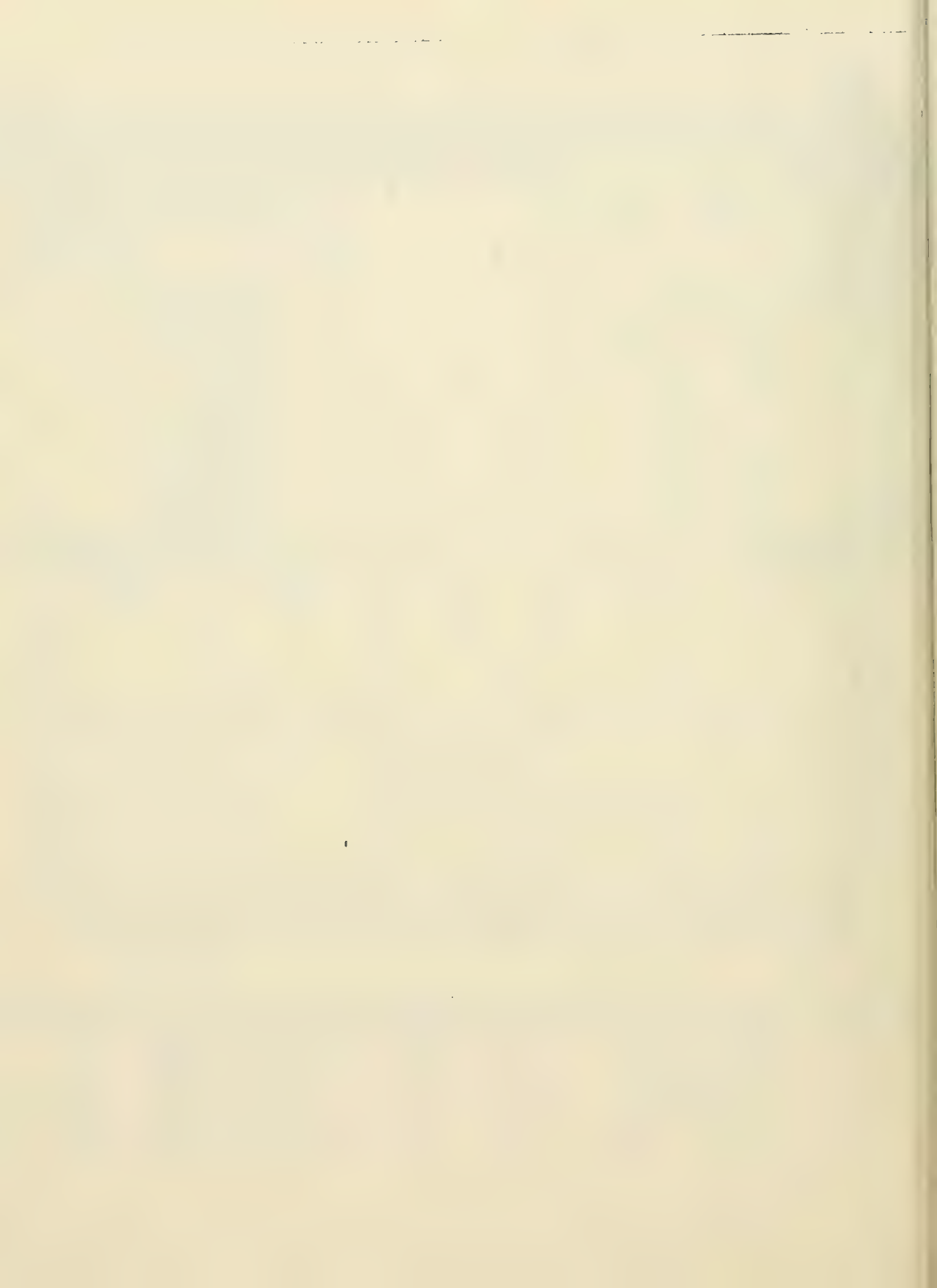
use 2φ due to short lead green time

Σ CLV 934  
 V/C 0.89  
 LOS D

30 % Reduction for Ped

ADT  
1334

CRITERIA (vph)	1st	2nd	3rd	4th
LOS A	636	900	858	825
B	735	1050	1000	965
C	840	1200	1140	1100
D	945	1350	1275	1225
E	1050	1500	1425	1375



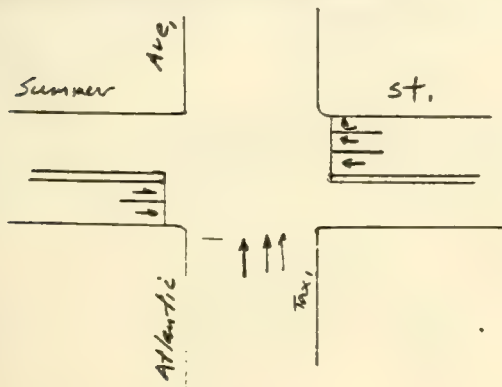




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INTERSECTION Atlantic Ave. / Summer St.  
 ALT. Build YEAR 1970 PERIOD PM  
 CALCULATED BY BY DATE 8/15 SHEET OF  
 CHECKED BY AB DATE 8/15 JOB NO. 0423

## INTERSECTION GEOMETRY



399 →

← 216  
← 583

121  
127

## Left Turn Check

- Number of change intervals per hour
- Left turn capacity on change interval, in vph
- G/C Ratio
- Opposing volume in vph
- Left turn capacity on green, in vph
- Left turn capacity in vph ( $b = e$ )
- Left turn volume in vph
- Is volume > capacity ( $g > 0$ )?

Approach

1 2 3 4

## PHASING $2\phi$ with Lead

(A)	(B)	(C)	(D)	(E)
↑	→ →	→ →		
↑ ↑ ↑ 555 555 555	72 → 72 →	216 211 212 121 127		
CLV = 555	CLV = 72	CLV = 292	CLV =	CLV =

$\Sigma$  CLV 919

VIC 0.87

LOS D

30 % Reduction for Ped

ADJ.  
1313

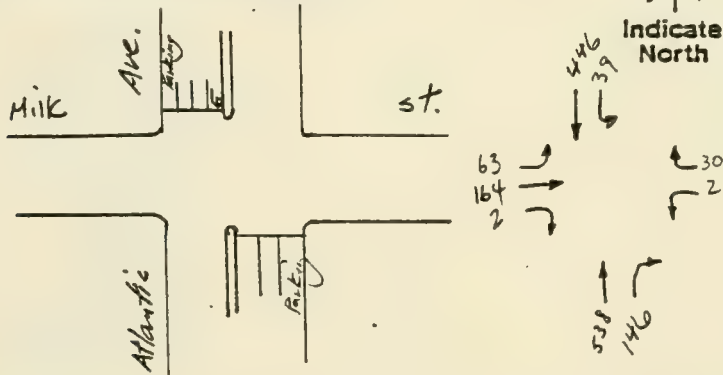
CRITERIA (vph)	1	2	3	4
LOS A	600	900	1100	1300
B	700	1050	1300	1500
C	800	1200	1400	1600
D	900	1350	1550	1700
E	1000	1500	1700	1800



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INTERSECTION Atlantic Ave. / Milk St.  
 ALT. Existing YEAR 1984 PERIOD AM  
 CALCULATED BY EC DATE \_\_\_\_\_ SHEET OF  
 CHECKED BY KB DATE \_\_\_\_\_ JOB NO. 0923

## INTERSECTION GEOMETRY



## Left Turn Check

	Approach		
	1	2	3
a. Number of change intervals per hour			
b. Left turn capacity on change interval, in vph			
c. G/C Ratio			
d. Opposing volume in vph			
e. Left turn capacity on green, in vph			
f. Left turn capacity in vph (b - e)			
g. Left turn volume in vph			
h. Is volume > capacity (g > f)?			

## PHASING 2φ

(A)	(B)	(C)	(D)	(E)
↓  ↑	↙  ↘			
223 ↓ 223 242 ↑ 242	63 ↙ 30 83 → 21 82 ↘ 2			
CLV = 342 + 39	CLV = 83 + 21	CLV =	CLV =	CLV =

Σ CLV 485

V/C 0.39

LOS A

17% Reduction for Ped

AOS  
584

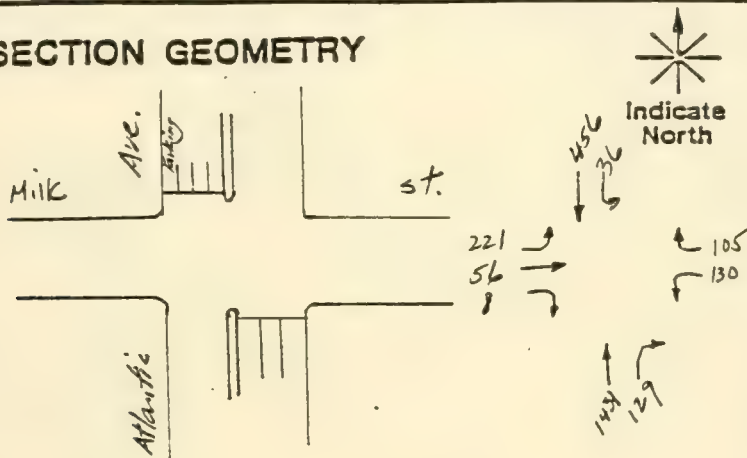
CRITERIA (vph)		LOS	2 φ	3 φ	4 φ
LOS	A	747	900	855	825
	B	572	1050	1000	965
	C	990	1200	1140	1100
	D	1129	1350	1275	1225
	E	1245	1500	1425	1375



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INTERSECTION Atlantic Ave. / Milk St.  
 ALT. Existing YEAR 1984 PERIOD PM  
 CALCULATED BY BG DATE \_\_\_\_\_ SHEET OF  
 CHECKED BY RB DATE \_\_\_\_\_ JOB NO. 0923

## INTERSECTION GEOMETRY



## Left Turn Check

	Approach			
	1	2	3	4
a. Number of change intervals per hour				
b. Left turn capacity on change interval, in vph				
c. G/C Ratio				
d. Opposing volume in vph				
e. Left turn capacity on green, in vph				
f. Left turn capacity in vph (b + e)				
g. Left turn volume in vph				
h. Is volume > capacity (g > f)?				

## PHASING 2φ

(A)	(B)	(C)	(D)	(E)
↓ ↑	↔ ↔			
↓ ↓ 36 221 221 ↑ ↑ 129 780 780	↗ 105 ↘ 130 → 32 ← 32 ↑			
CLV = 780 + 36	CLV = 221	CLV =	CLV =	CLV =

Σ CLV 1037

V/C 0.82

LOS C

14% Reduction for Peds

805  
1206

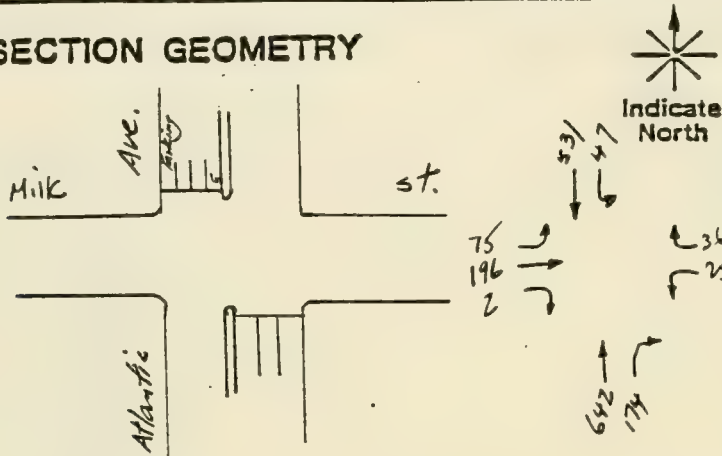
CRITERIA (vph)		1 S	2 S	3 S	4 S
LOS	A	774	900	855	825
	B	903	1050	1000	965
	C	946	1200	1140	1100
	D	1104	1350	1275	1225
	E	1240	1500	1425	1375



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INTERSECTION Atlantic Ave. / Milk St.  
 ALT. No-Build YEAR 1990 PERIOD AM  
 CALCULATED BY BR DATE 8/3/84 SHEET OF  
 CHECKED BY RR DATE 8/11 JOB NO. 0923

## INTERSECTION GEOMETRY



## Left Turn Check

	Approach		
	1	2	3
a. Number of change intervals per hour			
b. Left turn capacity on change interval, in vph			
c. G/C Ratio			
d. Opposing volume in vph			
e. Left turn capacity on green, in vph			
f. Left turn capacity in vph (b * e)			
g. Left turn volume in vph			
h. Is volume > capacity (g > f)?			

## PHASING 2φ

(A)	(B)	(C)	(D)	(E)
↓ ↑	↔ ↔			
↓ ↓ L 47 265 266 ↑ ↑ 174 408 408	↔ 36 ↔ 25 ↔ 99 ↔ 99 ↔ 2			
CLV = 408 + 47	CLV = 99 + 25	CLV =	CLV =	CLV =

Σ CLV 579 ADJ  
.698  
 V/C 0.47  
 LOS A  
 17% Reduction for Rds.

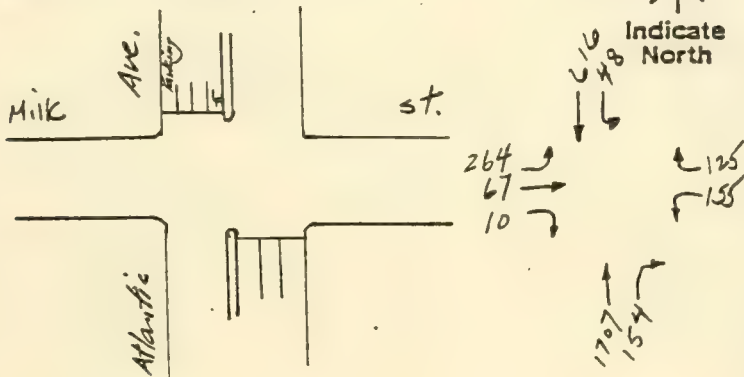
CRITERIA (vph)	ADJ	2 φ	3 φ	4 φ
LOS A	747	900	855	825
B	872	1050	1000	965
C	996	1200	1140	1100
D	1121	1350	1275	1225
E	1245	1500	1425	1375



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INTERSECTION Atlantic Ave. / Milk St.  
 ALT. No Build YEAR 1990 PERIOD PM  
 CALCULATED BY B.G. DATE 8/13 SHEET OF  
 CHECKED BY Z.R. DATE 8/13 JOB NO. 0923

## INTERSECTION GEOMETRY



## Left Turn Check

	Approach		
	1	2	3
a. Number of change intervals per hour			
b. Left turn capacity on change interval, in vph			
c. G/C Ratio			
d. Opposing volume in vph			
e. Left turn capacity on green, in vph			
f. Left turn capacity in vph (b + e)			
g. Left turn volume in vph			
h. Is volume > capacity (g > f)?			

## PHASING 2φ

(A)	(B)	(C)	(D)	(E)
↓ ↑	↔ ↔			
↓ 308 ↓ 308 ↓ 48 ↑ 731 ↑ 730 ↑ 154	264 39 38 10 125 155			
CLV = 931 + 48	CLV = 264	CLV =	CLV =	CLV =

Σ CLV 1243

V/C 0.76

LOS E

14% Reduction for Peds

ADP  
1445

CRITERIA (vph)	ADP	2 φ	3 φ	4 φ
LOS A	774	900	858	825
B	723	1050	1000	965
C	690	1200	1140	1100
D	661	1350	1275	1225
E	640	1500	1425	1375

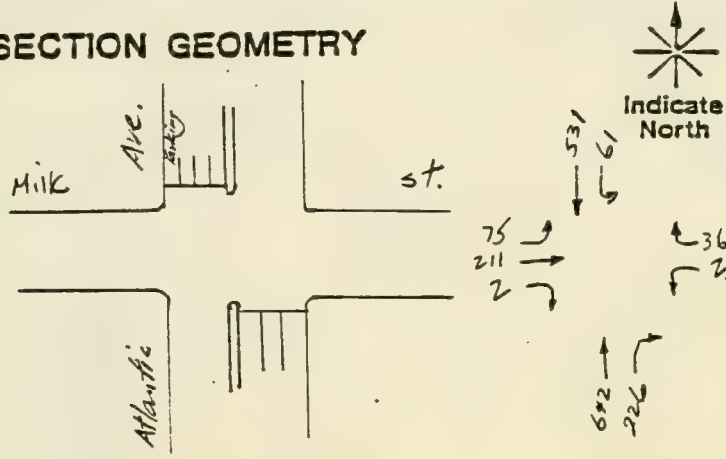




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INTERSECTION Atlantic Ave. / Milk St.  
 ALT. Build YEAR 1990 PERIOD AM  
 CALCULATED BY GG DATE \_\_\_\_\_ SHEET OF  
 CHECKED BY KB DATE 8/13 JOB NO. 0923

# INTERSECTION GEOMETRY



## Left Turn Check

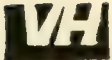
	Approach		
	1	2	3
a. Number of change intervals per hour			
b. Left turn capacity on change interval, in vph			
c. G/C Ratio			
d. Opposing volume in vph			
e. Left turn capacity on green, in vph			
f. Left turn capacity in vph (b + e)			
g. Left turn volume in vph			
h. Is volume > capacity (g > f)?			

## PHASING 2φ

(A)	(B)	(C)	(D)	(E)
↓ ↑	↔ ↔			
↓ ↓ ↓ 61 266 265 ↑ ↑ 226 434 434	75 ↔ 107 106 2 ↔ 36 ↔ 25			
CLV = 434 + 61	CLV = 107 + 25	CLV =	CLV =	CLV =

Σ CLV 627  
 V/C 0.50  
 LOS A  
 17% Reduction for Reds

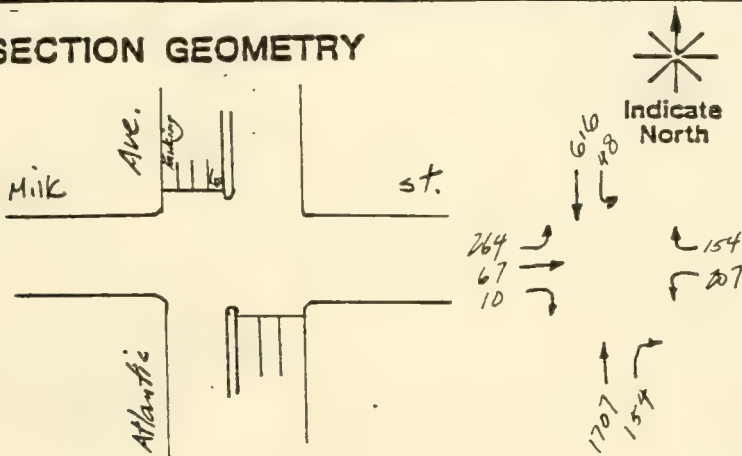
CRITERIA (vph)		1 φ	2 φ	3 φ	4 φ
LOS	A	747	900	1140	1375
	B	872	1050	1300	1565
	C	1121	1200	1440	1700
	D	1350	1350	1575	1825
	E	1500	1500	1725	1975



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INTERSECTION Atlantic Ave. / Milk St.  
 ALT. Build YEAR 1970 PERIOD PM  
 CALCULATED BY 39 DATE \_\_\_\_\_ SHEET \_\_\_\_\_ OF \_\_\_\_\_  
 CHECKED BY RR DATE 8/12 JOB NO. 0923

## INTERSECTION GEOMETRY



## Left Turn Check

	Approach		
	1	2	3
a. Number of change intervals per hour			
b. Left turn capacity on change interval, in vph			
c. G/C Ratio			
d. Opposing volume in vph			
e. Left turn capacity on green, in vph			
f. Left turn capacity in vph (b + e)			
g. Left turn volume in vph			
h. Is volume > capacity (g > f)?			

## PHASING 2φ

(A)	(B)	(C)	(D)	(E)
↓  ↑	↔  ↔			
308 306 ↓ ↓ 48  ↑ 154 221 200	264 154 ↔ ↗ 38 207 ↓ 10			
CLV = 931 + 48	CLV = 264	CLV =	CLV =	CLV =

Σ CLV 1243

V/C 0.96

LOS E

14% Reduction in Rds

AD5  
1445

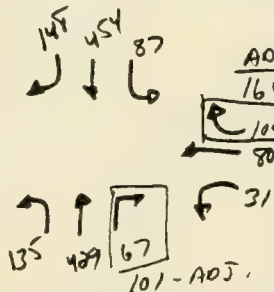
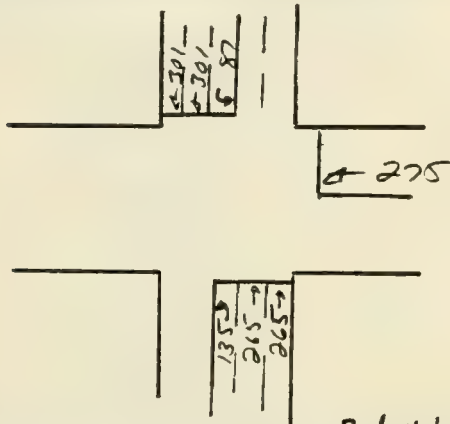
CRITERIA (vph)	1st	2nd	3rd	4th
LOS A	774	900	855	823
B	903	1050	1000	965
C	970	1200	1140	1100
D	1161	1350	1275	1225
E	1290	1500	1425	1375



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INTERSECTION Atlantic Av / State St.  
 ALT. 1984 YEAR 1984 PERIOD AM  
 CALCULATED BY RP DATE 10/23 SHEET OF  
 CHECKED BY DATE JOB NO. 0923

## INTERSECTION GEOMETRY



## Left Turn Check

- Number of change intervals per hour
- Left turn capacity on change interval, in vph
- G/C Ratio
- Opposing volume in vph
- Left turn capacity on green, in vph
- Left turn capacity in vph (b + e)
- Left turn volume in vph
- Is volume > capacity (g > f)?

Approach

1 2 3

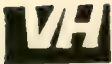
Ped Volumes - Heavy - 1.5 Adj Factor

PHASING 3  $\phi$  0-----0 Ped  $\phi$

(A)	(B)	(C)	(D)	(E)
265 + 87	275	135		
CLV=	CLV=	CLV=	CLV=	CLV=

$\Sigma$  CLV 762  
 V/C .53  
 LOS A

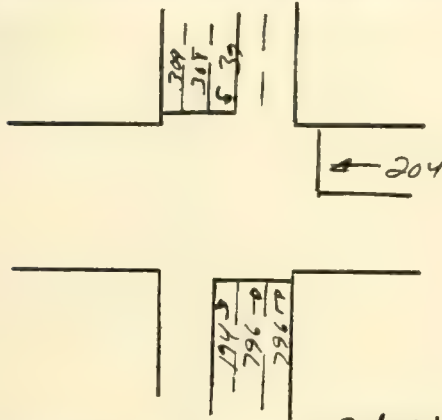
CRITERIA (vph)	2 $\phi$	3 $\phi$	4 $\phi$
LOS A	900	855	825
B	1050	1000	965
C	1200	1140	1100
D	1350	1275	1225
E	1500	1425	1375



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INTERSECTION Atlantic Av / State St.  
 ALT. EXISTING YEAR 1984 PERIOD PM  
 CALCULATED BY RS DATE 10/23/84 SHEET OF  
 CHECKED BY DATE JOB NO. 0923

## INTERSECTION GEOMETRY



## Left Turn Check

	Approach		
	1	2	3
a. Number of change intervals per hour			
b. Left turn capacity on change interval, in vph			
c. G/C Ratio			
d. Opposing volume in vph			
e. Left turn capacity on green, in vph			
f. Left turn capacity in vph (b + e)			
g. Left turn volume in vph			
h. Is volume > capacity (g > f)?			

Ped Volumes - Heavy - 1.5 Adj Factor

PHASING 3  $\phi$  0 - - - - 0 Ped  $\phi$

(A)	(B)	(C)	(D)	(E)
796 + 39	204	194		
CLV=	CLV=	CLV=	CLV=	CLV=

$\Sigma$  CLV 1233  
 V/C .87  
 LOS D

CRITERIA (vph)		2 $\phi$	3 $\phi$	4 $\phi$
LOS	A	900	855	825
	B	1050	1000	965
	C	1200	1140	1100
	D	1350	1275	1225
	E	1500	1425	1375

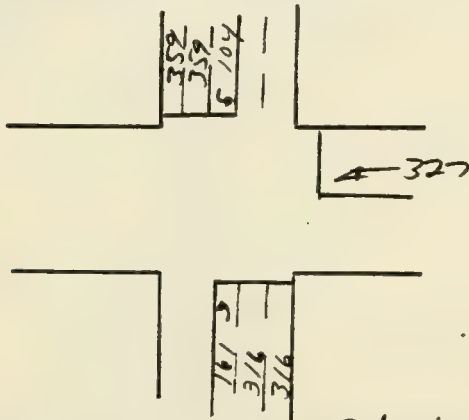




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INTERSECTION Atlantic Av / State St.  
 ALT. A-10 Build YEAR 1990 PERIOD Am  
 CALCULATED BY \_\_\_\_\_ DATE \_\_\_\_\_ SHEET OF  
 CHECKED BY \_\_\_\_\_ DATE \_\_\_\_\_ JOB NO. 0923

## INTERSECTION GEOMETRY



## Left Turn Check

- Number of change intervals per hour
- Left turn capacity on change interval, in vph
- G/C Ratio
- Opposing volume in vph
- Left turn capacity on green, in vph
- Left turn capacity in vph ( $b + e$ )
- Left turn volume in vph
- Is volume > capacity (g > 0)?

Approach

1 2 3

Ped Volumes - Heavy - 1.5 Adj Factor

PHASING 3  $\phi$  0 - - - - 0 Ped  $\phi$

(A)	(B)	(C)	(D)	(E)
316 + 104 <hr/> 420	327	161		
CLV = 420	CLV = 327	CLV = 161	CLV =	CLV =

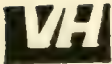
$\Sigma$  CLV 908

V/C .64

LOS B

CRITERIA (vph)		2 $\phi$	3 $\phi$	4 $\phi$
LOS	A	900	858	825
	B	1050	1000	968
	C	1200	1140	1100
	D	1350	1275	1225
	E	1500	1425	1375

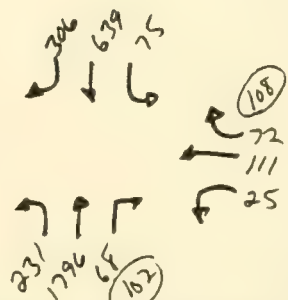
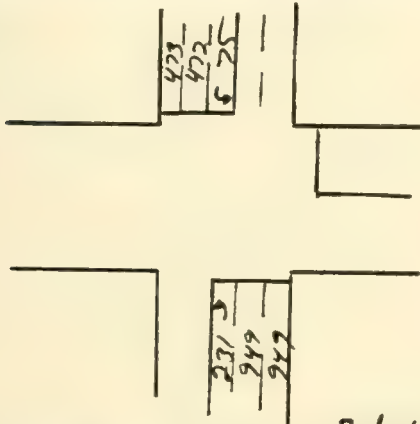




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INTERSECTION Atlantic Av / State St.  
 ALT. NO BUILD YEAR 1990 PERIOD PM  
 CALCULATED BY RR DATE 10/27/84 SHEET OF  
 CHECKED BY DATE JOB NO. 0923

## INTERSECTION GEOMETRY



Ped Volumes - Heavy - 1.5 Adj Factor

## Left Turn Check

	Approach		
	1	2	3
a. Number of change intervals per hour			
b. Left turn capacity on change interval, in vph			
c. G/C Ratio			
d. Opposing volume in vph			
e. Left turn capacity on green, in vph			
f. Left turn capacity in vph (b * e)			
g. Left turn volume in vph			
h. Is volume > capacity (g > f)?			

## PHASING 3 Ø 0-----0 Ped Ø

(A)	(B)	(C)	(D)	(E)
75 + 949	244	231		
CLV=	CLV=	CLV=	CLV=	CLV=

Σ CLV 1499  
 V/C 1.05  
 LOS E

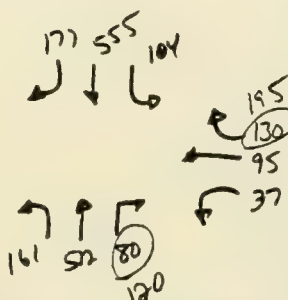
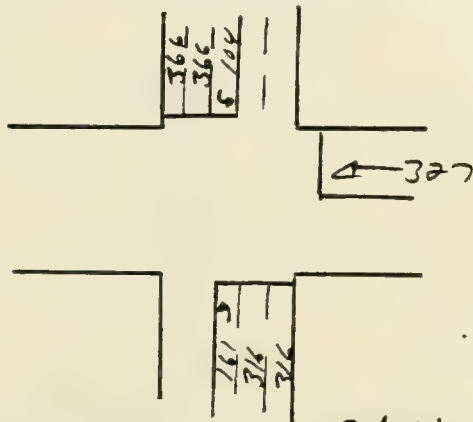
CRITERIA (vph)		2 Ø	3 Ø	4 Ø
LOS	A	900	855	825
	B	1050	1000	965
	C	1200	1140	1100
	D	1350	1275	1225
	E	1500	1425	1375



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INTERSECTION Atlantic Av / State St  
 ALT. Bu11A YEAR 1990 PERIOD AM  
 CALCULATED BY RB DATE 9/23/89 SHEET OF  
 CHECKED BY DATE JOB NO. 0927

## INTERSECTION GEOMETRY



Ped Volumes - Heavy - 1.5 Adj Factor

## Left Turn Check

	Approach		
	1	2	3
a. Number of change intervals per hour			
b. Left turn capacity on change interval, in vph			
c. G/C Ratio			
d. Opposing volume in vph			
e. Left turn capacity on green, in vph			
f. Left turn capacity in vph (b + e)			
g. Left turn volume in vph			
h. Is volume > capacity (g > f)?			

## PHASING

3  $\phi$

0-----0 Ped  $\phi$

(A)	(B)	(C)	(D)	(E)
316 + 104	327	161		
CLV=	CLV=	CLV=	CLV=	CLV=

$\Sigma$  CLV 905

V/C .64

LOS B

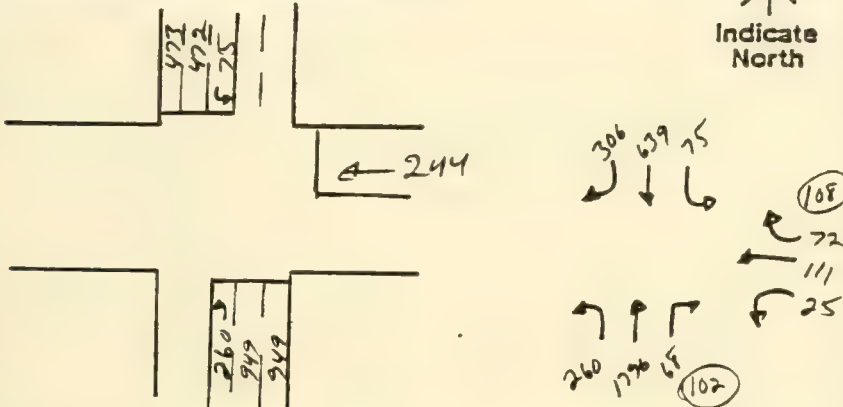
CRITERIA (vph)		2 $\phi$	3 $\phi$	4 $\phi$
LOS	A	900	855	825
	B	1050	1000	965
	C	1200	1140	1100
	D	1350	1275	1225
	E	1500	1425	1375



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INTERSECTION Atlantic Av / State St.  
 ALT. Build YEAR 1990 PERIOD PM  
 CALCULATED BY RB DATE 10/23/94 SHEET OF  
 CHECKED BY \_\_\_\_\_ DATE \_\_\_\_\_ JOB NO. 0923

## INTERSECTION GEOMETRY



## Left Turn Check

	Approach		
	1	2	3
a. Number of change intervals per hour			
b. Left turn capacity on change interval, in vph			
c. G/C Ratio			
d. Opposing volume in vph			
e. Left turn capacity on green, in vph			
f. Left turn capacity in vph (b * e)			
g. Left turn volume in vph			
h. Is volume > capacity (g > f)?			

Ped Volumes - Heavy - 1.5 Adj Factor

PHASING 3  $\phi$  0-----0 Ped  $\phi$

(A)	(B)	(C)	(D)	(E)
949 + 75	244	260		
CLV=	CLV=	CLV=	CLV=	CLV=

$\Sigma$  CLV 1525

V/C 1.07

LOS E

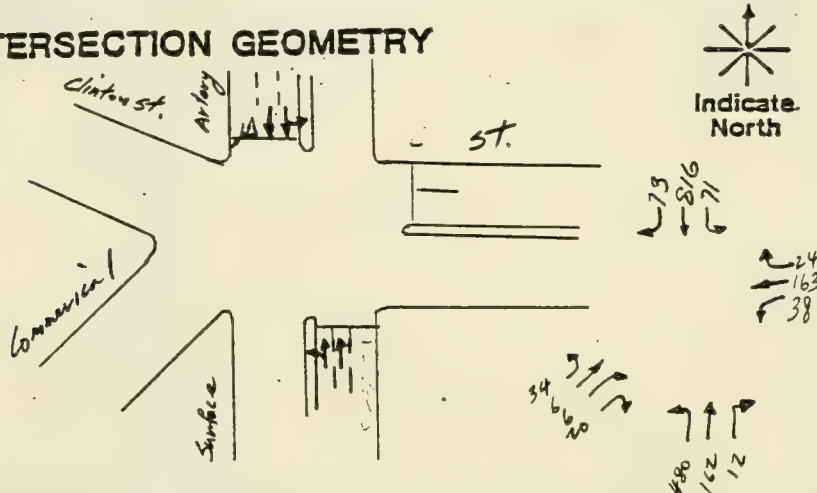
CRITERIA (vph)		2 $\phi$	3 $\phi$	4 $\phi$
LOS	A	900	855	825
	B	1050	1000	965
	C	1200	1140	1100
	D	1350	1275	1225
	E	1500	1425	1375



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INTERSECTION Surface Artery / Clinton St. / Commercial St.  
 ALT. Existing YEAR 1984 PERIOD AM  
 CALCULATED BY BL DATE \_\_\_\_\_ SHEET \_\_\_\_\_ OF \_\_\_\_\_  
 CHECKED BY RB DATE 8/16/84 JOB NO. 8923

## INTERSECTION GEOMETRY



## Left Turn Check

	Approach		
	1	2	3
a. Number of change intervals per hour			
b. Left turn capacity on change interval, in vph			
c. G/C Ratio			
d. Opposing volume in vph			
e. Left turn capacity on green, in vph			
f. Left turn capacity in vph (b + e)			
g. Left turn volume in vph			
h. Is volume > capacity (g > f)?			

## PHASING 2 $\phi$ w/ADV

(A)	(B)	(C)	(D)	(E)
↑↑	↓	←		
downward 6 cars per cycle 240 ↑ 174	443 ↓ 71 240 ↑	24 89 113 112 31 40 26	6 + 10 or 6 31	
CLV = 240	CLV = 443 + 240	CLV = 113 + 71	CLV =	CLV =

$\Sigma$  CLV 1042

V/C 0.87

LOS D

20% Reduction for Peds

ADV  
1303

CRITERIA (vph)	ACT	2 $\phi$	3 $\phi$	4 $\phi$
LOS A	730	900	885	825
B	740	1050	1025	965
C	900	1200	1140	1100
D	1050	1350	1275	1225
E	1200	1500	1463	1375



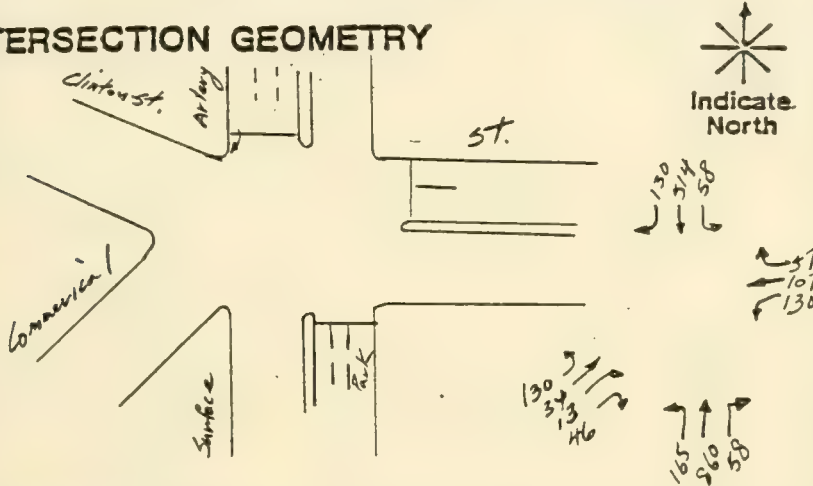




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INTERSECTION Surface Artery / Clinton St. / Commercial St.  
 ALT. Existing YEAR 1984 PERIOD PM  
 CALCULATED BY BG DATE 7/11/84 SHEET OF  
 CHECKED BY RB DATE 7/11/84 JOB NO. 1923

## INTERSECTION GEOMETRY



## Left Turn Check

- Approach
- |  | 1 | 2 | 3 |
|--|---|---|---|
| a. Number of change intervals per hour           |   |   |   |
| b. Left turn capacity on change interval, in vph |   |   |   |
| c. G/C Ratio                                     |   |   |   |
| d. Opposing volume in vph                        |   |   |   |
| e. Left turn capacity on green, in vph           |   |   |   |
| f. Left turn capacity in vph (b * e)             |   |   |   |
| g. Left turn volume in vph                       |   |   |   |
| h. Is volume > capacity (g > f)?                 |   |   |   |

## PHASING

(A)	(B)	(C)	(D)	(E)
↑↑	↑↑	↗↘		
165 165 330 330	1659 315 199 0 201 212	90 130 34 164 59		
CLV= 330	CLV= 315	CLV= 147+34	CLV=	CLV=

Assume only 1/2 LTB in } carry over = 423  
 Adv since mixed traffic

Σ CLV 826

V/C 0.67

LOS B

18% Reduction for Ped

AOS  
1007

CRITERIA (vph)	A	2 B	3 B	4 B
LOS A	735	900	855	825
B	861	1050	1025	965
C	984	1200	1140	1100
D	1107	1350	1275	1225
E	1230	1500	1425	1375

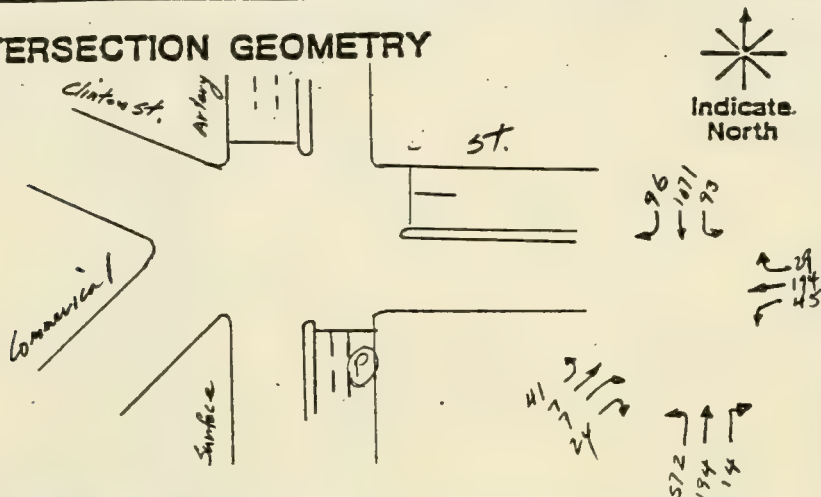




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INTERSECTION Surface Artery / Clinton St. / Commercial St.  
 ALT. No-Build YEAR 1990 PERIOD AM  
 CALCULATED BY BY DATE 8/10/90 SHEET OF  
 CHECKED BY RB DATE 8/10/90 JOB NO. 8923

## INTERSECTION GEOMETRY



## Left Turn Check

	Approach		
	1	2	3
a. Number of change intervals per hour			
b. Left turn capacity on change interval, in vph			
c. G/C Ratio			
d. Opposing volume in vph			
e. Left turn capacity on green, in vph			
f. Left turn capacity in vph (b + e)			
g. Left turn volume in vph			
h. Is volume > capacity (g > f)?			

## PHASING 2d

(A)	(B)	(C)	(D)	(E)
↑↑	↓ ↑↑	←		
Assumed 6 cars per cycle ↑↑ 240 240	582 582 ↓ 6093 332 ↑↑↑ 0	29 134 134 45 48 207 31		
CLV= 240	CLV= 582+332	CLV= 134+7	CLV=	CLV=

Carry = 4 ↑  
 over 332 0

Σ CLV 1295 <sup>405</sup>  
1618  
 VIC 1.08  
 LOS E

20% Reduction for Peds

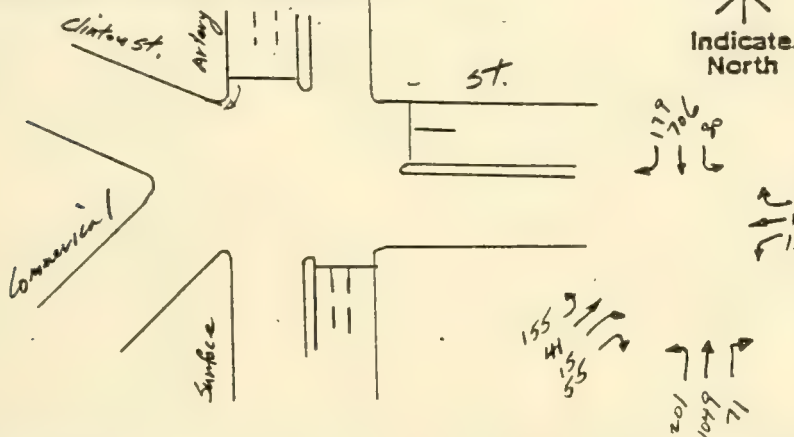
CRITERIA (vph)		1st	2nd	3rd	4th
LOS	A	720	900	868	825
	B	840	1050	1000	968
	C	900	1200	1140	1100
	D	1050	1350	1275	1225
	E	1200	1500	1425	1375



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INTERSECTION Surface Artery / Clinton St. / Commercial St.  
 ALT. No Build YEAR 1990 PERIOD PM  
 CALCULATED BY BG DATE \_\_\_\_\_ SHEET OF  
 CHECKED BY FR DATE \_\_\_\_\_ JOB NO. 8923

## INTERSECTION GEOMETRY



## Left Turn Check

- Number of change intervals per hour
- Left turn capacity on change interval, in vph
- G/C Ratio
- Opposing volume in vph
- Left turn capacity on green, in vph
- Left turn capacity in vph ( $b + e$ )
- Left turn volume in vph
- Is volume > capacity ( $g > 0$ )?

Approach

1 2 3

## PHASING

(A)	(B)	(C)	(D)	(E)
↑↑	↓	—		
150 ↑↑ 300 304	393 393 ↓ 480 51 ↑↑ 299 351	68 175 176 155 155 70 15 35		
CLV = 300	CLV = 393 + 51	CLV = 176 + 41	CLV =	CLV =

USE ADV of 300

Assume 1/2 LT

CARLANTER

↑  
51 599

opp vol = 706 × .75 = 530 LT FAC = 2.0

⇒

Σ CLV 961

V/C 0.78

LOS C

18% Reduction for Red

ADJ  
1172

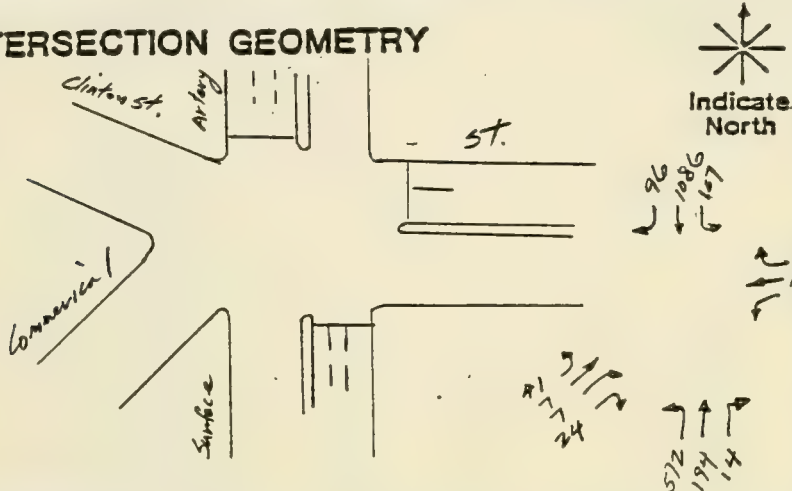
CRITERIA (vph)	ADJ	2 B	3 B	4 B
LOS A	738	900	888	825
B	861	1050	1000	968
C	954	1200	1140	1100
D	1107	1350	1275	1225
E	1230	1500	1425	1375



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INTERSECTION Surface Arterial / Clinton St. / Commercial St.  
 ALT. Build YEAR 1990 PERIOD AM  
 CALCULATED BY SG DATE 8/11 SHEET OF  
 CHECKED BY AK DATE 8/11 JOB NO. 8923

## INTERSECTION GEOMETRY



## Left Turn Check

	Approach		
	1	2	3
a. Number of change intervals per hour			
b. Left turn capacity on change interval, in vph			
c. G/C Ratio			
d. Opposing volume in vph			
e. Left turn capacity on green, in vph			
f. Left turn capacity in vph (b + e)			
g. Left turn volume in vph			
h. Is volume > capacity (g > f)?			

## PHASING

(A)	(B)	(C)	(D)	(E)
↑	↓	←		
240 9 ↑ 208	597 596 ↓ 107 332 0 ↑ 14	41 7 48 31 27 29 134 154 45		
CLV = 240	CLV = 597 + 332	CLV = 134 + 7	CLV =	CLV =

$\Sigma$  CLV 1310

V/C 1.09

LOS E

20% reduction for beds

ADJ  
1638

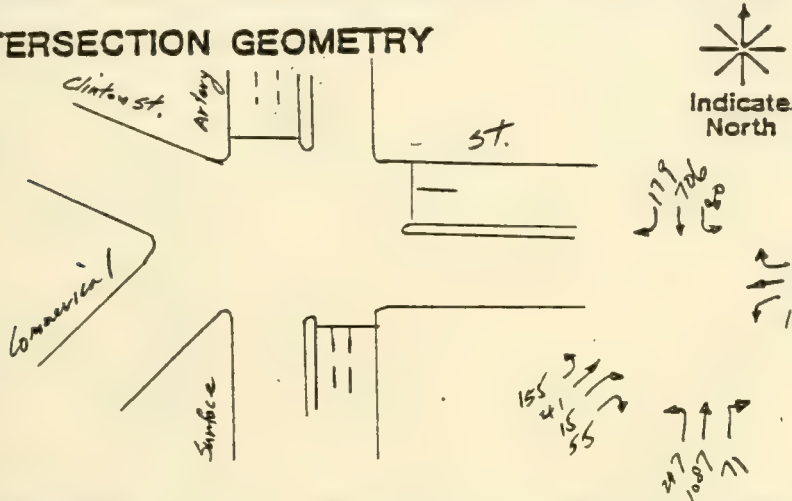
CRITERIA (vph)		ADJ	2 B	3 B	4 B
LOS	A	700	900	1155	1425
	B	840	1050	1000	965
	C	960	1200	1140	1100
	D	1050	1350	1275	1235
	E	1200	1500	1425	1375



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INTERSECTION Surface Avenue / Clinton St. / Commercial St.  
 ALT. Build YEAR 1990 PERIOD PM  
 CALCULATED BY BGT DATE \_\_\_\_\_ SHEET OF  
 CHECKED BY KLB DATE \_\_\_\_\_ JOB NO. 8923

## INTERSECTION GEOMETRY



## Left Turn Check

	Approach			
	1	2	3	4
a. Number of change intervals per hour				
b. Left turn capacity on change interval, in vph				
c. G/C Ratio				
d. Opposing volume in vph				
e. Left turn capacity on green, in vph				
f. Left turn capacity in vph (b + e)				
g. Left turn volume in vph				
h. Is volume > capacity (g > f)?				

## PHASING

(A)	(B)	(C)	(D)	(E)
↑	↓	←		
150 150 ↑ 300 300	393 393 ↓ 80 97 416	68 175 176 155 70		
CLV = 300	CLV = 416 + 80	CLV = 176 + 41	CLV =	CLV =

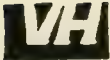
LT ADV = 1/2 TH ; CARRY OVER = 637 ↑  
 97 ↑  
 OPP VIL = 393 × 1.5 = 590 < 600  
 USE 2.6 LT FACTOR

Σ CLV 1013  
 V/C 0.83  
 LOS D

18' Reduction for Peds

CRITERIA (vph)	ACT	2 B	3 B	4 B
LOS A	738	900	888	825
B	841	1050	1000	968
C	984	1200	1140	1100
D	1107	1350	1275	1225
E	1230	1500	1425	1375

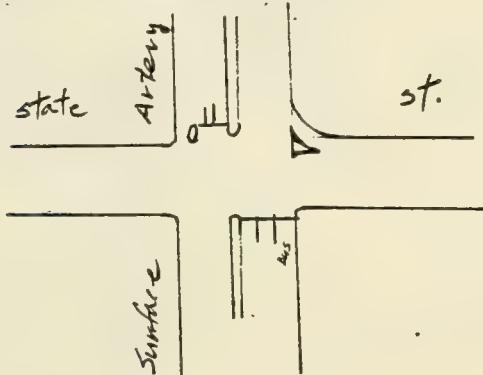




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INTERSECTION Surface Artery / state St.  
 ALT. Existing YEAR 1984 PERIOD AM  
 CALCULATED BY BG DATE \_\_\_\_\_ SHEET \_\_\_\_\_ OF \_\_\_\_\_  
 CHECKED BY AB DATE \_\_\_\_\_ JOB NO. 0923

## INTERSECTION GEOMETRY



Indicate North

## Left Turn Check

	Approach		
	1	2	3
a. Number of change intervals per hour			
b. Left turn capacity on change interval, in vph			
c. G/C Ratio			
d. Opposing volume in vph			
e. Left turn capacity on green, in vph			
f. Left turn capacity in vph (b + e)			
g. Left turn volume in vph			
h. Is volume > capacity (g > f)?			

## PHASING

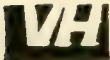
2φ

(A)	(B)	(C)	(D)	(E)
↓ ↑	—			
299 ↓ 287 ↓ 370 ↑ 370 572	82 ← 141 → 140 97			
CLV = 288 + 370	CLV = 141	CLV =	CLV =	CLV =

Σ CLV 799  
 V/C 0.53  
 LOS A

CRITERIA (vph)		2 φ	3 φ	4 φ
LOS	A	900	858	825
	B	1050	1000	965
	C	1200	1140	1100
	D	1350	1275	1225
	E	1500	1425	1375

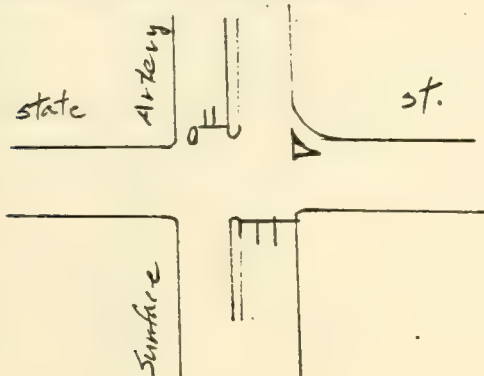




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INTERSECTION Surface Artery / state st.  
 ALT. Existing YEAR 1984 PERIOD PM  
 CALCULATED BY BG DATE \_\_\_\_\_ SHEET OF  
 CHECKED BY RB DATE \_\_\_\_\_ JOB NO. 0923

## INTERSECTION GEOMETRY



## Left Turn Check

	Approach		
	1	2	3
a. Number of change intervals per hour			
b. Left turn capacity on change interval, in vph			
c. G/C Ratio			
d. Opposing volume in vph			
e. Left turn capacity on green, in vph			
f. Left turn capacity in vph (b - e)			
g. Left turn volume in vph			
h. Is volume > capacity (g > f)?			

## PHASING 20

(A)	(B)	(C)	(D)	(E)
↓	→			
115 ↓ ↓ 287 288 203 → ↑ 479 652	125 → 154 154 115			
CLV = 682	CLV = 154	CLV =	CLV =	CLV =

Σ CLV 836  
 V/C 0.55  
 LOS A

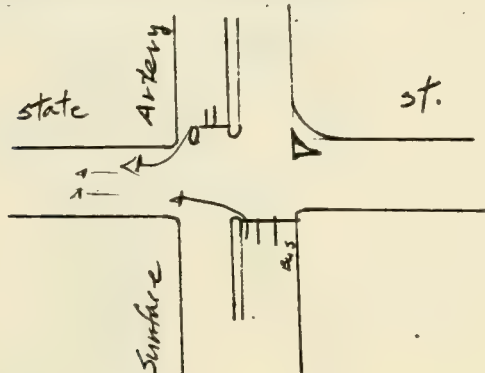
CRITERIA (vph)		2 B	3 B	4 B
LOS	A	900	865	825
	B	1050	1000	965
	C	1200	1140	1100
	D	1350	1275	1225
	E	1500	1425	1375



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INTERSECTION Surface Artery / State St.  
 ALT. No-Build YEAR 1990 PERIOD AM  
 CALCULATED BY BC DATE \_\_\_\_\_ SHEET OF  
 CHECKED BY RB DATE 7/13 JOB NO. 0923

## INTERSECTION GEOMETRY



Handwritten traffic volume data:  
 424 (left turn), 358 (through/right turn)  
 441 (left turn), 682 (through/right turn)  
 98 (left turn), 215 (through/right turn)  
 214 (left turn), 210 (through/right turn)

## Left Turn Check

- Number of change intervals per hour
- Left turn capacity on change interval, in vph
- G/C Ratio
- Opposing volume in vph
- Left turn capacity on green, in vph
- Left turn capacity in vph ( $b + e$ )
- Left turn volume in vph
- Is volume > capacity ( $g > 1$ )?

Approach			
1	2	3	

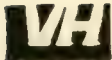
## PHASING

20

(A)	(B)	(C)	(D)	(E)
424 358 	98 215 214 210 			
CLV = 441 + 358	CLV = 215	CLV =	CLV =	CLV =

$\Sigma$  CLV 1014  
 V/C 0.68  
 LOS B

CRITERIA (vph)		2 B	3 B	4 B
LOS	A	900	855	825
	B	1050	1000	965
	C	1200	1140	1100
	D	1350	1275	1225
	E	1500	1425	1375

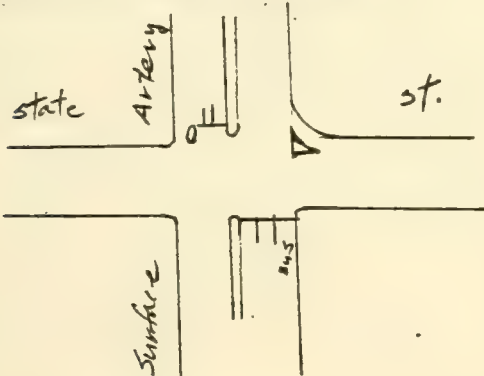


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INTERSECTION Surface Artery / State St.

ALT. No Build YEAR 1990 PERIOD PM  
 CALCULATED BY RG DATE 8/13 SHEET OF  
 CHECKED BY RG DATE 8/13 JOB NO. 0923

## INTERSECTION GEOMETRY



Indicate North

## Left Turn Check

	Approach			
	1	2	3	4
a. Number of change intervals per hour				
b. Left turn capacity on change interval, in vph				
c. G/C Ratio				
d. Opposing volume in vph				
e. Left turn capacity on green, in vph				
f. Left turn capacity in vph (b + e)				
g. Left turn volume in vph				
h. Is volume > capacity (g > f)?				

## PHASING 2φ

(A)	(B)	(C)	(D)	(E)
↓ ↑	←			
153 ↓ 382 381 242 329 571 813	179 ← 235 234 213			
CLV= 813	CLV= 235	CLV=	CLV=	CLV=

OPP VOL =  $382 \times 1.5 = 573$  LT FAC = 2.0

Σ CLV 1048

V/C 0.70

LOS C

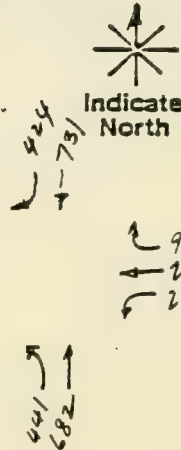
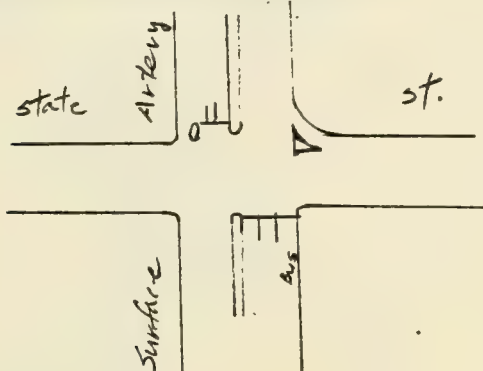
CRITERIA (vph)		2 φ	3 φ	4 φ
LOS	A	900	885	825
	B	1050	1000	985
	C	1200	1140	1100
	D	1380	1275	1225
	E	1500	1425	1375



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INTERSECTION Surface Avenue / State St.  
 ALT. Build YEAR 1990 PERIOD AM  
 CALCULATED BY OG DATE \_\_\_\_\_ SHEET \_\_\_\_\_ OF \_\_\_\_\_  
 CHECKED BY RB DATE 8/13 JOB NO. 0923

## INTERSECTION GEOMETRY



## Left Turn Check

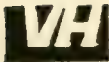
	Approach		
	1	2	3
a. Number of change intervals per hour			
b. Left turn capacity on change interval, in vph			
c. G/C Ratio			
d. Opposing volume in vph			
e. Left turn capacity on green, in vph			
f. Left turn capacity in vph (b + e)			
g. Left turn volume in vph			
h. Is volume > capacity (g > f)?			

## PHASING 2Ø

(A)	(B)	(C)	(D)	(E)
↓  ↑	←			
424 ↓ ↓ 366 365 441 → ↑ 682	98 ← 215 214 210			
CLV = 365 + 441	CLV = 215	CLV =	CLV =	CLV =

Σ CLV 1021  
 V/C 0.68  
 LOS B

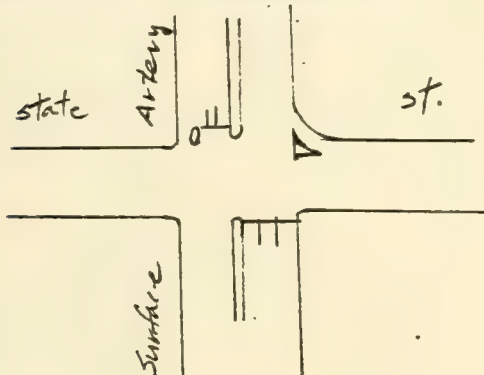
CRITERIA (vph)		2 Ø	3 Ø	4 Ø
LOS	A	900	855	825
	B	1050	1000	965
	C	1200	1140	1100
	D	1350	1275	1225
	E	1500	1425	1375



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INTERSECTION Surface Artery / State St.  
 ALT. Build YEAR 1990 PERIOD PM  
 CALCULATED BY BG DATE 7-17 SHEET OF  
 CHECKED BY YB DATE 7-17 JOB NO. 0723

## INTERSECTION GEOMETRY



Indicate North

## Left Turn Check

	Approach		
	1	2	3
a. Number of change intervals per hour			
b. Left turn capacity on change interval, in vph			
c. G/C Ratio			
d. Opposing volume in vph			
e. Left turn capacity on green, in vph			
f. Left turn capacity in vph (b - e)			
g. Left turn volume in vph			
h. Is volume > capacity (g > f)?			

## PHASING 20

(A)	(B)	(C)	(D)	(E)
↓  ↑	←			
381 382 ↓ ↓ 153  242 ↑ 598 841	208 ← 255 ← 234 213			
CLV= 841	CLV= 235	CLV=	CLV=	CLV=

$$\text{Opp Vol} = 382 \times 1.5 = 573 \quad \text{LT FAC} = 2.0$$

$\Sigma$  CLV 1016  
 V/C 0.72  
 LOS C

CRITERIA (vph)		2 B	3 B	4 B
LOS	A	900	855	825
	B	1050	1000	965
	C	1200	1140	1100
	D	1350	1275	1225
	E	1500	1425	1375

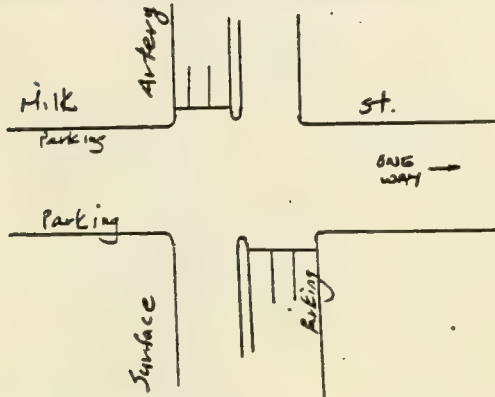




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INTERSECTION Surface Arterio / Milk St.  
 ALT. Existing YEAR 01984 PERIOD AM  
 CALCULATED BY RG DATE \_\_\_\_\_ SHEET OF  
 CHECKED BY RB DATE \_\_\_\_\_ JOB NO. 0723

## INTERSECTION GEOMETRY



## Left Turn Check

	Approach		
	1	2	3
a. Number of change intervals per hour			
b. Left turn capacity on change interval, in vph			
c. G/C Ratio			
d. Opposing volume in vph			
e. Left turn capacity on green, in vph			
f. Left turn capacity in vph (b * c)			
g. Left turn volume in vph			
h. Is volume > capacity (g > f)?			

## PHASING 2 Ø

(A)	(B)	(C)	(D)	(E)
↓ b ↑ f	↖ ↗			
504 143 ↓ b ↑ f 463 463	26 145 ↖ 107 ↗ 12			
CLV = 463 + 112	CLV = 145	CLV =	CLV =	CLV =

Opp Vol = 463 x 1.5 = 695 LT FAC = 4.0

Σ CLV 720  
 V/C 0.58  
 LOS A

77 % Reduction for Peds

CRITERIA (vph)		4.5 S	2 S	3 S	4 S
LOS	A	747	900	855	825
	B	872	1050	1000	965
	C	996	1200	1140	1100
	D	1127	1350	1275	1225
	E	1245	1500	1425	1375

## OPERATION SCHEDULE

DATE 7/20/77DATE FIRST IN SERVICE 5/23/74

## TIMING FOR AUTOMATIC OPERATION

[illegible]

Automatic Operation from 6:00 AM to 2:00 AM = 20  
hours per day.

Pedestrian Signal Operation from \_\_\_\_\_ to \_\_\_\_\_ =  
hours per day.

Remote P.B. Actuation from \_\_\_\_\_ to \_\_\_\_\_ =  
hours per day.

Flasher Operation from 2:00 AM to 6:00 AM = 4  
hours per day.

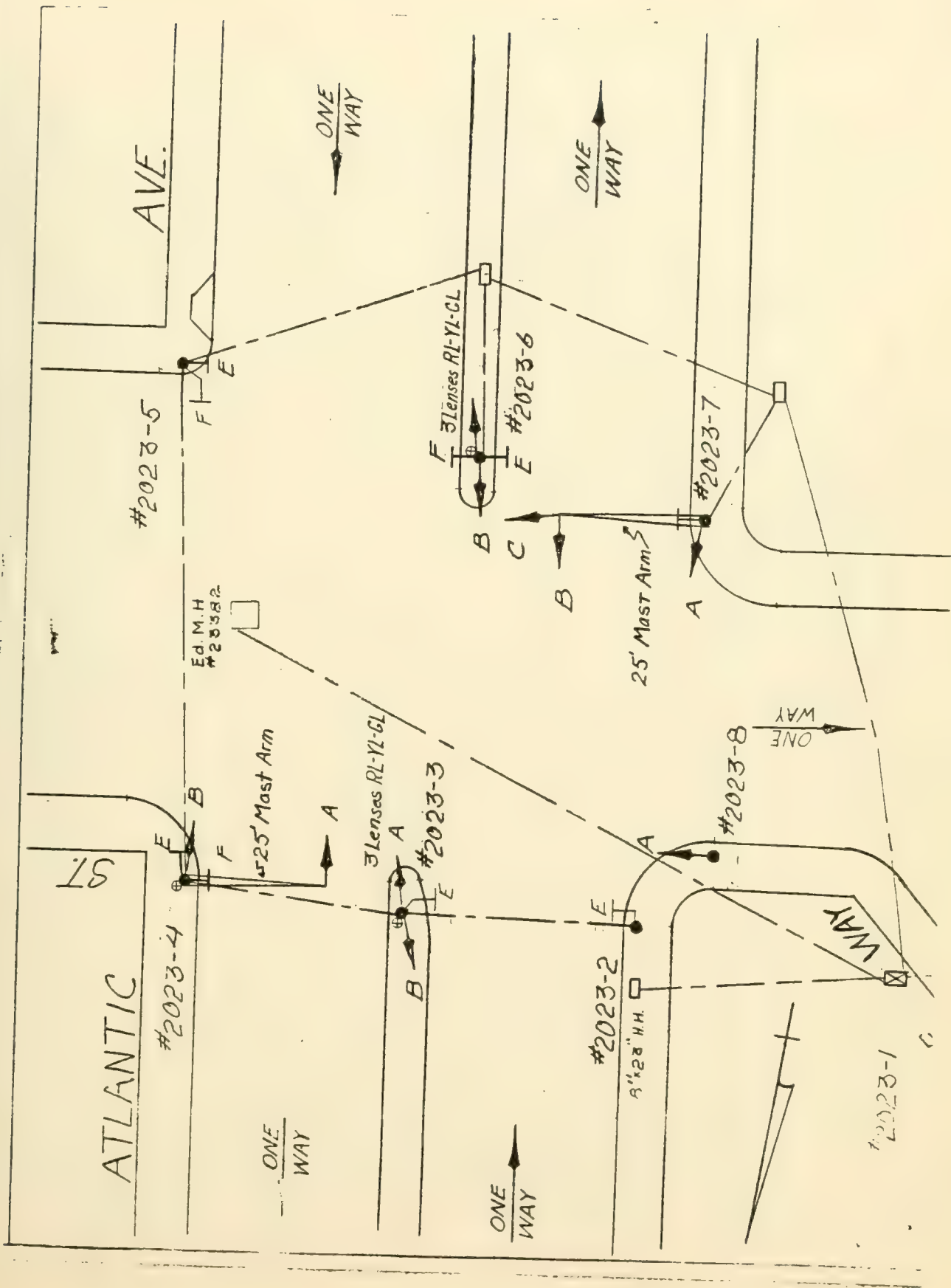
Timer-Type Crouse-Hinds Flasher-Type Crouse-Hinds

Coordinated ☒ Interconnected ☒ Non-Interconnected ☐

Master at Clinton St. & J.F.F. Expressway

[illegible][illegible]

REMARKS



## OPERATION SCHEDULE

DATE 8/15/77

DATE FIRST IN SERVICE \_\_\_\_\_ Installed by Stat. \_\_\_\_\_

[illegible]



Post	Ped. P.B.	Face	Top Lens	2nd Lens	3rd Lens	4th Lens	5th Lens
1	CB-	Atlantic Ave. and State St.					
2		E	DW	W			
3	X	A	RL	YL	GL		
		B	R	Y	G		
		C	R	Y	G		
		E/F	DW/DW	W/W			
4	X	A	R	Y	G		
		B	R	Y	G		
		C	R	Y	G		
		E/F	DW/DW	W/W			
5	X	E	DW	W			
		F	DW	W			
6		A	RL	YL	GL		
		B	R	Y	G		
		E	DW	W			
		F	DW	W			
7		A	R	Y	G		
		B	R	Y	G		
		C	R	Y	G		
		E	DW	W			
1	CB-	(junction) JFF. Surface and State					
2		A	R	Y	G		
		*B	R	Y	G		
3		*A	R	Y	G		
4		A	R	Y	G		
5		A	R	Y	G		
		B	R	Y	G		added 7/2/76
6		A	R	Y	G		
		*B	R	Y	G		
13	3	29	77	Total for Intersection			

Automatic Operation from \_\_\_\_\_ to \_\_\_\_\_ = 24 hours per day.

Pedestrian Signal Operation from \_\_\_\_\_ to \_\_\_\_\_ = \_\_\_\_\_ hours per day.

Remote P.B. Actuation from \_\_\_\_\_ to \_\_\_\_\_ = \_\_\_\_\_ hours per day.

Flasher Operation from \_\_\_\_\_ to \_\_\_\_\_ = 0 hours per day.

Timer-Type Crouse-Hinds Flasher-Type Crouse-Hinds

Coordinated ☒

Interconnected ☒

Non-Interconnected ☐

Master at Clinton St. and I.F.F. Expressway

Surface Rd.

OFFSETS	
	%
D1	
D2	
D3	

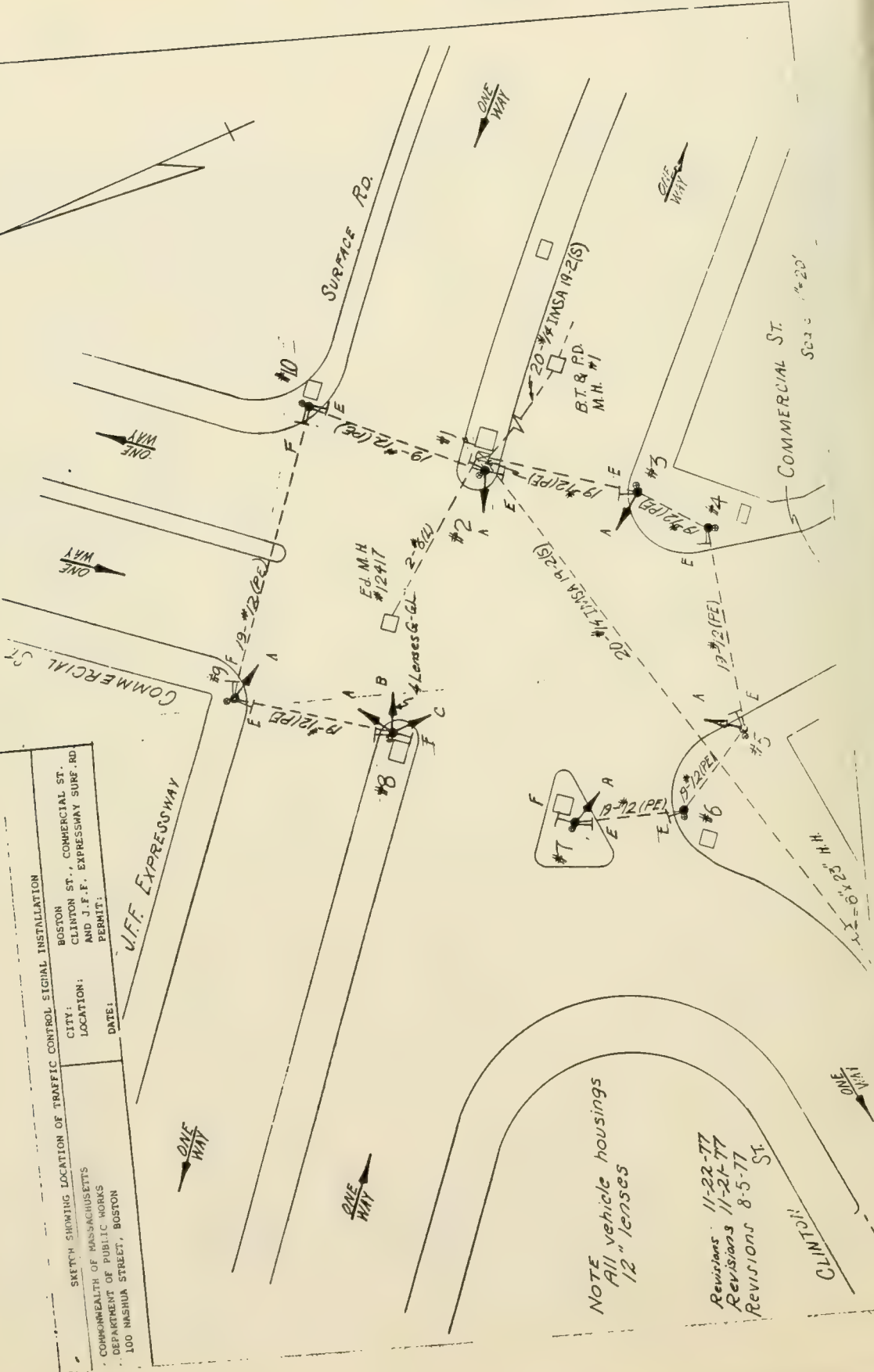
MASSACHUSETTS PERMIT	
Number	Date

## REMARKS

\*Optically programmed

All vehicle lenses 12" at Atl. & State

SKETCH SHOWING LOCATION OF TRAFFIC CONTROL SIGNAL INSTALLATION	
CITY: BOSTON LOCATION: CLINTON ST., COMMERCIAL ST. AND J.F.F. EXPRESSWAY SURF. RD. PERMIT:	DATE:
COMMONWEALTH OF MASSACHUSETTS DEPARTMENT OF PUBLIC WORKS 100 NASHUA STREET, BOSTON	



NOTE  
All vehicle housings  
12" lenses

Revisions 11-22-77  
Revisions 11-24-77  
Revisions 8-5-77

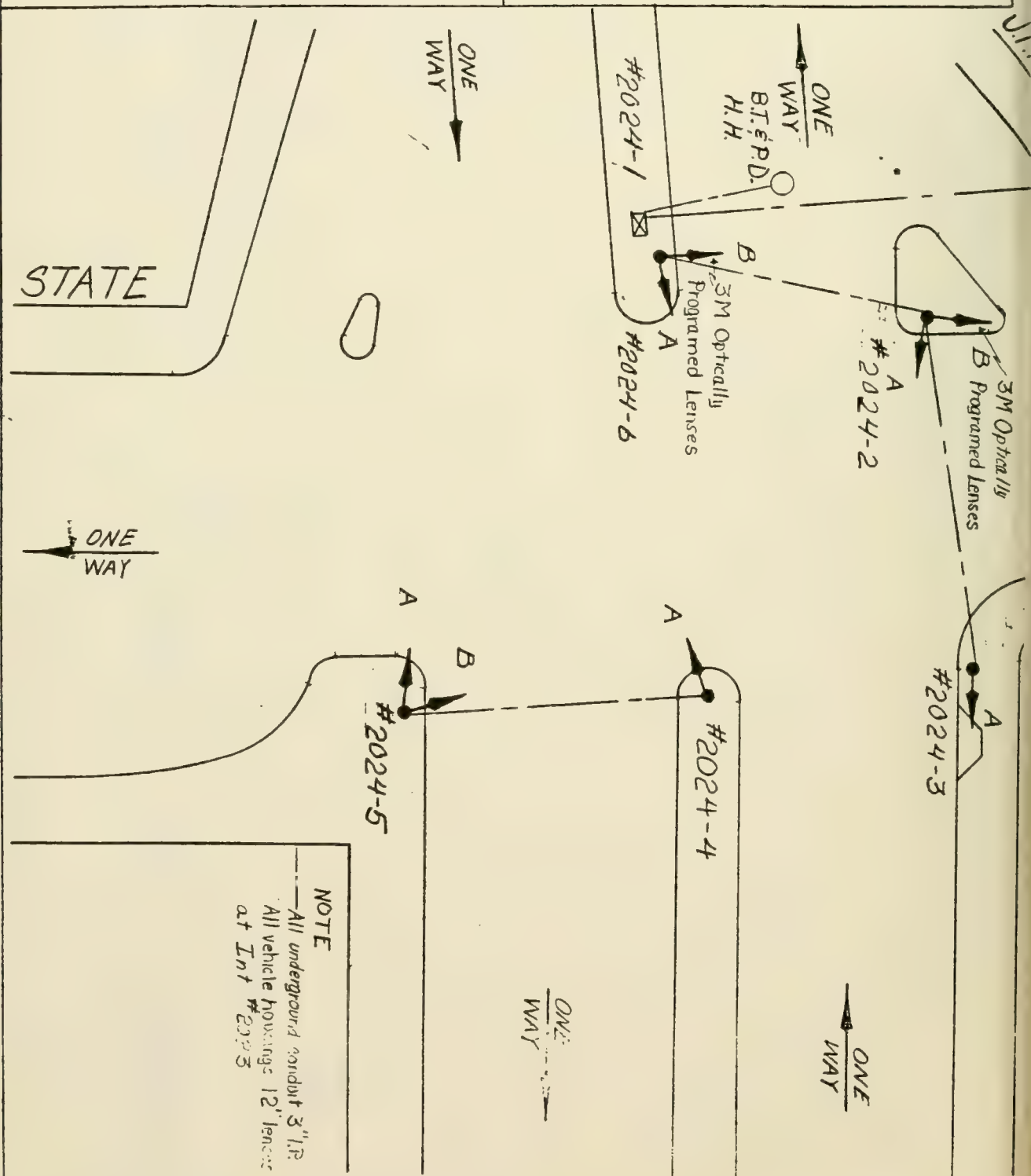
## OPERATION SCHEDULE

DATE 8-5-77

DATE FIRST IN SERVICE 5-25-76

CURRENT SUPPLY 115 VAC

Post	Ped. P.B.	Face	Top Lens	2nd Lens	3rd Lens	4th Lens	5th Lens
1		Control	Box				
	X	A	R	Y	G		
		E	DW	W			
		F	DW	W			
3	X	A	R	Y	G		
		E	DW	W			
4	X	E	DW	W			
5	X	A	R	Y	G		
		E	DW	W			
6	X	E	DW	W			
7	X	A	R	Y	G		
		E	DW	W			
	X	F	DW	W			
2	X	A	R	Y	G		
		E	DW	W			
		F	DW	W			
10	X	E	DW	W			
		F	DW	W			
10	9	22	53	ALL vehicle lenses 12" Total for Intersection			



**NOTE**  
—All underground conduit 3" I.P.  
All vehicle housings 12" length  
at Int #2003

## OPERATION SCHEDULE

DATE 8/15/77DATE FIRST IN SERVICE                      Installed by State                     

TIMING FOR AUTOMATIC OPERATION																Cycle Flash
	Without Ped.				18	7	4	7	5	4	15	4	2	4		
NORMAL	With Ped.															
to AM	Without Ped.															
to 30 AM	With Ped.				37	7	4	7	5	4	16	4	2	4		
to 30 PM	Without Ped.				<del>48</del> <del>34</del>						<del>15</del> <del>29</del>					
to 30 PM	With Ped.					7	4	7	5	4		4	2	4		
	Without Ped.															
	With Ped.															
	Without Ped.															
	With Ped.															
	Without Ped.															
	With Ped.															
	Without Ped.				*	To be 'G' in non-actuated cycle										
	With Ped.				**	To be 'DW' in non-actuated cycle										
	Without Ped.				O	To be FDW in non-actuated cycle										
	With Ped.															
Northbound Atlantic Ave.					RL	RL	RL	RL	RL	RL	GL	YL	RL	RL	Y L	
Southbound Atlantic Ave.					G	G	Y	R	R	R	*R	*R	*R	*R		
Atlantic Ave.					G	G	Y	R	R	R	R	R	R	R	R	
State St.					R	R	R	G	G	Y	R	R	R	R	R	
State St. @ Surface Rd.					R	R	R	G	G	G	G	G	G	Y	R	
J.F.F. Surface Rd.					G	G	Y	R	R	R	R	R	R	R		
C.W. 6E-7E					DW	DW	DW	DW	DW	DW	W	FDW	FDW	FDW		
C.W. 5F-6E					DW	DW	DW	W	FDW	FDW	DW	DW	DW	DW		
C.W. 4E-5E					W	FDW	FDW	DW	DW	DW	W	W	W	W		
S.W. 3F-4F					DW	DW	DW	W	W	W	W	FDW	FDW	FDW		
C.W. 2E-3E					DW	DW	DW	W	W	W	W	FDW	FDW	FDW		



Post	Ped. P.B.	Face	Top Lens	2nd Lens	3rd Lens	4th Lens	5th Lens
1	CB-	Atlantic Ave. and State St.					
2		E	DW	W			
3	X	A	RL	YL	GL		
		B	R	Y	G		
		C	R	Y	G		
		E/F	DW/DW	W/W			
4	X	A	R	Y	G		
		B	R	Y	G		
		C	R	Y	G		
		E/F	DW/DW	W/W			
5	X	E	DW	W			
		F	DW	W			
6		A	RL	YL	GL		
		B	R	Y	G		
		E	DW	W			
		F	DW	W			
7		A	R	Y	G		
		B	R	Y	G		
		C	R	Y	G		
		E	DW	W			
1	CB-	((junction)) JFF. Surface and State					
2		A	R	Y	G		
		*B	R	Y	G		
3		*A	R	Y	G		
4		A	R	Y	G		
5		A	R	Y	G		
		B	R	Y	G	added	
						7/2/76	
6		A	R	Y	G		
		*B	R	Y	G		
13	3	29	77	Total for Intersection			

Automatic Operation from \_\_\_\_\_ to \_\_\_\_\_ = 24 hours per day.

Pedestrian Signal Operation from \_\_\_\_\_ to \_\_\_\_\_ = \_\_\_\_\_ hours per day.

Remote P.B. Actuation from \_\_\_\_\_ to \_\_\_\_\_ = \_\_\_\_\_ hours per day.

Flasher Operation from \_\_\_\_\_ to \_\_\_\_\_ = 0 hours per day.

Timer-Type Crouse-Hinds Flasher-Type Crouse-Hinds

Coordinated ☒ Interconnected ☒ Non-Interconnected ☐

Master at Clinton St. and I F F Expressway Surface Rd.

OFFSETS	
	%
D1	
D2	
D3	

MASSACHUSETTS PERMIT	
Number	Date

### REMARKS

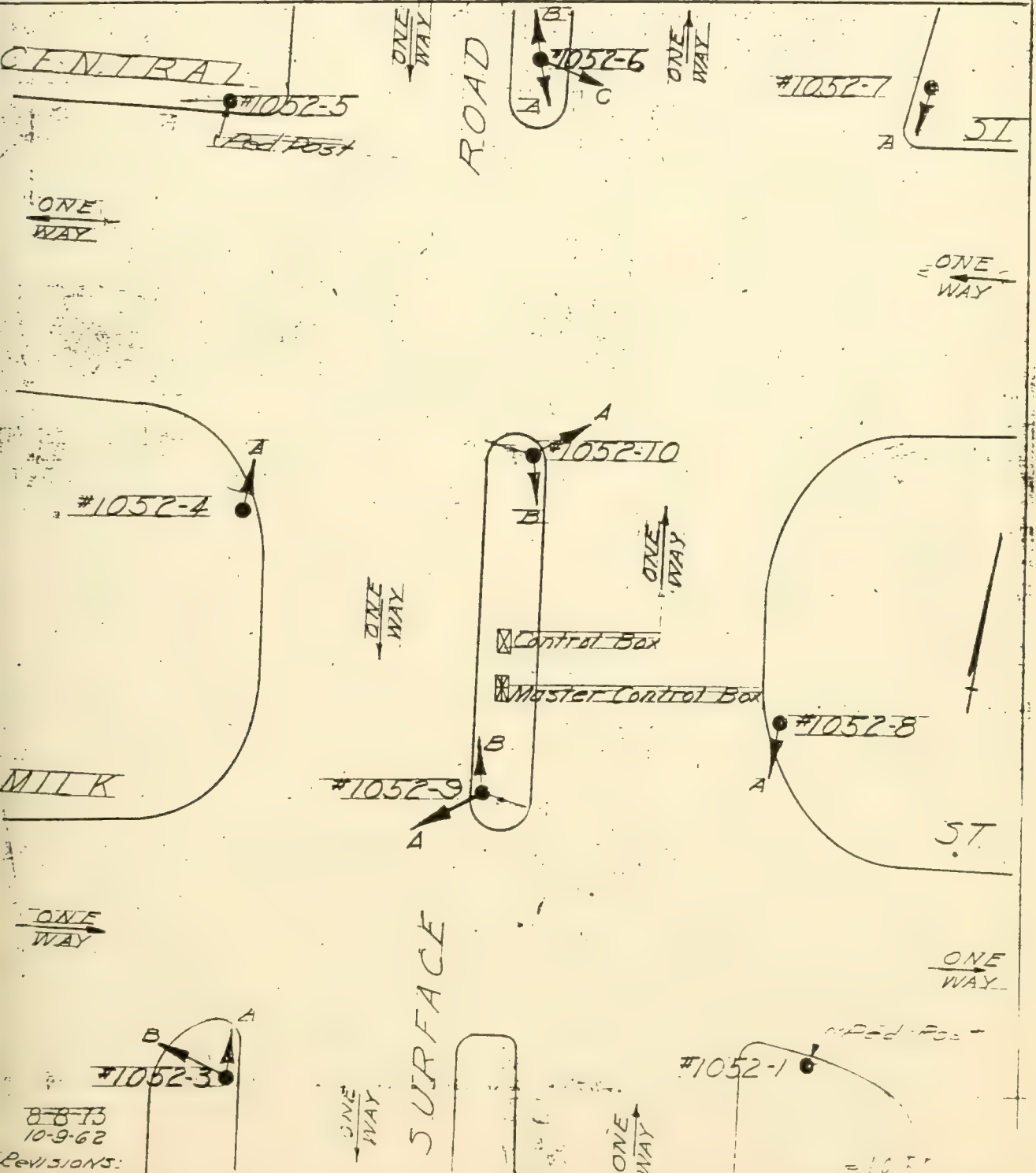
\*Optically programmed

All vehicle lenses 12" at Atl. & State

# SKETCH SHOWING LOCATION OF TRAFFIC CONTROL SIGNAL INSTALLATION

COMMONWEALTH OF MASSACHUSETTS  
DEPARTMENT OF PUBLIC WORKS  
100 NASHUA STREET, BOSTON

CITY BOSTON  
LOCATION: Central St., John F. Fitzgerald  
Expressway (Surface Road) & Milk St.  
DATE PERMIT



8-8-73  
10-9-62  
REVISIONS:

1052  
SHEET 1 OF 1

## OPERATION SCHEDULE

DATE 7/7/77

DATE FIRST IN SERVICE Prior to 1958

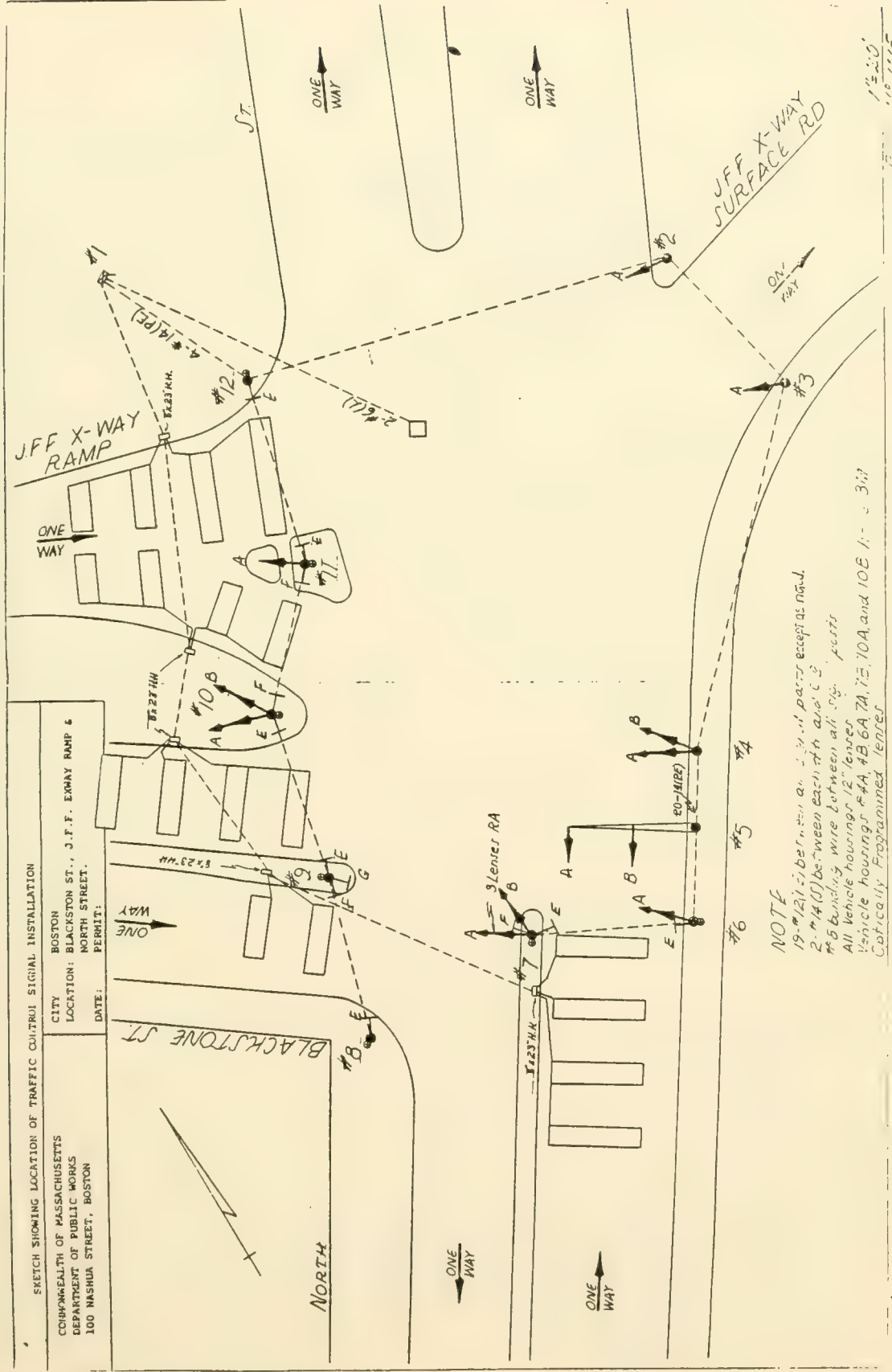
CURRENT SUPPLY 115 V. A. L.

TIMING FOR AUTOMATIC OPERATION											Fla
Post	Ped. P.B.	Face	Top Lens	2nd Lens	3rd Lens	4th Lens	5th Lens	Without Ped.	With Ped.	Cycle	
1			Control Box					NORMAL	41	70	
2	X	A	R	Y	G			With Ped.	26	70	
3	X	E	DW	W				Without Ped.	60	90	
		E	DW	W				With Ped.	45	90	
4	X	F	DW	W				Without Ped.	66	100	
		A	R	Y	G			With Ped.	51	100	
		B	R	Y	G						
		E	DW	W				Surface Rd.	G		
		F	DW	W				Milk St.	R		
5	X	A	R	Y	G			C.W. 3F-4F	DW		
		E	DW	W				C.W. 2E-3E; 4E-5E	DW		
		A	R	Y	G						
		B	R	Y	G	(mast)					
Automatic Operation from SEE MASTER = hours per day											
Flasher Operation from to = hours per day											
Timer-Type Crouse Hinds Flasher-Type Crouse Hinds											
Coordinated X Interconnected X Non-interconnected											
Offset Master at Clinton St. & J.F.F. Surface Rd.											
REMARKS											
on flash 7/7/77 to 7/20/77											

SKETCH SHOWING LOCATION OF TRAFFIC CONTROL SIGNAL INSTALLATION

CITY OF MASSACHUSETTS  
 DEPARTMENT OF PUBLIC WORKS  
 100 NASHUA STREET, BOSTON

CITY: BOSTON  
 LOCATION: BLACKSTONE ST., J.F.F. EXWAY RAMP & NORTH STREET  
 PERMIT: DATE:



NOTE  
 19-#1212 between each and 1/4 in part except as noted.  
 2-#1401 between each and 1/4 in part except as noted.  
 #5 binding wire between all sig. parts  
 All vehicle housings 12' fence  
 Vehicle housings #4, #6, #7, #10A and 10E 1' - 3' in  
 Catically Programmed fence

1/20/0  
 1/10/0

has been for 10th year and half

LOCATION Blackstone St., J.F. Fitzgerald Expressway Ramp RF and North St. DATE 8/28/78

INTERSECTION No 1115 DATE FIRST IN SERVICE 5/25/76

[illegible]



Automatic Operation from \_\_\_\_\_ to \_\_\_\_\_ = 24  
hours per day.

Pedestrian Signal Operation from \_\_\_\_\_ to \_\_\_\_\_ =  
hours per day.

Remote P.B. Actuation from \_\_\_\_\_ to \_\_\_\_\_ =  
hours per day.

Flasher Operation from \_\_\_\_\_ to \_\_\_\_\_ =  
hours per day.

Timer-Type \_\_\_\_\_ Flasher-Type \_\_\_\_\_

Coordinated ☐ Interconnected ☐ Non-Interconnected ☒

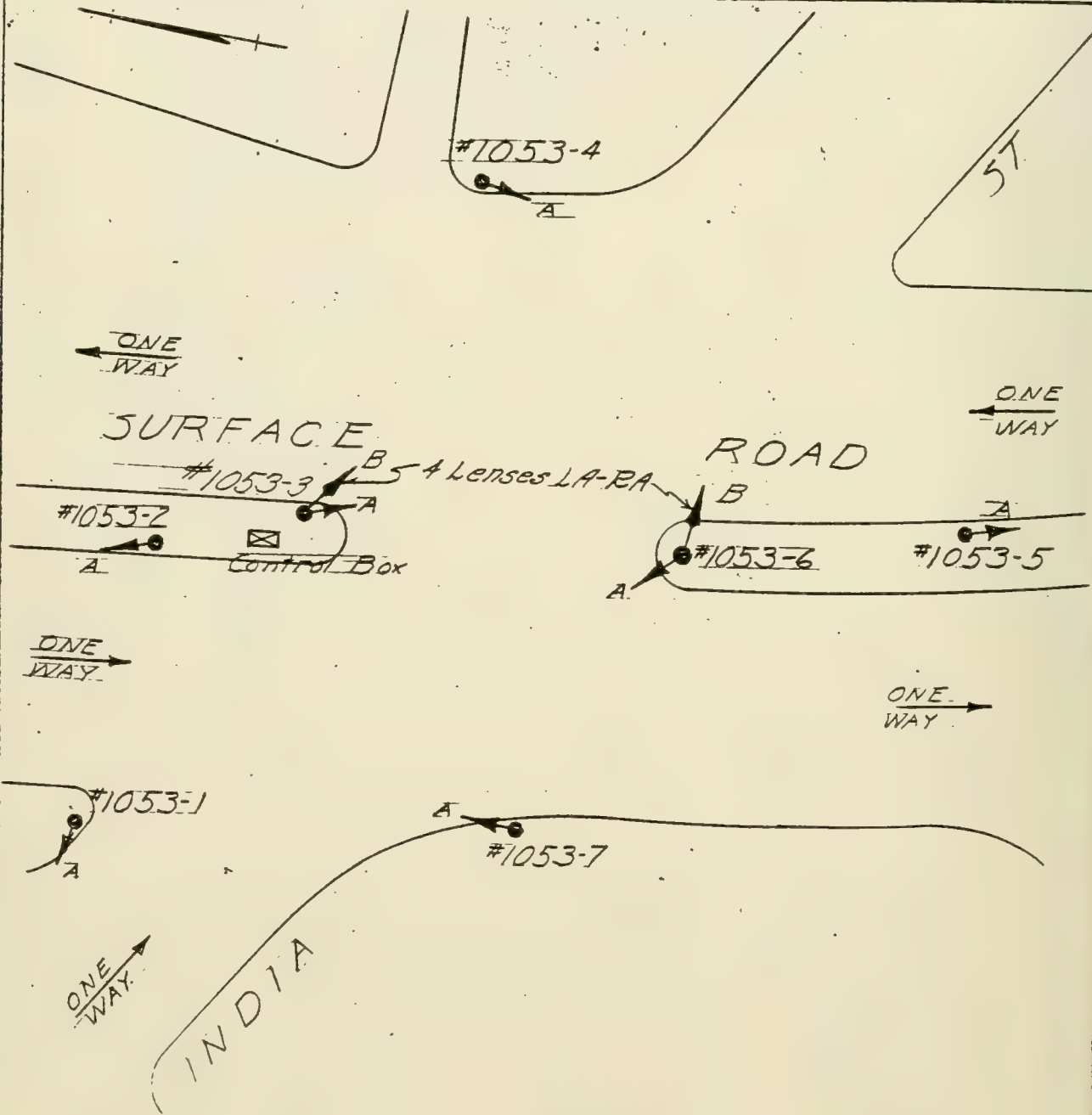
Master at \_\_\_\_\_

[illegible][illegible]

# SKETCH SHOWING LOCATION OF FLASHING SIGNAL INSTALLATION

COMMONWEALTH OF MASSACHUSETTS  
DEPARTMENT OF PUBLIC WORKS  
100 NASHUA STREET, BOSTON

CITY BOSTON  
LOCATION: India St. & John F. Fitzgerald  
(Surface Road)  
DATE PERMIT



E-25-72  
Esk 138d

## OPERATION SCHEDULE

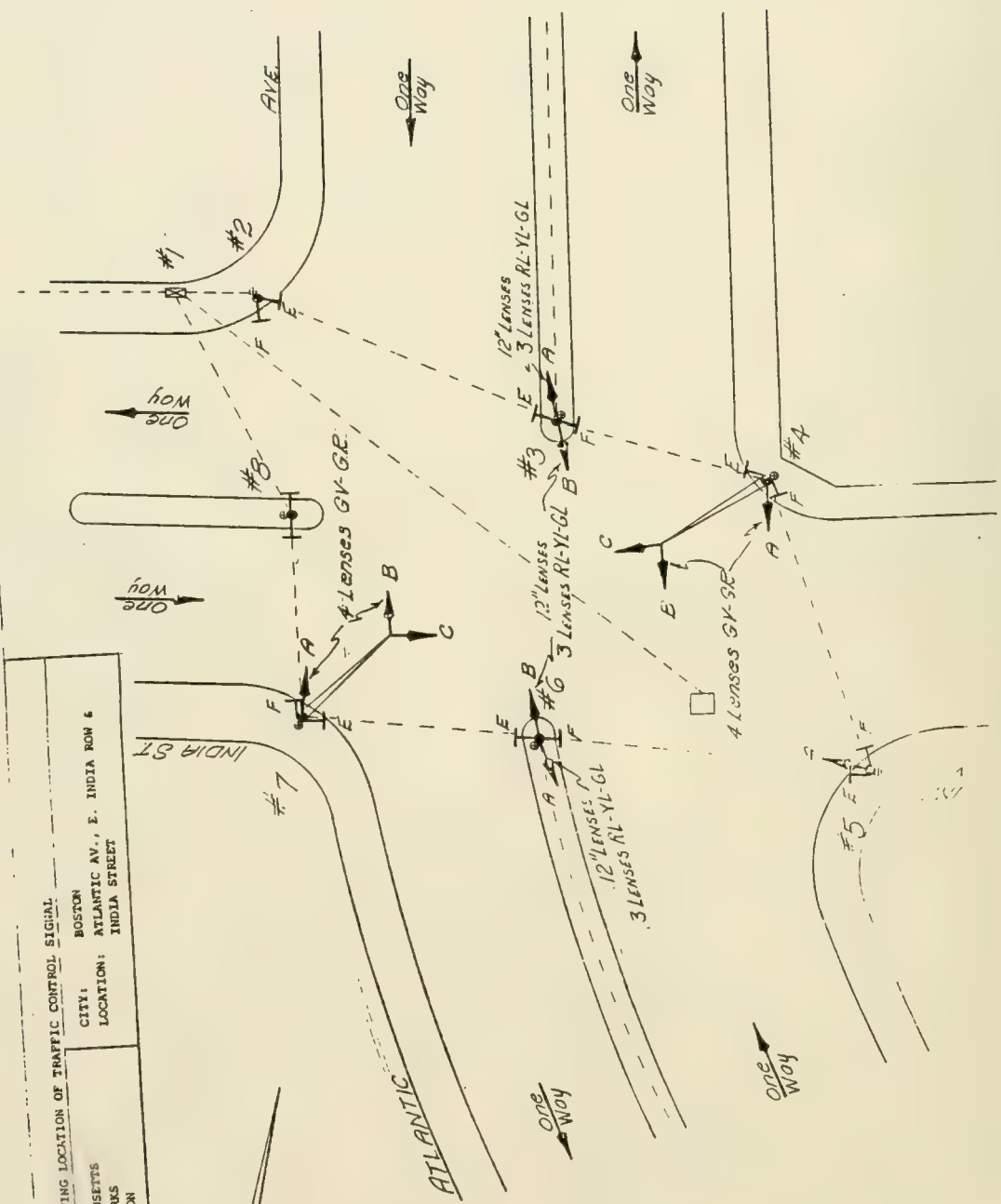
DATE June 10, 1958

DATE FIRST IN SERVICE Installed by State

CURRENT SUPPLY 115V.A.C.

TIMING FOR AUTOMATIC OPERATION										Code	Plate				
Post	Prod. P.D.	Face	Top Lens	2nd Lens	3rd Lens	4th Lens	5th Lens	Timing					90	Y	R
								Without Ped.	With Ped.	Without Ped.	With Ped.	Without Ped.			
Control	Box							41	5	40	4				
1	A	R	Y	G											
2	A	R	Y	G											
3	A	R	Y	G											
4	A	R	Y	G											
5	B	R	Y	G											
6	B	R	Y	G											
7	A	R	Y	G											
Automatic Operation from 6 a.m. to 2 a.m. = 20 hours per day															
Flasher Operation from 2 a.m. to 6 a.m. = 4 hours per day															
Timer—Type G. E.										Flasher—Type G. E.					
Coordinated <input checked="" type="checkbox"/>										Interconnected <input type="checkbox"/>		Non-interconnected <input type="checkbox"/>			
Offset <input checked="" type="checkbox"/> 10 sec.										Separate Central St., Expressway & Milk St.					
MASSACHUSETTS PERMIT No.										Date		REMARKS			
#1837										6-10-58		Signals reverted to State control from 5/1/60 to 2/1/61			
98										28		Total for Intersection			

SKETCH SHOWING LOCATION OF TRAFFIC CONTROL SIGNAL	
CITY: BOSTON LOCATION: ATLANTIC AV., E. INDIA ROW & INDIA STREET	COMMONWEALTH OF MASSACHUSETTS DEPARTMENT OF PUBLIC WORKS 100 NASHUA STREET, BOSTON



# OPERATION SCHEDULE

INTERSECTION N<sup>o</sup> 2007 DATE FIRST IN SERVICE 5/16/74

5/16/74

5/16/74

[illegible]



Automatic Operation from 6:00 am to 2:00 am = 20  
hours per day.

Pedestrian Signal Operation from \_\_\_\_\_ to \_\_\_\_\_  
hours per day.

Remote PB. Actuation from \_\_\_\_\_ to \_\_\_\_\_ =  
hours per day.

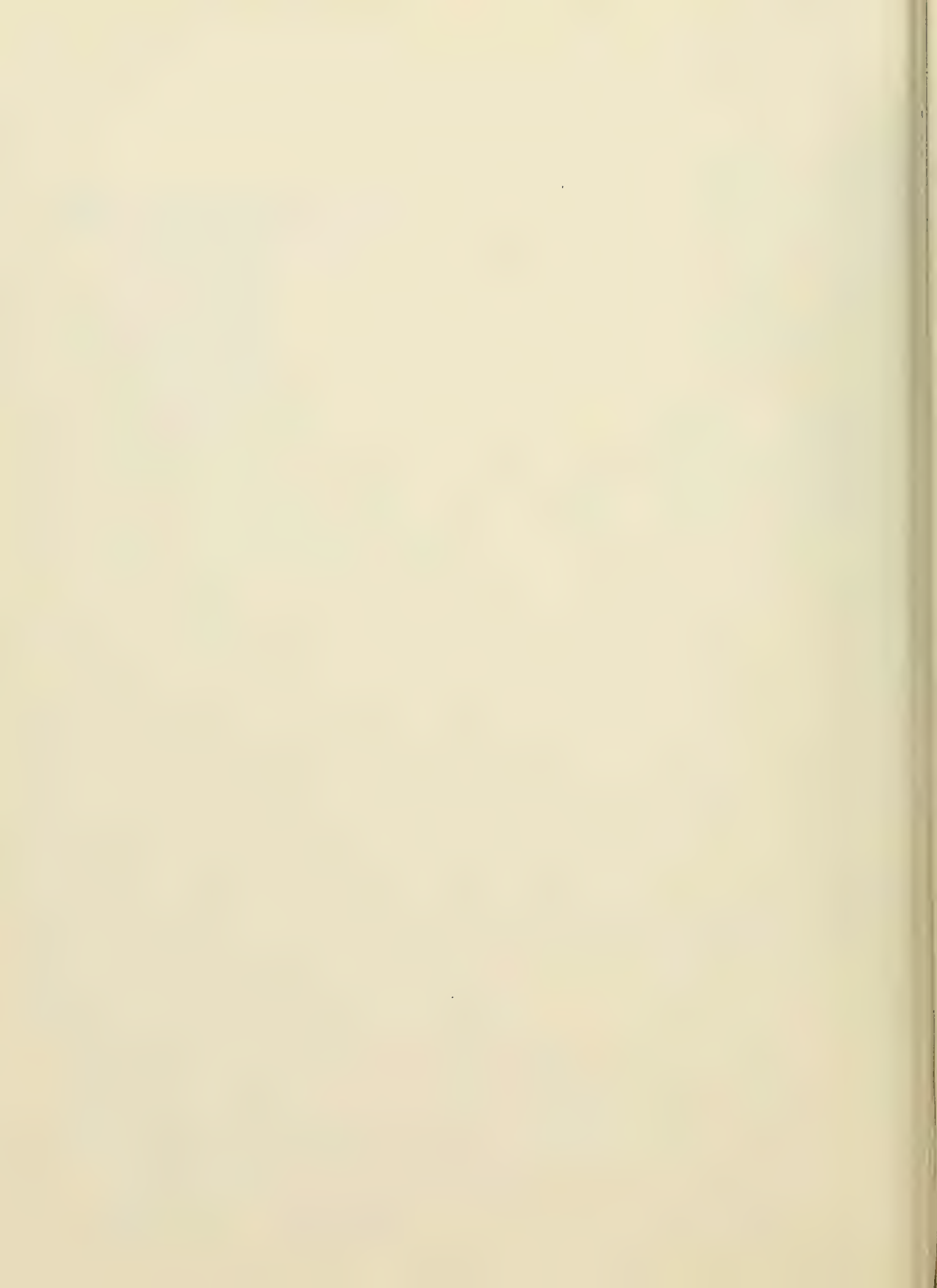
Flasher Operation from 2:00 am to 6:00 am = 4  
hours per day.

Timer-Type Crouse-Hinds Flasher-Type Crouse-Hinds

Coordinated ☒ Interconnected ☒ Non-Interconnected ☐

Master at CLINTON ST. & J.F.F. EXPRESSWAY

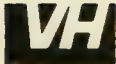
AIR QUALITY DATA





TITLE AIR QUALITY DATA REQUIREMENTS

Location	Date of Count	Peak Hour speed	Off-Peak speed	8 hr/1 hr factor
OLIVER ST. EB	9/22-23/76 Peak 8-hour = 7:00 AM - 3:00 PM	28	30	0.59
PURCHASE ST. S.B.	9/22-23/76 Peak 8-hour = 9:30 AM - 5:30 PM	28	35	0.75



**Vanasse / Hangen Engineering, Inc.**  
Consulting Engineers & Planners  
184 High Street, Boston, Massachusetts 02110  
617 / 482-1870

JOB: INTERNATIONAL PLACE JOB No. 0788  
LOCATION: \_\_\_\_\_ SHEET 1 OF 2  
CALCULATED BY: BC DATE: 4/9/84  
CHECKED BY: \_\_\_\_\_ DATE: \_\_\_\_\_  
TITLE AIR QUALITY DATA REQUIREMENTS

Location	Date of Count	Peak Hour Speed	Off-Peak speed	8 hr/1hr factor
* ATLANTIC AVE. (AT SURFACE ARTERY AND HIGH STREET) N.B. TO W.B. S.B. TO W.B.  SURFACE ARTERY N.B. (FROM X-WAY) S.B.	1981 1981  1981 1981	26 22  28 24	32 26  35 29	0.79 0.79  0.70 0.70
HIGH ST. / OLIVER ST.  HIGH ST. S.B.	11/14/80 Peak 8-hour 7:00AM-3:00PM	25	30	0.67
CONGRESS ST. E.B.  HIGH ST. S.B.	8/1-2/79 Peak 8-hour = 10:00 AM-6:00 PM 8/1-2/79 Peak 8-hour = 7:30 AM-3:00 PM	23  25	30  30	0.64  0.65
CONGRESS ST. E.B.  PURCHASE ST. S.B.	6/10/83 Peak 8-hour = 10:00 AM-6:00 PM 6/10/83 Peak 8-hour = 10:00 AM-6:00 PM	20  20	25  30	0.68  0.70

\* Values used on Rowes Wharf EIR.





**Vanasse / Hangen**  
Consulting Engineers & Planners  
184 High Street, Boston, Massachusetts 02110  
617 / 482-1870

JOB: International Place JOB No. 0923  
LOCATION: \_\_\_\_\_ SHEET \_\_\_\_\_ OF \_\_\_\_\_  
CALCULATED BY: BG DATE: \_\_\_\_\_  
CHECKED BY: \_\_\_\_\_ DATE: \_\_\_\_\_  
TITLE: AIR QUALITY CALCULATION

Intersection: Congress St. / Purchase

Congress St.  
EB

Peak hour = 1232  
Peak 8 hours = 6720  
factor = 0.68

Purchase St  
SB

Peak hour = 1283  
Peak 8 hours = 7272  
factor = 0.70

Intersection: Oliver St. / Purchase St.

Oliver St.  
EB

Peak hour = 460  
Peak 8 hours = 2173  
factor = 0.59

Purchase St.  
SB

Peak hour = 1179  
Peak 8 hours = 2080  
factor = 0.75

**Vanasse / Hangen**

Consulting Engineers &amp; Planners

184 High Street, Boston, Massachusetts 02110

617 / 482-1870

JOB: International Place JOB No. 0923

LOCATION: \_\_\_\_\_ SHEET \_\_\_\_\_ OF \_\_\_\_\_

CALCULATED BY: BCG DATE: \_\_\_\_\_

CHECKED BY: \_\_\_\_\_ DATE: \_\_\_\_\_

TITLE: AIR QUALITY CALCULATIONIntersection: Congress St. / High St.Congress St.  
EBHigh St  
SBPeak hour = 1093Peak 8 hours = 5,600factor = 0.64Peak hour = 690Peak 8 hours = 3,588factor = 0.65Intersection: High St. / Oliver St.High St.  
SBOliver StPeak hour = 618Peak 8 hours = 3,309factor = 0.67

RAPID TRANSIT RIDERSHIP



Andrew Station

Harvard Station - Ashmont Station

OUTBOUND						DATE: Mon July 2						DATE:						DATE:							
A.M.						WEATHER: Fair						WEATHER:						WEATHER:							
TIME:						V	Tot. Pass.	Aver.	Std. Cap.	O/U	V	Tot. Pass.	Aver.	Std. Cap.	O/U	V	Tot. Pass.	Aver.	Std. Cap.	O/U	V	Tot. Pass.	Aver.	Std. Cap.	O/U
5:00 - 6:00																									
6:01 - 6:30																									
6:31 - 7:00																									
Subtotal																									
7:01 - 7:30																									
7:31 - 8:00																									
8:01 - 8:30																									
8:31 - 9:00																									
Subtotal																									
9:01 - 9:30																									
9:31 - 10:00																									
10:01 - 10:30																									
10:31 - 11:00																									
11:01 - 11:30																									
11:31 - 12:00																									
12:01 - 12:30																									
12:31 - 1:00																									
1:01 - 1:30																									
1:31 - 2:00							4	170	43																
2:01 - 2:30							12	540	45																
2:31 - 3:00							12	620	52																
3:01 - 3:30							4	360	90																
3:31 - 4:00							12	855	71																
Subtotal							44	2545	58																
4:01 - 4:30							16	1620	101																
4:31 - 4:45							4	225	56																
4:46 - 5:00							8	1240	155																
5:01 - 5:15							4	800	200																
5:16 - 5:30							8	1425	184																
5:31 - 5:45							8	1150	144																
5:46 - 6:00							8	506	63																
Subtotal							56	7016	125																
6:01 - 6:30							8	620	78																
6:31 - 7:00							20	1000	50																
7:01 - 7:30							8	570	71																
7:31 - 8:00							12	525	44																
8:01 - 8:30							8	300	38																
8:31 - 9:00							4	380	95																
9:01 - 9:30							6	400	67																
9:31 - 10:00							4	110	28																
10:01 - 10:30																									
10:31 - 11:00																									
11:01 - 11:30																									
11:31 - 12:00																									
12:01 - 1:00																									
Subtotal							70	3925	56																
Total							170	13466	79																



# SUMMARY OF TRAFFIC COUNTS

LOCATION: *Andrew Station*

YEAR: *82*

ROUTE: *Harvard Brattle Station - Braintree Station*

OUTBOUND	Monday DATE: <i>Feb. 1</i>					Tuesday DATE: <i>Feb. 2</i>					Thurs. DATE: <i>July 13</i>					Thurs. DATE: <i>Nov. 30</i>				
	WEATHER: <i>Cloudy-Rain</i>					WEATHER: <i>Cloudy</i>					WEATHER: <i>Cloudy</i>					WEATHER: <i>Fair</i>				
A.M.	V	Tot. Pass.	Aver.	Std. Cap.	O/U	V	Tot. Pass.	Aver.	Std. Cap.	O/U	V	Tot. Pass.	Aver.	Std. Cap.	O/U	V	Tot. Pass.	Aver.	Std. Cap.	O/U
5:00 - 6:00	8	79	18								4	48	12							
6:01 - 6:30	8	59	7								4	57	14							
6:31 - 7:00	4	48	12								16	208	13							
Subtotal	20	186	9								24	313	13							
7:01 - 7:30	8	175	22								12	370	31							
7:31 - 8:00	8	163	20								12	192	16							
8:01 - 8:30	20	440	22								20	380	19							
8:31 - 9:00	23	278	14								20	167	8			20	367	18		
Subtotal	56	1054	19								64	1109	19			20	367	18		
9:01 - 9:30	12	192	16								24	216	9			24	247	10		
9:31 - 10:00	24	312	13								24	208	9			20	326	66		
10:01 - 10:30	16	250	17								12	180	15			16	208	13		
10:31 - 11:00	12	152	13								8	175	22			16	195	12		
11:01 - 11:30	8	97	12								12	396	33			12	177	15		
11:31 - 12:00	12	172	14								12	251	21			12	221	18		
12:01 - 12:30	8	238	30								12	304	25			12	271	23		
12:31 - 1:00	12	282	21								12	427	36			12	337	28		
1:01 - 1:30	12	330	28								12	381	32			12	422	35		
1:31 - 2:00	8	380	48								8	317	40							
2:01 - 2:30	12	445	37								12	498	42							
2:31 - 3:00	8	446	53								8	356	45							
3:01 - 3:30						12	800	67			8	963	120							
3:31 - 4:00						16	2840	178			12	915	76							
Subtotal	144	3270	23			28	3640	130			176	5537	32			136	2404	18		
4:01 - 4:30						12	2840	212			16	1628	102							
4:31 - 4:45						12	250	213			4	305	76							
4:46 - 5:00						8	260	300			12	200	208							
5:01 - 5:15						12	3135	261			8	1525	191							
5:16 - 5:30						4	1200	300			12	2800	238							
5:31 - 5:45						12	2335	194			6	605	101							
5:46 - 6:00						8	235	272			4	295	74							
Subtotal						68	11325	240			62	9718	157							
6:01 - 6:30						12	1820	155			12	2930	244							
6:31 - 7:00						24	874	36			22	686	31							
7:01 - 7:30						11	220	23			16	485	31							
7:31 - 8:00						8	225	28			10	876	88							
8:01 - 8:30						12	335	32			6	235	39							
8:31 - 9:00						8	200	25			4	190	48							
9:01 - 9:30						8	150	16			6	300	50							
9:31 - 10:00						8	270	34			4	120	30							
10:01 - 10:30						8	200	25			6	255	43							
10:31 - 11:00						8	210	33			4	180	45							
11:01 - 11:30						8	170	21			4	80	20							
11:31 - 12:00						8	130	16			4	65	16							
12:01 - 1:00						16	266	17			6	31	5							
Subtotal						74	5250	33			104	16443	62							
Total	220	4512	21			252	25215	107			220	23170	54			156	2771	18		

*Red Line*  
 PLANS AND SCHEDULES DEPARTMENT  
 SUMMARY OF TRAFFIC COUNTS

LOCATION: *Charles Street Station*YEAR: *84*ROUTE: *Ashmont & Braintree Stations - Harvard Station*

OUTBOUND	DATE: <i>Mon. Feb. 13</i>	DATE: <i>Thurs. May 17</i>	DATE: <i>Mon. July 2</i>	DATE:
A.M.	WEATHER: <i>Fair</i>	WEATHER: <i>Cloudy</i>	WEATHER: <i>Cloudy</i>	WEATHER:
TIME:	V Tot. Pass. Aver. Std. Cap. O/U	V Tot. Pass. Aver. Std. Cap. O/U	V Tot. Pass. Aver. Std. Cap. O/U	V Tot. Pass. Aver. Std. Cap. O/U
5:00 - 6:00				
6:01 - 6:30				
6:31 - 7:00				
Subtotal	<i>No Outbound</i>			
7:01 - 7:30				
7:31 - 8:00				
8:01 - 8:30				
8:31 - 9:00				
Subtotal	<i>Counts</i>			
9:01 - 9:30				
9:31 - 10:00				
10:01 - 10:30				
10:31 - 11:00				
11:01 - 11:30				
11:31 - 12:00				
12:01 - 12:30				
12:31 - 1:00				
1:01 - 1:30				
1:31 - 2:00				
2:01 - 2:30				
2:31 - 3:00				
3:01 - 3:30				
3:31 - 4:00				
Subtotal				
4:01 - 4:30				
4:31 - 4:45				
4:46 - 5:00				
5:01 - 5:15				
5:16 - 5:30				
5:31 - 5:45				
5:46 - 6:00				
Subtotal				
6:01 - 6:30				
6:31 - 7:00				
7:01 - 7:30				
7:31 - 8:00				
8:01 - 8:30				
8:31 - 9:00				
9:01 - 9:30				
9:31 - 10:00				
10:01 - 10:30				
10:31 - 11:00				
11:01 - 11:30				
11:31 - 12:00				
12:01 - 1:00				
Subtotal				
Total				

16 1780 111  
 16 1290 81  
 28 1730 108  
 20 1454 73  
 24 1792 75  
 104-8046-77

24 1230 51  
 16 950 59  
 8 280 35  
 16 2050 130  
 12 1700 142  
 20 2150 108  
 8 580 73  
 104-8940-86

20 1270 64  
 20 865 43  
 26 1053 41  
 16 679 42  
 6 389 65  
 10 515 52  
 10 445 45  
 8 403 50

116-5619-49  
 324-22605-70



# PLANS AND SCHEDULES DEPARTMENT

## SUMMARY OF TRAFFIC COUNTS

LOCATION: *Arlington St. Station*YEAR: *84*ROUTE: *830 North Station - Cleveland Circle*

OUTBOUND		DATE: <i>Fri. Jan. 20</i>					DATE: <i>Fri. Feb. 17</i>					DATE: <i>Tues. May 29</i>					DATE:				
A.M.		WEATHER: <i>Fair</i>					WEATHER: <i>cldy/rain</i>					WEATHER: <i>Rain</i>					WEATHER:				
TIME:		V	Tot. Pass.	Aver.	Std. Cap.	O/U	V	Tot. Pass.	Aver.	Std. Cap.	O/U	V	Tot. Pass.	Aver.	Std. Cap.	O/U	V	Tot. Pass.	Aver.	Std. Cap.	O/U
5:00 - 6:00		1	142	142			3	128	43			3	86	28							
6:01 - 6:30		2	61	31			3	184	61			3	210	73							
6:31 - 7:00		4	482	121			3	285	95			2	222	111							
Subtotal		7	685	98			9	597	66			8	518	65							
7:01 - 7:30		2	212	106			3	434	145			4	575	149							
7:31 - 8:00		5	842	167			5	769	154			5	810	162							
8:01 - 8:30		4	685	171			7	1039	148			8	1330	154							
8:31 - 9:00		1	180	180			6	1035	173			5	563	112							
Subtotal		12	1919	160			21	3277	156			22	3198	145							
9:01 - 9:30		2	185	93			10	811	81			8	908	114							
9:31 - 10:00		4	518	105			5	361	72			7	554	79							
10:01 - 10:30		7	693	99			7	351	50			7	228	32							
10:31 - 11:00		4	239	58			4	217	54			2	114	57							
11:01 - 11:30		7	388	55			6	350	58			9	402	44							
11:31 - 12:00		6	360	60			6	274	49			7	315	45							
12:01 - 12:30		4	399	100			6	444	41			5	390	78							
12:31 - 1:00		8	498	62			6	377	63			6	529	88							
1:01 - 1:30		5	347	70			5	318	64			7	585	84							
1:31 - 2:00		6	453	76			5	451	90			7	445	64							
2:01 - 2:30		3	251	84			6	612	102			6	457	76							
2:31 - 3:00		5	285	57			6	336	56			5	435	87							
3:01 - 3:30		7	364	52			6	644	107			5	694	139							
3:31 - 4:00		5	728	146			4	597	149			8	846	106							
Subtotal		73	5708	78			82	5743	73			89	6902	78							
4:01 - 4:30		7	892	127			8	613	77			6	650	108							
4:31 - 4:45		5	653	131			4	705	176			4	538	135							
4:46 - 5:00		2	360	180			3	438	146			3	508	169							
5:01 - 5:15		2	360	180			5	713	143			4	675	169							
5:16 - 5:30		1	180	180			4	720	180												
5:31 - 5:45		3	540	180			2	360	180			5	820	164							
5:46 - 6:00		5	875	175			3	540	180			4	637	159							
Subtotal		25	3860	155			29	4289	144			26	3838	147							
6:01 - 6:30		8	999	125			8	853	119			8	875	109							
6:31 - 7:00		3	406	135			7	560	80			3	485	165							
7:01 - 7:30		5	327	65			4	362	91			4	450	113							
7:31 - 8:00		4	344	86			4	218	55			3	325	108							
8:01 - 8:30		2	125	63			3	225	75			5	280	56							
8:31 - 9:00		5	273	55			4	200	50			4	258	65							
9:01 - 9:30		4	244	61			5	198	40			4	215	54							
9:31 - 10:00		2	66	33			2	128	64			4	205	51							
10:01 - 10:30		4	204	51			3	124	41			2	125	63							
10:31 - 11:00		5	261	52			5	142	28			3	138	43							
11:01 - 11:30		2	98	49			3	177	59			1	40	40							
11:31 - 12:00		3	126	42			3	222	74												
12:01 - 1:00		3	128	43			3	239	80												
Subtotal		130	5136	77			115	4083	71			44	3406	83							
Total			163	15831	94			175	17307	91			186	17852	96						

PLANS AND SCHEDULES DEPARTMENT  
SUMMARY OF TRAFFIC COUNTS

LOCATION: Arlington Street Station YEAR: 84  
ROUTE: 811 Government Center - Boston College

OUTBOUND	DATE: <u>Fri. Jan. 20</u>	DATE: <u>Fri. Feb. 17</u>	DATE: <u>Tues. May 29</u>	DATE:
A.M.	WEATHER: <u>Fair</u>	WEATHER: <u>Cloudy/Rain</u>	WEATHER: <u>Rain</u>	WEATHER:
TIME:	V Tot. Pass. Aver. Std. Cap. O/U	V Tot. Pass. Aver. Std. Cap. O/U	V Tot. Pass. Aver. Std. Cap. O/U	V Tot. Pass. Aver. Std. Cap. O/U
5:00 - 6:00	1 133 133	1 135 135	2 154 77	
6:01 - 6:30	4 279 70	4 243 61	3 98 33	
6:31 - 7:00		3 325 132	4 485 121	
Subtotal	5 412 82	8 773 97	9 737 82	
7:01 - 7:30	7 698 100	5 607 121	4 408 102	
7:31 - 8:00	3 540 180	5 780 156	4 680 170	
8:01 - 8:30	6 1080 180	6 1040 173	8 912 114	
8:31 - 9:00	1 180 180	9 1220 136	7 1004 143	
Subtotal	17-2598-147	25-3647-146	23-3004-131	
9:01 - 9:30	2 347 174	9 347 38	8 378 47	
9:31 - 10:00	8 1085 109	6 235 39	5 389 78	
10:01 - 10:30	11 1466 133	9 378 42	6 210 35	
10:31 - 11:00	4 259 65	6 211 35	2 130 65	
11:01 - 11:30	5 226 45	5 413 83	8 525 72	
11:31 - 12:00	7 430 61	6 341 57	6 284 48	
12:01 - 12:30	4 283 71	6 512 85	5 454 85	
12:31 - 1:00	6 474 79	4 332 25	6 527 88	
1:01 - 1:30	5 310 62	7 523 30	6 355 59	
1:31 - 2:00	6 393 66	5 315 63	7 698 100	
2:01 - 2:30	6 973 162	5 251 50	3 247 82	
2:31 - 3:00	6 309 52	4 444 111	8 525 66	
3:01 - 3:30	6 284 47	5 423 87	5 316 63	
3:31 - 4:00	4 437 109	3 447 139	7 453 65	
Subtotal	80 7276 91	80-5798-65	83-5511-66	
4:01 - 4:30	7 793 113	6 471 79	7 764 109	
4:31 - 4:45	2 360 180	2 345 173	4 258 64	
4:46 - 5:00	2 360 180	4 655 164	2 328 164	
5:01 - 5:15	2 360 180	5 425 85	3 455 152	
5:16 - 5:30	1 180 180		5 860 172	
5:31 - 5:45	2 360 180	5 730 146	3 387 129	
5:46 - 6:00	4 608 152	4 616 154	6 716 119	
Subtotal	20 3021 151	26-3242-125	30-3768-126	
6:01 - 6:30	5 730 146	4 616 154	7 907 129	
6:31 - 7:00	5 579 116	7 744 106	5 686 137	
7:01 - 7:30	4 349 87	4 445 111	4 485 121	
7:31 - 8:00	4 478 120	4 447 112	4 162 41	
8:01 - 8:30	2 220 110	3 161 54	2 180 90	
8:31 - 9:00	3 316 105	5 365 73	3 178 59	
9:01 - 9:30	5 474 95	4 374 94	4 215 54	
9:31 - 10:00	3 263 88	2 178 89	4 175 44	
10:01 - 10:30	3 250 83	5 429 86	3 210 70	
10:31 - 11:00	3 224 75	4 333 83	4 217 54	
11:01 - 11:30	4 390 97	3 215 72	1 30 30	
11:31 - 12:00	2 260 130	3 239 80		
12:01 - 1:00	3 257 86	4 346 87		
Subtotal	147-4826-103	53-4772-94	41-3475-84	
Total	169-18061-107	192-17352-93	186-16465-89	



LOCATION: *Arlington St. Sta.*  
 ROUTE: # *850* *Sechmere Sta.*

*D* *City*

YEAR: *83*

*Quiverside Sta.*

OUTBOUND	DATE: <i>Tues. Jan. 11</i>	DATE: <i>Tues. April 26</i>	DATE:	DATE:
A.M.	WEATHER: <i>Cloudy</i>	WEATHER: <i>Cloudy</i>	WEATHER:	WEATHER:
TIME:	V Tot. Pass. Aver. Std. Cap. O/U	V Tot. Pass. Aver. Std. Cap. O/U	V Tot. Pass. Aver. Std. Cap. O/U	V Tot. Pass. Aver. Std. Cap. O/U
5:00 - 5:00	2 47 29	1 68 68		
6:01 - 6:30	1 142 142	2 152 76		
6:31 - 7:00	2 200 100	1 131 131		
Subtotal	5 389 78	4 351 88		
7:01 - 7:20	2 234 117	4 417 104		
7:31 - 8:00	2 350 175	2 360 180		
8:01 - 8:30	4 580 145	8 1168 144		
8:31 - 9:00	9 537 60	9 1324 147		
Subtotal	17 1701 100	23 3269 142		
9:01 - 9:30	9 399 44	7 591 84		
9:31 - 10:00	5 176 35	5 357 71		
10:01 - 10:30	8 186 23	8 466 58		
10:31 - 11:00	6 179 30	7 357 71		
11:01 - 11:30	5 179 36	4 204 51		
11:31 - 12:00	5 189 38	6 320 53		
12:01 - 12:30	4 159 40	7 509 73		
12:31 - 1:00	6 312 52	5 401 80		
1:01 - 1:30	6 349 58	5 338 66		
1:31 - 2:00	5 460 92	5 445 89		
2:01 - 2:30	7 250 36	5 381 76		
2:31 - 3:00	1 180 180	5 423 85		
3:01 - 3:30	6 461 76	6 458 76		
3:31 - 4:00	8 605 76	9 865 96		
Subtotal	81 4084 50	84 6105 73		
4:01 - 4:30	7 624 89	6 671 112		
4:31 - 4:45	8 944 118	3 193 64		
4:46 - 5:00	3 310 103	5 536 107		
5:01 - 5:15	5 550 110	4 601 150		
5:16 - 5:30	4 200 175	3 502 151		
5:31 - 5:45	4 531 135	5 591 118		
5:46 - 6:00	6 501 83	4 355 89		
Subtotal	37 4160 113	30 3449 115		
6:01 - 6:30	8 659 82	6 573 97		
6:31 - 7:00	8 424 53	5 294 59		
7:01 - 7:30	8 498 62	5 508 102		
7:31 - 8:00	7 461 66	7 391 56		
8:01 - 8:30	3 385 128	7 353 50		
8:31 - 9:00	3 194 65	3 146 49		
9:01 - 9:30	4 285 71	3 313 104		
9:31 - 10:00	5 356 51	3 167 56		
10:01 - 10:30	3 158 53	2 94 37		
10:31 - 11:00	3 145 48	4 206 52		
11:01 - 11:30	3 149 50	3 162 54		
11:31 - 12:00	3 108 36	3 126 42		
12:01 - 1:00	6 213 36	6 151 25		
Subtotal	64 3935 61	67 3521 60		
Total	145 8269 70	200 16695 83		



## PLANS AND SCHEDULES DEPARTMENT SUMMARY OF TRAFFIC COUNTS

LOCATION:

ROUTE: 850

YEAR: 87

INBOUND						DATE: <u>Fri. Sept 30</u>						DATE: <u>Mon. Oct. 3</u>						DATE:					
A.M.						WEATHER: <u>Pt. cldy.</u>						WEATHER: <u>Fair</u>						WEATHER:					
TIME:	V	Tot. Pass.	Aver.	Std. Cap.	O/U	V	Tot. Pass.	Aver.	Std. Cap.	O/U	V	Tot. Pass.	Aver.	Std. Cap.	O/U	V	Tot. Pass.	Aver.	Std. Cap.	O/U			
5:00 - 6:00	7	32	5																				
6:01 - 6:30	6	75	13																				
6:31 - 6:45	5	57	11																				
6:46 - 7:00	3	42	14																				
Subtotal	21	206	10																				
7:01 - 7:15	2	22	11																				
7:16 - 7:30	3	97	32																				
7:31 - 7:45	4	73	18																				
7:46 - 8:00	2	32	16																				
8:01 - 8:15	1	14	16																				
8:16 - 8:30	6	85	14																				
8:31 - 8:45	4	39	10																				
8:46 - 9:00	2	51	26																				
Subtotal	24	415	17																				
9:01 - 9:30	5	48	10																				
9:31 - 10:00	10	60	6																				
10:01 - 10:30	6	35	6																				
10:31 - 11:00	4	29	7																				
11:01 - 11:30	6	32	5																				
11:31 - 12:00	7	53	8																				
12:01 - 12:30	6	90	15																				
12:31 - 1:00	4	69	17																				
1:01 - 1:30	3	22	74																				
1:31 - 2:00	2	104	52			6	197	33															
2:01 - 2:30						5	183	37															
2:31 - 3:00						4	227	32															
3:01 - 3:30						5	201	40															
3:31 - 4:00						5	379	76															
Subtotal	53	742	14			28	1187	42															
4:01 - 4:30						6	360	60															
4:31 - 5:00						5	440	88															
5:01 - 5:30						8	624	78															
5:31 - 6:00						4	325	81															
Subtotal						23	1749	76															
6:01 - 6:30						9	412	46															
6:31 - 7:00						4	151	38															
7:01 - 7:30						7	120	17															
7:31 - 8:00						5	96	19															
8:01 - 8:30						5	64	13															
8:31 - 9:00						5	80	16															
9:01 - 9:30						2	80	40															
9:31 - 10:00						5	81	16															
10:01 - 10:30																							
10:31 - 11:00																							
11:01 - 11:30																							
11:31 - 12:00																							
12:01 - 1:00																							
Subtotal						42	1084	26															
Total	98	1363	14			93	4020	43															

# Orange Line

## PLANS AND SCHEDULES DEPARTMENT

### SUMMARY OF TRAFFIC COUNTS

LOCATION: *North Station R.T.L.*

YEAR: 84

ROUTE:

*Forest Hills Station - Oak Grove Station*

OUTBOUND	DATE: <i>Tues. Jan. 10</i>	DATE: <i>Thurs. Feb. 2</i>	DATE: <i>Fri. May 18</i>	DATE: <i>Tues. June 19</i>
A.M.	WEATHER: <i>Cloudy</i>	WEATHER: <i>Fair</i>	WEATHER: <i>Cloudy</i>	WEATHER: <i>Cloudy</i>
TIME:	V Tot. Pass. Aver. Std. Cap. O/U	V Tot. Pass. Aver. Std. Cap. O/U	V Tot. Pass. Aver. Std. Cap. O/U	V Tot. Pass. Aver. Std. Cap. O/U
5:00 - 6:00			6 195 33	
6:01 - 6:30	10 256 26		10 302 30	
6:31 - 7:00	16 705 44		12 462 39	
Subtotal	26 961 37		28 959 34	
7:01 - 7:30	20 613 31		20 619 31	
7:31 - 8:00	28 1113 40		32 780 24	
8:01 - 8:30	32 705 22		24 286 12	
8:31 - 9:00	32 675 21		24 528 22	
Subtotal	112 3116 28		100 2213 22	
9:01 - 9:30	22 215 7		32 409 13	
9:31 - 10:00	16 119 7		32 204 6	
10:01 - 10:30	20 189 9		20 599 30	
10:31 - 11:00	16 196 12		24 326 14	
11:01 - 11:30	16 233 15		8 466 58	
11:31 - 12:00	16 190 12		32 816 25	
12:01 - 12:30	16 246 15		12 669 56	
12:31 - 1:00	16 245 22		16 459 29	
1:01 - 1:30	16 245 28		16 522 35	
1:31 - 2:00	12 230 23		20 523 25	
2:01 - 2:30	20 478 24		16 477 30	12 465 39
2:31 - 3:00	16 446 28		16 845 53	16 715 45
3:01 - 3:30	16 672 42	8 437 55	16 1455 91	16 1025 68
3:31 - 4:00	16 1371 86	20 1841 92	16 3070 129	20 2200 110
Subtotal	244 5425 23	28 2278-81	276-9810-36	64 14475-70
4:01 - 4:30	20 1822 91	32 2512 79	36 3408 95	36 2815 78
4:31 - 4:45	16 1943 121	16 1716 107	20 2020 101	20 2770 137
4:46 - 5:00	12 2410 201	12 2085 175	12 1840 153	12 2110 176
5:01 - 5:15	16 3906 244	20 3580 179	20 3320 170	16 2880 180
5:16 - 5:30	16 2572 161	16 2038 127	16 1300 81	16 2545 159
5:31 - 5:45	16 7678 105	20 1753 88	20 1306 65	16 1820 118
5:46 - 6:00	16 698 44	20 1298 65	20 1084 54	20 1880 94
Subtotal	112-15029-134	136-14992-110	144-14348-100	126-16840-124
6:01 - 6:30	20 585 29		20 1024 51	24 1025 43
6:31 - 7:00	16 491 31		24 742 31	
7:01 - 7:30	16 448 29		12 308 26	
7:31 - 8:00	8 313 39		6 591 99	
8:01 - 8:30	16 186 12		4 232 58	
8:31 - 9:00	12 298 25		6 296 49	
9:01 - 9:30	8 123 15		4 173 43	
9:31 - 10:00	12 108 9		4 145 36	
10:01 - 10:30	8 48 6			
10:31 - 11:00				
11:01 - 11:30				
11:31 - 12:00				
12:01 - 1:00				
Subtotal	116-1105-22		80-3511-44	24-1025-43
Total	310-27131-44	164-17270-105	628-30891-49	220-22320-95



*Orange Line*  
PLANS AND SCHEDULES DEPARTMENT  
SUMMARY OF TRAFFIC COUNTS

LOCATION: *Essex Street Station*YEAR: *84*ROUTE: *Oak Grove Station - Forest Hills Station*

OUTBOUND	DATE: <i>Thurs Jan 12</i>	DATE: <i>Thurs 6-19-84</i>	DATE: <i>Fri July 13</i>	DATE:
A.M.	WEATHER: <i>Cloudy</i>	WEATHER: <i>RAIN</i>	WEATHER: <i>Pr. C/dy</i>	WEATHER:
TIME:	V Tot. Pass. Aver. Std. Cap. O/U	V Tot. Pass. Aver. Std. Cap. O/U	V Tot. Pass. Aver. Std. Cap. O/U	V Tot. Pass. Aver. Std. Cap. O/U
5:00 - 6:00			8 34 7	
6:01 - 6:30	12 79 7		12 177 15	
6:31 - 7:00	24 397 17		24 357 15	
Subtotal	36 476 13		44 588 13	
7:01 - 7:30	28 478 14		28 345 12	
7:31 - 8:00	32 735 23		32 689 22	
8:01 - 8:30	32 599 16		32 253 24	
8:31 - 9:00	24 505 21		32 694 22	
Subtotal	116 2317 20		124 2481 20	
9:01 - 9:30	24 309 13		20 352 18	
9:31 - 10:00	8 442 55		16 315 20	
10:01 - 10:30	20 488 24		16 295 18	
10:31 - 11:00	24 434 18		12 305 25	
11:01 - 11:30	20 546 27		12 330 28	
11:31 - 12:00	12 512 43		16 355 22	
12:01 - 12:30	4 134 34		16 320 20	
12:31 - 1:00			16 405 25	
1:01 - 1:30	12 578 48		16 431 26	
1:31 - 2:00	4 880 220		16 585 37	
2:01 - 2:30	8 1215 152	12 698 59	16 815 51	
2:31 - 3:00	16 782 49	16 1200 75	12 620 52	
3:01 - 3:30	16 1209 76	16 1125 71	16 1145 72	
3:31 - 4:00	24 1191 49	24 1515 64	28 2160 77	
Subtotal	192 8720 45	68 4538 67	228 8423 37	
4:01 - 4:30	12 1372 114	36 2190 61	28 2970 106	
4:31 - 4:45		16 1055 66	12 855 71	
4:46 - 5:00		20 1475 74	16 1420 89	
5:01 - 5:15		20 1615 81	12 1490 124	
5:16 - 5:30	8 1760 220	12 1230 103	24 2918 124	
5:31 - 5:45	12 2640 220	16 1380 87	12 1170 99	
5:46 - 6:00	16 1993 125	16 850 54	16 1175 73	
Subtotal	48 7765 162	126 9795 73	120 1198 100	
6:01 - 6:30	20 1049 52	24 1445 61	24 1230 51	
6:31 - 7:00	16 533 33		8 380 48	
7:01 - 7:30	12 497 41		8 765 96	
7:31 - 8:00	12 430 36		16 450 28	
8:01 - 8:30	12 322 27		6 302 50	
8:31 - 9:00	8 235 29		6 263 44	
9:01 - 9:30	8 182 23		6 275 46	
9:31 - 10:00	12 246 21		2 72 36	
10:01 - 10:30	8 117 15			
10:31 - 11:00				
11:01 - 11:30				
11:31 - 12:00				
12:01 - 1:00				
Subtotal	108 3601 33	24 1445 61	76 3737 49	
Total	500 22879 46	228 15778 70	592 27227 46	

# Blue Line

## PLANS AND SCHEDULES DEPARTMENT

### SUMMARY OF TRAFFIC COUNTS

LOCATION: *Aquarium Station R.T.L.*

YEAR: 84

ROUTE: *Bowdoin Station - Wonderland Station*

OUTBOUND	DATE: <i>Wed. Jan. 11</i>	DATE: <i>Thurs. Jan. 12</i>	DATE: <i>Thurs. May 17</i>	DATE:
A.M.	WEATHER: <i>Fair</i>	WEATHER: <i>Fair</i>	WEATHER: <i>Cloudy</i>	WEATHER:
TIME:	V Tot. Pass. Aver. Std. Cap. O/U	V Tot. Pass. Aver. Std. Cap. O/U	V Tot. Pass. Aver. Std. Cap. O/U	V Tot. Pass. Aver. Std. Cap. O/U
5:00 - 6:00				
6:01 - 6:30		12 64 5		
6:31 - 7:00		28 241 9		
Subtotal		40 305 8		
7:01 - 7:30		24 416 17		
7:31 - 8:00		40 422 11		
8:01 - 8:30		20 597 30		
8:31 - 9:00		32 383 12		
Subtotal		116 1818 16		
9:01 - 9:30		28 290 10		
9:31 - 10:00		12 164 14		
10:01 - 10:30		16 174 11		
10:31 - 11:00		16 247 15		
11:01 - 11:30		16 322 20		
11:31 - 12:00		16 348 22		
12:01 - 12:30		16 306 19		
12:31 - 1:00		12 283 24		
1:01 - 1:30		16 386 24		
1:31 - 2:00		16 372 24	16 806 50	
2:01 - 2:30	12 331 28		16 744 47	
2:31 - 3:00	12 423 35		16 1820 114	
3:01 - 3:30	16 250 47		16 1420 89	
3:31 - 4:00	16 628 39		20 1474 74	
Subtotal	56 2132 38	164 2892 18	84 6264 75	
4:01 - 4:30	32 1659 52		32 2046 64	
4:31 - 4:45	16 1231 77		24 2429 101	
4:46 - 5:00	16 1083 68		16 1644 103	
5:01 - 5:15	12 1740 145		20 1928 96	
5:16 - 5:30	20 1538 77		16 1446 90	
5:31 - 5:45	20 1262 63		24 1380 58	
5:46 - 6:00	16 548 34		12 425 40	
Subtotal	132 7061 69		144 11348 78	
6:01 - 6:30	16 803 50		20 975 49	
6:31 - 7:00	16 460 29		10 680 68	
7:01 - 7:30	20 625 31		8 565 64	
7:31 - 8:00	12 337 28		8 385 48	
8:01 - 8:30	12 338 28		8 325 44	
8:31 - 9:00	8 235 29		6 230 38	
9:01 - 9:30	8 224 28		6 265 44	
9:31 - 10:00	8 277 35		2 60 30	
10:01 - 10:30	8 216 27			
10:31 - 11:00				
11:01 - 11:30				
11:31 - 12:00				
12:01 - 1:00				
Subtotal	108 3515 33		68 3435 51	
Total	296 14708 50	320 5015 16	286 21047 71	

COMMUTER RAIL RIDERSHIP





P. M. RUSH-HOUR PERFORMANCE  
PEAK

NORTH SERVICE

LINE	TRAIN	DESTIN.	LV. BOSTON	SCHLD. ARR.	No Cars	Average Ridingship	CAUSE/REMARKS
Eastern	231	IPS	1630	1725	4	300	
	533	RKPT	1700	1812	5	500	
	235	IPS	1710	1806	5	400	
	537	RKPT	1725	1838	3	350	
	239	IPS	1735	1830	3	330	
	541	RKPT	1800	1916	3	260	
Reading	819	RDG	1600	1627	4	150	
	121	HVRHL	1630	1736	3	250	
	823	RGD	1655	1722	4	275	
	125	HVRHL	1715	1820	4	500	
	827	RDG	1725	1752	5	265	
New Hamp.	323	LWL	1605	1644	2	150	
	925	WIN	1625	1640	3	75	
	327	LWL	1700	1739	4	420	
	929	WIN	1715	1730	2	150	
	331	LWL	1730	1810	3	255	
	933	WIN	1745	1800	2	90	
Gard./ Fitch.	609	S.ACT.	1600	1652	2	130	
	457	FITCH	1650	1818	4	350	
	611	S.ACT.	171	1801	3	165	
	413	GARD	1730	1916	3	400	

SOUTH SERVICE

Fram.	5361	FRAM.	1630	1710	4	330	
	5363	FRAM.	1655	1744	4	550	
	5369	FRAM.	1720	1810	6	575	
	5373	FRAM.	1745	1834	3	360	
Franklin	7159	FKLN.	1602	1652	5	400	
	7363	NOR.CTL.	1649	1719	5	450	
	7165	FKLN.	1707	1751	6	525	
	7169	FRKLN.	1725	1821	8	560	
Shore	8359	CANT.JCT.	1615	1639	8	320	
	8161	ATTIL.	1641	1729	7	630	
	8167	ATTIL.	1711	1755	7	725	
	8369	CANT.JCT.	1720	1742	6	440	
	8173	ATTIL.	1741	1825	5	525	
Stoughton	8963	STGN.	1645	1716	4	370	
	8967	STGN.	1715	1748	6	475	
	8973	STGN.	1745	1820	5	325	



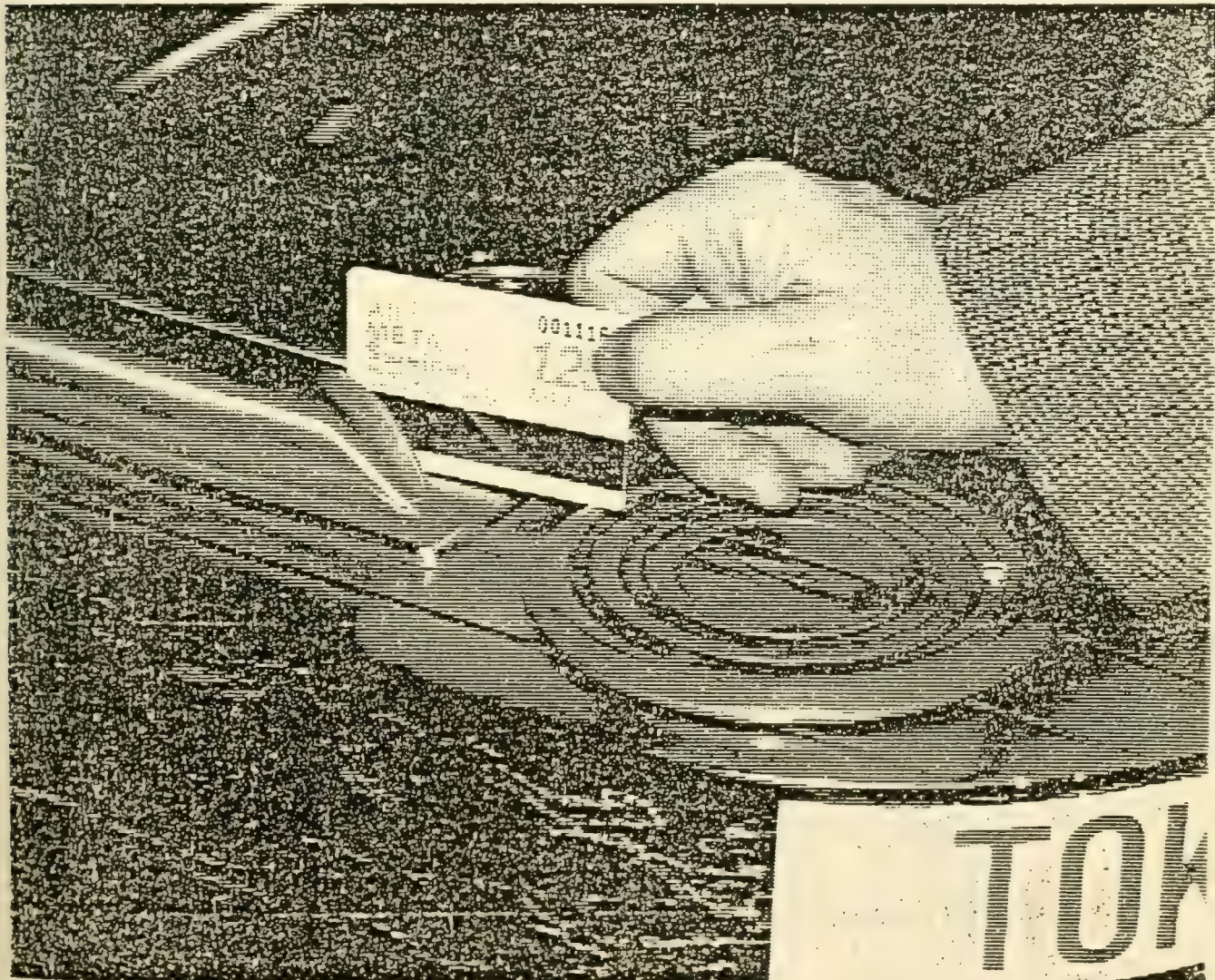
## RAPID TRANSIT CAPACITY





# Final Environmental and Socioeconomic Impact Report The M.B.T.A. Fare Increase

## Appendices



RED LINE "HYBRID" CAR

A) # SEATS/CAR	<u>58</u>		
B) STANDEE SPACE	<u>324 sq. ft.</u>		
C) STANDEE CAPACITY			
Normal load	<u>129</u>	Crush load	<u>186</u>
@ 2.5 sq. ft.		@ 1.75 sq. ft.	
D) TOTAL PASSENGERS/CAR			
Normal load	<u>187</u>	Crush load	<u>244</u>
E) TRAIN CAPACITY			
@ existing 4 cars		@ potential 6 cars	
Normal load	<u>748</u>	Normal load	<u>1,122</u>
Crush load	<u>976</u>	Crush load	<u>1,464</u>

ACTIVE FLEET 164

PEAK REQ'T 114 (26F + 2 Five)

ALLOWED TRIP TIME 78 minutes

CONSTRAINT (15% of Active Fleet) 140 (35F)

<u>TRAIN FREQUENCY</u>	<u>ACTUAL</u>	<u>POTENTIAL</u>	<u>DESIGN</u>	<u>CONSTRAINT (with current fleet)</u>	
				<u>4 cars/train</u>	<u>6 cars/train</u>
headway (minutes)	3.0	2.0	1.5	2.2	3.4
# trains/hour	20	30	40	27	18
effective capacity	.85	.78	.71	.80	.87

	<u>NORMAL LOAD</u>		<u>CRUSH LOAD</u>	
	<u>@ 4 Cars</u>	<u>@ 6 Cars</u>	<u>@ 4 Cars</u>	<u>@ 6 Cars</u>
ACTUAL	12,716	19,074	16,592	24,888
POTENTIAL	17,503	26,255	22,838	34,258
DESIGN	21,243	31,865	27,718	41,578
CONSTRAINT	16,157	19,571	21,082	22,926

ABSOLUTE THEORETICAL CAPACITY

	<u>NORMAL LOAD</u>		<u>CRUSH LOAD</u>	
	<u>@ 4 Cars</u>	<u>@ 6 Cars</u>	<u>@ 4 Cars</u>	<u>@ 6 Cars</u>
	29,920	44,880	39,040	58,560

CURRENT ESTIMATED PEAK HOUR VOLUME 15,000 (3/82)

ORANGE LINE

#2 MAIN

A) # SEATS/CAR	<u>58</u>		
B) STANDEE SPACE	<u>243 sq. ft.</u>		
C) STANDEE CAPACITY			
Normal load	<u>97</u>	Crush load	<u>139</u>
@ 2.5 sq. ft.		@ 1.75 sq. ft.	
D) TOTAL PASSENGERS/CAR			
Normal load	<u>155</u>	Crush load	<u>197</u>
E) TRAIN CAPACITY			
@ existing 4 cars		@ potential 6 cars	
Normal load	<u>620</u>	Normal load	<u>930</u>
Crush load	<u>788</u>	Crush load	<u>1,192</u>

ACTIVE FLEET 120 PEAK REQ'T 68 (17F)

ALLOWED TRIP TIME 77 minutes

CONSTRAINT (15% of Active Fleet) 102 (25F)

<u>TRAIN FREQUENCY</u>	<u>ACTUAL</u>	<u>POTENTIAL</u>	<u>DESIGN</u>	<u>CONSTRAINT (with current fleet)</u>	
				<u>4 cars/train</u>	<u>6 cars/train</u>
headway (minutes)	4.5	2.0	1.5	3.1	4.5
# trains/hour	13	30	40	19	13
effective capacity	.89	.78	.71	.85	.89

	<u>NORMAL LOAD</u>		<u>CRUSH LOAD</u>	
	<u>@ 4 Cars</u>	<u>@ 6 Cars</u>	<u>@ 4 Cars</u>	<u>@ 6 Cars</u>
ACTUAL	7,173	10,760	9,117	13,676
POTENTIAL	14,508	21,762	18,439	27,659
DESIGN	17,608	26,412	22,379	33,569
CONSTRAINT	10,013	12,726	10,760	13,676

ABSOLUTE THEORETICAL CAPACITY

	<u>NORMAL LOAD</u>		<u>CRUSH LOAD</u>	
	<u>@ 4 Cars</u>	<u>@ 6 Cars</u>	<u>@ 4 Cars</u>	<u>@ 6 Cars</u>
	24,800	37,200	31,520	47,280

CURRENT ESTIMATED PEAK HOUR VOLUME 7,000 (3/82)



BLUE LINE  
#4 EAST BOSTON

A) # SEATS/CAR 42

B) STANDEE SPACE 170 sq. ft.

C) STANDEE CAPACITY

Normal load                    68  
@ 2.5 sq. ft.

Crush load 97  
@ 1.75 sq.  
ft.

D) TOTAL PASSENGERS/CAR

Normal load 110

Crush load 139

E) TRAIN CAPACITY 4 CARS

Normal load      440

Crush load	556
------------	-----

ACTIVE FLEET 70

PEAK REQ'T 40 (10F)

ALLOWED TRIP TIME 45 minutes

CONSTRAINT (15% of Active Fleet) 60 (15F)

<u>TRAIN FREQUENCY</u>	<u>ACTUAL</u>	<u>POTENTIAL</u>	<u>SIGNAL DESIGN</u>	<u>CONSTRAINT (with current fleet)</u>
headway (minutes)	4.5	2.0	1.5	3.5
# trains/hour	13	30	40	20
effective capacity	.80	.78	.71	.85

	<u>NORMAL LOAD</u>	<u>CRUSH LOAD</u>
ACTUAL	5,091	6,432
POTENTIAL	10,296	13,010
DESIGN	12,496	15,790
CONSTRAINT	7,480	9,452

ABSOLUTE THEORETICAL CAPACITY  
(@ 4 Cars)

<u>NORMAL LOAD</u>	<u>CRUSH LOAD</u>
17,600	22,239

CURRENT ESTIMATED PEAK HOUR VOLUME 6,000 (3/82)

GREEN LINE "HYBRID" CAR

A) # SEATS/CAR 42 PCC/52 LRV

B) STANDEE SPACE 148 sq. ft. PCC/284 sq. ft. LRV

C) STANDEE CAPACITY  
 Normal load 59 PCC/113 LRV Crush load 84 PCC/162 LRV  
 @ 2.5 sq. ft. @ 1.75 sq. ft.

D) TOTAL PASSENGERS CAR  
 Normal load 101 PCC/165 LRV Crush load 126 PCC/214 LRV

E) TRAIN CAPACITY  
 3 existing (Hybrid of 1 LRV/2 PCC) 3 potential (Hybrid of 2 LRV/3 PCC)  
 Normal load 174 Normal load 363  
 Crush load 223 Crush load 449

ACTIVE FLEET 196 PEAK REQ'T 120

ALLOWED TRIP TIME 38

CONSTRAINT (15% of Active Fleet) 167(34T + 99S)

TRAIN FREQUENCY	ACTUAL	POTENTIAL <sup>1</sup>	CONSTRAINT	POTENTIAL <sup>2</sup> HYBRID	$\frac{3 \text{ car PCC}}{2 \text{ car LRV}}$
headway (seconds)	55	30	40	73	
# trains/hour	65	120	90	49	
effective capacity	.55	.25	.42	.65	

	NORMAL LOAD		CRUSH LOAD	
	Existing	Potential	Existing	Potential
ACTUAL	6,221	12,977	7,972	16,052
POTENTIAL	5,220	10,890	6,690	13,470
CONSTRAINT	6,577	11,562	8,429	14,300

ABSOLUTE THEORETICAL CAPACITY

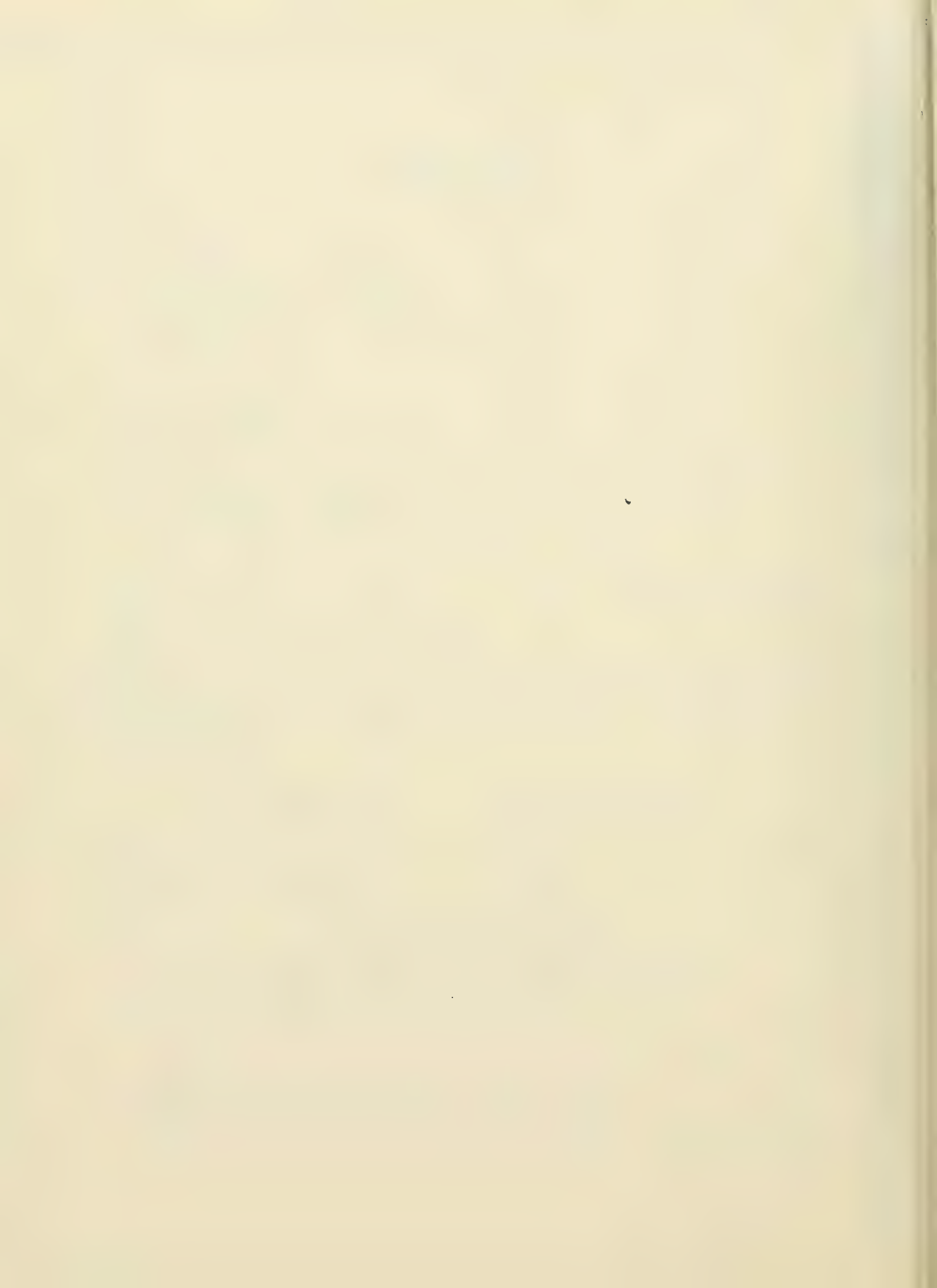
	NORMAL LOAD		CRUSH LOAD	
	Existing	Potential	Existing	Potential
	20,880	43,560	26,760	53,880

CURRENT ESTIMATED PEAK HOUR VOLUME 7,000

<sup>1</sup> Potential for currently used cars calculated by creating a "hybrid vehicle" and weighting an average for a 2 car PCC and 1 car LRV.

<sup>2</sup> Potential hybrid car train for future use has a capacity based on weighted average of 3 PCCs and 2 LRVs.





EXCERPTS FROM PREVIOUS REPORTS



### 3.2 LAND USE

"THIRD HARBOR TUNNEL, INTERSTATE 90/CENTRAL  
ARTERY, INTERSTATE 93" SUPPLEMENT TO THE  
DRAFT ENVIRONMENTAL IMPACT STATEMENT/REPORT  
DATED JUNE, 1983

The MBTA also operates a major surface bus terminal at Haymarket Station. Several bus routes serving the North Shore and utilizing the Sumner and Callahan Tunnels were described in the DEIS/DEIR. Numerous other routes also serve Haymarket Station. Bus Routes 92, 93, and 111 use local streets through Charlestown and City Square to arrive at the Haymarket terminal or downtown Boston destinations. Bus Routes 325, 326, 353, 354, and 426 enter Boston via Interstate Route 93 on the Mystic-Tobin Bridge and use the Haymarket exit from the Central Artery to enter the Haymarket terminal or continue to other downtown destinations. Bus Route 350 enters Boston via the Longfellow Bridge.

Private carrier bus routes operated through the study area include longer-distance routes serving communities in northeast Massachusetts, New Hampshire, Maine, and Vermont. These services are provided by Greyhound, Trailways, and Trombly Motor Coach, among others.

The MBTA also operates an extensive commuter rail system to the north and west of Boston from North Station. Five routes are currently operated, with their respective termini being located in Rockport, Ipswich, Haverhill, Lowell, and Gardner. All routes operate seven days per week with reduced service on Saturdays and Sundays. Amtrak trains depart from South Station throughout the day for points along the Northeast Corridor as far as Washington, DC, and to Chicago, Illinois.

### 3.2 LAND USE

This section briefly describes land use in the following districts: South Boston/Fort Point Channel; the Financial District; the Waterfront; Government Center; the North End; North Station; the West End; and Charlestown. These districts are shown on Figure 79. More detailed information on these areas is contained in the supplemental report on Land Use, Community Facilities and

Economic Activities prepared as part of this Supplemental DEIS/DEIR. These areas comprise the areas of potential additional effect of Alternatives 3A, 5A, 5A Modified, and 6 as compared to the No-Build Alternative and Alternatives 3 and 5 in the DEIS/DEIR. Major land uses in each area are listed in Table 59, are presented on Figures 80 and 81, and are described in the following subsections.

The DEIS/DEIR (Section 3.2) contains descriptions of land use in the remaining districts of the project area, including the South End, the residential portion of South Boston, the Industrial Triangle, the Leather District, Chinatown/South Cove, East Boston, Logan Airport, and Route 1A North. For more detailed information on these areas, refer to Section 3.2 and the supplemental report, Land Use, Community Facilities, and Economic Activity Inventory, of the DEIS/DEIR.

#### 3.2.1 Overview

The project area contains a diversity of land uses. The Financial District, Government Center and North Station areas house public and private offices, commercial and retail activities, transportation uses and entertainment facilities; these areas have very small residential populations.

Predominant activities in the South Boston/Fort Point Channel area are manufacturing, warehousing and food distribution activities. Vacant and underused parcels in this area will generate substantial mixed use development activity over the next decade.

The Waterfront has recently undergone a transformation from industry and warehousing, to high-priced residences and office space. Faneuil Hall Market Place and the New England Aquarium are significant tourist attractions.

The North End is a cohesive residential neighborhood, with a



Table 33

## MAJOR LAND USES IN THE PROJECT AREA

## SOUTH BOSTON (See Figure 1)

## Existing Uses

1. Peabody Place (condominiums)
2. Temporary housing for Navy
3. Small commercial buildings
4. 301 Congress Street (office)
5. Stone & Webster Engineering Corporation (office)
6. Neptune Lobster Company
7. Anthony's Pier & Restaurant, Pier Five
8. Pier Grill
9. Radio Lighter Company (office)
10. Fargo Building (U.S. Government)
11. The Clifton Company (industrial)
12. Manufacturing
13. Warehouse, industrial area
14. Lincoln Park
15. Boston Place and Window Glass
16. New England Railroad Center
17. Paul's Lobster Company, Boston
18. Bedford
19. Borden, Inc. (manufacturing)
20. Borden Company (manufacturing)
21. Boston Municipal
22. Boston Marine Industrial Park
23. Boston Marine Terminal
24. Boston Tea Party Ship Museum
25. Children's Museum
26. One Trip of Good Voyage Chapel
27. U.S. Post Office parking
28. South Boston Army Base

## Future Uses

29. Southern Avenue Bridge
30. Former Base Central Parcel (office)
31. Boston Wharf Preparation (office, residential)

33. 245-259 A Street (entire) studios
34. Commercial Pier, BOSCOM (Commercial)
35. Commercial Place (light industrial, offices)
36. Marine Marine Terminal

## FINANCIAL DISTRICT (See Figure 60)

## Existing Uses

1. Beaneville Tower (residential) (office)
2. Blue Cross Blue Shield Building (office)
3. 155 Federal Street (office)
4. Prudential Trust Building (office)
5. Railway's Bus Station
6. Systems Building (office)
7. Ruppert Street Garage
8. Western Union Building (office)
9. The Travelers' Building (office)
10. State Street Bank Building (office)
11. Madison Hotel
12. Merrimack Bank Building (office)
13. 100 Bank Building (office)
14. 100 Bank Building (office)
15. 100 Bank Building (office)
16. Grain Exchange (office)
17. Wharf Buildings (office)
18. 33 Broad Street (office)
19. One Liberty Square (office)
20. One Liberty Square (office)
21. One Post Office Square (office)
22. 33 State Street (office tower)
23. 40 State Street (office tower)
24. Downtown Crossing (Filene's, Jordan Marsh, Lafayette Place, etc.)
25. Shumet Bank Building (office)
26. Bank of Boston (office)
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10. John F. Kennedy Federal Building (office)
11. Boston Police Station, District A
12. Government Center Parking Garage
13. Mass. Dept. of Social Services State Service Center (Public Building and Lindemann Center)

## Future Uses

14. Parcel 7 (hotel, retail)
15. New Charbon/Warrenton Street parcel (future use unknown)

## PORTLAND (See Figure 80)

## Existing Uses

1. Cass Maria (elderly housing)
2. Thatcher Street Housing
3. McLaughlin Building
4. Concord Street
5. Salem, Manchester and connecting streets (retail and restaurants)
6. 27 North Washington Street (Commercial)
7. 13 North Washington Street
8. 13 North Washington Street
9. Old North Church and Museum
10. Paul Revere House
11. U.S. Food and Drug Administration
12. Coast Guard Support Center

## Future Uses

13. Waterfront Terrace (residential)

## PORT STATION (See Figure 80)

## Existing Uses

1. Boston Garden
2. Atlantic Building (office)
3. Atlantic Building (office)
4. Atlantic Building (office)

5. Massachusetts General Hospital
6. Boston City Hospital
7. Boston City Hospital
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59. Boston City Hospital
60. Boston City Hospital

## Future Uses

16. Charles River Park (retail and offices)

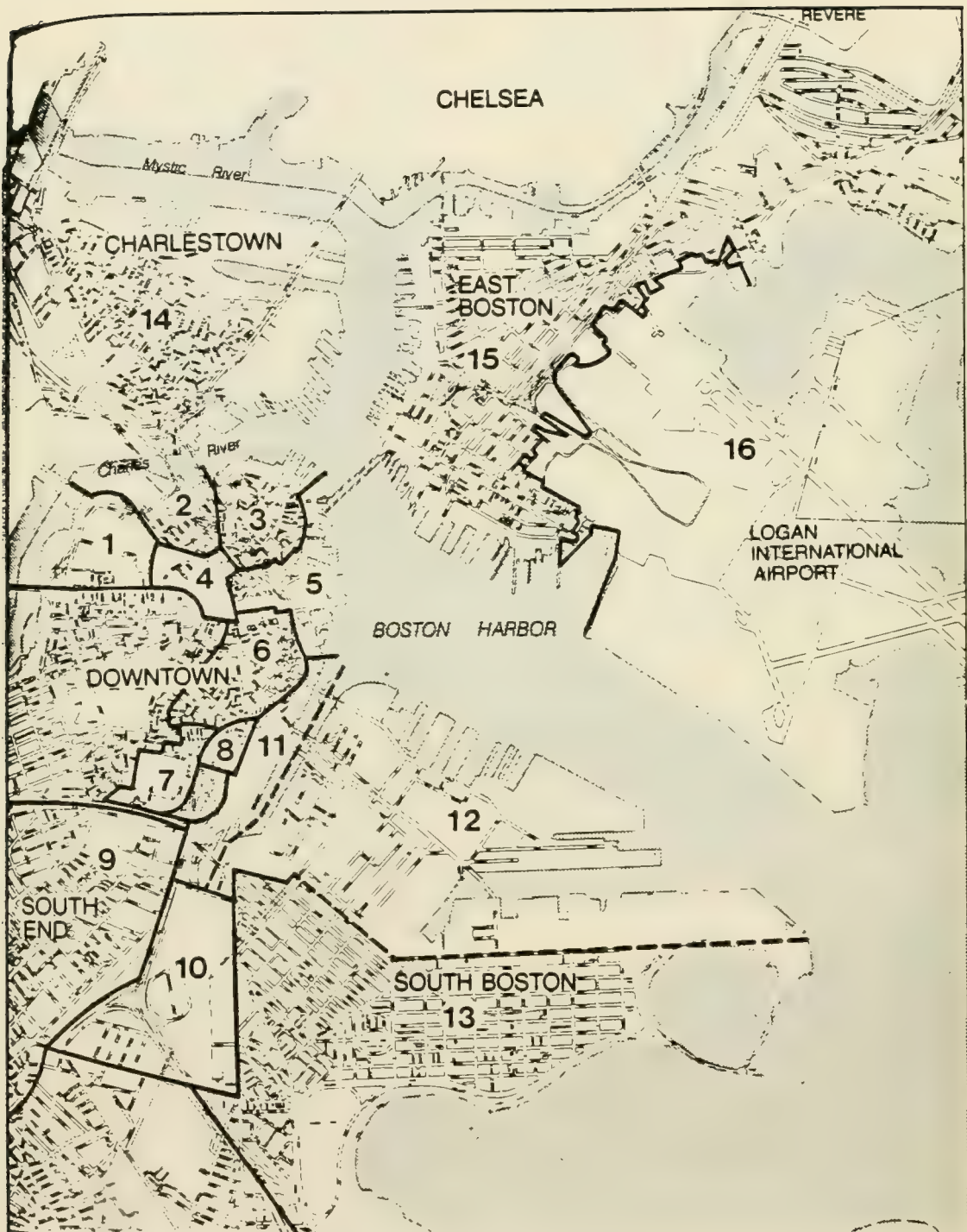
2. H.M. Paine Factory Store
3. Francis's Village
4. Joe's Auto Village
5. Brown, Bow and Company (Manufacturing)
6. New England Store Structures (Manufacturing)
7. Grand Square Building
8. Grand Square Building
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## Future Uses

21. MTA Substation
22. Parking Garage
23. Office Building
24. New Area
25. Retail development site, MTA
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28. Retail development site, MTA
29. Retail development site, MTA
30. Retail development site, MTA
31. Retail development site, MTA
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54. Retail development site, MTA
55. Retail development site, MTA
56. Retail development site, MTA
57. Retail development site, MTA
58. Retail development site, MTA
59. Retail development site, MTA
60. Retail development site, MTA

## Future Uses

1. Any Town House (elderly housing)
2. Charles River Park (residential)
3. The Stachems (elderly housing)
4. Any Town House (elderly housing)
5. Any Town House (elderly housing)
6. Any Town House (elderly housing)
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58. Any Town House (elderly housing)
59. Any Town House (elderly housing)
60. Any Town House (elderly housing)



- |                          |  |
|--------------------------|--|
| 1 - West End             | 9 - South End                                  |
| 2 - North Station        | 10 - Industrial Triangle                       |
| 3 - North End            | 11 - Fort Point Channel                        |
| 4 - Government Center    | 12 - S. Boston (Industrial)/Fort Point Channel |
| 5 - Waterfront           | 13 - S. Boston (Residential)                   |
| 6 - Financial District   | 14, 15, 16 - Identified on Map                 |
| 7 - Chinatown South Cove |  |
| 8 - Leather District     |  |

Figure 79  
Neighborhoods in the Project Area

0 900 1800 3200 Feet



EIS EIR for I-90—Third Harbor Tunnel I-93—Central Artery

Property of  
 DUNTON REDEVELOPMENT AUTHORITY

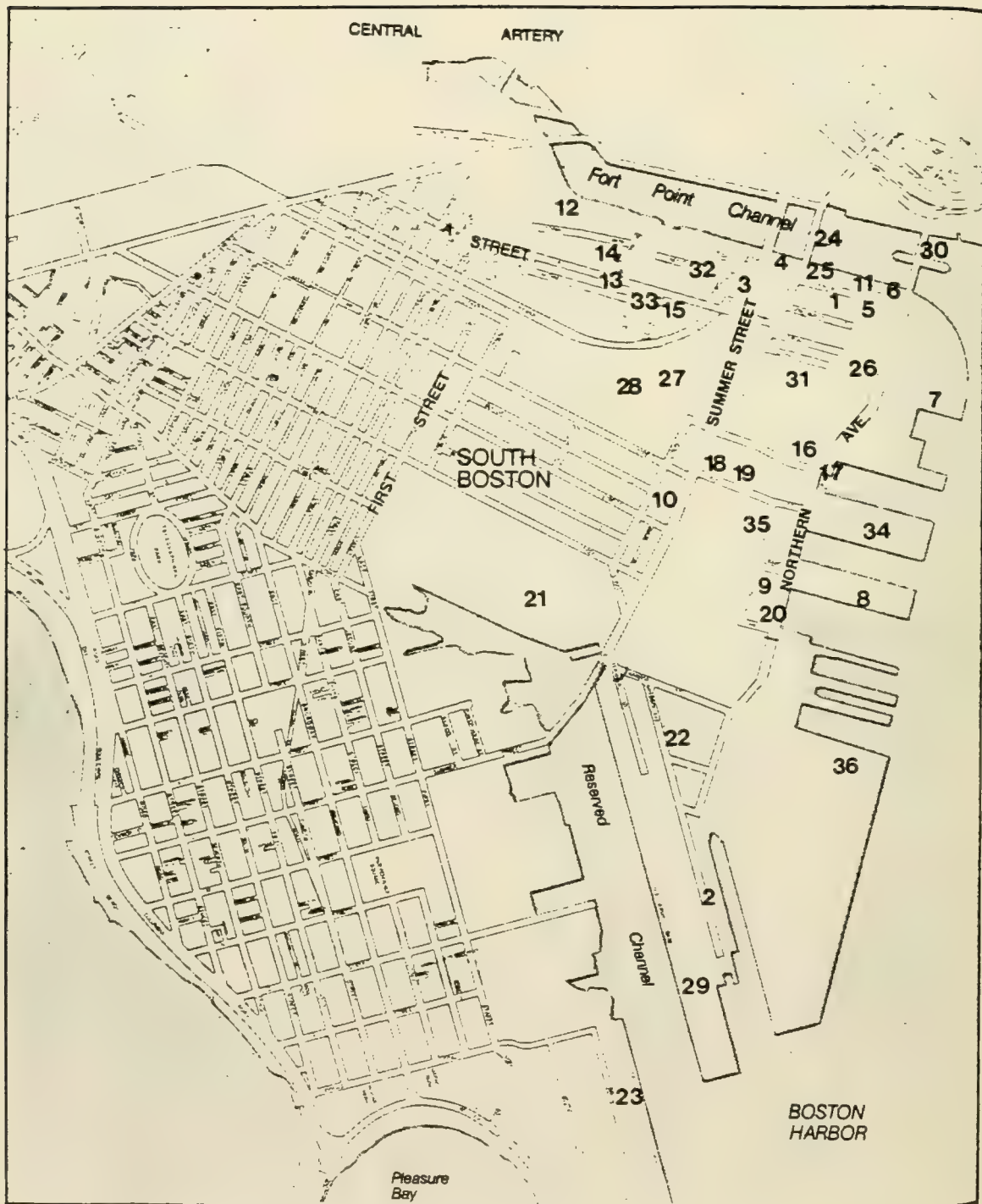
Figure 80  
 Major Land Uses

0 500 1000 Feet  
 ES/ER for 190 Third Harbor Tunnel 193 Central Artery

Legend  
 Land Use identified in Text  
 Neighborhood Boundaries







1 Land Uses Identified in Text

Figure 81  
Major Land Uses – South Boston

0 300 600 1200 Feet



EIS/EIR for I-90 – Third Harbor Tunnel; I-93 – Central Artery

strong Italian identity.

Non-residential uses are primarily ground floor retail establishments and restaurants which serve local and regional markets.

The West End houses Charles River Park, a large private apartment complex built in the 1960s and 1970s. The other major uses in this area are large health care facilities including the Massachusetts General Hospital.

The Central Artery is a significant land use component of downtown Boston. The structure of this highway in many instances defines the edges of neighborhoods, and land uses on either side of the Central Artery are quite different. In some cases the physical presence of the Artery has slowed changes which were encouraged by the city, for example, the development of the waterfront south of the Harbor Towers. In other areas, the Central Artery is perceived and commonly cited as protecting the character of an area where change is viewed ambiguously, for example, in the North End.

### 3.2.2 South Boston/Fort Point Channel

The inventory of land use prepared for the DEIS/DEIR treated South Boston and Fort Point Channel as two distinct areas. This Supplemental DEIS/DEIR includes a South Boston tunnel alignment (Alternative 5A) which runs across the southern part of the Fort Point Channel area and through the northern, industrial section of South Boston. For assessing the land use impacts of Alternative 5A, all of the area east of Fort Point Channel and north of First Street has been treated as one district (see Figure 81).

For those portions of South Boston and Fort Point Channel outside this new zone, the discussion of land use has been included in the DEIS/DEIR.

The South Boston/Fort Point Channel area is one of the most important districts for future residential, office, hotel and

industrial development in Boston.

Both renovation of existing structures and development of vacant sites is occurring. Although some development is taking place despite access problems, improvement of access within and to the area is a key ingredient to continued development interest.

As described in the DEIS/DEIR, the area immediately to the east of the Fort Point Channel contains a mix of land uses and is slowly changing from an industrial to a commercial and residential area. There are approximately 100 existing residences near Fort Point Channel; these include both developer-financed condominiums and artists' lofts. In addition there are many small businesses, including light industrial, commercial and office establishments in this area. The Gillette Company, a research and manufacturing firm with 3,200 employees, occupies a 21-acre site near the Fort Point Channel.

The Boston Wharf Company has substantial land holdings in this area and plans residential and office development. Stone & Webster Engineering Corporation is currently converting a warehouse structure into office space for 900 employees. Cabot, Cabot & Forbes plans to develop former Penn Central properties into a major office site. Piers 1-4, owned by Anthony Athanas, are the proposed site for 1.7 million square feet of offices, two hotels, residential development and a major marina.

Massport is a major land owner in South Boston. Plans for Massport property include a Computer Trade Center on Commonwealth Pier (BOSCOM) and nearby parcels; long-range plans for light industrial and office use on Commonwealth Flats; expansion of fish processing on the Fish Pier; and a container port at the Massport Marine Terminal, under lease from the Economic Development and Industrial Corporation of Boston (EDIC). The Boston Marine Industrial Park, a 101 acre area to the east of the Fish Pier (formerly the South Boston Naval Annex), is also under EDIC



jurisdiction, and contains industrial and marine-related uses. Across the Reserve Channel and to the east of Commonwealth Flats is the Castle Island industrial area, including the White Fuel storage and fuel transfer facility, a major generator of hazardous cargo truck traffic.

### 3.2.3 Financial District

The Financial District lies between Boston's downtown retail district to the west and the Central Artery to the east. It is the banking and financial center for the Boston metropolitan area and, to a large extent, for New England. The Financial District covers approximately 40 square blocks and consists of multi-story office buildings, with first floor retail activities.

The Financial District comprises two fairly distinct zones separated by the High Street exit ramp from the Central Artery.

One area, centered on Federal and Franklin Streets, is composed of new high-rise buildings occupied primarily by banking, insurance and related firms. Continued development of new office towers and renovation of existing buildings is occurring in this area. The largest site currently under consideration for development is the Fort Hill Garage site, where one to two million square feet of office space have been proposed. This zone also includes the new Meridien Hotel and Devonshire Towers, the first residential development to occur in the Financial District.

The second area, centered around Broad Street, is characterized by five- to six-story buildings and an irregular street pattern. The Broad Street area was originally laid out by the architect Charles Bulfinch and contains many attractive commercial buildings from succeeding periods. The Custom House National Register Historic District is located within this area and includes State Street, the original main street of commercial Boston. Significant recent

rehabilitation has taken place in this area, and many of the older buildings now house prime office space.

Downtown Crossing, Boston's retail core, is adjacent to the Financial District. Lafayette Place, a major retail and hotel development now under construction (225,000 square feet of retail space), will open in 1984.

### 3.2.4 Waterfront

The Waterfront is a recently redeveloped commercial, office and residential area. Faneuil Hall Market Place and the New England Aquarium draw substantial tourist traffic to the area. Renovation activities began in 1964, when the Waterfront was designated as an urban renewal area. Waterfront property is now extremely valuable, and most recent development has focused on luxury commercial and residential markets.

West of the Central Artery the district is occupied by Faneuil Hall Market Place and the Blackstone Block. Buildings are primarily historic three- to five-story brick or granite structures. Faneuil Hall Market Place attracts 12 million visitors per year and is a major retail center. Adjacent to the Market is Boston Redevelopment Authority (BRA) Parcel D-10, a surface parking lot soon to be developed for office and retail uses. Recent developments in the area include the 153-room Bostonian Hotel and a 680-car garage. The Haymarket area along Blackstone Street houses fresh food specialty shops, and is the site of an open air market on Fridays and Saturdays. A pedestrian tunnel crossing under the Central Artery links Haymarket with the North End.

The area lying between North Street, the Central Artery and Atlantic Avenue is composed of four- to six-story brick and granite buildings which are primarily residential. Two large housing developments for the elderly and a nursing home serving North End

Source: "Third Harbor Tunnel, Interstate 90/Central Artery, Interstate 93" Supplement to the Draft Environmental Impact Statement/Report dated June, 1983.

residents are also located in this area.

East of Atlantic Avenue are a series of wharves occupied by commercial, office and residential uses. Cruise, ferry and private boats dock at a variety of wharf locations. Christopher Columbus Park is a large park heavily used by Boston residents and tourists. The buildings on the wharves south of Long Wharf (State Street) are relatively new, and include the Harbor Towers condominium buildings and the New England Aquarium. South of Harbor Towers is the BRA's vacant Rows/Fosters Wharf. Development proposals for this site include office, retail and residential uses.

North of Long Wharf, and continuing to Union Wharf, the wharf buildings are mostly three- to four-story 19th century granite warehouses which have been converted to commercial, office and luxury residential space. North of this area non-residential uses, including the Bay State Lobster Company, currently predominate. Two residential development sites are under preliminary discussion; Sargent's Wharf, owned by the BRA, and an MBTA Powerhouse under discussion for rehabilitation as low cost housing by the Boston Archdiocese.

### 3.2.5 Government Center

Government Center contains the majority of the City of Boston's public offices, the major Federal office buildings in Boston, and a number of state and county offices. The functional area of Government Center extends across Cambridge Street to include the Suffolk County Courthouse and several state office buildings. In addition to government offices, there are several large private office buildings, parking facilities, and small shops and restaurants which serve the areas workers. There are no residential structures in the district.

The physical layout of the area

is quite different from most of Boston, with wide, heavily travelled streets bordering large "superblocks." The most significant landmark in the area is City Hall Plaza, which is both the major pedestrian circulation space in the district and the site of public demonstrations, performances, and city events.

Boston City Hall, the State Service Center and the JFK Federal Office Building draw a great number of visitors to the area each day, many of whom are unfamiliar with their surroundings. Limited parking facilities cause many people to use public transportation; the Government Center MBTA Station serves area employees, people making business trips, and a significant number of tourists visiting the historic downtown and Waterfront areas.

There are two publicly-owned vacant development parcels in this area; BRA Parcel 7, designated for hotel development, and the parcel at the intersection of Merrimac and New Chardon Streets (no designation for its use has been made).

### 3.2.6 North End

Directly north of the Waterfront and bounded by the Central Artery, North Washington Street and Boston Harbor lies the North End, one of Boston's oldest neighborhoods. Although separated from downtown Boston by the Central Artery, the North End is within walking distance of Faneuil Hall, Government Center, and the Financial District. Much of the North End is only a short walk from major public transportation services at Haymarket, Government Center and North Station (Green Line, Orange Line, Blue Line, Commuter Rail, bus).

The North End is architecturally homogeneous, with three- to five-story brick buildings lining narrow streets. It is largely residential, but also houses a significant commercial district



consisting of small shops and restaurants on the ground floors of residential buildings. The district is a major regional center for ethnic shopping, serving the large Italian-American population of metropolitan Boston.

Housing is the primary land use in the North End. At one time, the housing stock consisted primarily of rental units, but there are an increasing number of condominiums. The major commercial section of the North End is located around Hanover and Salem Streets.

Thousands of tourists visit the North End each year to follow the Freedom Trail past Paul Revere's house, the Old North Church and other historic sites.

Located on the periphery of the North End are larger businesses and institutions that are city-wide or regional in character. Expensive professional space has recently been developed on the eastern edge of the North End, essentially as an extension of the Waterfront district.

### 3.2.7 North Station

The North Station area lies between the Charles River, the Central Artery and Government Center. It contains retail, commercial, government, office, institutional and manufacturing uses. Major facilities are the MBTA's North Station commuter rail terminal and transit facilities, the Boston Garden sports arena, the Anelex Building, the Massachusetts Registry of Motor Vehicles and Department of Public Works, and the Massachusetts Rehabilitation Hospital. Commercial, retail, manufacturing and office uses are concentrated along Causeway Street.

The Bulfinch Triangle lies south of Causeway Street between North Washington Street and Merrimac Street. Its three- to nine-story brick buildings contain primarily manufacturing, commercial and warehousing uses. Private

rehabilitation of buildings in this 19th century industrial district is ongoing.

The North Station area presently contains a great deal of land used for surface parking; approximately 2,300 parking spaces exist. Roughly 60 percent of these are designated employee parking for the Massachusetts Department of Public Works, Massachusetts General Hospital, and the Massachusetts Rehabilitation Hospital.

At this time, the Boston Redevelopment Authority (BRA) is undertaking a federally-assisted urban renewal project in the North Station area. Recent planning studies have divided the area into three sections: Railyard and River Edge; North Station/Boston Garden Area; and Bulfinch Triangle. Redevelopment is currently in progress for the North Station/Boston Garden section (BRA Sub-area I), including site preparation for construction of a major General Services Administration (GSA) Federal Office Building. Other potential improvements in this area include relocation of the MBTA Green Line transit facilities; construction of a new Boston Sports Arena or other facility above extended MBTA commuter rail tracks; construction of a parking garage adjacent to Lomasney Way and the elevated Storrow Drive/Central Artery Connector Ramps; and discontinuance of a portion of Nashua Street (part of the GSA project). Construction of these improvements is expected to continue over the next decade. Planning is underway for the Railyard/River Edge section (BRA Sub-area II), with construction of any improvements not anticipated until 1990 or later.

### 3.2.8 West End

The West End lies between Beacon Hill, the Charles River, and Government Center. Until the late 1950's, the West End was composed primarily of early 20th century five-story apartment buildings. These low-rent buildings were razed in the

early 1960s during one of Boston's earliest and largest urban renewal projects. The 45-acre site is now occupied by Charles River Park, a development consisting of eight high rise apartment towers, a subsidized apartment tower for the elderly, an office building, a small commercial building, a synagogue and three parking garages. Landscaped paths wind through the development, and no through streets cross the area.

South of Charles River Park, the area has primarily institutional uses, including Massachusetts General Hospital, Massachusetts Eye and Ear Infirmary, the Suffolk County Jail and two churches. Charles River Plaza, a shopping center along Cambridge Street, contains stores, movie theaters, restaurants, a major hotel and a large privately-owned parking area. There remain a few five-story residential buildings with commercial uses on the ground floor in this area.

There is one undeveloped parcel at Charles River Park at the intersection at Lomasney Way and Staniford Streets; no proposals are under consideration at this time. The remainder of the West End is fully developed.

### 3.2.9 Charlestown

Existing conditions in Charlestown are described in the Final Environmental Impact Statement for the North Area project (Federal Highway Administration and Massachusetts Department of Public Works, 1979). Charlestown is a stable residential community. The housing stock is predominantly older, two- and three-story structures, with many multi-family and row houses. Charlestown is also a major employment center, with industrial and warehousing activities located to the west of Interstate Route 93, along Rutherford Avenue, and along the Waterfront. Bunker Hill Community College is also located in Charlestown, north of the John F. Gilmore Bridge and east of Interstate Route 93. There are local commercial

establishments along Bunker Hill Street and Main Street. Several historic sites, including the USS Constitution and the Bunker Hill Monument, attract visitors to the area.

### 3.3 NEIGHBORHOOD CHARACTERISTICS AND COMMUNITY FACILITIES

This section describes the major characteristics and significant community facilities of the Waterfront, Government Center, North End, North Station and West End neighborhoods. The City of Boston is used as a baseline for discussion of demographic characteristics. As for land use, these areas comprise the areas of potential additional effects of Alternatives 3A, 5A, 5A Modified, and 6 as compared to the No-Build Alternative and Alternatives 3 and 5 in the DEIS/DEIR. Major community facilities are listed in Table 60 and are shown on Figure 82. Neighborhood characteristics and major facilities are described below.

The neighborhood facilities and characteristics section of the DEIS/DEIR (Section 3.3) should be referred to for comparable discussions of South Boston, Chinatown/South Cove, and East Boston.

Primary sources of information on population and housing are U.S. Census of Population and Housing (1980), the 1979 Boston Redevelopment Authority (BRA) Household Survey and BRA Neighborhood Profiles.

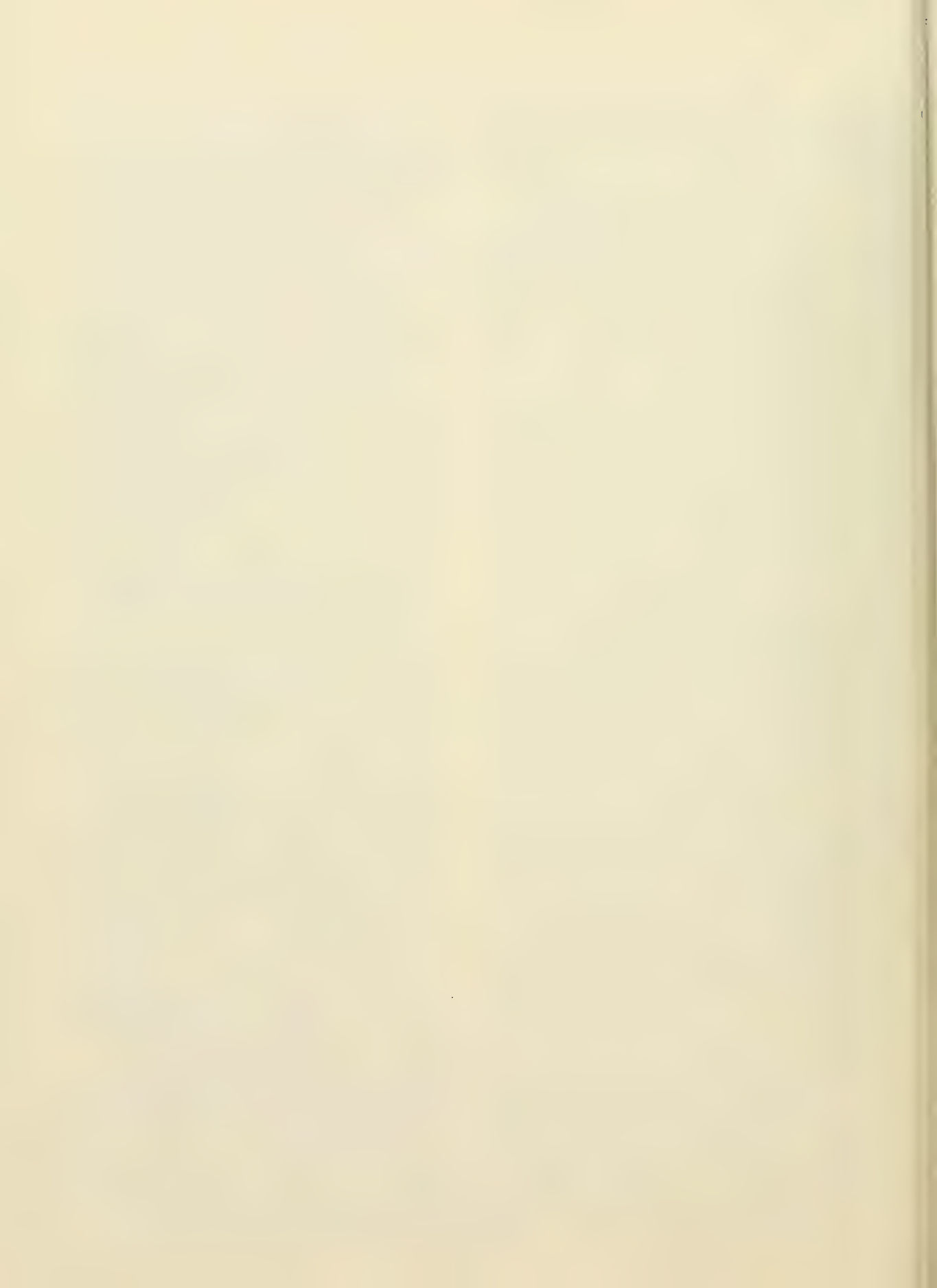
#### 3.3.1 Waterfront

##### General Characteristics

The Waterfront has been a residential community since urban renewal projects began in the late 1960s. The Waterfront housing stock consists of newly constructed apartments and condominiums and older warehouse buildings that have been rehabilitated for residential use.

The population of the Waterfront area increased dramatically during the period of redevelopment;

Source: "Third Harbor Tunnel, Interstate 90/Central Artery, Interstate 93" supplement to the Draft Environmental Impact Statement/Report dated June, 1983.





## 2.0 TRAFFIC FORECASTING PROCEDURE

"THIRD HARBOR TUNNEL PROJECT, INTERSTATE  
90" DRAFT ENVIRONMENTAL IMPACT STATEMENT/  
REPORT DATED DECEMBER, 1982

## 2.0 TRAFFIC FORECASTING PROCEDURE

### 2.1 General

In contemporary practice, traffic forecasting for large highway projects is generally done through use of a computerized traffic analysis procedure known as traffic assignment. This procedure has been developed by the Federal Highway Administration (FHWA) and the Urban Mass Transportation Administration (UMTA) over the past 25 years, and is used throughout the world. In this procedure, a computerized representation of the highway network is constructed. This network, consisting of highway links (streets) and nodes (intersections), covers the area of analytical interest and usually includes most highway facilities other than minor local streets. Associated with this network is a system of zones covering the same geographical area. A trip table, or matrix of trips, that identifies zone-to-zone vehicular flows is prepared as part of this process. In the traffic assignment procedure, vehicular trips from the trip table are assigned to links in the highway network. This is done by using one of several mathematical computer programs or algorithms that assign vehicles from origin zones to destination zones via minimum time paths.

There are usually several stages of analysis in the transportation planning process. In the first stage, a travel survey is taken. This identifies the zone-to-zone flows of trips. Associated with this travel survey are traffic counts made at various points throughout the highway network. These two types of data together constitute what are known as the base case trip table and base case traffic volumes.

The second stage of analysis is traffic assignment model calibration. In this stage, traffic assignments are performed, assigning the trips from the trip table to the computerized highway network. These traffic assignments use the computer programs

developed by the FHWA and UMTA. In these assignments, trip table volumes and highway network characteristics are adjusted until assigned volumes on the computerized network are close to the volumes of traffic actually counted. Following this procedure the base case model is said to be calibrated.

In the third stage of analysis, future networks and trips are developed. The highway network is altered to incorporate changes anticipated by the horizon year of analysis, and separate versions of the network are prepared that include the various project alternatives to be tested. Parallel to this work, projections of future trip volumes are made. These projections are based on such factors as growth of future population and employment. From the projections come trip tables for future years.

When the future networks and trip tables are complete, the future trips are assigned to the future networks. These assignments yield the traffic volumes associated with the various plan alternatives. From these assignments, various statistics are available. These include traffic volumes and speeds by link or in total for the network, vehicle hours, vehicle miles, and a variety of other statistics. These various statistics are used in evaluating the proposed alternatives.

Once the basic traffic assignments have been undertaken, a number of subsidiary analyses may be performed. These may include analyses of such issues as vehicle turning movements at intersections, truck traffic, traffic in small areas or on particular streets, and construction staging. These all contribute to the overall evaluation of traffic associated with project alternatives.

In the Third Harbor Tunnel EIS/EIR traffic analysis, the traffic assignment procedure described above has been followed. Base case and future networks and trips were

developed (or used from earlier studies); traffic assignments were performed; and, a number of subsidiary and follow-up analyses were undertaken. In the remainder of this section, the specific parts of the analysis are discussed in order as follows:

1. Travel and Traffic Data
2. Base Case Networks and Zones
3. Base Case Trip Tables
4. Base Case Traffic Assignment Model and Model Calibration
5. Future Trips
6. Logan Airport Trips
7. Future Networks
8. Future Assignments
9. Manual Assignments: East Boston and South Boston
10. Truck Volumes
11. Construction Staging
12. Induced Traffic

The following general discussion is intended to provide an overview of the analysis. For specific details of the analysis, technical memoranda are available from CTPS. They are referenced at the end of this Appendix.

## 2.2 Travel and Traffic Data

The basic source of travel and traffic data used for the Third Harbor Tunnel EIS/EIR is the Boston Central Artery 1977 Origin-Destination Study prepared for the Massachusetts Department of Public Works (MDPW) [1]. In this study, travelers crossing a cordon line around downtown Boston were surveyed with regard to the origins and destinations of their trips. This survey provided travel information for trips to and through the downtown Boston area. Data from this survey had earlier been combined with regional travel data from the 1963 Boston origin-destination survey [2], updated to 1975 [3], to create the regional trip tables that were used for 1977 average weekday traffic (AWDT) assignments in the Corridor Planning Study for Rt. I-93 and I-90: The Central Artery and Third Harbor Tunnel [4]. These same data are the basis for the trip tables that have

been used for AM peak, PM peak, and average weekday daily traffic (AWDT) assignments for the Third Harbor Tunnel traffic analysis.

Traffic counts for the 1977 base case assignment model calibration came from a number of sources [5]. These include cordon counts and arterial street counts from the Central Artery Origin-Destination (O-D) Survey, supplemental counts performed for the O-D Survey by the MDPW, counts from the 1974 Boston Cordon Count [6], counts from the Seaport Access Study [7], counts from permanent MDPW counting stations, MDPW coverage counts, and special MDPW counts conducted as part of this study. For model calibration, a total of 159 count locations were used for an "inner" area in and around downtown Boston, and 114 in an "outer" area extending about 4 to 5 miles from the Boston core. Another 62 counts were used for an outer fringe area which extends to just beyond Route 128.

In addition to counts, balanced expressway volumes created by CTPS were used for model calibration.

## 2.3 Base Case Networks and Zones

The highway network initially used for 1977 AWDT traffic assignments and used in the Central Artery Corridor Planning Study is a large network containing 11,400 links, and stretching to just beyond Route 128. Within the area of coverage, it includes all expressways, all major arterial routes, and most minor arterial routes. For the downtown Boston area, there is more detail, and most local streets are included.

During the course of Third Harbor Tunnel analysis, a number of changes were made in the initial AWDT network. Speeds and capacities were corrected on a number of expressway links, and network geometry was changed in several locations to better reflect the actual highway network.

Major network changes were made in East Boston and South Boston. In



these areas, detailed evaluative work was required for Third Harbor Tunnel analysis, for the original network did not include all the required streets. Thus, the network was made more detailed in both of these areas [8]. The final AWDT network links and nodes for East Boston and South Boston are shown in Figure 2 and Figure 3.

The zone system for the AWDT network covers roughly the same geographical area as the network, extending to just beyond Route 128; boundaries are shown in Figure 4. Initially, the zone system included 217 zones, of which about 60 were within downtown Boston. Because of the detailed evaluation requirements of Third Harbor Tunnel analysis, the initial large zones of East Boston and South Boston were disaggregated into smaller zones [8]. Initially, East Boston had only four zones and South Boston had six. In the final system, East Boston had 17 zones and South Boston had 13. Correspondingly, the final AWDT system had 239 zones. The zones ultimately used in Third Harbor Tunnel traffic analysis for East Boston and South Boston are shown, respectively, in Figures 5 and 6.

For AM and PM peak period assignments, smaller networks and zone systems were used. These networks, containing about 6,900 links, stretch to just north of Revere and Medford, to Arlington, Watertown, and Newton to the west, and to just south of the Neponset River (see Figure 7). Within their geographical area of coverage, the AM and PM networks include the same highway facilities as the AWDT network. As initially developed, these networks had 168 zones. These smaller systems were developed for AM and PM peak period assignments because they are easier to use and are much cheaper in computer time than the much larger AWDT network and zone system. For purposes of Third Harbor Tunnel analysis, they yield results equivalent in quality to those of the larger system.

As with the AWDT network, a substantial number of changes were

made in the AM and PM base case networks. Many of these were related to making link capacities and speeds more accurate, and to improving network geometry. Others were made to accomplish the same network detailing in East Boston and South Boston that was done for the AWDT network.

Zone systems for the AM and PM networks were also disaggregated in East Boston and South Boston to the same zones as for the AWDT network. The final AM and PM zone systems include 188 zones each.

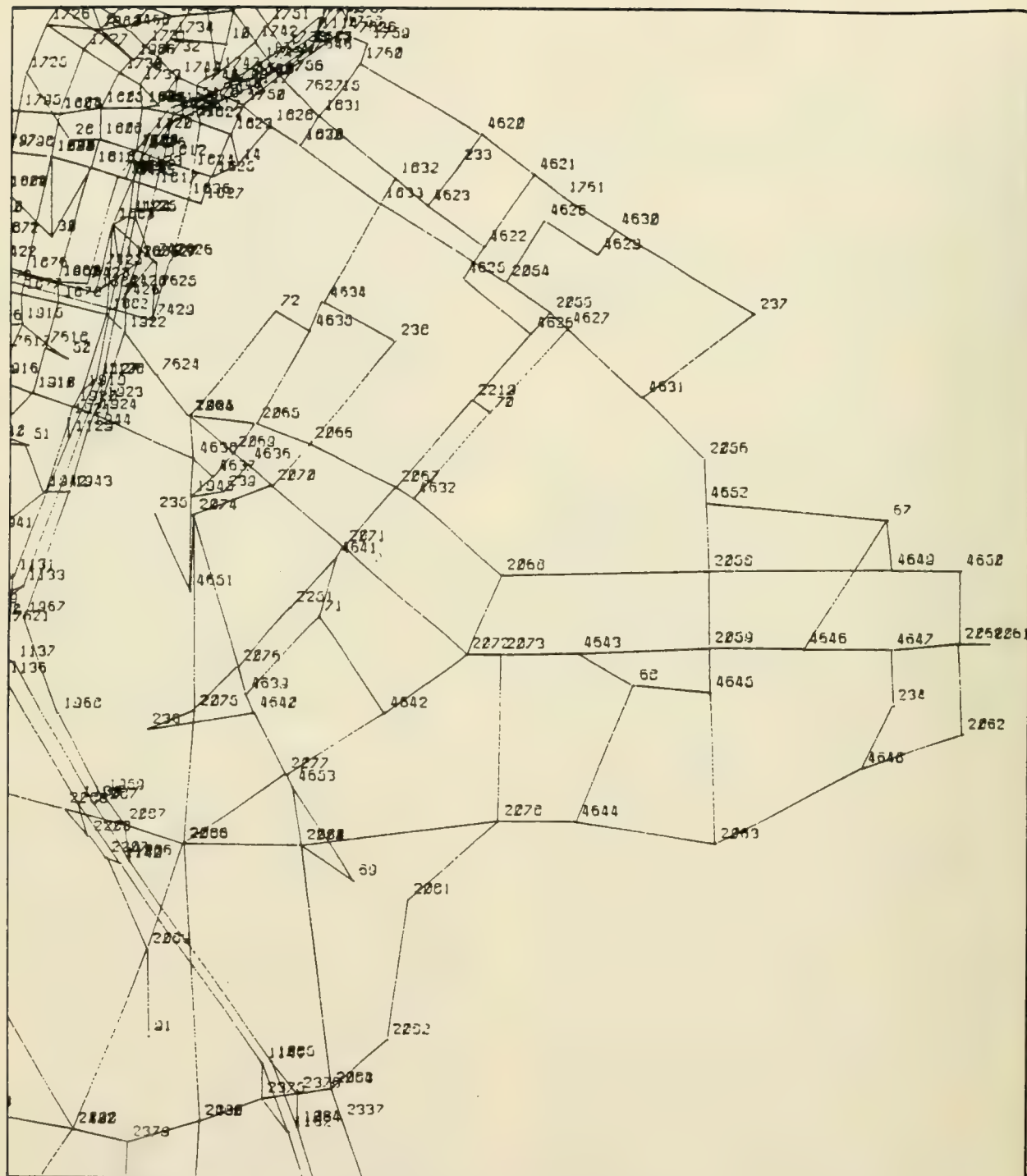
## 2.4 Base Case Trip Tables

As indicated above, 1977 base case AWDT trip tables had previously been prepared and used for AWDT traffic assignments for the Central Artery Corridor Planning Study. For Third Harbor Tunnel analysis, these trip tables were used substantially as they had been developed earlier, except that they were disaggregated in East and South Boston to reflect the smaller zones created in those areas. The disaggregation process involved determining, at a census tract level, the fractions of trips for each original zone that were residentially and non-residentially related, and then aggregating the census tract fractions up to the new zone systems in accordance with the original zonal residential and non-residential trip totals [9, 10, 11, 12, 13, 14, 15, 16]. Trips from the new zones were assumed to be distributed to other zones in the same proportions as had been the case in the original zones.

Prior to the Third Harbor Tunnel analysis, a 1977 base case AM peak trip table had been prepared for 7:00 AM to 10:00 AM using the same data sources as had been used in creating the AWDT trip table. This trip table was used for Third Harbor Tunnel AM peak base case assignments, with its values somewhat modified through the traffic assignment model calibration process. As with the AWDT trip table, a disaggregation process was required for the new smaller zones in East Boston and South Boston [17,

— Network Links  
223 Network Nodes





— Network Links  
 222 Network Nodes

Figure 3

### South Boston Links and Nodes Average Weekday Traffic Network

0 1666 Feet



EIS/EIR for I-90, The Third Harbor Tunnel

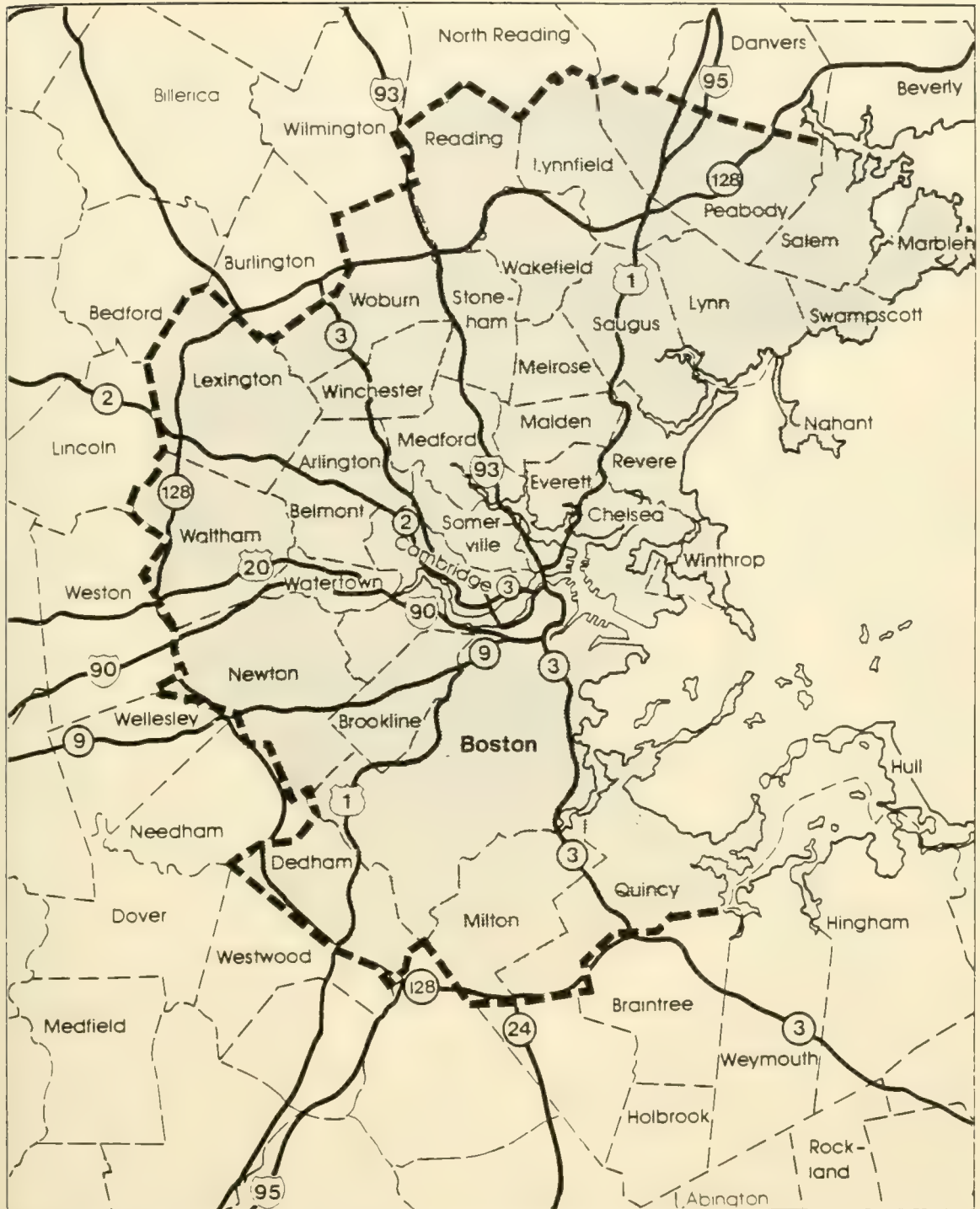





Figure 4

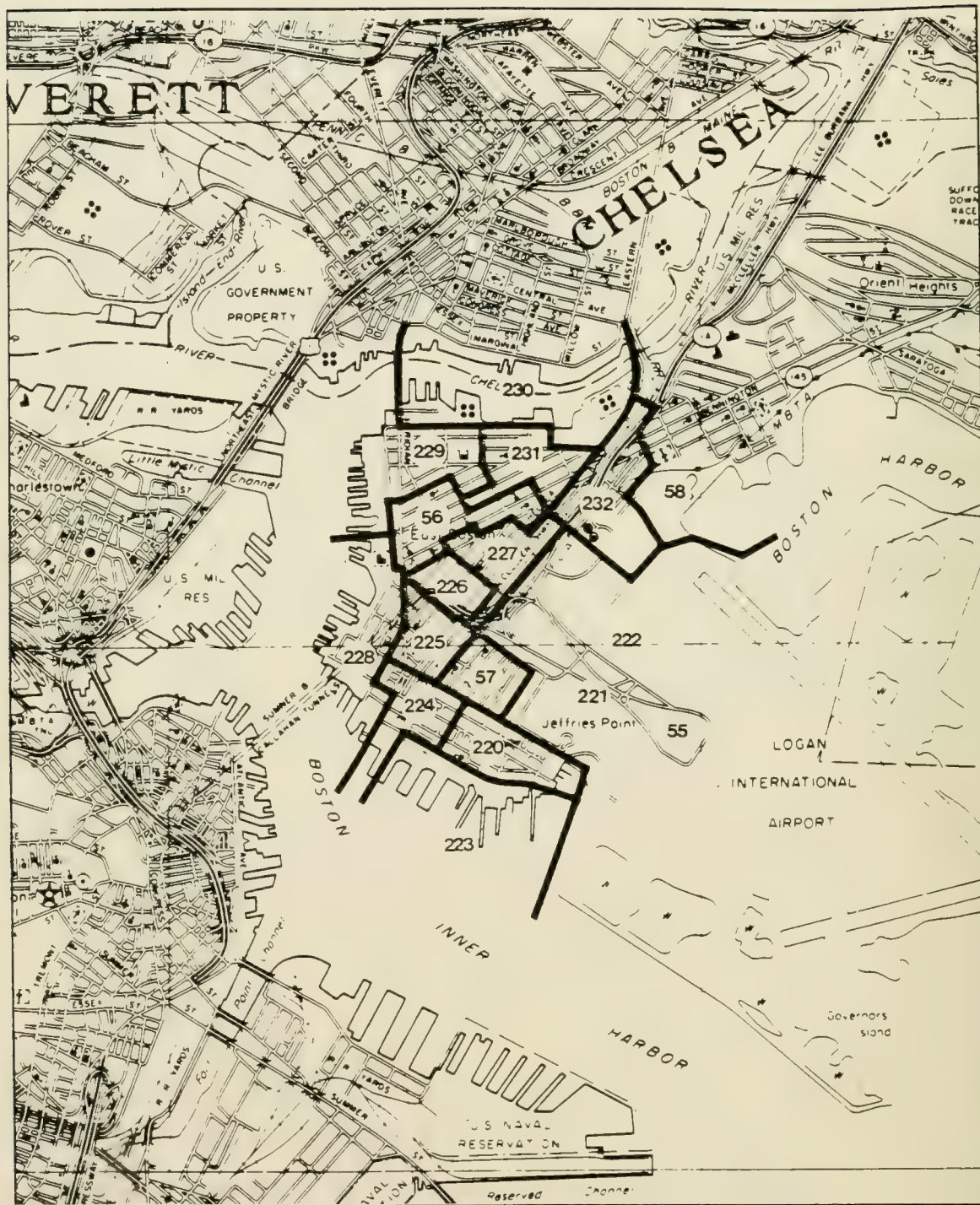
### Outer Boundary of Average Weekday Traffic Zone System

-  Average Weekday Traffic Zone System
-  Outer Boundary of Average Weekday Traffic Zone System
-  Major Highways

0 1 2 4 Miles



EIS/EIR for I-90, The Third Harbor Tunnel



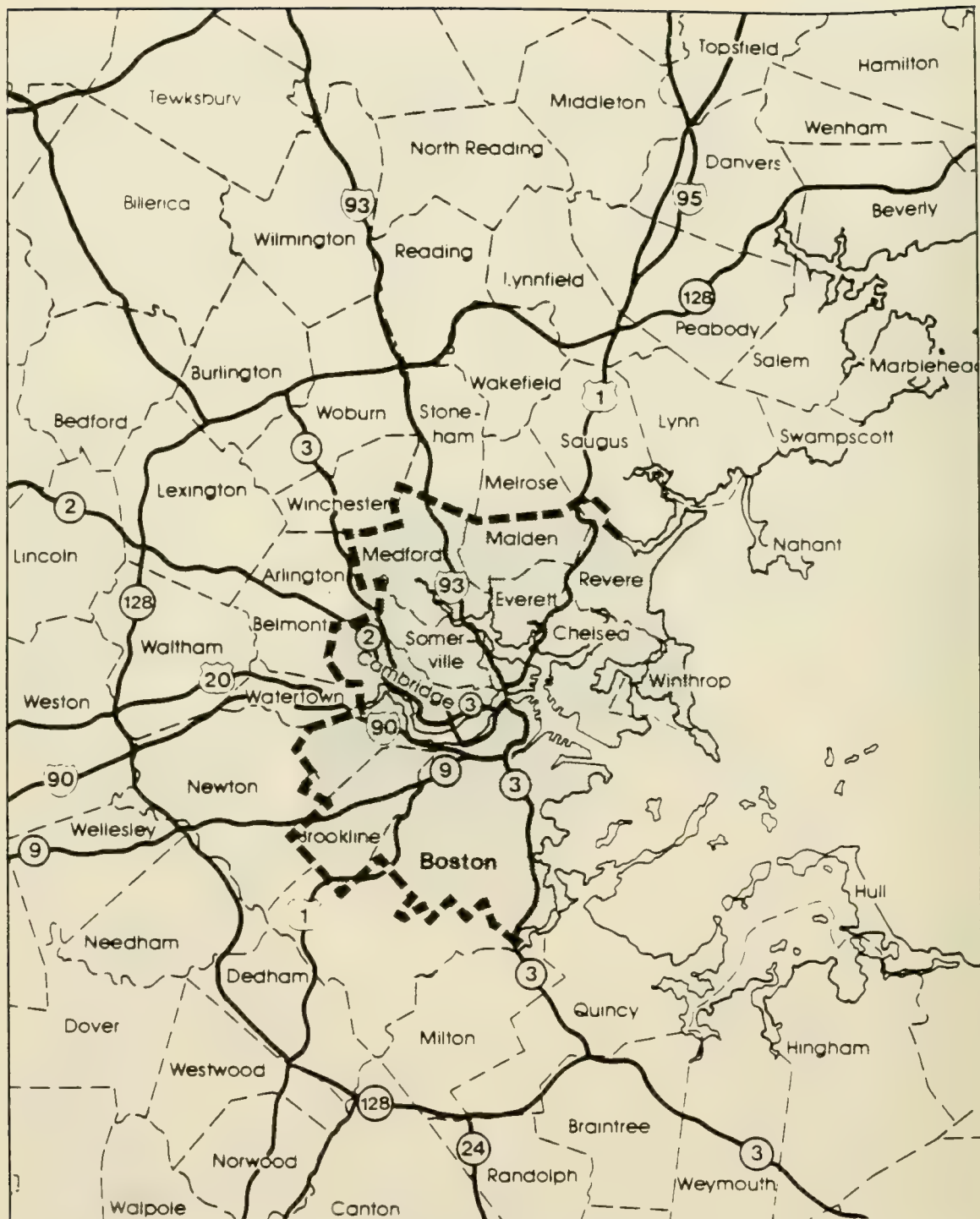
— Zone Boundary  
 00 Zone Number

Figure 5  
 East Boston Zone System for Disaggregated  
 Average Weekday Traffic Network

0 1 2 Mile  
 EIS/EIR for I-90, The Third Harbor Tunnel










-  A.M. & P.M. Peak Traffic Zone System
-  Outer Boundary of A.M. & P.M. Peak Traffic Zone System
-  Major Highways

Figure 7

### Outer Boundary of A.M. & P.M. Peak Traffic Zone System

0 1 2 4 Miles



EIS/EIR for I-90, The Third Harbor Tunnel



18, 19]. This process was analogous to the one undertaken for the AWDT trip table.

Prior to the Third Harbor Tunnel Study, no PM peak period trip table had been created. Such a table for this study was initially developed for 1977 for the PM peak period (3:00 PM to 6:00 PM), by reversing the AM peak base case trip table [20, 21, 22, 23]. This reversal was based on the assumption that trips from Zone A to Zone B during the AM peak go from Zone B to Zone A during the PM peak. The initial base case PM trip table was substantially altered during the model calibration process, in order to account for actual differences between PM peak travel and the reverse of AM peak travel.

For the PM peak base case trip table, a disaggregation process was made for East Boston and South Boston following the same procedure as that used for the AM peak base case trip table.

## 2.5 Base Case Traffic Assignment Model and Model Calibration

All traffic assignments for Third Harbor Tunnel analysis utilized the Urban Transportation Planning System battery of traffic assignment programs of UMTA. For AWDT, "equal-or-nothing" assignments were run. For AM and PM, "all-or-nothing" assignments were performed. For AWDT assignments, seven iterations were used for calibrating the base case 1977 model. For AM and PM peak period assignments, five iterations were used.

Because the AWDT assignment model was already quite well calibrated from the earlier Central Artery Corridor Planning Study, only a relatively small amount of calibration work was necessary. A total of ten calibration runs were conducted [24]. These runs had three purposes. The first was to compensate for the speed, capacity, and geometric changes that had been incorporated during network editing. The second was to redistribute Logan Airport trips more

in accordance with the results of the 1978 Logan Airport Survey [25]. The third was to incorporate the disaggregated zones for East Boston and South Boston.

An extensive process of calibration was undertaken for both the AM and the PM traffic assignment models. For the AM peak, a total of twenty-eight traffic assignment trials was undertaken in model calibration [26]. These trials had a variety of purposes ranging from bringing corridor traffic volumes into conformance with counts, to adjusting Logan Airport trip totals and distributions to agree with survey results. For the PM peak, a total of twenty model calibration runs were undertaken [27]. They had purposes roughly parallel to those of the AM peak. For both the AM peak and PM peak, disaggregation was done for zones in East Boston and South Boston. A portion of the graphical computer output from a typical model assignment is illustrated in Figure 7.

## 2.6 Future Trips

It was originally anticipated that future trips for AM, PM, and AWDT would be based on CTPS Interim Projections of 1977 extended to the Third Harbor Crossing horizon year of 2010 [28, 29]. An early analysis of the difference between CTPS Interim Projections and new projections based on the 1980 Census [30], however, indicated that new projections based on the 1980 census were much lower than the earlier ones. Because the difference was considerable, it was decided to use new projections based on the 1980 Census. For this purpose, Metropolitan Area Planning Council (MAPC) projections of population and employment growth [31, 32] were converted from the town level projections of MAPC to the zone system of CTPS [28, 29, 33, 34]. These projections were then applied to the base case trip tables of 1977 in order to create trip tables for 1990 and 2010.

Because of the desire for more

accuracy of traffic assignments in East Boston and South Boston, special attention was paid to future population and employment factors in those areas. Census tracts in East and South Boston were examined individually, and forecasts were made and then aggregated to the zone level. Planned developments such as those on the Massport and Athenas properties in South Boston were specifically considered [35, 36]. The growth factors from these projections were incorporated into the 1990 and 2010 trip tables.

## 2.7 Logan Airport Trips

Because of the considerable importance of Logan Airport trips in future harbor crossing volumes, special care was devoted to Logan Airport trips both for the base case and for future trips. As indicated above, under base case model calibration, Logan trips were redistributed to agree with existing travel patterns [37]. For projections of future Logan trips, the following procedure was undertaken. First, base case traffic was broken down by activity: air passengers, employees, and air cargo, for the airport survey year of 1979 [38]. Then the proportions of traffic for each activity were applied to the 1977 base year traffic [39]. Following this, a new forecast of Logan air traffic prepared by Massport [40] was combined with a specific forecast for Bird Island Flats activity [41], to create projections of ground traffic to Logan Airport for the year 2010 [42]. For the 2010 projections, three scenarios were envisioned. In one, it was assumed that travel mode choices to and from the airport would remain much as they are today. In the second, it was assumed that the present trend toward non-private auto modes would continue. In the third, it was assumed that there would be maximum use of public transit. It was decided to use the first scenario for trip tables for Third Harbor Tunnel build alternatives, and the second for the No-Build Alternative, reflecting the potential effect of the project on

mode choice. Ultimately, 1990 trip projections were made using these same assumptions [43].

## 2.8 Future Networks

Future networks were constructed for the No-Build alternative and the four Third Harbor Tunnel build alternatives. All future networks were based on the so-called "L-2" network for the Central Artery North Area Project, and included future committed projects, such as widening of the Southeast Expressway, construction of the Seaport Access Road in South Boston, and construction of the Southwest Arterial. The Revere Beach Connector and the Salem-Peabody Connector were not included in the future networks. The 1990 future networks were the same as those for 2010.

## 2.9 Future Assignments

For future AWDT, multiple sets of assignments were run. Following the first set of assignments [44], certain anomalies were noted in some of the volumes. After an extensive network check and certain network corrections, a second set was run [45]. This second set of assignments was much better, and was used for Third Harbor Tunnel AWDT traffic volumes.

For AM and PM traffic, multiple sets of assignments were also run. Four test sets of AM assignments were performed [46], and then production sets of AM and PM assignments were run [47, 48, 49, 50]. In analyzing the results of these production assignments, it was found that the results were distorted in certain areas where main routes compete with alternative routes [51]. This occurred because of inadequate numerical convergence of the assignments. Thus, the production assignments were rerun using nine rather than five iterations [52, 53] of the assignment algorithm. The results of this second set of production assignments were much better than those of the first set,



and they were used for Third Harbor Tunnel AM and PM traffic volumes.

For all production assignments--AM, PM, and AWDT--the following were produced for 1990 and 2010 for all five Third Harbor Tunnel alternatives:

1. Traffic Volumes
2. Congested Speeds
3. Turning Movements at forty intersections
4. Total Vehicle Hours
5. Total Vehicle Miles

#### 2.10 Manual Assignments: East Boston and South Boston

Despite model disaggregation in East Boston and South Boston, it was not possible for the computer model to produce accurate traffic assignments for local streets in these areas. This was partly because the traffic zones were still too large to allow accurate volumes on the smallest streets, and partly because detailed model calibration could not be carried out for East Boston and South Boston. It was also because the traffic assignment model cannot replicate queuing behavior, which is a significant factor on local streets.

For these reasons, manual assignments for South Boston and East Boston streets were performed [54, 55, 56, 57, 58, 59]. In performing these manual assignments, base case volumes were taken largely from the 1982 counts collected as part of the Third Harbor Tunnel EIS/EIR. These were adjusted for future years and alternatives by incorporating the differences between the base case computer assignments and the computer assignments for future years and alternatives. Effort was expended to have the manual assignments agree with the machine assignments at the entry points to East Boston and South Boston.

For purposes of these manual assignments, only three alternatives were assigned in East Boston (Alternatives 1, 4, and 5) and three in South Boston (Alternatives 1, 2,

and 4). It was assumed that local differences in alternative networks in South Boston would not affect volumes in East Boston and vice versa; e.g., Alternatives 4 and 5 would have the same traffic arrangements in South Boston despite their differences in East Boston.

For all manual assignments, turning movement analyses were performed for 13 intersections in South Boston and fourteen in East Boston. The turning movement analyses were based on the changes in the assignments from the 1982 base to the various years and alternatives. A total of 312 turning movement analyses were thus undertaken.

#### 2.11 Truck Volumes

No explicit truck traffic assignments were performed for the Third Harbor Tunnel EIS/EIR analysis. It was assumed that truck percentages in the future would generally mirror those of today [60]. For entries to and exits from Logan Airport, specific truck projections were made [61]. For East Boston and South Boston, future truck volumes were based on the manual assignment volumes for all vehicles [54, 55, 56, 57, 58, 59].

#### 2.12 Construction Staging

Traffic was assigned for seven construction stages/alternatives. Three of these were for the AM peak and four for the PM peak. For these stages/alternatives, various links in the future highway network were altered or deleted in accord with the roadway changes associated with the given stage and alternative. In the construction staging assignments, no manual adjustments were made.

#### 2.13 Induced Traffic

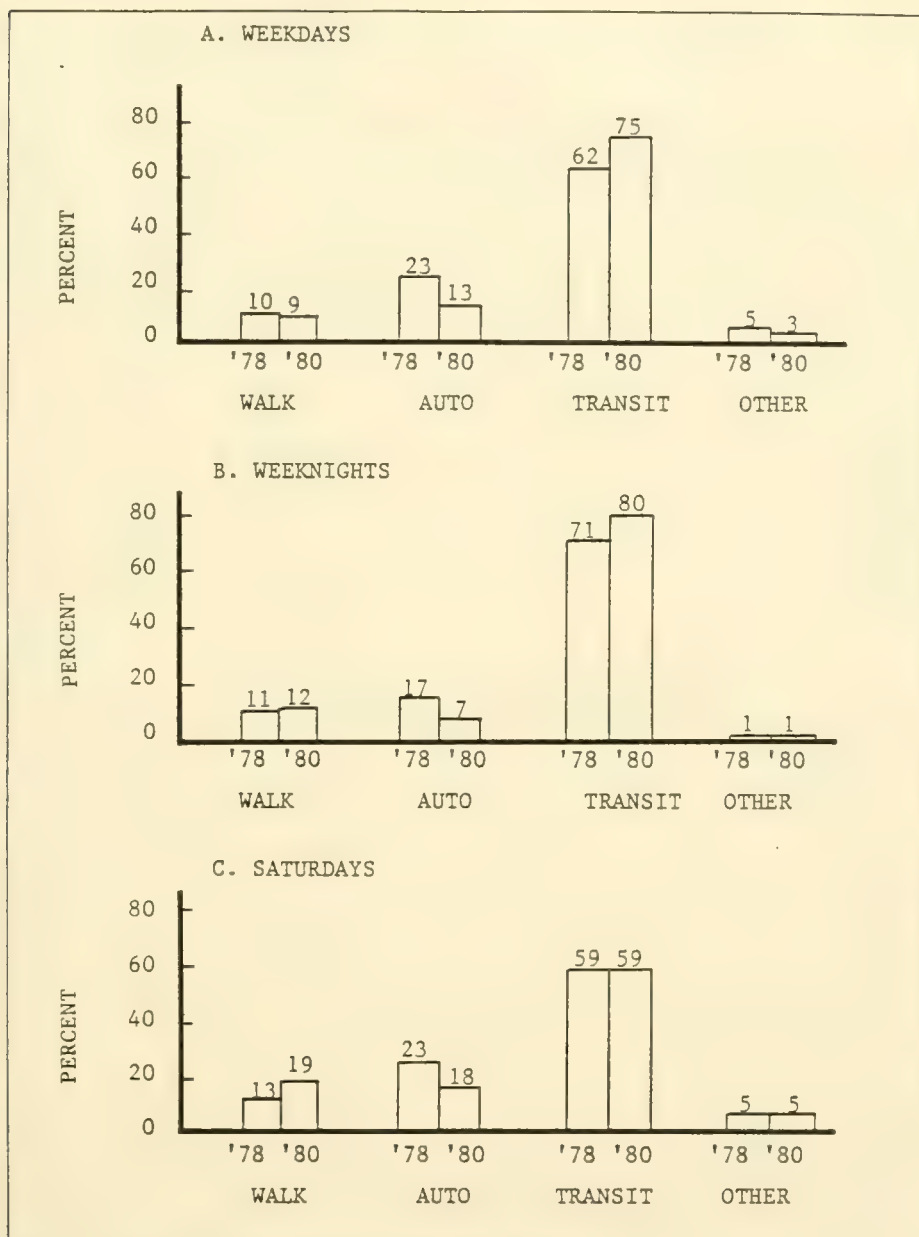
Consideration of induced traffic was limited to analysis of the build alternatives as a group versus No-Build for Logan Airport traffic. As indicated above, it was assumed in the No-Build case that increasing traffic congestion would force Logan

passengers into non-private automobile modes, as has been happening over the past decade. For all build alternatives, it was assumed that this shift would not continue to take place. The difference between the traffic volumes associated with the two assumptions could be considered to be "induced" traffic, and amounted to approximately 12,800 trips daily. More accurately, added traffic associated with the build alternatives is traffic growth that would be constrained and could not take place in the No-Build Alternative.



"DOWNTOWN CROSSING: AUTO RESTRICTED ZONE  
IN BOSTON" FINAL REPORT DATED JULY, 1982





SOURCE: Pedestrian Interview Surveys, 1978 and 1980

Table taken from "Downtown Crossing: Auto Restricted Zone in Boston" Final Report Dated July, 1982.

FIGURE 8-9. MODE OF TRAVEL TO DOWNTOWN BOSTON

TABLE 8-2. MODE OF TRAVEL TO WORK

	% Share	
	1978	1980
Walk Only	5.4	5.7
Auto Only	23.7	16.7
Subway Only	25.5	28.0
MBTA Bus	9.5	10.9
Other Bus	5.4	5.1
Commuter Rail	10.2	10.0
Taxi	0.4	0.2
Bus to Subway	12.7	14.0
Rail to Subway	0.5	0.6
Auto to Subway	4.7	6.5
Rail to Bus	0.4	0.2
Auto to Bus	0.9	0.8
Bicycle and Miscellaneous	0.6	1.2
	100.0	100.0

Source: Employee Surveys, 1978 and 1980 (29 buildings surveyed in both years).  
 Table taken from "Downtown Crossing: Auto Restricted Zone in Boston"  
 Final Report Dated July, 1982.



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APPENDIX C



## **Appendix C**

### **Methodology for Projecting Future Parking Demand**



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## Appendix C: Methodology for Projecting Future Parking Demand

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### Overview

Projections of future parking demand generated by new office, retail, and hotel development were made using a three step process:

- trip generation: application of standard trip rates to planned square footage of development to obtain estimated numbers of daily person-trips generated, by trip purpose (work and non-work).
- modal split: splitting the projected number of trips generated among different travel modes: automobile, transit, and other (walk, bike, etc.)
- turnover: applying turnover rates for work (long-term) and non-work (short-term) trips made by automobile to yield peak parking demand.

Parking demand for new residential developments was estimated based on auto ownership information from the 1970 census. This appendix presents the trip generation, modal split, turnover, and other assumptions employed for the calculations of future parking demand in Chapter 3.

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### Trip Generation

Table C.1 presents trip generation rates for office, retail and hotel uses. These rates were primarily derived from the Institute of Traffic Engineers' Trip Generation Report, which is based on data collected in a range of US urban areas. The rates shown are for round trips. Each rate is broken down in the table into a work trip generation rate and a non-work trip generation rate according to observed trips per employee ratios (see footnotes to table). This was done to allow the methodology to distinguish between long-term and short-term parking demand.

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### Modal Split/Auto Occupancy

Once the number of trips "generated" by new development is known, the total number of parkers can be established by determining the proportion of



TABLE C.1

Trip Generation Rates  
(Round Person-Trips Attracted Daily)

Office 6/1000 sq ft<sup>A</sup>

- 3.9 work trips<sup>B</sup> (employees)
- 2.1 non-work trips (visitors)

Retail 20/1000 sq ft<sup>C</sup>

- 2.8 work trips<sup>D</sup> (employees)
- 17.2 non-work trips (shoppers and visitors)

Hotels 5/room<sup>D</sup>

- 1 work trip (employees)
- 4 non-work trips (includes multiple guest trips and restaurant visitors)

- A This is the average trip rate for general offices reported in the National Cooperative Highway Research Program (NCHRP) Report 187, "Quick Response Urban Travel Estimation Techniques and Transferable Parameters" (1977). The original source of this figure is the Institute of Traffic Engineers (ITE) Trip Generation Report.
- B Given the attraction rate per office square footage and assuming an average rate of 4.6 workers 11,000 square feet for Class A office space (Boston Redevelopment Authority: The Office Industry Survey, Part II, 1979), the member of work trips generated per 1,000 sq. ft. of office is estimated to be 3.9, or 65 percent of all trips generated.
- C This is the average retail attraction rate for high density central business districts reported in NCHRP Report 187 (based on the ITE Trip Generation Report)
- D Knowing the total trip attraction rate, the number of work trips per 1,000 sq. ft. can be determined by assuming a rate of 3.2 employees per 1,000 sq. ft, and the standard rule of thumb of 1.7 (one-way) trips/employee/day.
- E Source: NCHRP Report 187 and ITE Trip Generation Report. The estimate of 1 work trip for every five trips was based on professional judgement.

trips made by automobile and the average number of occupants per automobile. In Boston, the following information on modal split and auto occupancy is available:

a. 1982 Cordon Count (adjusted for through trips--see Chapter Two)

		Percent of daily person-trips (6 am - midnite)
automobile		59%
public transportation		33%
bicycle/walk		8%
auto occupancy:	1.33 (6-9 am)	
(not adjusted for through trips)	1.42 (6 am - midnite)	

b. Building Surveys--(see Appendix B)

Zone	Building	Work Trips			Auto Occupancy	N
		Auto	Transit	Other		
7a	500 Boyston St.	35%	51%	14%	1.90	141
1b	470 Atlantic Ave.	44%	53%	3%	2.02	500
1a	125 High Street	43%	54%	3%	1.72	516
1a	Shawmut Bank	27%	67%	6%	1.67	1,171
1b	Fed. Reserve Bank	38%	57%	5%	2.04	931
	All Buildings	36%	59%	5%	1.84	2,259

Zone	Building	Non-Work Trips			Auto Occupancy	N
		Auto	Transit	Other		
7a	500 Boyston St.	60%	24%	16%	1.72	25
1b	470 Atlantic Ave.	87%	9%	4%	1.52	23
1a	125 High Street	77%	13%	10%	1.29	40
1a	Shawmut Bank	51%	33%	16%	1.35	129
1b	Fed. Reserve Bank	NA	NA	NA	NA	0
	All Buildings	61%	26%	13%	1.40	217

c. Central Transportation Planning Staff (CTPS) 1975 Trip Tables

<u>Zone</u>	<u>Percent of Trips by Transit</u>		
	<u>home-based work</u>	<u>home-based other</u>	<u>non-home-based</u>
1	45%	26%	13%
2	49	30	17
3	35	17	11
4	38	18	10
5	50	35	17
6	33	16	10
7	38	20	12
8	21	10	6
9	32	17	9
10	25	15	6
11	32	16	9
12	29	16	10
<hr/>			
All Zones	41%	17%	12%

d. Fanueil Hall Shopper Survey (Rouse, 1977)

<u>trip origin (weekday)</u>		<u>mode (weekday)</u>	
home	46%	auto	43%
work	21%	transit	16%
tourist	15%	walk/other	35%

e. BRA Office Tenant Survey (March, 1979)

<u>Location</u>	<u>Percent of Work Trips by Auto</u>
Financial District	32%
Government Center	30%
MidTown	33%
Back Bay	40%
All Areas	34%

f. Downtown Crossing Evaluation Building Surveys  
 (Cambridge Systematics, 1980)

<u>Building</u>	<u>% by Auto</u>
79 Milk	44.4%
100 Federal	40.7
1 Federal	35.5
80 Boylston	32.9
1 Court	31.0
18 Tremont	30.8
100 Summer	28.2
10, 24 Federal	25.9
89 Broad	24.7
1 Washington Mall	24.2
Prudential	23.8
89 State	23.5
City Hall	23.0
230 Congress	21.7
141 Milk	21.4
600 Washington	21.3
60 State	20.7
140 Federal	20.5
185 Tremont	20.0
53 State	19.4
27 School	19.4
10 High	19.0
45 School	18.4
294 Washington	18.0
1 Boston Place	17.0
75 Federal	16.7
99 High	16.7
125 High	16.7
262 Washington	14.3
1 Beacon	14.3
<hr/>	
All Buildings	23.7%

Needless to say, there is considerable variation in both modal split and auto occupancy among sources. However, it is clear that modal split varies from area to area of the downtown, according to the level of transit access and parking availability. Based on the available information, together with judgement about relative levels of transit and auto access to the different analysis zones, assumptions about modal split were made for the zones in which new development is projected to occur. These are shown in Table C-2. Auto occupancy was assumed not to vary in a systematic manner by zone, but

in general appeared to be higher for work trips than for non-work trips. Average auto occupancies of 1.51 for work trips and 1.31 for non-work trips were assumed, and are consistent with the all-day average of 1.42 observed in the recent cordon count.

These modal split and auto occupancy assumptions were applied to projected numbers of work and non-work person trips to obtain estimates of the number of total daily parkers. The one exception to this, however was non-work trips generated by new hotels. Instead, peak (non-work) parking demand of .25 spaces per room was assumed, based on judgement.

### Turnover

Turnover rates of 1 for work-related parkers and 2.67 for non-work related parkers were assumed, based on national experience.

### Residential Parking Demand

Peak parking demand per dwelling unit was calculated based on an auto ownership assumptions derived from the 1970 census of .74 autos per dwelling unit, and an assumption that 75 percent of autos owned by residents would be left at home during the day.



TABLE C.2

Modal Split Assumptions: Percent of Trips by Auto

<u>Zone</u>	<u>Work Trips</u>	<u>Non-Work Trips</u>
1a	35%	27.5%
1b	40	39
2a	35	38.5
3	30	35
4	30	35
5a	30	35
5b	40	42
7a	40	48
7b	45	52
9a	45	52
11b	40	48
12	60	56

Example Calculation of Peak Parking Demand: Zone 9a (1985)

Development:           845,000 sq. ft. office  
                          300,000 sq. ft. retail  
                          1,900 hotel rooms  
                          400 dwelling units

Work-Trips Generated:  $845 (3.9) + 300 (2.8) + 1900 (1) = 6036$

Non-Work Trips Generated:  $845 (2.1) + 300 (17.2) + 1900 (4) = 14,535$

Work Trips by Auto:  $6036 (.45)/1.51 = 1798$

Non-Work Trips by Auto:  $14,535 (.52)/1.31 = 5769$

Work-Related Parking Demand:  $1798/1 = 1798$

Non-Work-Related Parking Demand:

$$(14,535 - 4(1900)) (.52)/(1.31)(2.67) + .25(1900) = 1506$$

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APPENDIX D



## **Appendix D**

### **Adapting Boston's Parking Freeze in Response to a Changing Downtown Environment**





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## 1. Background

Instituted in 1976, the present freeze on commercial parking spaces in downtown Boston limits the number of commercial spaces to the 1973 level of 35,503. New construction of commercial spaces can be done only after the Boston Air Pollution Control Commission (BAPCC) issues a freeze permit. Freeze permits are issued contingent on the proposed facility meeting the BAPCC's criteria, which are:

- sufficient spaces are available in the freeze bank. (Spaces are added to the bank when on- or off-street parking spaces are removed in the freeze area);
- the facility will not add parking to an area already adequately served by existing parking facilities or with adequate transit access;
- it will not contribute significantly to peak period traffic;
- it is located and designed so that the surrounding sidewalks and streets are sufficient to accommodate pedestrians and vehicular movements;
- it has satisfactory access to the major highway serving the area;
- it directly serves development in the surrounding area, and
- its design, including height, bulk, ground floor use, and landscaping, is in accordance with and consistent with architectural and land use patterns in the surrounding area and is itself aesthetically pleasing.

All non-commercial spaces, including residential, and reserved employee and visitor spaces are exempt from the freeze. However, the APCC must grant a special exemption before non-commercial facilities may be constructed.

The boundaries of the freeze area coincide with the area termed "Boston Proper". Boston's zoning code, which was revised in 1973 to eliminate minimum parking requirements for all but residential uses, established a Restricted Parking District (RPD), in which non-residential parking would be considered a Conditional Use, subject to Zoning Board of Appeal approval. The boundaries of the RPD include the freeze area, and extend to the medical area in the Fenway, and parts of South Boston and Dorchester down to

Columbia Point. Zoning Board of Appeal conditions on approval of facilities within the RPD include:

- the facility will serve a traffic demand not adequately provided for by public transportation, or
- it will replace existing off-street parking spaces in one or more nearby parking facilities, or it will replace legal on-street parking spaces that have been physically eliminated through permanent modification or elimination, or
- it is accessory and ancillary to a use which by its nature does not contribute significantly to traffic flows during peak traffic periods, or
- the facility constitutes a temporary parking lot use of land and that serious intent to reuse the land for an allowed use within a specified period of time has been demonstrated to the satisfaction of the Board of Appeal.

Thus, Boston has two overlapping mechanisms for controlling new parking construction. While criteria for approval are similar, the freeze provides a much stricter control tool.

## 2. Impacts of the Freeze to Date

The APCC began administering the freeze in 1976. In 1981, the City of Boston conducted a study<sup>1</sup> to assess its impacts to date. Major findings of this study were:

- The parking freeze has been successful at limiting the number of commercial spaces to the ceiling level of 35,503.
- Employee and other non-commercial spaces increased by 18% between 1973 and 1980 to a total of 20,260 spaces. However, this increase in non-commercial spaces is less than that which occurred in the five years between 1968 and 1973 (a 35% increase).
- Downtown development has proceeded at a healthy pace, unimpeded by the freeze. Between 1973 and 1980, over 8 million square feet of office space were completed, and 5 million additional square feet were under construction.

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<sup>1</sup>Ellen Collins, Boston Redevelopment Authority, Transportation Planning Department, "Downtown Boston Parking Programs", prepared for the Traffic and Parking Department, City of Boston, sponsored by the Metropolitan Area Planning Council, July, 1981.



- The parking freeze has been a contributing factor in restraining automobile usage, further encouraging the use of mass transit, and thus keeping air pollution in check. Between 1964 and 1974, automobile travel to Boston proper increased 20% and transit ridership declined by 11%. Between 1973 and 1980, the split between transit and automobile trips to the downtown did not change significantly.
- The parking freeze has been a valuable tool for preventing the proliferation of open lots downtown, and preserving older buildings which may otherwise have been demolished for parking.

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### 3. Changes in the Downtown Environment Since 1973

While the freeze has been very successful at achieving its objectives, a number of changes have occurred since 1973 which provide reason for giving serious consideration to modifying the freeze:

- Unprecedented downtown development has occurred, increasing office square footage by 35 percent between 1973 and 1982.
- An additional 6 million square feet of office and retail space are planned to come on line between 1982 and 1985.
- Peak occupancies of downtown parking facilities have increased from 82 percent in 1972 to 93% in 1982. This occupancy level is sufficiently high to trigger concern about meeting the needs of new development, and in particular, the midday parker.
- Presently, more than 5000 cars are parking in surface lots in the Fort Point Channel, which presently serves as a "pressure valve" for financial district parking needs. As development replaces surface lots in this area, the parking needs of both the Fort Point Channel and the financial district will have to be addressed.
- Increasing development of the Fort Point Channel area, which is not now included in the freeze area, could potentially result in provision of parking for more cars than the street system can efficiently handle. Further, there is a danger that the existing residential areas of South Boston on the fringe of the development area would be threatened by an influx of parking lots and traffic.
- The proliferation of surface lots in East Boston (which is also not included in the freeze area) many of which cater to airport users, is and may continue to infringe on residential neighborhoods in the area.
- The economics of parking construction have changed dramatically, due to rising interest rates and construction costs. This change has made many developers reluctant to build more parking than they feel is absolutely necessary for the economic viability of their buildings.

- Recent downtown parking initiatives in Boston have emphasized meeting the needs of residents and short-term parkers through reserving on-street space in neighborhoods for residential use, expanding the overall on-street parking supply and strictly enforcing these spaces to maintain a high turnover.
- Many surface lots are parking far more cars than their official licensed capacities. The City of Boston will be relicensing these at higher capacities, which could remove as many as 690 spaces from the bank.<sup>1</sup>
- New, innovative strategies are being successfully pursued in many cities throughout the country, which make approval of new development contingent on developer and/or employer commitments to transit and ridesharing incentive programs. These programs have proved to be very effective in increasing the use of transit, carpools and vanpools to the site, which alleviates traffic and parking pressures.

#### 4. Recommended Freeze Modifications

With occupancies of downtown public parking facilities presently at 93 percent, a projected parking space deficit of 8114 spaces by 1985, and 22,632 spaces by 1990, meeting the access needs of future development is a serious concern. Simply relaxing the freeze to allow construction of more parking to satisfy the projected deficit is not a desirable option, on traffic congestion, air quality and economic feasibility grounds. Instead, options should be considered which make the freeze into a more flexible tool for managing future downtown access by (a) increasing parking supply in specific locations on the fringes of downtown where growth in automobile trips can be efficiently handled by the street system and encouraging better use of existing parking facilities, (b) ensuring that adequate space is reserved for midday parkers, (c) encouraging increased use of transit, carpools, and vanpools for access to the downtown, and (d) protecting the residential neighborhoods in East Boston, and across the Fort Point Channel in South Boston.

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<sup>1</sup>This number was derived by subtracting the licensed capacities of lots in the study area from the number of vehicles observed during recent occupancy checks.

Recommended mechanisms for achieving these objectives are described in the following pages and summarized in Table 1.

MODIFICATION A-1: INCREASE SOUTH STATION SUPPLY

DESCRIPTION: Expand the freeze bank to include an additional 500 spaces at South Station, and an additional 2,500, conditional on a facility designed with a direct link to the highway system. These additional spaces would only be available for allocation to the South Station development site, and not to the rest of the freeze area.

RATIONALE: This modification is aimed at increasing the downtown parking supply to accommodate the access needs of new development, in a manner that will minimize impacts on traffic. South Station is one of the few locations where sufficient roadway capacity exists to handle additional peak period automobile trips. Its fringe location and proximity to the highway system also mean that adding parking will not significantly increase traffic through neighborhoods or on the downtown street network.

Mechanisms for increasing the South Station parking supply by up to 3,000 spaces are presently being studied. These involve incorporating a direct link between the parking facility and the highway system. If and when such a design is committed to, an increase of 3,000 spaces for South Station should be instituted.

IMPACTS: The downtown public parking supply would be increased by between 500 and 3,000 spaces. While the primary use of these spaces would be for commuter (long-term) parking, additional peak traffic could be accommodated without significant deterioration in traffic flow conditions.

Increased parking supply would serve new development in the South Station area, and would accommodate some of the financial district employees now parking in the Fort Point Channel when surface lots there are replaced by new development.

MODIFICATION A-2: INCREASE NORTH STATION SUPPLY

DESCRIPTION: Expand the freeze bank to include an additional 1,500 spaces at North Station. These additional spaces would only be available for allocation to the North Station development site, and not to the rest of the freeze area.

RATIONALE: Aside from South Station, North Station is the only other logical downtown location for significantly expanding the parking supply without adversely impacting traffic conditions. Assuming that minor improvements are made to the Central Artery, an additional 1,500 parking spaces could be added to the North Station area (Zone 3), assuming that the majority of new vehicles would use the Leverett Circle bridge for access to the site.

IMPACTS: Increased public parking availability in the North Station area over and above what would be possible without modifying the freeze.



# MODIFICATION B: CONVERSION OF EMPLOYEE SPACES TO PUBLIC SPACES

**Description:** Allow existing freeze-exempt employee spaces (which have been granted exemptions by December 31, 1983) to be opened up to the public for a fee and expand the freeze bank accordingly.

**Rationale:** This modification would serve two purposes. First, it would allow spaces in existing reserved employee facilities which are not now used to be made available for public parking. Second, opening employee facilities to the public for a charge would have the added benefit of adequately pricing scarce downtown parking facilities.

**Impacts:** There are approximately 13,000 reserved employee parking spaces downtown in 134 garages and lots: 42 percent are owned by federal, state and local government organizations, 22 percent by institutional employers (museums, hospitals, churches, charitable organizations, and schools), and 36 percent by other private employers. Average peak occupancy of private facilities is currently 90 percent. If one half of existing reserved employee spaces were opened to the public, an additional 650 spaces (= 10 percent of 6500) would be made available. While many employers feel that reserved employee parking is an important fringe benefit, it is also an expensive one. This freeze modification would provide an incentive for employers to open their facilities to the public, by offering them the opportunity to realize revenues from parking.

A number of studies have shown that employer-provided free parking is an extremely important incentive for commuters to drive alone to work, rather than using transit or ridesharing. One of these studies<sup>1</sup> estimates that approximately 20 percent of those who now drive alone and receive free parking would form carpools or begin using transit to work if required to pay for parking. Applying this figure to the Boston situation (assuming 50 percent of those parking in reserved employee facilities do so for free), overall demand for parking would be reduced by between 440 and 1300 spaces.<sup>2</sup>

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<sup>1</sup>Shoup, Donald, and Pickrell, D., "Free Parking as a Transportation Problem," DOT-RSPA-OPB-50/80/16, October, 1980

<sup>2</sup>The low estimate assumes all 20 percent would shift to carpools; the high estimate assumes all would shift to transit.

MODIFICATION C: MIDDAY PARKING BANK

DESCRIPTION: Expand the freeze bank to include a "midday parking bank" starting January 1, 1984. Spaces would be added to this bank as existing private employee facilities are physically eliminated. Spaces from this bank would be allocated for new facilities on the condition that they would not open before 10 a.m. on weekday mornings.

RATIONALE: Meeting the parking needs of shoppers and visitors to the downtown is an important goal of the City. Observed average occupancies of parking facilities at 10 a.m. are nearing the 90 percent mark, which means that many facilities are full by the time shoppers and other visitors arrive downtown. Future commuter parking demand projections indicate that even if the downtown parking supply were expanded considerably, commuters would continue to occupy most of the spaces and there would still be an availability problem for other kinds of parkers. Therefore, efforts should be made to begin reserving a portion of the downtown parking supply for non-commuter use.

IMPACTS: The maximum number of parking spaces which could potentially be "deposited" into the short-term parking bank is 13,400, the total number of reserved employee spaces. However, those in lots (8545) are more likely to be eliminated. The actual number of these employee spaces which will be eliminated over the next 5-10 years is difficult to predict. Assuming that past trends will continue, between 150 and 200 employee spaces per year would be eliminated, which means that 300-400 would be eliminated by the end of 1985, and 1050-1400 would be eliminated by the end of 1990. Therefore, this modification could result in up to 1400 reserved short-term parking spaces downtown by 1990.

MODIFICATION D: ADDITIONAL FREEZE CRITERION - MIDDAY PARKING NEEDS

DESCRIPTION: Add to the existing freeze criteria: "The facility will serve non-commuter parking needs in the area."

RATIONALE: Because of the projected shortage of visitor/shopper parking in Boston, it is important to ensure that newly constructed facilities will accommodate non-commuter parking needs, in addition to serving all-day parkers. Each new parking facility proposal should be evaluated with respect to existing and projected short-term parking needs in the area, and steps should be taken to ensure that a portion of the facility's capacity will be available for parkers arriving in the middle of the day. Such steps might include: opening a portion of the facility after 10 a.m. or establishing a pricing structure in which the all-day rate is more than 4-5 times the 1-hour rate.

IMPACTS: This modification will only impact new facilities which require freeze permits. At present, only 610 spaces are available in the freeze bank. An additional 3000 spaces may be added to the bank from the four city garages which will be sold (Government Center, Kilby St., St. James Ave., and Fort Hill Sq.), as well as potentially 900 spaces which are now in open lots in the North Station development area. All together, 5310 spaces might be available for freeze permits in the next five to ten years (in the existing freeze area). If other recommended modifications are approved, at least 2000 spaces at North and South Stations and 3500 in the Fort Point Channel area would be added as well, for a total of 10,810 spaces. The portion of these new spaces to be reserved for short-term parking would depend on identified needs at particular locations. While demand projections indicate an additional 3700 spaces needed for short-term parkers by 1985, and an additional 7500 needed (over the present) by 1990, it is unlikely that this many spaces would be reserved. Twenty-five percent of the total spaces, or 2700 spaces is a reasonable estimate of the number which might ultimately be reserved as a result of this modification. (This number is net of the number to be reserved as a result of modification C.)

MODIFICATION E-1: ACCESS PLANS FOR ACCESSORY PARKING APPROVAL

**DESCRIPTION:** Make freeze permits for new public parking facilities and granting of exemptions for employee spaces which are ancillary to developments over 100,000 gross square feet contingent on BAPCC review and BRA approval of an access plan for the site, which includes an analysis of expected peak and off-peak travel to the site, and commits to traffic mitigation measures.

**RATIONALE:** In order to accommodate planned and proposed future development, it will be important to encourage increased use of vanpools, carpools and transit by commuters to downtown. One of the most effective ways of doing this is through marketing these alternatives and offering incentives and assistance at the work-site. A number of cities, including San Francisco and Seattle, are incorporating "access planning" into their development review and approval processes, which requires developers to analyze and mitigate the traffic impacts of their new developments. This approach makes sense for Boston, given the amount of development the city would like to attract and the limited capacity of the street system to handle additional traffic.

**IMPACTS:** This modification, along with E-2, will result in the establishment of transit and ridesharing marketing and incentive programs in new major developments. This in turn, will encourage greater use of transit and provide employees with increased carpooling and vanpooling opportunities. The impacts on traffic and parking demand are difficult to predict, though if 100 additional vanpools were established (there are presently about 100 in use by downtown commuters; as a comparison, Aetna in Hartford has 100 alone), this would reduce future commuter parking demand by 900 spaces.

However, a reasonable yet ambitious parking reduction goal for this strategy, in combination with other ridesharing and transit incentives and driving disincentives discussed in the body of this report is 13,250 spaces. This assumes that 150 commuters who would otherwise drive alone (given present commute conditions) would form vanpools, 150 would form three-person carpools, and 11,000 would ride either the MBTA or newly-formed subscription bus services.



MODIFICATION E-2: ACCESS PLANS FOR MAJOR DEVELOPMENT APPROVAL

- DESCRIPTION: Amend Section 6-3A of Boston's Zoning Code to require BAPCC review and BRA approval of access plans for new developments with over 100,000 gross square feet within the Restricted Parking District.
- RATIONALE: Same as for E-1.
- IMPACTS: This would make approval of all large developments (with or without accessory parking) contingent on an acceptable access plan. Impacts are discussed under E-1.



MODIFICATION F: ADDITIONAL FREEZE CRITERION - FACILITY DESIGNS FOR VANPOOLS VEHICLES

- DESCRIPTION: Add the following criterion for freeze approval: "The facility is designed to accommodate vanpool vehicles."
- RATIONALE: Vanpooling is a commuting option which has considerable potential for providing future access to the downtown in an efficient manner. Parking facilities should be designed so that clearances and striping of spaces will accommodate vanpool vehicles.
- IMPACTS: The modification will prevent construction of new parking facilities which do not allow for vanpool access, thus assuring that vanpoolers will have the same parking opportunities as people commuting in smaller vehicles.

MODIFICATION G-1: FORT POINT CHANNEL/SOUTH BOSTON PARKING MANAGEMENT DISTRICT

DESCRIPTION: Establish a new "parking management district" encompassing the Fort Point Channel area (Zone 12) and South Boston. Freeze the number of total public parking spaces in this area at the existing 3500 spaces (to be increased if roadway capacity improvements presently under consideration are made). Make approval of new facilities in this area subject to existing BAPCC freeze criteria with the following additional one: "The facility will not increase traffic through residential neighborhoods or displace existing residential land uses."

RATIONALE: Over 1.4 million square feet of development is planned or proposed for the Fort Point Channel area. This development will displace open parking lots which presently park over 5000 cars, and will create the demand for an additional 4500 parking spaces. With the present number of parking spaces, the Northern Avenue bridge is already operating at capacity during peak hours. Thus, unless capacity improvements are made, allowing much more than 5000 parking spaces in this area may worsen an already severe congestion problem.

There is also the concern that the high demand for parking in this area could result in developers acquiring now-residential land for parking facility construction, which would adversely affect the South Boston neighborhood.

IMPACTS: This modification would limit parking supply in the Fort Point Channel area to a level which is in line with existing traffic capacity constraints. It would also protect residential neighborhoods from traffic and parking pressures.

MODIFICATION G-2: EAST BOSTON PARKING MANAGEMENT DISTRICT

DESCRIPTION: Establish a new "parking management district" encompassing East Boston. Make approval of new facilities in this area subject to existing BAPCC freeze criteria and the additional one: "The facility will not increase traffic through residential neighborhoods or displace existing residential uses."

RATIONALE: The proliferation of surface lots in East Boston has raised concerns about resultant impacts on the neighborhoods, namely, displacement of residential uses and increased traffic through neighborhoods as a result of new parking facilities.

IMPACTS: Making approval of new parking facilities subject to the "neighborhood protection" freeze criterion above, and the others, including the one stating that no commercial off-street parking should be added to an area which is already adequately served by existing parking facilities should discourage further proliferation of lots in the area.

## 5. Impacts of the Recommended Modification Package

The recommended package of modifications to the parking freeze and city zoning code provides for a controlled expansion of the downtown commercial parking supply, while emphasizing management of the parking supply in order to improve overall utilization and reservation of spaces for midday (non-commuter) parkers. It also incorporates measures to manage future access to the downtown by involving developers and employers in programs which mitigate potential traffic and parking impacts of developments. Finally, it establishes mechanisms to protect neighborhoods now outside of the freeze area from traffic and parking pressures.

The following table summarizes the quantitative impact assessments of the individual measures:

<u>Modification</u>	<u>Increase in Public Parking Supply</u>	<u>Potential No. of Spaces Reserved For Midday Parkers</u>	<u>Potential Reduction in Commuter Park- ing Demand</u>
A-1 Increase South Station Supply	500-3000		
A-2 Increase North Station Supply	1500		
B Conversion of Employee Spaces to Public Spaces	650 <sup>1</sup>		[440-1300] <sup>2</sup>
C Midday Parking Bank	1050-1400 <sup>1</sup>	1050-1400	
D Midday Parking Needs Criteria		2700	
E-1 & Access Plans			13,250
E-2			
TOTALS	3700-6550	2750-4100	13,250

<sup>1</sup>would be matched by equivalent decreases in private spaces, and thus would not reduce overall parking deficit.

<sup>2</sup> Included in estimated demand reduction for E-1 and E-2.

The numbers shown above are meant to indicate "order of magnitude" impacts of the modifications package, and must be interpreted in close

association with the assumptions on which they are based. However, they indicate that a substantial proportion of the overall public supply increase would be offset by spaces reserved for midday parkers. Thus, the modifications would enable the city to accommodate many more midday parkers than it could otherwise, while increasing the public parking supply available for commuters only slightly.

The air quality implications of the proposed modifications--particularly of an increase in the public parking supply must be assessed by comparing two future scenarios, with and without modifications.

The number of peak automobile trips bound for downtown Boston in 1990 will depend on the amount of development which occurs between now and then, the total (public and private) parking supply, and "exogenous" factors, such as street capacity and the level of transit service available. It is unlikely that the proposed modifications will significantly affect the amount of development which occurs; this will be determined by economic conditions and larger-scale transportation access changes, such as transit service and street capacity improvements.

The impact of the modifications on the total parking supply is difficult to predict, as the number of private spaces would still not be limited by the freeze. Assuming that the same ratio of private spaces per 1000 sq. ft. would be built as between 1968 and 1982, with or without the modifications, total supply would be at most eight percent higher than it would be without them. This is conservative, as it is likely that more private spaces would be built without the modification rather than less.

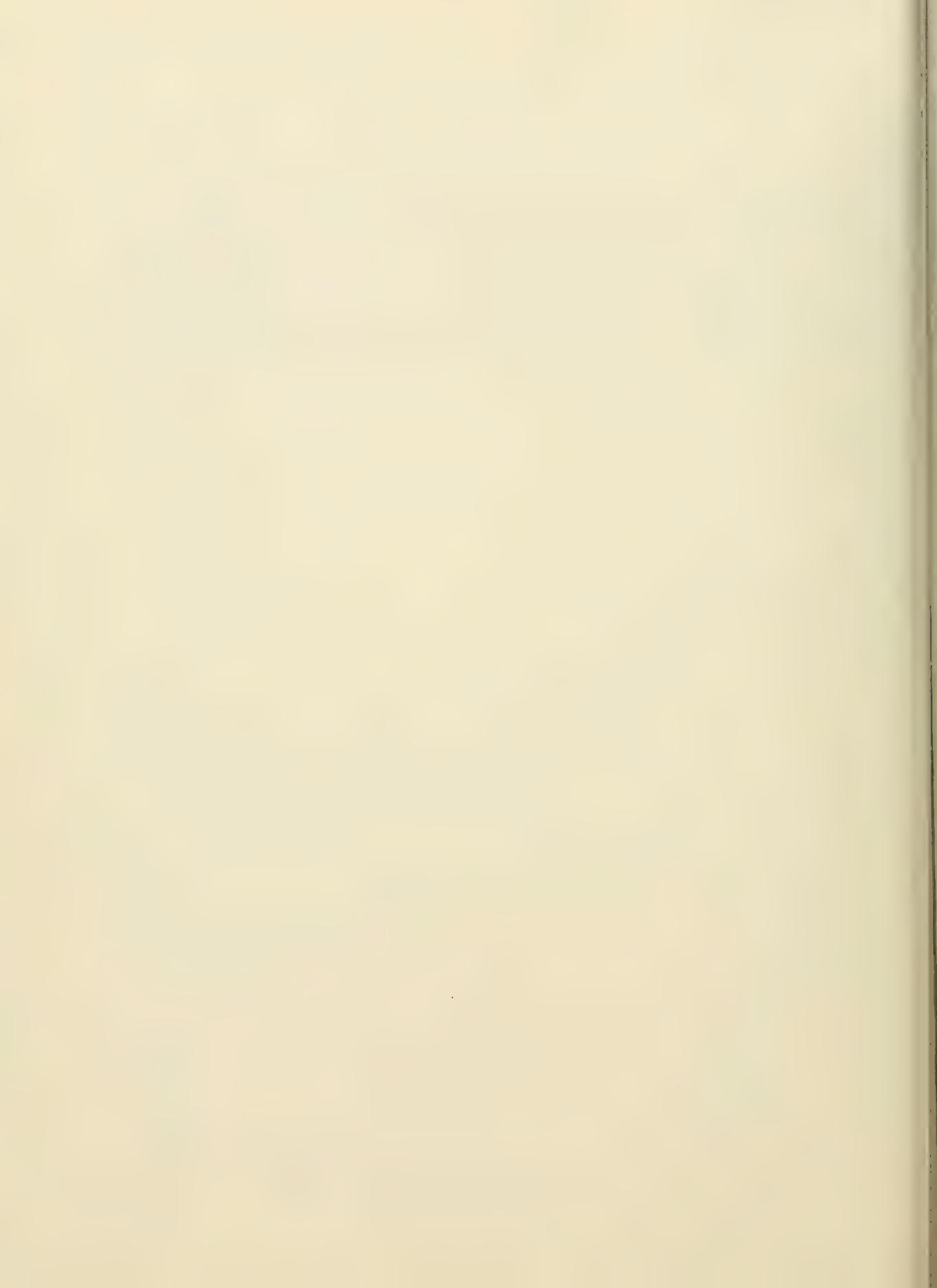
Despite the potential increases in parking supply which may occur with the modifications, the number of commuters parking downtown is likely to be the same as it would be without the modifications. This is due to the fact that without the modifications, commuters would occupy most (if not all) of the downtown parking supply. The modifications ensure that a portion of spaces are reserved for midday parkers.

Thus, peak period automobile travel is not likely to be significantly higher if the modifications are instituted (as compared to a "no action" scenario). All-day vehicle miles of travel are likely to be higher, as more downtown parking spaces would be used by short-term parkers.



In sum, the proposed freeze modifications will not have a major impact on future travel patterns. Rather, they will provide the City with policy tools for accommodating future development in a manner which minimizes negative impacts such as reduction in space available for short-term parkers, spillover parking in neighborhoods and illegal on-street parking, and encourages developers and employers to become more involved in providing opportunities and incentives for more efficient ways of commuting.

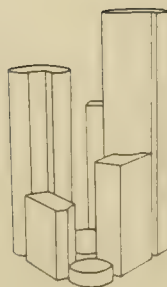




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# Air Quality

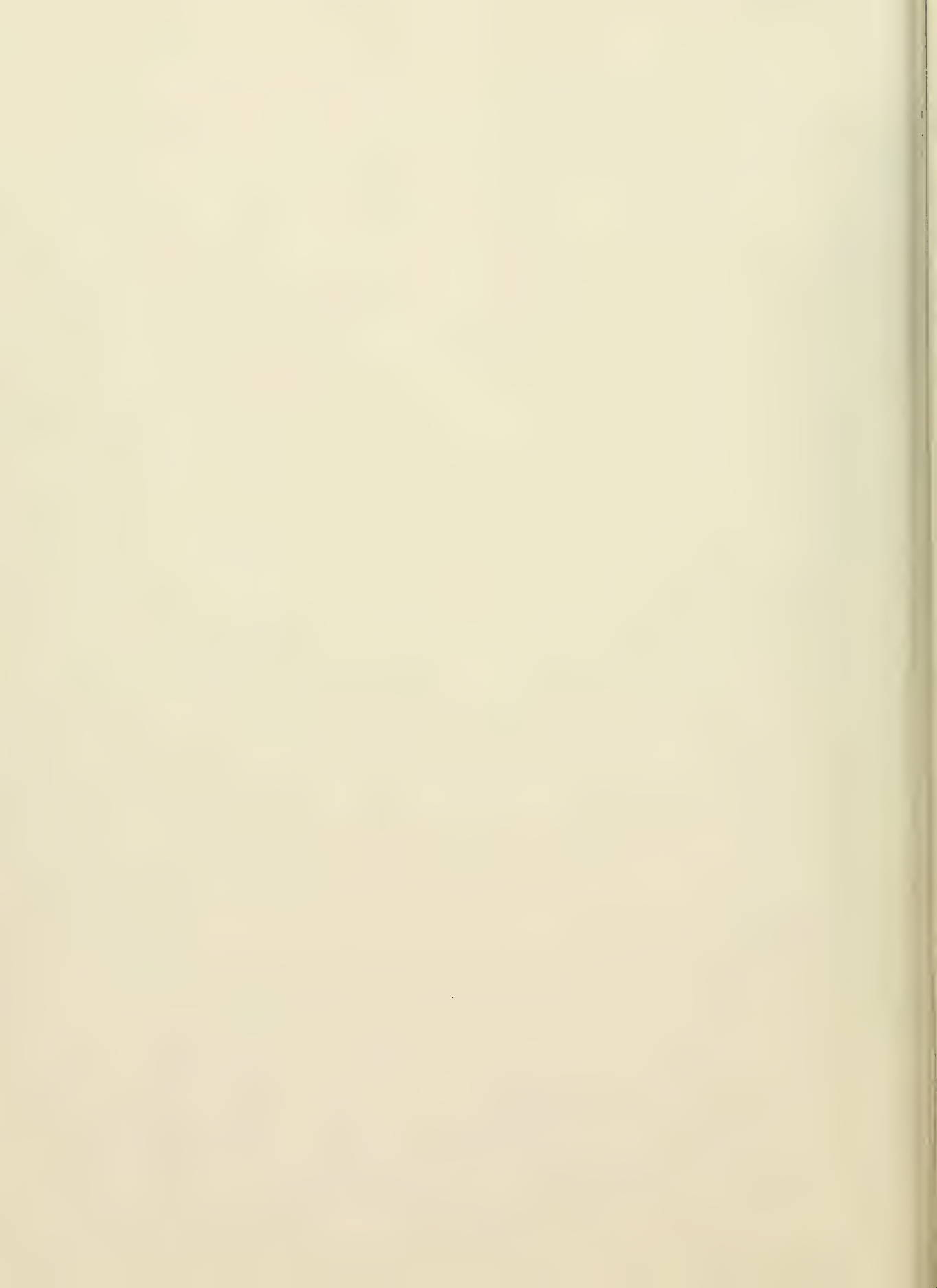






AQ APPENDIX B

INTERSECTION ANALYSIS WORKSHEETS



WORKSHEET 1 - TRAFFIC INFORMATION

Intersection Atlantic Ave and Surface Artery  
Case # 1 Year 1984

1. Road segment or intersection approach identification	SN	AN	AS	SS
2. Observed 1-hr volume (vph)	1010	1176	602	981
Observed 8-hr volume (vph)	707	929	476	687
Projected 1-hr peak demand (vph)	---	---	---	---
Projected 8-hr peak demand (vph)	---	---	---	---
3. Percentage cold starts	50/20.6	---	---	---
4. Percentage trucks and buses	5.8	---	---	---
5. Metropolitan population	---	---	---	---
6. Slope	---	---	---	---
7. Free-flow parameters				
Number of lanes	2	2	3	3
Average lane width (ft)	12	12	11	12
Design speed (mph)	28/35	26/32	22/26	24/29
Highway type (see Figures 2-5)	Urban Arteries			
8. Intersection parameters				
Intersection designation	---	---	---	---
Approach width (ft)	---	---	---	---
Percentage right turns	0	40	0	0
Percentage left turns	11	45	81	0
Type control and description of signal controller	---	---	---	---
9. Area source parameters				
Parking lot gate designation	---	---	---	---
Projected 1-hr peak entrance demand (vph)	---	---	---	---
Projected 1-hr peak exit demand (vph)	---	---	---	---
Projected 8-hr peak entrance demand (vph)	---	---	---	---
Projected 8-hr peak exit demand (vph)	---	---	---	---
Parking lot area (m <sup>2</sup> )	---	---	---	---
Parking lot capacity (veh)	---	---	---	---
Running time required to access auxiliary parking (s)	---	---	---	---
Facility emptying time	---	---	---	---
Average cars per stall	---	---	---	---
Average area per stall (m <sup>2</sup> )	---	---	---	---

SS right turns  
have no conflicts

SN = Surface Artery N.B. (Xway offramp)

AN = Atlantic Ave N.B. to WB

AS = Atlantic Ave SB to WB

SS = Surface Artery SB

WORKSHEET 1 - TRAFFIC INFORMATION

Intersection Atlantic Avenue and Surface Artery  
 Case # 2 Year 1990

1. Road segment or intersection approach identification	SN	AN	AS	SS	HE
2. Observed 1-hr volume (vph)	---	---	---	---	---
Observed 8-hr volume (vph)	---	---	---	---	---
Projected 1-hr peak demand (vph)	<u>1507</u>	<u>1480</u>	<u>888</u>	<u>1036</u>	204
Projected 8-hr peak demand (vph)	<u>1055</u>	<u>1169</u>	<u>702</u>	<u>725</u>	137
3. Percentage cold starts	<u>50/20.6</u>	---	---	---	---
4. Percentage trucks and buses	<u>5.8</u>	---	---	---	---
5. Metropolitan population	---	---	---	---	---
6. Slope	---	---	---	---	---
7. Free-flow parameters					
Number of lanes	<u>2</u>	<u>2</u>	<u>3</u>	<u>3</u>	2
Average lane width (ft)	<u>12</u>	<u>12</u>	<u>11</u>	<u>12</u>	12
Design speed (mph)	<u>28/35</u>	<u>26/32</u>	<u>22/26</u>	<u>24/29</u>	24/30
Highway type (see Figures 2-5)	<u>Urban Arterials</u>				
8. Intersection parameters					
Intersection designation	---	---	---	---	---
Approach width (ft)	<u>0</u>	<u>0</u>	<u>0</u>	<u>0</u>	100
Percentage right turns	<u>14</u>	<u>60</u>	<u>100</u>	<u>0</u>	0
Percentage left turns	---	---	---	---	---
Type control and description of signal controller	---				---
9. Area source parameters					
Parking lot gate designation	---	---	---	---	---
Projected 1-hr peak entrance demand (vph)	---	---	---	---	---
Projected 1-hr peak exit demand (vph)	---	---	---	---	---
Projected 8-hr peak entrance demand (vph)	---	---	---	---	---
Projected 8-hr peak exit demand (vph)	---	---	---	---	---
Parking lot area (m <sup>2</sup> )	---	---	---	---	---
Parking lot capacity (veh)	---	---	---	---	---
Running time required to access auxiliary parking (s)	---	---	---	---	---
Facility emptying time	---	---	---	---	---
Average cars per stall	---	---	---	---	---
Average area per stall (m <sup>2</sup> )	---	---	---	---	---

WORKSHEET 1 - TRAFFIC INFORMATION

Intersection Atlantic Ave And Surface Artery  
 Case # 3 Year 1990

1. Road segment or intersection approach identification	SN	AN	AS	SS	HE
2. Observed 1-hr volume (vph)	---	---	---	---	---
Observed 8-hr volume (vph)	---	---	---	---	---
Projected 1-hr peak demand (vph)	1512	1528	888	1104	212
Projected 8-hr peak demand (vph)	1058	1207	702	773	142
3. Percentage cold starts	50	20.6	---	---	---
4. Percentage trucks and buses	5.8	---	---	---	---
5. Metropolitan population	---	---	---	---	---
6. Slope	---	---	---	---	---
7. Free-flow parameters	---	---	---	---	---
Number of lanes	2	2	3	3	2
Average lane width (ft)	12	12	11	12	12
Design speed (mph)	28/35	26/32	22/26	24/29	24/30
Highway type (see Figures 2-5)	Urban Arterial				---
8. Intersection parameters	---	---	---	---	---
Intersection designation	---	---	---	---	---
Approach width (ft)	---	---	---	---	---
Percentage right turns	0	0	0	0	100
Percentage left turns	14	58	100	0	0
Type control and description of signal controller	---	---	---	---	---
9. Area source parameters	---	---	---	---	---
Parking lot gate designation	---	---	---	---	---
Projected 1-hr peak entrance demand (vph)	---	---	---	---	---
Projected 1-hr peak exit demand (vph)	---	---	---	---	---
Projected 8-hr peak entrance demand (vph)	---	---	---	---	---
Projected 8-hr peak exit demand (vph)	---	---	---	---	---
Parking lot area (m <sup>2</sup> )	---	---	---	---	---
Parking lot capacity (veh)	---	---	---	---	---
Running time required to access auxiliary parking (s)	---	---	---	---	---
Facility emptying time	---	---	---	---	---
Average cars per stall	---	---	---	---	---
Average area per stall (m <sup>2</sup> )	---	---	---	---	---



WORKSHEET B - CAPACITY ANALYSIS

Intersection Atlantic Ave And Surface Artery  
 Case # 1 Year 1990

Step	Symbol	Input/Units	SN	AN	AS	SS
1	i	Road segment (or approach) designation				
2		<u>Free flow capacity computation:</u>				
2.1	M <sub>i</sub>	Number of lanes				
2.2	W <sub>p</sub>	Adjustment for lane width (Table B-1)				
2.3	T <sub>i</sub>	Adjustment for trucks (Table B-2)				
2.4	C <sub>i</sub>	Free flow capacity				
3		<u>Signalized intersection capacity:</u>				
3.1	j	Green signal phase identification	A	B	E	D
3.2	wa <sub>i</sub>	Approach width with parking (ft)	32	32	30	52
3.3		Percent right turners	0	0	100	0
3.4		Percent left turners	0	11	0	0
3.5		Metropolitan area size				
3.6	Cs <sub>i,j</sub>	Capacity service volume (vph or green)	3500	3200	1750	3500
4		<u>Signalized intersection green phase and cycle length:</u>				
4.1	V <sub>i,j</sub>	Demand Volume for approach and phase				
4.2	V <sub>i,j</sub> /Cs <sub>i,j</sub>	Volume to green capacity ratio				
4.3	approx G/Cy	Approximate G/Cy				
4.4	Σmax(V <sub>i,j</sub> /Cs <sub>i,j</sub> ) <sub>j</sub>	Sum of the maximum V/C ratios for each signal phase				
4.5	Cy	Signal cycle time (sec)				
4.6	Gj	Green phase length				
4.7	Gj/Cy	Green phase to cycle time ratio				
4.8	C <sub>i,j</sub>	Capacity for approach i phase j				
5		<u>Two-way stop, two-way yield or uncontrolled intersection:</u>				
5.1	V <sub>m</sub> +V <sub>n</sub>	Major street two-way volume				
5.2	C <sub>i</sub>	Cross street capacity				
6		<u>Four-way stop intersections:</u>				
6.1	V <sub>i</sub>	Approach volume				
6.2	Sp <sub>i</sub>	Demand split on cross streets				
6.3	C <sub>i</sub>	Capacity of approach				
7	C <sub>i</sub>	Approach capacity Σ C <sub>i,j</sub> 5.2 for a four-way stop or 6.3 for a two-way stop				

ΦA S.N. All Movements and A.N Right 12s.  
 ΦB S.N. Left and Straight, SS and  
     A.N. Right 46s.  
 ΦC A.S 18s.  
 ΦD A.N. All Movements 24s.  
 Total 100s.

Traffic is assumed  
 to move on amber.  
 ΦE = ΦA + ΦB = 58s  
 ΦF = 100s.

WORKSHEET B - CAPACITY ANALYSIS

Intersection Atlantic Ave and Surface Artery  
Case # 2, 3 Year 1990

Step	Symbol	Input/Units	SN	AN	AS	SS
1	1	Road segment (or approach) designation	SN	AN	AS	SS
2		Free flow capacity computation:				
2.1	$M_i$	Number of lanes				
2.2	$W_p$	Adjustment for lane width (Table B-1)				
2.3	$T_i$	Adjustment for trucks (Table B-2)				
2.4	$C_i$	Free flow capacity				
3		Signalized intersection capacity:				
3.1	j	Green signal phase identification	A	B	E	D
3.2	$W_{a1}$	Approach width with parking (ft)	32	32	20	32
3.3		Percent right turners	0	0	100	0
3.4		Percent left turners	0	14	0	0
3.5		Metropolitan area size				
3.6	$CS_{1,j}$	Capacity service volume (vph or green)	3500	3200	1750	3500
4		Signalized intersection green phase and cycle length:				
4.1	$V_{1,j}$	Demand Volume for approach and phase				
4.2	$V_{1,j}/CS_{1,j}$	Volume to green capacity ratio				
4.3	approx G/Cy	Approximate G/Cy				
4.4	$\sum \max(V_{1,j}/CS_{1,j})$	Sum of the maximum V/C ratios for each signal phase				
4.5	Cy	Signal cycle time (sec)				
4.6	Gj	Green phase length				
4.7	Gj/Cy	Green phase to cycle time ratio				
4.8	$C_{1,j}$	Capacity for approach i phase j				
5		Two-way stop, two-way yield or uncontrolled intersection:				
5.1	$V_m + V_n$	Major street two-way volume				
5.2	$C_1$	Cross street capacity				
6		Four-way stop intersections:				
6.1	$V_1$	Approach volume				
6.2	Sp1	Demand split on cross streets				
6.3	$C_1$	Capacity of approach				
7	$C_1$	Approach capacity $\sum C_{1,j}$ 5.2 for a four-way stop or 6.3 for a two-way stop				

HE

Cross  
street  
Capacity

Case 2

$$3222 \div 2 / 2255 \div 2$$

$$248 / 364$$

Case 3

$$3303 \div 2 / 2312 \div 2$$

$$240 / 357$$

HE Capacity is based on a 4.5 sec critical gap  
Signal Timing:

$$\phi A = 11$$

$$\phi B = 38$$

$$\phi C = 24$$

$$\phi D = 27$$

$$\phi E = \phi A + \phi B = 49$$

$$\text{Total} = 100$$

## EPA VOLUME 9 (REVISED) INDIRECT SOURCE GUIDELINE MODEL - WORKSHEET #2

INTERSECTION: ATLANTIC AVE AND SURFACE ARTERY  
CASE # 1 YEAR: 1984 AVERAGING TIME: 1-HOUR

LINE 1	ROAD SEGMENT ID	SN	AN	AS	SS
LINE 2	DEMAND VOLUME (VPH)	1010	1176	602	981
LINE 4	CRUISE SPEED (MPH)	28	26	22	24
LINE 5	FREE-FLOW EMISSIONS (G-VEH/M)	0.0409	0.0443	0.0519	0.0408
LINE 6.1	NUMBER OF LANES	2	2	3	3
LINE 6.3	CAPACITY SERVICE VOLUME (VPH OF GREEN)	3500	1750	3800	3200
LINE 6.3	CAPACITY SERVICE VOLUME (VPH OF GREEN)	3200	3500	0	4800
LINE 6.4	DEMAND VOLUME (VPH)	209	471	602	103
LINE 6.4	DEMAND VOLUME (VPH)	881	705	0	878
LINE 6.5	SIGNAL CYCLE LENGTH (S)	100			
LINE 6.6	GREEN PHASE LENGTH (S)	12	58	18	100
LINE 6.6	GREEN PHASE LENGTH (S)	46	24	0	46
LINE 6.7	CAPACITY (VPH)	1892	1855	684	5408
LINE 6.8	PROPORTION OF VEHICLES THAT STOP	0.936	0.575	0.974	0.0
LINE 6.8	PROPORTION OF VEHICLES THAT STOP	0.720	0.952	0.0	0.651
LINE 6.9	NUMBER OF VEHICLES THAT STOP PER CYCLE	5.433	7.519	16.293	0.0
LINE 6.9	NUMBER OF VEHICLES THAT STOP PER CYCLE	16.027	10.637	0.0	16.118
LINE 7.0	AVERAGE NUMBER OF VEHICLES IN QUEUE	1.15	1.73	7.34	0.22
LINE 8.0	LENGTH OF QUEUE (M/LANE)	49.17	60.66	34.27	23.69
LINE 9.0	AVERAGE EXCESS RUNNING TIME (S/VEH)	26.12	29.87	78.59	16.12
LINE 10.	EMISSIONS FROM ACCELERATION (G/VEH-M)	0.103	0.109	0.120	0.113
LINE 11.	EMISSIONS FROM DECELERATION (G/VEH-M)	0.034	0.036	0.041	0.039
LINE 12.	EMISSION RATE FOR ACC. AND DEC. (G/M-S)	0.029	0.038	0.026	0.024
LINE 13.	LENGTH OF ACC. AND DEC. (M)	70.1	60.4	43.3	51.5
LINE 14.	LENGTH FOR EXCESS EMISSIONS (M)	140.2	120.9	86.5	103.0
LINE 15.	IDLING EMISSION RATE (G/S)	1.463	2.047	3.151	0.783
LINE 16.	AVERAGE EMISSION RATE (G/S-M)	0.0251	0.0359	0.0405	0.0199
LINE 17.	ADJUSTED EXCESS EMISSION RATE (G/S-M)	0.0332	0.0484	0.0743	0.0266
LINE 18	FREE-FLOW EMISSION RATE (G/S-M)	0.0115	0.0145	0.0087	0.0111

## EPA VOLUME 9 (REVISED) INDIRECT SOURCE GUIDELINE MODEL - WORKSHEET #2

INTERSECTION ATLANTIC AVE AND SURFACE ARTERIAL  
CASE # 1 YEAR 1984 AVERAGING TIME 8-HOUR

LINE	ROAD SEGMENT ID	SN	AN	AS	SS
LINE 2	DEMAND VOLUME (VPH)	707	929	476	687
LINE 4	CRUISE SPEED (MPH)	35	32	26	29
LINE 5	FREE-FLOW EMISSIONS (G/VEH/M)	0.0215	0.0238	0.0300	0.0266
LINE 6 1	NUMBER OF LANES	2	2	3	3
LINE 6 3	CAPACITY SERVICE VOLUME (VPH OF GREEN)	3500	1750	3800	3200
LINE 6 3	CAPACITY SERVICE VOLUME (VPH OF GREEN)	3200	3500	0	4800
LINE 6 4	DEMAND VOLUME (VPH)	146	372	476	72
LINE 6 4	DEMAND VOLUME (VPH)	561	557	0	615
LINE 6 5	SIGNAL CYCLE LENGTH (S)	100			
LINE 6 6	GREEN PHASE LENGTH (S)	12	58	18	100
LINE 6 6	GREEN PHASE LENGTH (S)	46	24	0	46
LINE 6 7	CAPACITY (VPH)	1892	1855	584	5408
LINE 6 8	PROPORTION OF VEHICLES THAT STOP	0.918	0.533	0.937	0.0
LINE 6 8	PROPORTION OF VEHICLES THAT STOP	0.655	0.904	0.0	0.619
LINE 6 9	NUMBER OF VEHICLES THAT STOP PER CYCLE	3.724	5.512	12.395	0.0
LINE 6 9	NUMBER OF VEHICLES THAT STOP PER CYCLE	10.204	13.984	0.0	10.581
LINE 7 0	AVERAGE NUMBER OF VEHICLES IN QUEUE	0.60	1.00	2.29	0.15
LINE 8 0	LENGTH OF QUEUE (M/LANE)	31.59	44.59	21.29	15.55
LINE 9 0	AVERAGE EXCESS RUNNING TIME (S/VEH)	23.51	27.02	50.48	15.07
LINE 10	EMISSIONS FROM ACCELERATION (G/VEH-M)	0.095	0.098	0.109	0.101
LINE 11	EMISSIONS FROM DECELERATION (G/VEH-M)	0.028	0.030	0.036	0.032
LINE 12	EMISSION RATE FOR ACC. AND DEC. (G/M-S)	0.017	0.025	0.018	0.014
LINE 13	LENGTH OF ACC. AND DEC. (M)	109.5	91.5	60.4	75.2
LINE 14	LENGTH FOR EXCESS EMISSIONS (M)	219.0	183.1	120.9	150.4
LINE 15	IDLING EMISSION RATE (G/S)	0.823	1.352	1.521	0.449
LINE 16	AVERAGE EMISSION RATE (G/S-M)	0.0123	0.0199	0.0216	0.0100
LINE 17	ADJUSTED EXCESS EMISSION RATE (G/S-M)	0.0109	0.0178	0.0207	0.0085
LINE 18	FREE-FLOW EMISSION RATE (G/S-M)	0.0042	0.0061	0.0040	0.0051

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## EPA VOLUME 9 (REVISED) INDIRECT SOURCE GUIDELINE MODEL - WORKSHEET #2

INTERSECTION: ATLANTIC AVE AND SURFACE ARTERY  
CASE # 2 YEAR 1990 AVERAGING TIME 1-HOUR

LINE		SN	AN	AS	SS
LINE 1	ROAD SEGMENT ID				
LINE 2	DEMAND VOLUME (VPH)	1507	1480	888	1036
LINE 4	CRUISE SPEED (MPH)	28	26	22	24
LINE 5	FREE-FLOW EMISSIONS (G-VEH/M)	0.0198	0.0214	0.0251	0.0232
LINE 6.1	NUMBER OF LANES	2	2	3	3
LINE 6.3	CAPACITY SERVICE VOLUME (VPH OF GREEN)	3500	1750	3800	4800
LINE 6.3	CAPACITY SERVICE VOLUME (VPH OF GREEN)	3200	3500	0	0
LINE 6.4	DEMAND VOLUME (VPH)	350	593	888	1036
LINE 6.4	DEMAND VOLUME (VPH)	1157	887	0	0
LINE 6.5	SIGNAL CYCLE LENGTH (S)	100			
LINE 6.6	GREEN PHASE LENGTH (S)	11	49	24	38
LINE 6.6	GREEN PHASE LENGTH (S)	38	27	0	0
LINE 6.7	CAPACITY (VPH)	1601	1803	912	1824
LINE 6.8	PROPORTION OF VEHICLES THAT STOP	0.989	0.771	0.992	0.791
LINE 6.8	PROPORTION OF VEHICLES THAT STOP	0.971	0.978	0.0	0.0
LINE 6.9	NUMBER OF VEHICLES THAT STOP PER CYCLE	9.614	12.707	24.463	22.753
LINE 6.9	NUMBER OF VEHICLES THAT STOP PER CYCLE	31.211	24.092	0.0	0.0
LINE 7.0	AVERAGE NUMBER OF VEHICLES IN QUEUE	16.03	4.59	37.00	1.31
LINE 8.0	LENGTH OF QUEUE (M/LANE)	123.66	90.02	89.12	34.90
LINE 9.0	AVERAGE EXCESS RUNNING TIME (S/VEH)	69.38	38.44	183.74	27.10
LINE 10	EMISSIONS FROM ACCELERATION (G/VEH-M)	0.103	0.109	0.120	0.113
LINE 11	EMISSIONS FROM DECELERATION (G/VEH-M)	0.034	0.036	0.041	0.039
LINE 12	EMISSION RATE FOR ACC AND DEC (G/M-S)	0.056	0.053	0.039	0.035
LINE 13	LENGTH OF ACC. AND DEC. (M)	70.1	60.4	43.3	51.5
LINE 14	LENGTH FOR EXCESS EMISSIONS (M)	140.2	120.9	89.1	103.0
LINE 15	IDLING EMISSION RATE (G/S)	6.782	3.471	11.236	1.630
LINE 16	AVERAGE EMISSION RATE (G/S-M)	0.0763	0.0554	0.1452	0.0331
LINE 17	ADJUSTED EXCESS EMISSION RATE (G/S-M)	0.0484	0.0331	0.1013	0.0192
LINE 18	FREE-FLOW EMISSION RATE (G/S-M)	0.0083	0.0088	0.0062	0.0067



## EPA VOLUME 9 (REVISED) INDIRECT SOURCE GUIDELINE MODEL - WORKSHEET #2

INTERSECTION ATLANTIC AVE AND SURFACE ARTERY  
CASE # 2 YEAR 1990 AVERAGING TIME 8-HOUR

LINE	ROAD SEGMENT ID	SN	AN	AS	SS
LINE 2	DEMAND VOLUME (VPH)	1055	1169	702	725
LINE 4	CRUISE SPEED (MPH)	35	32	26	29
LINE 5	FREE-FLOW EMISSIONS (G-VEH/M)	0.0111	0.0122	0.0155	0.0137
LINE 6 1	NUMBER OF LANES	2	2	3	3
LINE 6 3	CAPACITY SERVICE VOLUME (VPH OF GREEN)	3500	1750	3800	4800
LINE 6 3	CAPACITY SERVICE VOLUME (VPH OF GREEN)	3200	3500	0	0
LINE 6 4	DEMAND VOLUME (VPH)	245	458	702	725
LINE 6 4	DEMAND VOLUME (VPH)	810	701	0	0
LINE 6 5	SIGNAL CYCLE LENGTH (S)	100			
LINE 6 6	GREEN PHASE LENGTH (S)	11	41	24	38
LINE 6 6	GREEN PHASE LENGTH (S)	38	27	0	0
LINE 6 7	CAPACITY (VPH)	1601	1803	912	1824
LINE 6 8	PROPORTION OF VEHICLES THAT STOP	0.957	0.696	0.932	0.730
LINE 6 8	PROPORTION OF VEHICLES THAT STOP	0.830	0.913	0.0	0.0
LINE 6 9	NUMBER OF VEHICLES THAT STOP PER CYCLE	6.513	9.050	18.178	14.708
LINE 6 9	NUMBER OF VEHICLES THAT STOP PER CYCLE	18.678	17.775	0.0	0.0
LINE 7 0	AVERAGE NUMBER OF VEHICLES IN QUEUE	1.93	1.85	3.34	0.66
LINE 8 0	LENGTH OF QUEUE (M/LANE)	58.99	62.36	31.21	22.28
LINE 9 0	AVERAGE EXCESS RUNNING TIME (S/VEH)	33.99	30.77	48.62	23.94
LINE 10	EMISSIONS FROM ACCELERATION (G/VEH-M)	0.095	0.098	0.109	0.101
LINE 11	EMISSIONS FROM DECELERATION (G/VEH-M)	0.028	0.030	0.036	0.032
LINE 12	EMISSION RATE FOR ACC. AND DEC. (G/M-S)	0.031	0.034	0.026	0.020
LINE 13	LENGTH OF ACC AND DEC. (M)	109.5	91.5	60.4	75.2
LINE 14	LENGTH FOR EXCESS EMISSIONS (M)	219.0	183.1	120.9	150.4
LINE 15	IDLING EMISSION RATE (G/S)	2.009	2.010	2.151	0.928
LINE 16	AVERAGE EMISSION RATE (G/S-M)	0.0247	0.0281	0.0310	0.0160
LINE 17	ADJUSTED EXCESS EMISSION RATE (G/S-M)	0.0103	0.0116	0.0136	0.0064
LINE 18	FREE-FLOW EMISSION RATE (G/S-M)	0.0033	0.0040	0.0030	0.0028

## EPA VOLUME 9 (REVISED) INDIRECT SOURCE GUIDELINE MODEL - WORKSHEET #2

INTERSECTION: ATLANTIC AVE AND SURFACE ARTERY  
CASE # 2 YEAR 1990 AVERAGING TIME: 1-HOUR

LINE 1	ROAD SEGMENT ID	HE
LINE 2	DEMAND VOLUME (VPH)	204
LINE 4	CRUISE SPEED (MPH)	24
LINE 5	FREE-FLOW EMISSIONS (G/VEH/M)	0.0232
LINE 6.1	NUMBER OF LANES	2
LINE 6.3	CAPACITY SERVICE VOLUME (VPH OF GREEN)	0
LINE 6.4	DEMAND VOLUME (VPH)	0
LINE 6.5	SIGNAL CYCLE LENGTH (S)	0
LINE 6.6	GREEN PHASE LENGTH (S)	0
LINE 6.7	CAPACITY (VPH)	248
LINE 6.8	PROPORTION OF VEHICLES THAT STOP	0.0
LINE 6.9	NUMBER OF VEHICLES THAT STOP PER CYCLE	0.0
LINE 7.0	AVERAGE NUMBER OF VEHICLES IN QUEUE	4.64
LINE 8.0	LENGTH OF QUEUE (M/LANE)	10.08
LINE 9.0	AVERAGE EXCESS RUNNING TIME (S/VEH)	67.30
LINE 10	EMISSIONS FROM ACCELERATION (G/VEH-M)	0.113
LINE 11	EMISSIONS FROM DECELERATION (G/VEH-M)	0.039
LINE 12	EMISSION RATE FOR ACC. AND DEC. (G/M-S)	0.009
LINE 13	LENGTH OF ACC. AND DEC. (M)	51.5
LINE 14	LENGTH FOR EXCESS EMISSIONS (M)	103.0
LINE 15	IDLING EMISSION RATE (G/S)	0.900
LINE 16	AVERAGE EMISSION RATE (G/S-M)	0.0130
LINE 17	ADJUSTED EXCESS EMISSION RATE (G/S-M)	0.0083
LINE 18	FREE-FLOW EMISSION RATE (G/S-M)	0.0013

## EPA VOLUME 9 (REVISED) INDIRECT SOURCE GUIDELINE MODEL - WORKSHEET #2

INTERSECTION ATLANTIC AVE AND SURFACE ARTERY  
CASE # 2 YEAR 1990 AVERAGING TIME 8-HOUR

LINE 1	ROAD SEGMENT ID	HE
LINE 2	DEMAND VOLUME (VPH)	137
LINE 4	CRUISE SPEED (MPH)	30
LINE 5	FREE-FLOW EMISSIONS (G/VEH/M)	0.0132
LINE 6.1	NUMBER OF LANES	2
LINE 6.3	CAPACITY SERVICE VOLUME (VPH OF GREEN)	0
LINE 6.4	DEMAND VOLUME (VPH)	0
LINE 6.5	SIGNAL CYCLE LENGTH (S)	0
LINE 6.6	GREEN PHASE LENGTH (S)	0
LINE 6.7	CAPACITY (VPH)	364
LINE 6.8	PROPORTION OF VEHICLES THAT STOP	0.0
LINE 6.9	NUMBER OF VEHICLES THAT STOP PER CYCLE	0.0
LINE 7.0	AVERAGE NUMBER OF VEHICLES IN QUEUE	0.60
LINE 8.0	LENGTH OF QUEUE (M/LANE)	1.31
LINE 9.0	AVERAGE EXCESS RUNNING TIME (S/VEH)	5.97
LINE 10	EMISSIONS FROM ACCELERATION (G/VEH-M)	0.100
LINE 11	EMISSIONS FROM DECELERATION (G/VEH-M)	0.031
LINE 12	EMISSION RATE FOR ACC AND DEC (G/M-S)	0.005
LINE 13	LENGTH OF ACC AND DEC (M)	80.5
LINE 14	LENGTH FOR EXCESS EMISSIONS (M)	160.9
LINE 15	IDLING EMISSION RATE (G/S)	-0.000
LINE 16	AVERAGE EMISSION RATE (G/S-M)	0.0025
LINE 17	ADJUSTED EXCESS EMISSION RATE (G/S-M)	0.0008
LINE 18	FREE-FLOW EMISSION RATE (G/S-M)	0.0005

## EPA VOLUME 9 (REVISED) INDIRECT SOURCE GUIDELINE MODEL - WORKSHEET #2

INTERSECTION: ATLANTIC AVE AND SURFACE ARTERY  
CASE # 3 YEAR: 1990 AVERAGING TIME: 1-HOUR

LINE	ROAD SEGMENT ID	SN	AN	AS	SS
LINE 2	DEMAND VOLUME (VPH)	1512	1528	888	1104
LINE 4	CRUISE SPEED (MPH)	28	26	22	24
LINE 5	FREE-FLOW EMISSIONS (G-VEH/M)	0.0198	0.0214	0.0251	0.0232
LINE 6.1	NUMBER OF LANES	2	2	3	3
LINE 6.3	CAPACITY SERVICE VOLUME (VPH OF GREEN)	3500	1750	3800	4800
LINE 6.3	CAPACITY SERVICE VOLUME (VPH OF GREEN)	3200	3500	0	0
LINE 6.4	DEMAND VOLUME (VPH)	350	641	888	1104
LINE 6.4	DEMAND VOLUME (VPH)	1162	887	0	0
LINE 6.5	SIGNAL CYCLE LENGTH (S)	100			
LINE 6.6	GREEN PHASE LENGTH (S)	11	45	24	38
LINE 6.6	GREEN PHASE LENGTH (S)	38	27	0	0
LINE 6.7	CAPACITY (VPH)	1601	1803	912	1824
LINE 6.8	PROPORTION OF VEHICLES THAT STOP	0.989	0.805	0.992	0.805
LINE 6.8	PROPORTION OF VEHICLES THAT STOP	0.974	0.978	0.0	0.0
LINE 6.9	NUMBER OF VEHICLES THAT STOP PER CYCLE	9.614	14.330	24.463	24.693
LINE 6.9	NUMBER OF VEHICLES THAT STOP PER CYCLE	31.423	24.092	0.0	0.0
LINE 7.0	AVERAGE NUMBER OF VEHICLES IN QUEUE	16.99	5.57	37.00	1.53
LINE 8.0	LENGTH OF QUEUE (M/LANE)	126.21	95.67	89.12	38.03
LINE 9.0	AVERAGE EXCESS RUNNING TIME (S/VEH)	71.58	40.44	183.74	27.99
LINE 10	EMISSIONS FROM ACCELERATION (G/VEH-M)	0.103	0.109	0.120	0.113
LINE 11	EMISSIONS FROM DECELERATION (G/VEH-M)	0.034	0.036	0.041	0.039
LINE 12	EMISSION RATE FOR ACC. AND DEC. (G/M-S)	0.056	0.056	0.039	0.038
LINE 13	LENGTH OF ACC. AND DEC. (M)	70.1	60.4	43.3	51.5
LINE 14	LENGTH FOR EXCESS EMISSIONS (M)	140.2	120.9	89.1	103.0
LINE 15	IDLING EMISSION RATE (G/S)	7.039	3.800	11.236	1.806
LINE 16	AVERAGE EMISSION RATE (G/S-M)	0.0783	0.0593	0.1452	0.0363
LINE 17	ADJUSTED EXCESS EMISSION RATE (G/S-M)	0.0498	0.0357	0.1013	0.0211
LINE 18	FREE-FLOW EMISSION RATE (G/S-M)	0.0083	0.0091	0.0062	0.0071

## EPA VOLUME 9 (REVISED) INDIRECT SOURCE GUIDELINE MODEL - WORKSHEET #2

INTERSECTION: PURCHASE STREET & CONGRESS STREET  
CASE # 3 YEAR: 1990 AVERAGING TIME: 8-HOUR

LINE	ROAD SEGMENT ID	PS	CE
LINE 1	ROAD SEGMENT ID		
LINE 2	DEMAND VOLUME (VPH)	1543	1645
LINE 4	CRUISE SPEED (MPH)	30	25
LINE 5	FREE-FLOW EMISSIONS (G/VEH/M)	0.0132	0.0161
LINE 6.1	NUMBER OF LANES	4	4
LINE 6.3	CAPACITY SERVICE VOLUME (VPH OF GREEN)	5100	5700
LINE 6.3	CAPACITY SERVICE VOLUME (VPH OF GREEN)	7100	0
LINE 6.4	DEMAND VOLUME (VPH)	329	1645
LINE 6.4	DEMAND VOLUME (VPH)	1214	0
LINE 6.5	SIGNAL CYCLE LENGTH (S)	90	
LINE 6.6	GREEN PHASE LENGTH (S)	16	35
LINE 6.6	GREEN PHASE LENGTH (S)	39	0
LINE 6.7	CAPACITY (VPH)	3983	2217
LINE 6.8	PROPORTION OF VEHICLES THAT STOP	0.879	0.748
LINE 6.8	PROPORTION OF VEHICLES THAT STOP	0.684	0.0
LINE 6.9	NUMBER OF VEHICLES THAT STOP PER CYCLE	7.229	19.549
LINE 6.9	NUMBER OF VEHICLES THAT STOP PER CYCLE	20.745	0.0
LINE 7.0	AVERAGE NUMBER OF VEHICLES IN QUEUE	0.63	0.89
LINE 8.0	LENGTH OF QUEUE (M/LANE)	31.11	22.23
LINE 9.0	AVERAGE EXCESS RUNNING TIME (S/VEH)	21.22	22.03
LINE 10	EMISSIONS FROM ACCELERATION (G/VEH-M)	0.190	0.111
LINE 11	EMISSIONS FROM DECELERATION (G/VEH-M)	0.031	0.038
LINE 12	EMISSION RATE FOR ACC. AND DEC. (G/M-S)	0.041	0.032
LINE 13	LENGTH OF ACC. AND DEC (M)	80.5	55.9
LINE 14	LENGTH FOR EXCESS EMISSIONS (M)	160.9	111.7
LINE 15	IDLING EMISSION RATE (G/S)	1.867	1.255
LINE 16	AVERAGE EMISSION RATE (G/S-M)	0.0307	0.0274
LINE 17	ADJUSTED EXCESS EMISSION RATE (G/S-M)	0.0121	0.0110
LINE 18	FREE-FLOW EMISSION RATE (G/S-M)	0.0057	0.0047



WORKSHEET 5 - INTERSECTION CO DISPERSION ANALYSIS

Intersection Purchase And Congress Streets  
 Case # 1 Year 1984 Averaging Time 1 Hour

Line No. Symbol	Input/Units	PS	Traffic Stream CE
1 SC	Stability Class	D	
2 U	Wind Speed ( $m s^{-1}$ )	1.0	
3 $\theta$	Wind-Road Angle (deg)	16	-74
4 x	Lateral Distance (m)	11	13
5 Yu	Maximum Longitudinal Distance (m)	92	NA <sup>+</sup>
6 Yd	Minimum Longitudinal Distance (m)	20	NA <sup>+</sup>
7 $\sigma_{z0}$	Initial Dispersion (m)	5.0	
8 Qe	Excess Emissions Rate ( $gm^{-1}s^{-1}$ )	.0675	.0568
9 Qf	Free Flow Emissions Rate ( $gm^{-1}s^{-1}$ )	.0202	.0193
9a	Street Canyon? Yes or No	NO	
DISPERSION ANALYSIS			
10 XUQ <sup>-1</sup>	Normalized Concentration ( $10^{-3}m^{-1}$ ) Free Flow	440	NA
Qf	Enter Line 9	x .0202 x	.0193 x
11 XU	Normalized Concentration ( $mg m^{-2}s^{-1}$ )		
U	Enter Line 2	÷ 1.0 ÷	÷ ÷
12 X	CO Concentration ( $mg m^{-3}$ ) Through Emissions	8.9	0.0
13 XUQ <sup>-1</sup>	Normalized Concentration (For Yu)	375	NA
Qe	Enter Line 8	.0675	.0568
14 XU	Normalized Concentration ( $mg m^{-2}s^{-1}$ )		
U	Enter Line 2	1.0	
15 X	CO Concentration-"Maximum Queue"	25.3	0.0
16 XUQ <sup>-1</sup>	Normalized Concentration (For Yd)	0	NA
Qe	Enter Line 8	x .0675 x	.0568 x
17 XU	Normalized Concentration ( $mg m^{-2}s^{-1}$ )		
U	Enter Line 2	1.0	
18 X	CO Concentration-"Imaginary Queue"	÷ 0.0 ÷	÷ 0.0 ÷
19 X	CO ( $mg m^{-3}$ ) Total	34.2	0.0
20 X	CO Concentration (ppm)-- Total	29.8	0.0
OPTIONAL z-CORRECTION (Heights Other than 1.8m Above the Ground)			
21 z	Height of Receptor (m)		
22	z-Correction Factor		
23 X'	CO Concentration at Height z ( $mg m^{-3}$ )		
24 X'	CO Concentration at Height z (ppm)		

29.8 ppm

\* Down wind of Receptor

## EPA VOLUME 9 (REVISED) INDIRECT SOURCE GUIDELINE MODEL - WORKSHEET #2

INTERSECTION: ATLANTIC AVE AND SURFACE ARTERY  
CASE # 3 YEAR 1990 AVERAGING TIME 8-HOUR

LINE	ROAD SEGMENT ID	HE
LINE 2	DEMAND VOLUME (VPH)	142
LINE 4	CRUISE SPEED (MPH)	30
LINE 5	FREE-FLOW EMISSIONS (G-VEH/M)	0.0132
LINE 6.1	NUMBER OF LANES	2
LINE 6.3	CAPACITY SERVICE VOLUME (VPH OF GREEN)	0.
LINE 6.4	DEMAND VOLUME (VPH)	0.
LINE 6.5	SIGNAL CYCLE LENGTH (S)	0.
LINE 6.6	GREEN PHASE LENGTH (S)	0.
LINE 6.7	CAPACITY (VPH)	357
LINE 6.8	PROPORTION OF VEHICLES THAT STOP	0.0
LINE 6.9	NUMBER OF VEHICLES THAT STOP PER CYCLE	0.0
LINE 7.0	AVERAGE NUMBER OF VEHICLES IN QUEUE	0.66
LINE 8.0	LENGTH OF QUEUE (M/LANE)	1.44
LINE 9.0	AVERAGE EXCESS RUNNING TIME (S/VEH)	6.66
LINE 10.	EMISSIONS FROM ACCELERATION (G/VEH-M)	0.100
LINE 11.	EMISSIONS FROM DECELERATION (G/VEH-M)	0.031
LINE 12.	EMISSION RATE FOR ACC. AND DEC. (G/M-S)	0.005
LINE 13.	LENGTH OF ACC. AND DEC. (M)	80.5
LINE 14.	LENGTH FOR EXCESS EMISSIONS (M)	160.9
LINE 15.	IDLING EMISSION RATE (G/S)	0.007
LINE 16.	AVERAGE EMISSION RATE (G/S-M)	0.0026
LINE 17.	ADJUSTED EXCESS EMISSION RATE (G/S-M)	0.0009
LINE 18.	FREE-FLOW EMISSION RATE (G/S-M)	0.0005

WORKSHEET 5 - INTERSECTION CO DISPERSION ANALYSIS

Intersection Atlantic Ave and Surface Artery  
 Case # 1 Year 1984 Averaging Time 1 Hour

Line No. Symbol	Input/Units	SN	Traffic Stream		SS
		AN	AS		
1 SC	Stability Class	D			
2 U	Wind Speed ( $m s^{-1}$ )	1.0			
3 $\theta$	Wind-Road Angle (deg)	40	30	85	40
4 x	Lateral Distance (m)	40	16	51	43
5 Yu	Maximum Longitudinal Distance (m)	57	63	20	171
6 Yd	Minimum Longitudinal Distance (m)	0	0	0	68
7 $\sigma_{z0}$	Initial Dispersion (m)	5.0			
8 Qe	Excess Emissions Rate ( $gm^{-1}s^{-1}$ )	.0332	.0484	.0743	.0266
9 Qf	Free Flow Emissions Rate ( $gm^{-1}s^{-1}$ )	.0115	.0145	.0087	.0111
9a	Street Canyon? Yes or No	NO			
DISPERSION ANALYSIS					
10 XUQ <sup>-1</sup>	Normalized Concentration ( $10^{-3}m^{-1}$ ) Free Flow	170	260	115	165
Qf	Enter Line 9	x .0115	x .0145	x .0087	x .0111
11 XU	Normalized Concentration ( $mg m^{-2}s^{-1}$ )				
U	Enter Line 2	÷ 1.0	÷	÷	÷
12 x	CO Concentration ( $mg m^{-3}$ ) Through Emissions	2.0	3.8	1.0	1.8
13 XUQ <sup>-1</sup>	Normalized Concentration (For Yu)	40	230	50	160
Qe	Enter Line 8	x .0332	x .0484	x .0743	x .0266
14 XU	Normalized Concentration ( $mg m^{-2}s^{-1}$ )				
U	Enter Line 2	1.0			
15 x	CO Concentration--"Maximum Queue"	1.3	11.1	3.7	4.3
16 XUQ <sup>-1</sup>	Normalized Concentration (For Yd)	0	0	0	80
Qe	Enter Line 8	x .0332	x .0484	x .0743	x .0266
17 XU	Normalized Concentration ( $mg m^{-2}s^{-1}$ )				
U	Enter Line 2	1.0			
18 x	CO Concentration--"Imaginary Queue"	0	0	0	2.1
19 x	CO ( $mg m^{-3}$ ) Total	3.3	14.9	4.7	4.0
20 x	CO Concentration (ppm)-- Total	2.9	13.0	4.1	3.5
OPTIONAL z-CORRECTION (Heights Other than 1.8m Above the Ground)					
21 z	Height of Receptor (m)				
22	z-Correction Factor				
23 x	CO Concentration at Height z ( $mg m^{-3}$ )				
24 x	CO Concentration at Height z (ppm)				

23.5 ppm

WORKSHEET 5 - INTERSECTION CO DISPERSION ANALYSIS

Intersection Atlantic Ave and Surface Artery  
 Case # 1 Year 1984 Averaging Time 8 Hour

Line No. Symbol	Input/Units	Traffic Stream			
		SN	AN	AS	SS
1 SC	Stability Class	D			
2 U	Wind Speed ( $m s^{-1}$ )	1.6			
3 $\theta$	Wind-Road Angle (deg)	40	30	85	40
4 x	Lateral Distance (m)	40	16	51	43
5 Yu	Maximum Longitudinal Distance (m)	57	63	20	218
6 Yd	Minimum Longitudinal Distance (m)	0	0	0	68
7 $\sigma_{z0}$	Initial Dispersion (m)	5.0			
8 Qe	Excess Emissions Rate ( $gm^{-1}s^{-1}$ )	.0109	.0178	.0207	.0085
9 Qf	Free Flow Emissions Rate ( $gm^{-1}s^{-1}$ )	.0042	.0061	.0040	.0051
9a	Street Canyon? Yes or No	NO			
DISPERSION ANALYSIS					
10 $xuQ^{-1}$	Normalized Concentration ( $10^{-3}m^{-1}$ ) Free Flow	170	260	115	165
Qf	Enter Line 9	$\times .0042$	$\times .0061$	$\times .0040$	$\times .0051$
11 xu	Normalized Concentration ( $mg m^{-2}s^{-1}$ )				
U	Enter Line 2	$\div 1.6$	$\div$	$\div$	$\div$
12 x	CO Concentration ( $mg m^{-3}$ ) Through Emissions	0.4	1.0	0.3	0.5
13 $xuQ^{-1}$	Normalized Concentration (For Yu)	40	230	50	160
Qe	Enter Line 8	$\times .0109$	$\times .0178$	$\times .0207$	$\times .0085$
14 xu	Normalized Concentration ( $mg m^{-2}s^{-1}$ )				
U	Enter Line 2	1.6			
15 x	CO Concentration-"Maximum Queue"	0.3	2.6	0.6	0.9
16 $xuQ^{-1}$	Normalized Concentration (For Yd)	0	0	0	80
Qe	Enter Line 8	$\times .0109$	$\times .0178$	$\times .0207$	$\times .0085$
17 xu	Normalized Concentration ( $mg m^{-2}s^{-1}$ )				
U	Enter Line 2	1.6			
18 x	CO Concentration-"Imaginary Queue"	$\div 0$	$\div 0$	$\div 0$	$\div 0.4$
19 x	CO ( $mg m^{-3}$ ) Total	0.7	3.6	0.9	1.0
20 x	CO Concentration (ppm)-- Total	0.6	3.1	0.8	0.9
OPTIONAL z-CORRECTION (Heights Other than 1.8m Above the Ground)					
21 z	Height of Receptor (m)				
22	z-Correction Factor				
23 $x''$	CO Concentration at Height z ( $mg m^{-3}$ )				
24 $x''$	CO Concentration at Height z (ppm)				

5.4 ppm

WORKSHEET 5 - INTERSECTION CO DISPERSION ANALYSIS

Intersection Atlantic Ave and Surface Artery  
 Case # 2 Year 1990 Averaging Time 1 Hour

Line No. Symbol	Input/Units	SN	Traffic Stream		SS	HE
		AN	AS			
1 SC	Stability Class	D				
2 U	Wind Speed ( $m s^{-1}$ )	1.0				
3 $\theta$	Wind-Road Angle (deg)	40	30	85	40	50
4 x	Lateral Distance (m)	40	16	51	43	33
5 Yu	Maximum Longitudinal Distance (m)	57	63	20	171	190
6 Yd	Minimum Longitudinal Distance (m)	0	0	0	68	87
7 $\sigma_{z0}$	Initial Dispersion (m)	5.0				
8 Qe	Excess Emissions Rate ( $gm^{-1}s^{-1}$ )	.0484	.0331	.1013	.0192	.0083
9 Qf	Free Flow Emissions Rate ( $gm^{-1}s^{-1}$ )	.0083	.0088	.0062	.0067	.0013
9a	Street Canyon? Yes or No	NO				
DISPERSION ANALYSIS						
10 $xUQ^{-1}$	Normalized Concentration ( $10^{-3}m^{-1}$ ) Free Flow	170	260	115	165	150
Qf	Enter Line 9	x	x	x	x	
11 XU	Normalized Concentration ( $mg m^{-2}s^{-1}$ )					
U	Enter Line 2	÷ 1.0	÷	÷	÷	
12 x	CO Concentration ( $mg m^{-3}$ ) Through Emissions	1.4	2.2	0.7	1.1	0.2
13 $xUQ^{-1}$	Normalized Concentration (For Yu)	40	230	50	160	170
Qe	Enter Line 8					
14 XU	Normalized Concentration ( $mg m^{-2}s^{-1}$ )					
U	Enter Line 2	1.0				
15 x	CO Concentration-"Maximum Queue"	1.9	7.6	5.1	3.1	1.4
16 $xUQ^{-1}$	Normalized Concentration (For Yd)	0	0	0	80	170
Qe	Enter Line 8	x	x	x	x	
17 XU	Normalized Concentration ( $mg m^{-2}s^{-1}$ )					
U	Enter Line 2	1.0				
18 x	CO Concentration-"Imaginary Queue"	÷ 0	÷ 0	÷ 0	÷ 1.5	1.4
19 x	CO ( $mg m^{-3}$ ) Total	3.3	9.8	5.8	2.7	0.2
20 x	CO Concentration (ppm)-- Total	2.9	8.5	5.0	2.3	0.2
OPTIONAL z-CORRECTION (Heights Other than 1.8m Above the Ground)						
21 z	Height of Receptor (m)					
22	z-Correction Factor					
23 x'	CO Concentration at Height z ( $mg m^{-3}$ )					
24 x'	CO Concentration at Height z (ppm)					

18.9 ppm



WORKSHEET 5 - INTERSECTION CO DISPERSION ANALYSIS

Intersection Atlantic Ave and Surface Artery  
 Case # 2 Year 1990 Averaging Time 8 Hour

Line No. Symbol	Input/Units	SN	Traffic Stream AN	AS	SS	HE
1 SC	Stability Class	D				
2 U	Wind Speed ( $m s^{-1}$ )	1.6				
3 $\theta$	Wind-Road Angle (deg)	40	30	85	40	50
4 x	Lateral Distance (m)	40	16	51	43	33
5 Yu	Maximum Longitudinal Distance (m)	57	63	20	218	247
6 Yd	Minimum Longitudinal Distance (m)	0	0	0	68	87
7 $\sigma_{z0}$	Initial Dispersion (m)	5.0				
8 Qe	Excess Emissions Rate ( $gm^{-1}s^{-1}$ )	.0103	.0116	.0136	.0064	.0008
9 Qf	Free Flow Emissions Rate ( $gm^{-1}s^{-1}$ )	.0033	.0040	.0030	.0028	.0005
9a	Street Canyon? Yes or No	NO				
DISPERSION ANALYSIS						
10 XUQ <sup>-1</sup>	Normalized Concentration ( $10^{-3}m^{-1}$ ) Free Flow	170	260	115	165	150
	Enter Line 9	x	x	x	x	
11 XU	Normalized Concentration ( $mg m^{-2}s^{-1}$ )					
	Enter Line 2	÷ 1.6	÷	÷	÷	
12 x	CO Concentration ( $mg m^{-3}$ ) Through Emissions	0.4	0.7	0.2	0.3	0.0
13 XUQ <sup>-1</sup>	Normalized Concentration (For Yu)	40	230	50	160	170
	Enter Line 8					
14 XU	Normalized Concentration ( $mg m^{-2}s^{-1}$ )					
	Enter Line 2	÷ 1.6				
15 x	CO Concentration-"Maximum Queue"	0.3	1.7	0.4	0.6	0.1
16 XUQ <sup>-1</sup>	Normalized Concentration (For Yd)	0	0	0	80	170
	Enter Line 8	x	x	x	x	
17 XU	Normalized Concentration ( $mg m^{-2}s^{-1}$ )					
	Enter Line 2	÷ 1.6				
18 x	CO Concentration-"Imaginary Queue"	0	0	0	0.3	0.1
19 x	CO ( $mg m^{-3}$ ) Total	0.7	2.4	0.6	0.6	0.0
20 x	CO Concentration (ppm)-- Total	0.6	2.1	0.5	0.5	0.0
OPTIONAL z-CORRECTION (Heights Other than 1.8m Above the Ground)						
21 z	Height of Receptor (m)					
22	z-Correction Factor					
23 x'	CO Concentration at Height z ( $mg m^{-3}$ )					
24 x'	CO Concentration at Height z (ppm)					

3.7 ppm

WORKSHEET 5 - INTERSECTION CO DISPERSION ANALYSIS

Intersection Atlantic Ave and Surface Artery  
 Case # 3 Year 1990 Averaging Time 1 Hour

Line No. Symbol	Input/Units	SN	Traffic Stream		SS	HE
		AN	AS			
1 SC	Stability Class	D				
2 U	Wind Speed ( $m s^{-1}$ )	1.0				
3 $\theta$	Wind-Road Angle (deg)	40	30	85	40	50
4 x	Lateral Distance (m)	40	16	51	43	33
5 Yu	Maximum Longitudinal Distance (m)	57	63	20	171	190
6 Yd	Minimum Longitudinal Distance (m)	0	0	0	68	87
7 $\sigma_{z0}$	Initial Dispersion (m)	5.0				
8 Qe	Excess Emissions Rate ( $gm^{-1}s^{-1}$ )	.0498	.0357	.1013	.0211	.0136
9 Qf	Free Flow Emissions Rate ( $gm^{-1}s^{-1}$ )	.0083	.0091	.0062	.0071	.0014
9a	Street Canyon? Yes or No	NO				
DISPERSION ANALYSIS						
10 $xUQ^{-1}$	Normalized Concentration ( $10^{-3}m^{-1}$ ) Free Flow	170	260	115	165	150
Qf	Enter Line 9	x	x	x	x	
11 XU	Normalized Concentration ( $mg m^{-2}s^{-1}$ )					
U	Enter Line 2	÷ 1.0	÷	÷	÷	
12 x	CO Concentration ( $mg m^{-3}$ ) Through Emissions	1.4	2.4	0.7	1.2	0.2
13 $xUQ^{-1}$	Normalized Concentration (For Yu)	40	230	50	160	170
Qe	Enter Line 8					
14 XU	Normalized Concentration ( $mg m^{-2}s^{-1}$ )					
U	Enter Line 2	1.0				
15 x	CO Concentration- "Maximum Queue"	2.0	8.2	5.1	3.3	2.3
16 $xUQ^{-1}$	Normalized Concentration (For Yd)	0	0	0	80	170
Qe	Enter Line 8	x	x	x	x	
17 XU	Normalized Concentration ( $mg m^{-2}s^{-1}$ )					
U	Enter Line 2	1.0				
18 x	CO Concentration- "Imaginary Queue"	÷ 0	÷ 0	÷ 0	÷ 1.7	2.3
19 x	CO ( $mg m^{-3}$ ) Total	3.4	10.6	5.8	2.8	0.2
20 x	CO Concentration (ppm)-- Total	3.0	9.2	5.0	2.4	0.2
OPTIONAL z-CORRECTION (Heights Other than 1.8m Above the Ground)						
21 z	Height of Receptor (m)					
22	z-Correction Factor					
23 x	CO Concentration at Height z ( $mg m^{-3}$ )					
24 x	CO Concentration at Height z (ppm)					

19.8 ppm

WORKSHEET 5 - INTERSECTION CO DISPERSION ANALYSIS

Intersection Atlantic Ave and Surface Artery  
 Case # 3 Year 1990 Averaging Time 8 Hour

Line No. Symbol	Input/Units	SN	Traffic Stream			HE
		AN	AS	SS		
1 SC	Stability Class	<u>D</u>				
2 U	Wind Speed ( $m s^{-1}$ )	<u>1.6</u>				
3 $\theta$	Wind-Road Angle (deg)	<u>40</u>	<u>30</u>	<u>85</u>	<u>40</u>	<u>50</u>
4 x	Lateral Distance (m)	<u>40</u>	<u>16</u>	<u>51</u>	<u>43</u>	<u>33</u>
5 Yu	Maximum Longitudinal Distance (m)	<u>57</u>	<u>63</u>	<u>20</u>	<u>218</u>	<u>247</u>
6 Yd	Minimum Longitudinal Distance (m)	<u>0</u>	<u>0</u>	<u>0</u>	<u>65</u>	<u>87</u>
7 $\sigma_{z0}$	Initial Dispersion (m)	<u>5.0</u>				
8 Qe	Excess Emissions Rate ( $gm^{-1}s^{-1}$ )	<u>.0103</u>	<u>.0121</u>	<u>.0136</u>	<u>.0070</u>	<u>.0009</u>
9 Qf	Free Flow Emissions Rate ( $gm^{-1}s^{-1}$ )	<u>.0033</u>	<u>.0041</u>	<u>.0030</u>	<u>.0029</u>	<u>.0005</u>
9a	Street Canyon? Yes or No	<u>NO</u>				
DISPERSION ANALYSIS						
10 $xUQ^{-1}$	Normalized Concentration ( $10^{-3}m^{-1}$ ) Free Flow	<u>170</u>	<u>260</u>	<u>115</u>	<u>165</u>	<u>150</u>
	Enter Line 9	x	x	x	x	
11 xU	Normalized Concentration ( $mg m^{-2}s^{-1}$ )					
	Enter Line 2	$\div$ <u>1.6</u>	$\div$	$\div$	$\div$	
12 x	CO Concentration ( $mg m^{-3}$ ) Through Emissions	<u>0.4</u>	<u>0.7</u>	<u>0.2</u>	<u>0.3</u>	<u>0.0</u>
13 $xUQ^{-1}$	Normalized Concentration (For Yu)	<u>40</u>	<u>230</u>	<u>50</u>	<u>160</u>	<u>170</u>
	Enter Line 8					
14 xU	Normalized Concentration ( $mg m^{-2}s^{-1}$ )					
	Enter Line 2	<u>1.6</u>				
15 x	CO Concentration-"Maximum Queue"	<u>0.3</u>	<u>1.7</u>	<u>0.4</u>	<u>0.7</u>	<u>0.1</u>
16 $xUQ^{-1}$	Normalized Concentration (For Yd)	<u>0</u>	<u>0</u>	<u>0</u>	<u>80</u>	<u>170</u>
	Enter Line 8	x	x	x	x	
17 xU	Normalized Concentration ( $mg m^{-2}s^{-1}$ )					
	Enter Line 2	<u>1.6</u>				
18 x	CO Concentration-"Imaginary Queue"	$\div$ <u>0</u>	$\div$ <u>0</u>	$\div$ <u>0</u>	$\div$ <u>0.3</u>	<u>0.1</u>
19 x	CO ( $mg m^{-3}$ ) Total	<u>0.7</u>	<u>2.4</u>	<u>0.6</u>	<u>0.7</u>	<u>0.0</u>
20 x	CO Concentration (ppm)-- Total	<u>0.6</u>	<u>2.1</u>	<u>0.5</u>	<u>0.6</u>	<u>0.0</u>
OPTIONAL z-CORRECTION (Heights Other than 1.8m Above the Ground)						
21 z	Height of Receptor (m)					
22	z-Correction Factor					
23 x'	CO Concentration at Height z ( $mg m^{-3}$ )					
24 x'	CO Concentration at Height z (ppm)					

**3.8ppm**

WORKSHEET 1 - TRAFFIC INFORMATION

Intersection Purchase And Congress Streets  
Case # 1 Year 1984

1. Road segment or intersection approach identification	<u>PS</u>	<u>CE</u>	---	---
2. Observed 1-hr volume (vph)	<u>1293</u>	<u>1232</u>	---	---
Observed 8-hr volume (vph)	<u>905</u>	<u>838</u>	---	---
Projected 1-hr peak demand (vph)	---	---	---	---
Projected 8-hr peak demand (vph)	---	---	---	---
3. Percentage cold starts (1Hr/8Hr)	<u>50.0</u>	<u>20.6</u>	---	---
4. Percentage trucks and buses	<u>3.0</u>	---	---	---
5. Metropolitan population	---	---	---	---
6. Slope	---	---	---	---
7. Free-flow parameters				
Number of lanes	<u>4</u>	<u>4</u>	---	---
Average lane width (ft)	<u>15</u>	<u>13</u>	---	---
Design speed (mph) (1Hr/8Hr)	<u>20/30</u>	<u>20/25</u>	---	---
Highway type (see Figures 2-5)	<u>Urban Artery</u>			
8. Intersection parameters				
Intersection designation	---	---	---	---
Approach width (ft)	<u>60</u>	<u>52</u>	---	---
Percentage right turns	<u>0</u>	<u>12</u>	---	---
Percentage left turns	<u>51</u>	<u>0</u>	---	---
Type control and description of signal controller	<u>Signalized</u>			
9. Area source parameters				
Parking lot gate designation	---	---	---	---
Projected 1-hr peak entrance demand (vph)	---	---	---	---
Projected 1-hr peak exit demand (vph)	---	---	---	---
Projected 8-hr peak entrance demand (vph)	---	---	---	---
Projected 8-hr peak exit demand (vph)	---	---	---	---
Parking lot area (m <sup>2</sup> )	---	---	---	---
Parking lot capacity (veh)	---	---	---	---
Running time required to access auxiliary parking (s)	---	---	---	---
Facility emptying time	---	---	---	---
Average cars per stall	---	---	---	---
Average area per stall (m <sup>2</sup> )	---	---	---	---

PS = Purchase Street S.B.  
CE = Congress Street E.B.

WORKSHEET 1 - TRAFFIC INFORMATION

Intersection Purchase And Congress Streets  
 Case # 2 Year 1990

1. Road segment or intersection approach identification	PS	CE
2. Observed 1-hr volume (vph)	---	---
Observed 8-hr volume (vph)	---	---
Projected 1-hr peak demand (vph)	2071	1459
Projected 8-hr peak demand (vph)	1450	992
3. Percentage cold starts (1Hr/8Hr)	50.0	20.6
4. Percentage trucks and buses	3.0	---
5. Metropolitan population	---	---
6. Slope	---	---
7. Free-flow parameters		
Number of lanes	4	4
Average lane width (ft)	15	13
Design speed (mph) (1Hr/8Hr)	20/30	20/25
Highway type (see Figures 2-5)	Urban Artery	
8. Intersection parameters		
Intersection designation	---	---
Approach width (ft)	60	52
Percentage right turns	0	22
Percentage left turns	41	0
Type control and description of signal controller	Signalized	
9. Area source parameters		
Parking lot gate designation	---	---
Projected 1-hr peak entrance demand (vph)	---	---
Projected 1-hr peak exit demand (vph)	---	---
Projected 8-hr peak entrance demand (vph)	---	---
Projected 8-hr peak exit demand (vph)	---	---
Parking lot area (m <sup>2</sup> )	---	---
Parking lot capacity (veh)	---	---
Running time required to access auxiliary parking (s)	---	---
Facility emptying time	---	---
Average cars per stall	---	---
Average area per stall (m <sup>2</sup> )	---	---



WORKSHEET 1 - TRAFFIC INFORMATION

Intersection Purchase And Congress Streets  
 Case # 3 Year 1990

1. Road segment or intersection approach identification	<u>PS</u>	<u>CE</u>
2. Observed 1-hr volume (vph)	_____	_____
Observed 8-hr volume (vph)	_____	_____
Projected 1-hr peak demand (vph)	<u>2204</u>	<u>1537</u>
Projected 8-hr peak demand (vph)	<u>1543</u>	<u>1045</u>
3. Percentage cold starts (1hr/8hr)	<u>50.0</u>	<u>20.6</u>
4. Percentage trucks and buses	<u>3.0</u>	_____
5. Metropolitan population	_____	_____
6. Slope	_____	_____
7. Free-flow parameters		
Number of lanes	<u>4</u>	<u>4</u>
Average lane width (ft)	<u>15</u>	<u>13</u>
Design speed (mph)	<u>20/30</u>	<u>20/25</u>
Highway type (see Figures 2-5)	<u>Urban Artery</u>	
8. Intersection parameters		
Intersection designation	_____	_____
Approach width (ft)	<u>60</u>	<u>52</u>
Percentage right turns	<u>0</u>	<u>21</u>
Percentage left turns	<u>40</u>	<u>0</u>
Type control and description of signal controller	_____	_____
9. Area source parameters		
Parking lot gate designation	_____	_____
Projected 1-hr peak entrance demand (vph)	_____	_____
Projected 1-hr peak exit demand (vph)	_____	_____
Projected 8-hr peak entrance demand (vph)	_____	_____
Projected 8-hr peak exit demand (vph)	_____	_____
Parking lot area (m <sup>2</sup> )	_____	_____
Parking lot capacity (veh)	_____	_____
Running time required to access auxiliary parking (s)	_____	_____
Facility emptying time	_____	_____
Average cars per stall	_____	_____
Average area per stall (m <sup>2</sup> )	_____	_____

WORKSHEET B - CAPACITY ANALYSIS

Intersection Purchase And Congress Streets

Case # 1 Year 1984

Step	Symbol	Input/Units		
1	i	Road segment (or approach) designation	<u>PS</u>	<u>CE</u>
2		<u>Free flow capacity computation:</u>		
2.1	$M_i$	Number of lanes		
2.2	$W_p$	Adjustment for lane width (Table B-1)		
2.3	$T_i$	Adjustment for trucks (Table B-2)		
2.4	$C_i$	Free flow capacity		
3		<u>Signalized intersection capacity:</u>		
3.1	j	Green signal phase identification	<u><math>\phi A / \phi B</math></u>	<u><math>\phi C</math></u>
3.2	$wa_i$	Approach width with parking (ft)	<u>45/68</u>	<u>52</u>
3.3		Percent right turners	<u>0</u>	<u>12</u>
3.4		Percent left turners	<u>0</u>	<u>0</u>
3.5		Metropolitan area size	<u>2 5 M</u>	
3.6	$CS_{i,j}$	Capacity service volume (vph or green)	<u>5100/7800*</u>	<u>9700</u>
4		<u>Signalized intersection green phase and cycle length:</u>		
4.1	$V_{i,j}$	Demand Volume for approach and phase		
4.2	$V_{i,j} / CS_{i,j}$	Volume to green capacity ratio		
4.3	approx G/Cy	Approximate G/Cy		
4.4	$\sum \max(V_{i,j} / CS_{i,j})$	Sum of the maximum V/C ratios for each signal phase		
4.5	Cy	Signal cycle time (sec)		
4.6	Gj	Green phase length		
4.7	Gj/Cy	Green phase to cycle time ratio		
4.8	$C_{i,j}$	Capacity for approach i phase j		
5		<u>Two-way stop, two-way yield or uncontrolled intersection:</u>		
5.1	$V_m + V_n$	Major street two-way volume		
5.2	$C_i$	Cross street capacity		
6		<u>Four-way stop intersections:</u>		
6.1	$V_i$	Approach volume		
6.2	$Sp_i$	Demand split on cross streets		
6.3	$C_i$	Capacity of approach		
7	$C_i$	Approach capacity $\sum_j C_{i,j}$ 5.2 for a four-way stop or 6.3 for a two-way stop		

\* 8hr capacity assumes parking 50% of the time along one side of Purchase Street (observed - not legal). Capacity lowers to 7800.

WORKSHEET B - CAPACITY ANALYSIS

Intersection Purchase And Congress Streets  
 Case # 2 Year 1990

Step	Symbol	Input/Units	PS	CE
1	i	Road segment (or approach) designation	<u>PS</u>	<u>CE</u>
2		<u>Free flow capacity computation:</u>		
2.1	$M_i$	Number of lanes	_____	_____
2.2	$W_p$	Adjustment for lane width (Table B-1)	_____	_____
2.3	$T_i$	Adjustment for trucks (Table B-2)	_____	_____
2.4	$C_i$	Free flow capacity	_____	_____
3		<u>Signalized intersection capacity:</u>		
3.1	j	Green signal phase identification	<u>φA/φB</u>	<u>φC</u>
3.2	$wa_i$	Approach width with parking (ft)	<u>45/68</u>	<u>52</u>
3.3		Percent right turners	<u>0</u>	<u>22</u>
3.4		Percent left turners	<u>0</u>	<u>0</u>
3.5		Metropolitan area size	<u>2.5M</u>	
3.6	$CS_{i,j}$	Capacity service volume (vph or green)	<u>5100/7800*</u>	<u>5700</u>
4		<u>Signalized intersection green phase and cycle length:</u>		
4.1	$V_{i,j}$	Demand Volume for approach and phase	_____	_____
4.2	$V_{i,j}/CS_{i,j}$	Volume to green capacity ratio	_____	_____
4.3	approx G/Cy	Approximate G/Cy	_____	_____
4.4	$\sum_j \max(V_{i,j}/CS_{i,j})$	Sum of the maximum V/C ratios for each signal phase	_____	_____
4.5	Cy	Signal cycle time (sec)	_____	_____
4.6	Gj	Green phase length	_____	_____
4.7	Gj/Cy	Green phase to cycle time ratio	_____	_____
4.8	$C_{i,j}$	Capacity for approach i phase j	_____	_____
5		<u>Two-way stop, two-way yield or uncontrolled intersection:</u>		
5.1	$V_m + V_n$	Major street two-way volume	_____	_____
5.2	$C_i$	Cross street capacity	_____	_____
6		<u>Four-way stop intersections:</u>		
6.1	$V_i$	Approach volume	_____	_____
6.2	$S_{pi}$	Demand split on cross streets	_____	_____
6.3	$C_i$	Capacity of approach	_____	_____
7	$C_i$	Approach capacity $\sum_j C_{i,j}$ 5.2 for a four-way stop or 6.3 for a two-way stop	_____	_____

WORKSHEET B - CAPACITY ANALYSIS

Intersection Purchase And Congress Streets  
 Case # 3 Year 1990

Step	Symbol	Input/Units		
1	$i$	Road segment (or approach) designation	<u>PS</u>	<u>CE</u>
2		<u>Free flow capacity computation:</u>		
2.1	$M_i$	Number of lanes	_____	_____
2.2	$W_p$	Adjustment for lane width (Table B-1)	_____	_____
2.3	$T_i$	Adjustment for trucks (Table B-2)	_____	_____
2.4	$C_i$	Free flow capacity	_____	_____
3		<u>Signalized intersection capacity:</u>		
3.1	$j$	Green signal phase identification	<u><math>\phi A / \phi B</math></u>	<u><math>\phi C</math></u>
3.2	$wa_i$	Approach width with parking (ft)	<u>45/68</u>	<u>52</u>
3.3		Percent right turners	<u>0</u>	<u>21</u>
3.4		Percent left turners	<u>0</u>	<u>0</u>
3.5		Metropolitan area size	<u>2.5M</u>	
3.6	$Cs_{i,j}$	Capacity service volume (vph or green)	<u>5100/7500*</u>	<u>5700</u>
4		<u>Signalized intersection green phase and cycle length:</u>		
4.1	$V_{i,j}$	Demand Volume for approach and phase	_____	_____
4.2	$V_{i,j}/Cs_{i,j}$	Volume to green capacity ratio	_____	_____
4.3	approx $G/Cy$	Approximate $G/Cy$	_____	_____
4.4	$\sum_j \max(V_{i,j}/Cs_{i,j})$	Sum of the maximum V/C ratios for each signal phase	_____	_____
4.5	$Cy$	Signal cycle time (sec)	_____	_____
4.6	$Gj$	Green phase length	_____	_____
4.7	$Gj/Cy$	Green phase to cycle time ratio	_____	_____
4.8	$C_{i,j}$	Capacity for approach i phase j	_____	_____
5		<u>Two-way stop, two-way yield or uncontrolled intersection:</u>		
5.1	$V_m + V_n$	Major street two-way volume	_____	_____
5.2	$C_i$	Cross street capacity	_____	_____
6		<u>Four-way stop intersections:</u>		
6.1	$V_i$	Approach volume	_____	_____
6.2	$Sp_i$	Demand split on cross streets	_____	_____
6.3	$C_i$	Capacity of approach	_____	_____
7	$C_i$	Approach capacity $\sum_j C_{i,j}$ 5.2 for a four-way stop or 6.3 for a two-way stop	_____	_____

## EPA VOLUME 9 (REVISED) INDIRECT SOURCE GUIDELINE MODEL - WORKSHEET #2

INTERSECTION: PURCHASE STREET & CONGRESS STREET  
CASE # 1 YEAR: 1984 AVERAGING TIME: 1-HOUR

LINE		PS	CE
LINE 1	ROAD SEGMENT ID		
LINE 2	DEMAND VOLUME (VPH)	1293.	1232.
LINE 4	CRUISE SPEED (MPH)	20	20
LINE 5	FREE-FLOW EMISSIONS (G/VEH/M)	0.0563	0.0563
LINE 6.1	NUMBER OF LANES	4	4
LINE 6.3	CAPACITY SERVICE VOLUME (VPH OF GREEN)	5100.	5700.
LINE 6.3	CAPACITY SERVICE VOLUME (VPH OF GREEN)	7800.	0.
LINE 6.4	DEMAND VOLUME (VPH)	470.	1232.
LINE 6.4	DEMAND VOLUME (VPH)	823.	0.
LINE 6.5	SIGNAL CYCLE LENGTH (S)	90.	
LINE 6.6	GREEN PHASE LENGTH (S)	16.	38.
LINE 6.6	GREEN PHASE LENGTH (S)	36.	0.
LINE 6.7	CAPACITY (VPH)	4027.	2407.
LINE 6.8	PROPORTION OF VEHICLES THAT STOP	0.966	0.737
LINE 6.8	PROPORTION OF VEHICLES THAT STOP	0.671	0.0
LINE 6.9	NUMBER OF VEHICLES THAT STOP PER CYCLE	10.642	22.702
LINE 6.9	NUMBER OF VEHICLES THAT STOP PER CYCLE	13.801	0.0
LINE 7.0	AVERAGE NUMBER OF VEHICLES IN QUEUE	0.47	1.06
LINE 8.0	LENGTH OF QUEUE (M/LANE)	27.10	25.83
LINE 9.0	AVERAGE EXCESS RUNNING TIME (S/VEH)	24.13	20.73
LINE 10.	EMISSIONS FROM ACCELERATION (G/VEH-M)	0.130	0.130
LINE 11.	EMISSIONS FROM DECELERATION (G/VEH-M)	0.046	0.046
LINE 12.	EMISSION RATE FOR ACC. AND DEC. (G/M-S)	0.048	0.044
LINE 13.	LENGTH OF ACC. AND DEC. (M)	35.8	35.8
LINE 14.	LENGTH FOR EXCESS EMISSIONS (M)	71.5	71.5
LINE 15	IDLING EMISSION RATE (G/S)	1.837	1.455
LINE 16.	AVERAGE EMISSION RATE (G/S-M)	0.0496	0.0425
LINE 17	ADJUSTED EXCESS EMISSION RATE (G/S-M)	0.0675	0.0568
LINE 18.	FREE-FLOW EMISSION RATE (G/S-M)	0.0202	0.0193



## EPA VOLUME 9 (REVISED) INDIRECT SOURCE GUIDELINE MODEL - WORKSHEET #2

INTERSECTION: PURCHASE STREET & CONGRESS STREET  
CASE # 1 YEAR: 1984 AVERAGING TIME: 8-HOUR

LINE	ROAD SEGMENT ID	PS	CE
LINE 2	DEMAND VOLUME (VPH)	905	838
LINE 4	CRUISE SPEED (MPH)	30	25
LINE 5	FREE-FLOW EMISSIONS (G/VEH-M)	0.0256	0.0312
LINE 6.1	NUMBER OF LANES	4	4
LINE 6.3	CAPACITY SERVICE VOLUME (VPH OF GREEN)	5100	5700
LINE 6.3	CAPACITY SERVICE VOLUME (VPH OF GREEN)	7100	0
LINE 6.4	DEMAND VOLUME (VPH)	329	838
LINE 6.4	DEMAND VOLUME (VPH)	576	0
LINE 6.5	SIGNAL CYCLE LENGTH (S)	90	
LINE 6.6	GREEN PHASE LENGTH (S)	16	38
LINE 6.6	GREEN PHASE LENGTH (S)	36	0
LINE 6.7	CAPACITY (VPH)	3747	2407
LINE 6.8	PROPORTION OF VEHICLES THAT STOP	0.879	0.677
LINE 6.8	PROPORTION OF VEHICLES THAT STOP	0.653	0.0
LINE 6.9	NUMBER OF VEHICLES THAT STOP PER CYCLE	7.229	14.191
LINE 6.9	NUMBER OF VEHICLES THAT STOP PER CYCLE	0.463	0.0
LINE 7.0	AVERAGE NUMBER OF VEHICLES IN QUEUE	0.32	0.53
LINE 8.0	LENGTH OF QUEUE (M/LANE)	18.43	16.01
LINE 9.0	AVERAGE EXCESS RUNNING TIME (S/VEH)	23.35	18.41
LINE 10.	EMISSIONS FROM ACCELERATION (G/VEH-M)	0.100	0.111
LINE 11.	EMISSIONS FROM DECELERATION (G/VEH-M)	0.031	0.038
LINE 12.	EMISSION RATE FOR ACC. AND DEC. (G/M-S)	0.024	0.023
LINE 13	LENGTH OF ACC AND DEC (M)	80.5	55.9
LINE 14	LENGTH FOR EXCESS EMISSIONS (M)	100.9	111.7
LINE 15.	IDLING EMISSION RATE (G/S)	1.108	0.793
LINE 16.	AVERAGE EMISSION RATE (G/S-M)	0.0190	0.0188
LINE 17	ADJUSTED EXCESS EMISSION RATE (G/S-M)	0.0167	0.0164
LINE 18	FREE-FLOW EMISSION RATE (G/S-M)	0.0064	0.0073

## EPA VOLUME 9 (REVISED) INDIRECT SOURCE GUIDELINE MODEL - WORKSHEET #2

INTERSECTION: PURCHASE STREET & CONGRESS STREET  
CASE # 2 YEAR: 1990 AVERAGING TIME: 1-HOUR

LINE	ROAD SEGMENT ID	PS	CE
LINE 2	DEMAND VOLUME (VPH)	2871	1459
LINE 4	CRUISE SPEED (MPH)	20	20
LINE 5	FREE-FLOW EMISSIONS (G-VEH/M)	0.0271	0.0271
LINE 6.1	NUMBER OF LANES	4	4
LINE 6.3	CAPACITY SERVICE VOLUME (VPH OF GREEN)	5100	5700
LINE 6.3	CAPACITY SERVICE VOLUME (VPH OF GREEN)	7800	0
LINE 6.4	DEMAND VOLUME (VPH)	470	1459
LINE 6.4	DEMAND VOLUME (VPH)	1601	0
LINE 6.5	SIGNAL CYCLE LENGTH (S)	90	
LINE 6.6	GREEN PHASE LENGTH (S)	16	35
LINE 6.6	GREEN PHASE LENGTH (S)	39	0
LINE 6.7	CAPACITY (VPH)	4287	2217
LINE 6.8	PROPORTION OF VEHICLES THAT STOP	0.906	0.821
LINE 6.8	PROPORTION OF VEHICLES THAT STOP	0.713	0.0
LINE 6.9	NUMBER OF VEHICLES THAT STOP PER CYCLE	10.642	29.959
LINE 6.9	NUMBER OF VEHICLES THAT STOP PER CYCLE	28.539	0.0
LINE 7.0	AVERAGE NUMBER OF VEHICLES IN QUEUE	0.93	1.93
LINE 8.0	LENGTH OF QUEUE (M/LANE)	43.63	34.67
LINE 9.0	AVERAGE EXCESS RUNNING TIME (S/VEH)	22.45	25.71
LINE 10.	EMISSIONS FROM ACCELERATION (G/VEH-M)	0.130	0.130
LINE 11.	EMISSIONS FROM DECELERATION (G/VEH-M)	0.046	0.046
LINE 12.	EMISSION RATE FOR ACC. AND DEC. (G/M-S)	0.077	0.059
LINE 13.	LENGTH OF ACC AND DEC (M)	35.8	35.8
LINE 14.	LENGTH FOR EXCESS EMISSIONS (M)	71.5	71.5
LINE 15.	IDLING EMISSION RATE (G/S)	2.695	2.235
LINE 16.	AVERAGE EMISSION RATE (G/S-M)	0.0760	0.0605
LINE 17	ADJUSTED EXCESS EMISSION RATE (G/S-M)	0.0444	0.0358
LINE 18.	FREE-FLOW EMISSION RATE (G/S-M)	0.0156	0.0110

## EPA VOLUME 9 (REVISED) INDIRECT SOURCE GUIDELINE MODEL - WORKSHEET #2

INTERSECTION: PURCHASE STREET & CONGRESS STREET  
CASE # 2 YEAR: 1990 AVERAGING TIME: 8-HOUR

LINE	ROAD SEGMENT ID	PS	CE
LINE 2	DEMAND VOLUME (VPH)	1450	992
LINE 4	CRUISE SPEED (MPH)	30	25
LINE 5	FREE-FLOW EMISSIONS (G/VEH/M)	0.0132	0.0161
LINE 6.1	NUMBER OF LANES	4	4
LINE 6.3	CAPACITY SERVICE VOLUME (VPH OF GREEN)	5100	5700
LINE 6.3	CAPACITY SERVICE VOLUME (VPH OF GREEN)	7100	0
LINE 6.4	DEMAND VOLUME (VPH)	329	992
LINE 6.4	DEMAND VOLUME (VPH)	1121	0
LINE 6.5	SIGNAL CYCLE LENGTH (S)	90	
LINE 6.6	GREEN PHASE LENGTH (S)	16	35
LINE 6.6	GREEN PHASE LENGTH (S)	39	0
LINE 6.7	CAPACITY (VPH)	3983	2217
LINE 6.8	PROPORTION OF VEHICLES THAT STOP	0.879	0.740
LINE 6.8	PROPORTION OF VEHICLES THAT STOP	0.673	0.0
LINE 6.9	NUMBER OF VEHICLES THAT STOP PER CYCLE	7.229	18.349
LINE 6.9	NUMBER OF VEHICLES THAT STOP PER CYCLE	18.858	0.0
LINE 7.0	AVERAGE NUMBER OF VEHICLES IN QUEUE	0.57	0.81
LINE 8.0	LENGTH OF QUEUE (M/LANE)	28.99	20.84
LINE 9.0	AVERAGE EXCESS RUNNING TIME (S/VEH)	21.16	21.66
LINE 10	EMISSIONS FROM ACCELERATION (G/VEH-M)	0.100	0.111
LINE 11	EMISSIONS FROM DECELERATION (G/VEH-M)	0.031	0.038
LINE 12	EMISSION RATE FOR ACC. AND DEC. (G/M-S)	0.038	0.030
LINE 13	LENGTH OF ACC. AND DEC. (M)	80.5	55.9
LINE 14	LENGTH FOR EXCESS EMISSIONS (M)	160.9	111.7
LINE 15	IDLING EMISSION RATE (G/S)	1.551	1.166
LINE 16	AVERAGE EMISSION RATE (G/S-M)	0.0206	0.0256
LINE 17	ADJUSTED EXCESS EMISSION RATE (G/S-M)	0.0113	0.0103
LINE 18	FREE-FLOW EMISSION RATE (G/S-M)	0.0053	0.0044

## EPA VOLUME 9 (REVISED) INDIRECT SOURCE GUIDELINE MODEL - WORKSHEET #2

INTERSECTION: PURCHASE STREET & CONGRESS STREET  
CASE # 3 YEAR: 1990 AVERAGING TIME: 1-HOUR

LINE		PS	CE
LINE 1	ROAD SEGMENT ID		
LINE 2	DEMAND VOLUME (VPH)	2294.	1537.
LINE 4	CRUISE SPEED (MPH)	20	20
LINE 5	FREE-FLOW EMISSIONS (G-VEH/M)	0.0271	0.0271
LINE 6.1	NUMBER OF LANES	4	4
LINE 6.3	CAPACITY SERVICE VOLUME (VPH OF GREEN)	5100.	5700.
LINE 6.3	CAPACITY SERVICE VOLUME (VPH OF GREEN)	7800	0.
LINE 6.4	DEMAND VOLUME (VPH)	470	1537.
LINE 6.4	DEMAND VOLUME (VPH)	1734.	0.
LINE 6.5	SIGNAL CYCLE LENGTH (S)	90.	
LINE 6.6	GREEN PHASE LENGTH (S)	15	35.
LINE 6.6	GREEN PHASE LENGTH (S)	39	0.
LINE 6.7	CAPACITY (VPH)	4287.	2217.
LINE 6.8	PROPORTION OF VEHICLES THAT STOP	0.966	0.837
LINE 6.8	PROPORTION OF VEHICLES THAT STOP	0.729	0.0
LINE 6.9	NUMBER OF VEHICLES THAT STOP PER CYCLE	10.642	32.152
LINE 6.9	NUMBER OF VEHICLES THAT STOP PER CYCLE	31.587	0.0
LINE 7.0	AVERAGE NUMBER OF VEHICLES IN QUEUE	1.06	2.26
LINE 8.0	LENGTH OF QUEUE (M/LANE)	47.07	37.42
LINE 9.0	AVERAGE EXCESS RUNNING TIME (S/VEH)	22.05	26.08
LINE 10.	EMISSIONS FROM ACCELERATION (G/VEH-M)	0.130	0.130
LINE 11	EMISSIONS FROM DECELERATION (G/VEH-M)	0.046	0.046
LINE 12.	EMISSION RATE FOR ACC. AND DEC. (G/M-S)	0.083	0.083
LINE 13.	LENGTH OF ACC. AND DEC (M)	35.8	35.8
LINE 14.	LENGTH FOR EXCESS EMISSIONS (M)	71.5	71.5
LINE 15	IDLING EMISSION RATE (G/S)	2.901	2.460
LINE 16.	AVERAGE EMISSION RATE (G/S-M)	0.0818	0.0658
LINE 17	ADJUSTED EXCESS EMISSION RATE (G/S-M)	0.0479	0.0390
LINE 18	FREE-FLOW EMISSION RATE (G/S-M)	0.0165	0.0116

## EPA VOLUME 9 (REVISED) INDIRECT SOURCE GUIDELINE MODEL - WORKSHEET #2

INTERSECTION ATLANTIC AVE AND SURFACE ARTERY  
CASE # 3 YEAR 1990 AVERAGING TIME 8-HOUR

LINE	ROAD SEGMENT ID	SN	AN	AS	SS
LINE 2	DEMAND VOLUME (VPH)	1058	1207	702	773
LINE 4	CRUISE SPEED (MPH)	35	32	26	29
LINE 5	FREE-FLOW EMISSIONS (G-VEH/M)	0 0111	0 0122	0 0155	0 0137
LINE 6.1	NUMBER OF LANES	2	2	3	3
LINE 6.3	CAPACITY SERVICE VOLUME (VPH OF GREEN)	3500	1750	3800	4800
LINE 6.3	CAPACITY SERVICE VOLUME (VPH OF GREEN)	3200	3500	0	0
LINE 6.4	DEMAND VOLUME (VPH)	245	506	702	773
LINE 6.4	DEMAND VOLUME (VPH)	813	701	0	0
LINE 6.5	SIGNAL CYCLE LENGTH (S)	100			
LINE 6.6	GREEN PHASE LENGTH (S)	11	49	24	38
LINE 6.6	GREEN PHASE LENGTH (S)	38	27	0	0
LINE 6.7	CAPACITY (VPH)	1601	1803	912	1824
LINE 6.8	PROPORTION OF VEHICLES THAT STOP	0 957	0 717	0 932	0 739
LINE 6.8	PROPORTION OF VEHICLES THAT STOP	0 831	0 913	0 0	0 0
LINE 6.9	NUMBER OF VEHICLES THAT STOP PER CYCLE	6 513	10 084	18 178	15 868
LINE 6.9	NUMBER OF VEHICLES THAT STOP PER CYCLE	18 771	17 775	0 0	0 0
LINE 7.0	AVERAGE NUMBER OF VEHICLES IN QUEUE	1 95	2 03	3 34	0 74
LINE 8.0	LENGTH OF QUEUE (M/LANE)	59 23	65 00	31 21	24 08
LINE 9.0	AVERAGE EXCESS RUNNING TIME (S/VEH)	34 04	31 07	48 62	24 36
LINE 10	EMISSIONS FROM ACCELERATION (G/VEH-M)	0 095	0 098	0 109	0 101
LINE 11	EMISSIONS FROM DECELERATION (G/VEH-M)	0 028	0 030	0 036	0 032
LINE 12	EMISSION RATE FOR ACC AND DEC (G/M-S)	0 031	0 036	0 026	0 021
LINE 13	LENGTH OF ACC AND DEC (M)	109 5	91 5	60 4	75 2
LINE 14	LENGTH FOR EXCESS EMISSIONS (M)	219 0	183 1	120 9	150 4
LINE 15	IDLING EMISSION RATE (G/S)	2 019	2 101	2 151	1 012
LINE 16	AVERAGE EMISSION RATE (G/S-M)	0 0248	0 0293	0 0310	0 0173
LINE 17	ADJUSTED EXCESS EMISSION RATE (G/S-M)	0 0103	0 0121	0 0136	0 0070
LINE 18	FREE-FLOW EMISSION RATE (G/S-M)	0 0033	0 0041	0 0030	0 0029



## EPA VOLUME 9 (REVISED) INDIRECT SOURCE GUIDELINE MODEL - WORKSHEET #2

INTERSECTION: ATLANTIC AVE AND SURFACE ARTERY  
CASE # 3 YEAR: 1990 AVERAGING TIME: 1-HOUR

LINE 1	ROAD SEGMENT ID	HE
LINE 2	DEMAND VOLUME (VPH)	212
LINE 4	CRUISE SPEED (MPH)	24
LINE 5	FREE-FLOW EMISSIONS (G-VEH/M)	0.0232
LINE 6.1	NUMBER OF LANES	2
LINE 6.3	CAPACITY SERVICE VOLUME (VPH OF GREEN)	0
LINE 6.4	DEMAND VOLUME (VPH)	0
LINE 6.5	SIGNAL CYCLE LENGTH (S)	0
LINE 6.6	GREEN PHASE LENGTH (S)	0
LINE 6.7	CAPACITY (VPH)	240.
LINE 6.8	PROPORTION OF VEHICLES THAT STOP	0.0
LINE 6.9	NUMBER OF VEHICLES THAT STOP PER CYCLE	0.0
LINE 7.0	AVERAGE NUMBER OF VEHICLES IN QUEUE	7.57
LINE 8.0	LENGTH OF QUEUE (M/LANE)	16.47
LINE 9.0	AVERAGE EXCESS RUNNING TIME (S/VEH)	113.57
LINE 10.	EMISSIONS FROM ACCELERATION (G/VEH-M)	0.113
LINE 11.	EMISSIONS FROM DECELERATION (G/VEH-M)	0.039
LINE 12.	EMISSION RATE FOR ACC AND DEC. (G/M-S)	0.009
LINE 13.	LENGTH OF ACC. AND DEC. (M)	51.5
LINE 14.	LENGTH FOR EXCESS EMISSIONS (M)	103.0
LINE 15.	IDLING EMISSION RATE (G/S)	1.627
LINE 16.	AVERAGE EMISSION RATE (G/S-M)	0.0203
LINE 17.	ADJUSTED EXCESS EMISSION RATE (G/S-M)	0.0136
LINE 18.	FREE-FLOW EMISSION RATE (G/S-M)	0.0014

WORKSHEET 5 - INTERSECTION CO DISPERSION ANALYSIS

Intersection Purchase And Congress Streets

Case # 1 Year 1984 Averaging Time 8 Hour

Line No. Symbol	Input/Units	PS	Traffic Stream CE
1 SC	Stability Class	D	
2 U	Wind Speed ( $m s^{-1}$ )	1.6	
3 $\theta$	Wind-Road Angle (deg)	10	-80
4 x	Lateral Distance (m)	11	13
5 Yu	Maximum Longitudinal Distance (m)	181	NA
6 Yd	Minimum Longitudinal Distance (m)	20	NA
7 $\sigma_{z0}$	Initial Dispersion (m)	5.0	
8 Qe	Excess Emissions Rate ( $gm^{-1}s^{-1}$ )	.0167	.0164
9 Qf	Free Flow Emissions Rate ( $gm^{-1}s^{-1}$ )	.0064	.0073
9a	Street Canyon? Yes or No	No	
DISPERSION ANALYSIS			
10 XUQ <sup>-1</sup>	Normalized Concentration ( $10^{-3}m^{-1}$ ) Free Flow	625	NA
Qf	Enter Line 9	x .0064 x .0073 x	
11 XU	Normalized Concentration ( $mg m^{-2}s^{-1}$ )		
U	Enter Line 2	÷ 1.6 ÷	
12 x	CO Concentration ( $mg m^{-3}$ ) Through Emissions	2.5	0.0
13 XUQ <sup>-1</sup>	Normalized Concentration (For Yu)	500	NA
Qe	Enter Line 8	.0167	.0164
14 XU	Normalized Concentration ( $mg m^{-2}s^{-1}$ )		
U	Enter Line 2	1.6	
15 x	CO Concentration-"Maximum Queue"	5.2	0.0
16 XUQ <sup>-1</sup>	Normalized Concentration (For Yd)	0	NA
Qe	Enter Line 8	x .0167 x .0164 x	
17 XU	Normalized Concentration ( $mg m^{-2}s^{-1}$ )		
U	Enter Line 2	1.6	
18 x	CO Concentration-"Imaginary Queue"	÷ 0.0 ÷ 0.0 ÷	
19 x	CO ( $mg m^{-3}$ ) Total	7.7	0.0
20 x	CO Concentration (ppm)-- Total	6.7	0.0
OPTIONAL z-CORRECTION (Heights Other than 1.8m Above the Ground)			
21 z	Height of Receptor (m)		
22	z-Correction Factor		
23 x"	CO Concentration at Height z ( $mg m^{-3}$ )		
24 x"	CO Concentration at Height z (ppm)		

6.7 ppm

WORKSHEET 5 - INTERSECTION CO DISPERSION ANALYSIS

Intersection Purchase And Congress Streets  
 Case # 2 Year 1990 Averaging Time 1 Hour

Line No.	Symbol	Input/Units	PS	Traffic Stream CE
1	SC	Stability Class	D	
2	U	Wind Speed ( $m s^{-1}$ )	1.0	
3	$\theta$	Wind-Road Angle (deg)	16	-74
4	x	Lateral Distance (m)	11	13
5	Yu	Maximum Longitudinal Distance (m)	92	NA
6	Yd	Minimum Longitudinal Distance (m)	20	NA
7	$\sigma_{zo}$	Initial Dispersion (m)	5.0	
8	Qe	Excess Emissions Rate ( $gm^{-1}s^{-1}$ )	.0444	.0358
9	QF	Free Flow Emissions Rate ( $gm^{-1}s^{-1}$ )	.0156	.0110
9a		Street Canyon? Yes or No	No	
DISPERSION ANALYSIS				
10	$xUQ^{-1}$	Normalized Concentration ( $10^{-3}m^{-1}$ ) Free Flow	440	NA
	QF	Enter Line 9	$\times .0156$	$\times .0110$
11	XU	Normalized Concentration ( $mg m^{-2}s^{-1}$ )		
	U	Enter Line 2	$\div 1.0$	$\div$
12	x	CO Concentration ( $mg m^{-3}$ ) Through Emissions	6.9	0.0
13	$xUQ^{-1}$	Normalized Concentration (For Yu)	375	NA
	Qe	Enter Line 8	.0444	.0358
14	XU	Normalized Concentration ( $mg m^{-2}s^{-1}$ )		
	U	Enter Line 2	1.0	
15	x	CO Concentration--"Maximum Queue"	16.7	0.0
16	$xUQ^{-1}$	Normalized Concentration (For Yd)	0	NA
	Qe	Enter Line 8	$\times .0444$	$\times .0358$
17	XU	Normalized Concentration ( $mg m^{-2}s^{-1}$ )		
	U	Enter Line 2	1.0	
18	x	CO Concentration--"Imaginary Queue"	$\div 0.0$	$\div 0.0$
19	x	CO ( $mg m^{-3}$ ) Total	23.6	0.0
20	x	CO Concentration (ppm)-- Total	20.5	0.0
OPTIONAL z-CORRECTION (Heights Other than 1.8m Above the Ground)				
21	z	Height of Receptor (m)		
22		z-Correction Factor		
23	$x^z$	CO Concentration at Height z ( $mg m^{-3}$ )		
24	$x^z$	CO Concentration at Height z (ppm)		

20.5 pp

WORKSHEET 5 - INTERSECTION CO DISPERSION ANALYSIS

Intersection Purchase And Congress Streets  
 Case # 2 Year 1990 Averaging Time 8 Hour

Line No. Symbol	Input/Units	PS	Traffic Stream CE
1 SC	Stability Class	D	
2 U	Wind Speed ( $m s^{-1}$ )	1.6	
3 $\theta$	Wind-Road Angle (deg)	10	-80
4 x	Lateral Distance (m)	11	13
5 Yu	Maximum Longitudinal Distance (m)	181	NA
6 Yd	Minimum Longitudinal Distance (m)	20	NA
7 $\sigma_{z0}$	Initial Dispersion (m)	5.0	
8 Qe	Excess Emissions Rate ( $gm^{-1}s^{-1}$ )	.0113	.0103
9 Qf	Free Flow Emissions Rate ( $gm^{-1}s^{-1}$ )	.0053	.0044
9a	Street Canyon? Yes or No	NO	
DISPERSION ANALYSIS			
10 $xUQ^{-1}$	Normalized Concentration ( $10^{-3}m^{-1}$ ) Free Flow	6.25	NA
Qf	Enter Line 9	x .0053 x	.0044 x
11 XU	Normalized Concentration ( $mg m^{-2}s^{-1}$ )		
U	Enter Line 2	÷ 1.6 ÷	÷ ÷
12 x	CO Concentration ( $mg m^{-3}$ ) Through Emissions	2.1	0.0
13 $xUQ^{-1}$	Normalized Concentration (For Yu)	5.00	NA
Qe	Enter Line 8	.0113	.0103
14 XU	Normalized Concentration ( $mg m^{-2}s^{-1}$ )		
U	Enter Line 2	1.6	
15 x	CO Concentration-"Maximum Queue"	3.5	0.0
16 $xUQ^{-1}$	Normalized Concentration (For Yd)	0	NA
Qe	Enter Line 8	x .0113 x	.0103 x
17 XU	Normalized Concentration ( $mg m^{-2}s^{-1}$ )		
U	Enter Line 2	1.6	
18 x	CO Concentration-"Imaginary Queue"	0.0	0.0
19 x	CO ( $mg m^{-3}$ ) Total	5.6	0.0
20 x	CO Concentration (ppm)-- Total	4.9	0.0
OPTIONAL z-CORRECTION (Heights Other than 1.8m Above the Ground)			
21 z	Height of Receptor (m)		
22	z-Correction Factor		
23 x'	CO Concentration at Height z ( $mg m^{-3}$ )		
24 x'	CO Concentration at Height z (ppm)		

4.9 ppm

WORKSHEET 5 - INTERSECTION CO DISPERSION ANALYSIS

Intersection Purchase And Congress Streets  
 Case # 3 Year 1990 Averaging Time 1 Hour

Line No. Symbol	Input/Units	PS	Traffic Stream CE
1 SC	Stability Class	D	
2 U	Wind Speed ( $m s^{-1}$ )	1.0	
3 $\theta$	Wind-Road Angle (deg)	16	-74
4 x	Lateral Distance (m)	11	13
5 Yu	Maximum Longitudinal Distance (m)	97	NA
6 Yd	Minimum Longitudinal Distance (m)	20	NA
7 $\sigma_{z0}$	Initial Dispersion (m)	5.0	
8 Qe	Excess Emissions Rate ( $gm^{-1}s^{-1}$ )	.0479	.0390
9 QF	Free Flow Emissions Rate ( $gm^{-1}s^{-1}$ )	.0166	.0116
9a	Street Canyon? Yes or No	NO	
DISPERSION ANALYSIS			
10 $xuQ^{-1}$	Normalized Concentration ( $10^{-3}m^{-1}$ ) Free Flow	440	NA
QF	Enter Line 9	$\times .0166 \times$	$\times .0116 \times$
11 XU	Normalized Concentration ( $mg m^{-2}s^{-1}$ )		
U	Enter Line 2	$\div 1.0 \div$	$\div \div$
12 X	CO Concentration ( $mg m^{-3}$ ) Through Emissions	7.3	0.0
13 $xuQ^{-1}$	Normalized Concentration (For Yu)	375	NA
Qe	Enter Line 8	.0479	.0390
14 XU	Normalized Concentration ( $mg m^{-2}s^{-1}$ )		
U	Enter Line 2	1.0	
15 X	CO Concentration--"Maximum Queue"	18.0	0.0
16 $xuQ^{-1}$	Normalized Concentration (For Yd)	0	NA
Qe	Enter Line 8	$\times .0479 \times$	$\times .0390 \times$
17 XU	Normalized Concentration ( $mg m^{-2}s^{-1}$ )		
U	Enter Line 2	1.0	
18 X	CO Concentration--"Imaginary Queue"	$\div 0.0 \div$	$\div 0.0 \div$
19 X	CO ( $mg m^{-3}$ ) Total	25.3	0.0
20 X	CO Concentration (ppm)-- Total	22.0	0.0
OPTIONAL z-CORRECTION (Heights Other than 1.8m Above the Ground)			
21 z	Height of Receptor (m)		
22	z-Correction Factor		
23 $x'$	CO Concentration at Height z ( $mg m^{-3}$ )		
24 $x'$	CO Concentration at Height z (ppm)		

22.0 ppm



WORKSHEET 5 - INTERSECTION CO DISPERSION ANALYSIS

Intersection Purchase And Congress Streets  
 Case # 3 Year 1990 Averaging Time 8 Hour

Line No.	Symbol	Input/Units	PS	Traffic Stream CE
1	SC	Stability Class	D	
2	U	Wind Speed ( $m s^{-1}$ )	7.6	
3	$\theta$	Wind-Road Angle (deg)	10	-80
4	x	Lateral Distance (m)	11	13
5	Yu	Maximum Longitudinal Distance (m)	181	NA
6	Yd	Minimum Longitudinal Distance (m)	20	NA
7	$\sigma_{z0}$	Initial Dispersion (m)	5.0	
8	Qe	Excess Emissions Rate ( $gm^{-1}s^{-1}$ )	.0121	.0110
9	Qf	Free Flow Emissions Rate ( $gm^{-1}s^{-1}$ )	.0057	.0047
9a		Street Canyon? Yes or No	No	
DISPERSION ANALYSIS				
10	$xUQ^{-1}$	Normalized Concentration ( $10^{-3}m^{-1}$ ) Free Flow	6.25	NA
	Qf	Enter Line 9	$\times .0057 \times$	$\times .0047 \times$
11	xU	Normalized Concentration ( $mg m^{-2}s^{-1}$ )	$\div 1.6 \div$	$\div \div$
	U	Enter Line 2		
12	x	CO Concentration ( $mg m^{-3}$ ) Through Emissions	2.2	0.0
13	$xUQ^{-1}$	Normalized Concentration (For Yu)	500	NA
	Qe	Enter Line 8	.0121	.0110
14	xU	Normalized Concentration ( $mg m^{-2}s^{-1}$ )	$\div 1.6 \div$	$\div \div$
	U	Enter Line 2		
15	x	CO Concentration--"Maximum Queue"	3.8	0.0
16	$xUQ^{-1}$	Normalized Concentration (For Yd)	0	NA
	Qe	Enter Line 8	$\times .0121 \times$	$\times .0110 \times$
17	xU	Normalized Concentration ( $mg m^{-2}s^{-1}$ )	$\div 1.6 \div$	$\div \div$
	U	Enter Line 2		
18	x	CO Concentration--"Imaginary Queue"	$\div 0.0 \div$	$\div 0.0 \div$
19	x	CO ( $mg m^{-3}$ ) Total	6.0	0.0
20	x	CO Concentration (ppm)-- Total	5.2	0.0
OPTIONAL z-CORRECTION (Heights Other than 1.8m Above the Ground)				
21	z	Height of Receptor (m)		
22		z-Correction Factor		
23	x'	CO Concentration at Height z ( $mg m^{-3}$ )		
24	x'	CO Concentration at Height z (ppm)		

5.2 ppm

WORKSHEET 1 - TRAFFIC INFORMATION

Intersection Purchase St and I.P. Access Drive  
 Case # 1 Year 84

1. Road segment or intersection approach identification	<u>PS</u>
2. Observed 1-hr volume (vph)	_____
Observed 8-hr volume (vph)	_____
Projected 1-hr peak demand (vph)	<u>1902</u>
Projected 8-hr peak demand (vph)	<u>1427</u>
3. Percentage cold starts	<u>50/20.6</u>
4. Percentage trucks and buses	<u>5.8%</u>
5. Metropolitan population	<u>2.5 x 10<sup>6</sup></u>
6. Slope	_____
7. Free-flow parameters	
Number of lanes	<u>3</u>
Average lane width (ft)	<u>12</u>
Design speed (mph)	<u>28/35</u>
Highway type (see Figures 2-5)	<u>Urban Arterial</u>
8. Intersection parameters	
Intersection designation	_____
Approach width (ft)	_____
Percentage right turns	<u>0</u>
Percentage left turns	<u>0</u>
Type control and description of signal controller	_____
9. Area source parameters	
Parking lot gate designation	_____
Projected 1-hr peak entrance demand (vph)	_____
Projected 1-hr peak exit demand (vph)	_____
Projected 8-hr peak entrance demand (vph)	_____
Projected 8-hr peak exit demand (vph)	_____
Parking lot area (m <sup>2</sup> )	_____
Parking lot capacity (veh)	_____
Running time required to access auxiliary parking (s)	_____
Facility emptying time	_____
Average cars per stall	_____
Average area per stall (m <sup>2</sup> )	_____

PS = Purchase Street Southbound

WORKSHEET 1 - TRAFFIC INFORMATION

Intersection Purchase St and I. P. Access Drive  
Case # 2 year 90

1. Road segment or intersection approach identification	<u>PS</u>
2. Observed 1-hr volume (vph)	_____
Observed 8-hr volume (vph)	_____
Projected 1-hr peak demand (vph)	<u>3346</u>
Projected 8-hr peak demand (vph)	<u>2510</u>
3. Percentage cold starts	<u>50/60.6</u>
4. Percentage trucks and buses	<u>5.3%</u>
5. Metropolitan population	<u>2.5x10<sup>6</sup></u>
6. Slope	_____
7. Free-flow parameters	
Number of lanes	<u>3</u>
Average lane width (ft)	<u>12</u>
Design speed (mph)	<u>28/35</u>
Highway type (see Figures 2-5)	<u>Urban Arterial</u>
8. Intersection parameters	
Intersection designation	_____
Approach width (ft)	_____
Percentage right turns	<u>0</u>
Percentage left turns	<u>0</u>
Type control and description of signal controller	_____
9. Area source parameters	
Parking lot gate designation	_____
Projected 1-hr peak entrance demand (vph)	_____
Projected 1-hr peak exit demand (vph)	_____
Projected 8-hr peak entrance demand (vph)	_____
Projected 8-hr peak exit demand (vph)	_____
Parking lot area (m <sup>2</sup> )	_____
Parking lot capacity (veh)	_____
Running time required to access auxiliary parking (s)	_____
Facility emptying time	_____
Average cars per stall	_____
Average area per stall (m <sup>2</sup> )	_____

\* Peak 1-hr volume is constrained to 97% of capacity.

WORKSHEET 1 - TRAFFIC INFORMATION

Intersection Purchase St. and I.P. Access Drive  
 Case # 3 Year 90

1. Road segment or intersection approach identification	PS	AE
2. Observed 1-hr volume (vph)	---	---
Observed 8-hr volume (vph)	---	---
Projected 1-hr peak demand (vph)	3346	357*
Projected 8-hr peak demand (vph)	2510	110
3. Percentage cold starts	50/20.6	---
4. Percentage trucks and buses	6.8%	---
5. Metropolitan population	2.5 x 10 <sup>6</sup>	---
6. Slope	---	---
7. Free-flow parameters		
Number of lanes	3	1
Average lane width (ft)	12	12
Design speed (mph)	28/35	5/5
Highway type (see Figures 2-5)	Urban Arterial	---
8. Intersection parameters		
Intersection designation	---	---
Approach width (ft)	---	---
Percentage right turns	0	100
Percentage left turns	0	0
Type control and description of signal controller	---	---
9. Area source parameters		
Parking lot gate designation	---	---
Projected 1-hr peak entrance demand (vph)	---	---
Projected 1-hr peak exit demand (vph)	---	---
Projected 8-hr peak entrance demand (vph)	---	---
Projected 8-hr peak exit demand (vph)	---	---
Parking lot area (m <sup>2</sup> )	---	---
Parking lot capacity (veh)	---	---
Running time required to access auxiliary parking (s)	---	---
Facility emptying time	---	---
Average cars per stall	---	---
Average area per stall (m <sup>2</sup> )	---	---

AE = International Place Access Drive Eastbound.

\* Peak 1-hr volume is constrained to 97% of capacity.

WORKSHEET B - CAPACITY ANALYSIS

Intersection Purchase St and I.P. Access Drive  
 Case # 3 Year 90

Step	Symbol	Input/Units				
1	$i$	Road segment (or approach) designation	<u>AE</u>	<u>AE</u>	<u>AE</u>	<u>AE</u>
2		<u>Free flow capacity computation:</u>	<u>Case 3</u>	<u>Case 3</u>	<u>Case 4</u>	<u>Case 4</u>
2.1	$M_i$	Number of lanes	<u>1-hr</u>	<u>8-hr</u>	<u>1-hr</u>	<u>8-hr</u>
2.2	$W_p$	Adjustment for lane width (Table B-1)				
2.3	$T_i$	Adjustment for trucks (Table B-2)				
2.4	$C_i$	Free flow capacity				
3		<u>Signalized intersection capacity:</u>				
3.1	$j$	Green signal phase identification				
3.2	$wa_i$	Approach width with parking (ft)				
3.3		Percent right turners				
3.4		Percent left turners				
3.5		Metropolitan area size				
3.6	$Cs_{i,j}$	Capacity service volume (vph or green)				
4		<u>Signalized intersection green phase and cycle length:</u>				
4.1	$V_{i,j}$	Demand Volume for approach and phase				
4.2	$V_{i,j}/Cs_{i,j}$	Volume to green capacity ratio				
4.3	approx $G/Cy$	Approximate $G/Cy$				
4.4	$\sum_j \max(V_{i,j}/Cs_{i,j})$	Sum of the maximum V/C ratios for each signal phase				
4.5	$Cy$	Signal cycle time (sec)				
4.6	$Gj$	Green phase length				
4.7	$Gj/Cy$	Green phase to cycle time ratio				
4.8	$C_{i,j}$	Capacity for approach $i$ phase $j$				
5		<u>Two-way stop, two-way yield or uncontrolled intersection:</u>				
5.1	$V_m + V_n$	Major street two-way volume	<u>3346 ÷ 3</u>	<u>2510 ÷ 3</u>	<u>313 ÷ 3</u>	<u>2485 ÷ 3</u>
5.2	$C_i$	Cross street capacity (1 exit lane)	<u>368</u>	<u>453</u>	<u>371</u>	<u>456</u>
6		<u>Four-way stop intersections:</u>				
6.1	$V_i$	Approach volume				
6.2	$Sp_i$	Demand split on cross streets				
6.3	$C_i$	Capacity of approach				
7	$C_i$	Approach capacity $\sum_j C_{i,j}$ 5.2 for a four-way stop or 6.3 for a two-way stop				

AE capacity is based on 4.5 sec critical gap.



## EPA VOLUME 9 (REVISED) INDIRECT SOURCE GUIDELINE MODEL - WORKSHEET #2

INTERSECTION PURCHASE STREET AND INTERNATIONAL PLACE ACCESS DRIVE  
CASE # 1 YEAR 1984 AVERAGING TIME 1-HOUR

LINE 1	ROAD SEGMENT ID	PS
LINE 2	DEMAND VOLUME (VPH)	1902
LINE 4	CRUISE SPEED (MPH)	28
LINE 5	FREE-FLOW EMISSIONS (G/VEH/M)	0.0385 .0409
LINE 6.1	NUMBER OF LANES	3
LINE 6.3	CAPACITY SERVICE VOLUME (VPH OF GREEN)	0
LINE 6.4	DEMAND VOLUME (VPH)	0
LINE 6.5	SIGNAL CYCLE LENGTH (S)	0
LINE 6.6	GREEN PHASE LENGTH (S)	0
LINE 6.7	CAPACITY (VPH)	0
LINE 6.8	PROPORTION OF VEHICLES THAT STOP	0.0
LINE 6.9	NUMBER OF VEHICLES THAT STOP PER CYCLE	0.0
LINE 7.0	AVERAGE NUMBER OF VEHICLES IN QUEUE	0.0
LINE 8.0	LENGTH OF QUEUE (M/LANE)	0.0
LINE 9.0	AVERAGE EXCESS RUNNING TIME (S/VEH)	0.0
LINE 10.	EMISSIONS FROM ACCELERATION (G/VEH-M)	0.0
LINE 11.	EMISSIONS FROM DECELERATION (G/VEH-M)	0.0
LINE 12.	EMISSION RATE FOR ACC. AND DEC. (G/M-S)	0.0
LINE 13.	LENGTH OF ACC. AND DEC. (M)	0.0
LINE 14.	LENGTH FOR EXCESS EMISSIONS (M)	0.0
LINE 15	IDLING EMISSION RATE (G/S)	0.0
LINE 16.	AVERAGE EMISSION RATE (G/S-M)	0.0
LINE 17	ADJUSTED EXCESS EMISSION RATE (G/S-M)	0.0
LINE 18	FREE-FLOW EMISSION RATE (G/S-M)	0.0203 .0203

## EPA VOLUME 9 (REVISED) INDIRECT SOURCE GUIDELINE MODEL - WORKSHEET #2

INTERSECTION: PURCHASE STREET AND INTERNATIONAL PLACE ACCESS DRIVE  
CASE # 1 YEAR: 1984 AVERAGING TIME: 8-HOUR

LINE 1	ROAD SEGMENT ID	PS
LINE 2	DEMAND VOLUME (VPH)	1427.
LINE 4	CRUISE SPEED (MPH)	35
LINE 5	FREE-FLOW EMISSIONS (G-VEH/M)	0.0203 .0215
LINE 6.1	NUMBER OF LANES	3
LINE 6.3	CAPACITY SERVICE VOLUME (VPH OF GREEN)	0.
LINE 6.4	DEMAND VOLUME (VPH)	0.
LINE 6.5	SIGNAL CYCLE LENGTH (S)	0.
LINE 6.6	GREEN PHASE LENGTH (S)	0.
LINE 6.7	CAPACITY (VPH)	0.
LINE 6.8	PROPORTION OF VEHICLES THAT STOP	0.0
LINE 6.9	NUMBER OF VEHICLES THAT STOP PER CYCLE	0.0
LINE 7.0	AVERAGE NUMBER OF VEHICLES IN QUEUE	0.0
LINE 8.0	LENGTH OF QUEUE (M/LANE)	0.0
LINE 9.0	AVERAGE EXCESS RUNNING TIME (S/VEH)	0.0
LINE 10.0	EMISSIONS FROM ACCELERATION (G/VEH-M)	0.0
LINE 11.0	EMISSIONS FROM DECELERATION (G/VEH-M)	0.0
LINE 12.0	EMISSION RATE FOR ACC. AND DEC. (G/M-S)	0.0
LINE 13.0	LENGTH OF ACC. AND DEC. (M)	0.0
LINE 14.0	LENGTH FOR EXCESS EMISSIONS (M)	0.0
LINE 15.0	IDLING EMISSION RATE (G/S)	0.0
LINE 16.0	AVERAGE EMISSION RATE (G/S-M)	0.0
LINE 17.0	ADJUSTED EXCESS EMISSION RATE (G/S-M)	0.0
LINE 18.0	FREE-FLOW EMISSION RATE (G/S-M)	0.0080 .0085

## EPA VOLUME 9 (REVISED) INDIRECT SOURCE GUIDELINE MODEL - WORKSHEET #2

INTERSECTION: PURCHASE STREET AND INTERNATIONAL PLACE ACCESS DRIVE  
CASE # 2 YEAR: 1990 AVERAGING TIME: 1-HOUR

LINE 1	ROAD SEGMENT ID	PS
LINE 2	DEMAND VOLUME (VPH)	<del>2322</del> 3246
LINE 4	CRUISE SPEED (MPH)	28
LINE 5	FREE-FLOW EMISSIONS (G/VEH/M)	<del>0.0180</del> .0198
LINE 6 1	NUMBER OF LANES	3
LINE 6 3	CAPACITY SERVICE VOLUME (VPH OF GREEN)	0
LINE 6 4	DEMAND VOLUME (VPH)	0
LINE 6 5	SIGNAL CYCLE LENGTH (S)	0
LINE 6 6	GREEN PHASE LENGTH (S)	0
LINE 6 7	CAPACITY (VPH)	0
LINE 6 8	PROPORTION OF VEHICLES THAT STOP	0 0
LINE 6 9	NUMBER OF VEHICLES THAT STOP PER CYCLE	0 0
LINE 7 0	AVERAGE NUMBER OF VEHICLES IN QUEUE	0 0
LINE 8 0	LENGTH OF QUEUE (M/LANE)	0 0
LINE 9 0	AVERAGE EXCESS RUNNING TIME (S/VEH)	0 0
LINE 10	EMISSIONS FROM ACCELERATION (G/VEH-M)	0 0
LINE 11	EMISSIONS FROM DECELERATION (G/VEH-M)	0 0
LINE 12	EMISSION RATE FOR ACC AND DEC. (G/M-S)	0 0
LINE 13	LENGTH OF ACC. AND DEC. (M)	0 0
LINE 14	LENGTH FOR EXCESS EMISSIONS (M)	0 0
LINE 15	IDLING EMISSION RATE (G/S)	0 0
LINE 16	AVERAGE EMISSION RATE (G/S-M)	0 0
LINE 17	ADJUSTED EXCESS EMISSION RATE (G/S-M)	0 0
LINE 18	FREE-FLOW EMISSION RATE (G/S-M)	<del>0.0116</del> .0184

## EPA VOLUME 9 (REVISED) INDIRECT SOURCE GUIDELINE MODEL - WORKSHEET #2

INTERSECTION: PURCHASE STREET AND INTERNATIONAL PLACE ACCESS DRIVE  
CASE # 2 YEAR: 1990 AVERAGING TIME: 8-HOUR

LINE 1	ROAD SEGMENT ID	PS
LINE 2	DEMAND VOLUME (VPH)	1742.000
LINE 4	CRUISE SPEED (MPH)	35
LINE 5	FREE-FLOW EMISSIONS (G-VEH/M)	0.0100
LINE 6.1	NUMBER OF LANES	3
LINE 6.3	CAPACITY SERVICE VOLUME (VPH OF GREEN)	0.
LINE 6.4	DEMAND VOLUME (VPH)	0.
LINE 6.5	SIGNAL CYCLE LENGTH (S)	0.
LINE 6.6	GREEN PHASE LENGTH (S)	0.
LINE 6.7	CAPACITY (VPH)	0.
LINE 6.8	PROPORTION OF VEHICLES THAT STOP	0.0
LINE 6.9	NUMBER OF VEHICLES THAT STOP PER CYCLE	0.0
LINE 7.0	AVERAGE NUMBER OF VEHICLES IN QUEUE	0.0
LINE 8.0	LENGTH OF QUEUE (M/LANE)	0.0
LINE 9.0	AVERAGE EXCESS RUNNING TIME (S/VEH)	0.0
LINE 10.	EMISSIONS FROM ACCELERATION (G/VEH-M)	0.0
LINE 11.	EMISSIONS FROM DECELERATION (G/VEH-M)	0.0
LINE 12.	EMISSION RATE FOR ACC. AND DEC. (G/M-S)	0.0
LINE 13.	LENGTH OF ACC. AND DEC. (M)	0.0
LINE 14.	LENGTH FOR EXCESS EMISSIONS (M)	0.0
LINE 15.	IDLING EMISSION RATE (G/S)	0.0
LINE 16.	AVERAGE EMISSION RATE (G/S-M)	0.0
LINE 17.	ADJUSTED EXCESS EMISSION RATE (G/S-M)	0.0
LINE 18.	FREE-FLOW EMISSION RATE (G/S-M)	0.0048 0.0077

## EPA VOLUME 9 (REVISED) INDIRECT SOURCE GUIDELINE MODEL - WORKSHEET #2

INTERSECTION: PURCHASE STREET AND INTERNATIONAL PLACE DRIVE  
CASE # 3 YEAR: 1990 AVERAGING TIME: 1-HOUR

LINE	ROAD SEGMENT ID	PS	AE
LINE 2	DEMAND VOLUME (VPH)	3346	357
LINE 4	CRUISE SPEED (MPH)	28	5
LINE 5	FREE-FLOW EMISSIONS (G/VEH/M)	0.0198	0.0842
LINE 6.1	NUMBER OF LANES	3	1
LINE 6.3	CAPACITY SERVICE VOLUME (VPH OF GREEN)	0	0
LINE 6.4	DEMAND VOLUME (VPH)	0	0
LINE 6.5	SIGNAL CYCLE LENGTH (S)	0	0
LINE 6.6	GREEN PHASE LENGTH (S)	0	0
LINE 6.7	CAPACITY (VPH)	0	368
LINE 6.8	PROPORTION OF VEHICLES THAT STOP	0.0	0.0
LINE 6.9	NUMBER OF VEHICLES THAT STOP PER CYCLE	0.0	0.0
LINE 7.0	AVERAGE NUMBER OF VEHICLES IN QUEUE	0.0	32.45
LINE 8.0	LENGTH OF QUEUE (M/LANE)	0.0	141.18
LINE 9.0	AVERAGE EXCESS RUNNING TIME (S/VEH)	0.0	317.49
LINE 10.	EMISSIONS FROM ACCELERATION (G/VEH-M)	0.0	0.260
LINE 11.	EMISSIONS FROM DECELERATION (G/VEH-M)	0.0	0.195
LINE 12.	EMISSION RATE FOR ACC. AND DEC. (G/M-S)	0.0	0.045
LINE 13.	LENGTH OF ACC. AND DEC. (M)	0.0	2.2
LINE 14.	LENGTH FOR EXCESS EMISSIONS (M)	0.0	141.2
LINE 15	IDLING EMISSION RATE (G/S)	0.0	7.972
LINE 16	AVERAGE EMISSION RATE (G/S-M)	0.0	0.0572
LINE 17	ADJUSTED EXCESS EMISSION RATE (G/S-M)	0.0	0.0340
LINE 18.	FREE-FLOW EMISSION RATE (G/S-M)	0.0184	0.0083



## EPA VOLUME 9 (REVISED) INDIRECT SOURCE GUIDELINE MODEL - WORKSHEET #2

INTERSECTION: PURCHASE STREET AND INTERNATIONAL PLACE ACCESS DRIVE  
CASE # 3 YEAR: 1990 AVERAGING TIME: 8-HOUR

LINE	ROAD SEGMENT ID	PS	AE
LINE 2	DEMAND VOLUME (VPH)	2510	110
LINE 4	CRUISE SPEED (MPH)	35	5
LINE 5	FREE-FLOW EMISSIONS (G-VEH/M)	0 0111	0 0605
LINE 6.1	NUMBER OF LANES	3	1
LINE 6.3	CAPACITY SERVICE VOLUME (VPH OF GREEN)	0	0
LINE 6.4	DEMAND VOLUME (VPH)	0	0
LINE 6.5	SIGNAL CYCLE LENGTH (S)	0	
LINE 6.6	GREEN PHASE LENGTH (S)	0	0
LINE 6.7	CAPACITY (VPH)	0	453
LINE 6.8	PROPORTION OF VEHICLES THAT STOP	0 0	0 0
LINE 6.9	NUMBER OF VEHICLES THAT STOP PER CYCLE	0 0	0 0
LINE 7.0	AVERAGE NUMBER OF VEHICLES IN QUEUE	0 0	0.32
LINE 8.6	LENGTH OF QUEUE (M/LANE)	0 0	1.40
LINE 9.0	AVERAGE EXCESS RUNNING TIME (S/VEH)	0.0	2.55
LINE 10.	EMISSIONS FROM ACCELERATION (G/VEH-M)	0.0	0.260
LINE 11.	EMISSIONS FROM DECELERATION (G/VEH-M)	0.0	0.195
LINE 12.	EMISSION RATE FOR ACC AND DEC. (G/M-S)	0 0	0 014
LINE 13.	LENGTH OF ACC AND DEC. (M)	0 0	2.2
LINE 14.	LENGTH FOR EXCESS EMISSIONS (M)	0 0	40 0
LINE 15.	IDLING EMISSION RATE (G/S)	0.0	0 012
LINE 16	AVERAGE EMISSION RATE (G/S-M)	6 0	0 0011
LINE 17.	ADJUSTED EXCESS EMISSION RATE (G/S-M)	0 0	-0 0013
LINE 18.	FREE-FLOW EMISSION RATE (G/S-M)	0 0077	0 0018

WORKSHEET 5 - INTERSECTION CO DISPERSION ANALYSIS

Intersection Purchase St. and I.P. Access Drive  
 Case # 1 Year 1984 Averaging Time 1 Hour

Line No. Symbol	Input/Units	PS	Traffic Stream
1 SC	Stability Class	D	
2 U	Wind Speed ( $m s^{-1}$ )	1.0	
3 $\theta$	Wind-Road Angle (deg)	4	
4 x	Lateral Distance (m)	12	
5 Yu	Maximum Longitudinal Distance (m)	N/A	
6 Yd	Minimum Longitudinal Distance (m)	N/A	
7 $\sigma_{z0}$	Initial Dispersion (m)	5	
8 Qe	Excess Emissions Rate ( $gm^{-1}s^{-1}$ )	0	
9 Qf	Free Flow Emissions Rate ( $gm^{-1}s^{-1}$ )	.0216	
9a	Street Canyon? Yes or No	No	
DISPERSION ANALYSIS			
10 $xUQ^{-1}$	Normalized Concentration ( $10^{-3}m^{-1}$ ) Free Flow	800	
Qf	Enter Line 9	x	x
11 XU	Normalized Concentration ( $mg m^{-2}s^{-1}$ )		
U	Enter Line 2	+	+
12 x	CO Concentration ( $mg m^{-3}$ ) Through Emissions	17.3	
13 $xUQ^{-1}$	Normalized Concentration (For Yu)	N/A	
Qe	Enter Line 8		
14 XU	Normalized Concentration ( $mg m^{-2}s^{-1}$ )		
U	Enter Line 2		
15 x	CO Concentration-"Maximum Queue"		
16 $xUQ^{-1}$	Normalized Concentration (For Yd)	N/A	
Qe	Enter Line 8	x	x
17 XU	Normalized Concentration ( $mg m^{-2}s^{-1}$ )		
U	Enter Line 2		
18 x	CO Concentration-"Imaginary Queue"	+	+
19 x	CO ( $mg m^{-3}$ ) Total	17.3	
20 x	CO Concentration (ppm)-- Total	15.1	
OPTIONAL z-CORRECTION (Heights Other than 1.8m Above the Ground)			
21 z	Height of Receptor (m)		
22	z-Correction Factor		
23 $x'$	CO Concentration at Height z ( $mg m^{-3}$ )		
24 $x''$	CO Concentration at Height z (ppm)		

15.1 ppm

WORKSHEET 5 - INTERSECTION CO DISPERSION ANALYSIS

Intersection Purchase St. and I.P. Access Drive  
 Case # 1 Year 1984 Averaging Time 8 Hour

Line No. Symbol	Input/Units	Traffic Stream
		<u>DS</u>
1 SC	Stability Class	<u>D</u>
2 U	Wind Speed ( $m s^{-1}$ )	<u>1.6</u>
3 $\theta$	Wind-Road Angle (deg)	<u>4</u>
4 x	Lateral Distance (m)	<u>12</u>
5 Yu	Maximum Longitudinal Distance (m)	<u>N/A</u>
6 Yd	Minimum Longitudinal Distance (m)	<u>N/A</u>
7 $\sigma_{z0}$	Initial Dispersion (m)	<u>5</u>
8 Qe	Excess Emissions Rate ( $gm^{-1}s^{-1}$ )	<u>0</u>
9 Qf	Free Flow Emissions Rate ( $gm^{-1}s^{-1}$ )	<u>.0085</u>
9a	Street Canyon? Yes or No	<u>No</u>
DISPERSION ANALYSIS		
10 $xuQ^{-1}$	Normalized Concentration ( $10^{-3}m^{-1}$ ) Free Flow	<u>800</u>
Qf	Enter Line 9	x _____ x _____ x _____ x _____
11 xu	Normalized Concentration ( $mg m^{-2}s^{-1}$ )	
U	Enter Line 2	+ <u>1.6</u> + _____ + _____ + _____
12 x	CO Concentration ( $mg m^{-3}$ ) Through Emissions	<u>4.3</u>
13 $xuQ^{-1}$	Normalized Concentration (For Yu)	<u>N/A</u>
Qe	Enter Line 8	
14 xu	Normalized Concentration ( $mg m^{-2}s^{-1}$ )	
U	Enter Line 2	
15 x	CO Concentration--"Maximum Queue"	
16 $xuQ^{-1}$	Normalized Concentration (For Yd)	<u>N/A</u>
Qe	Enter Line 8	x _____ x _____ x _____ x _____
17 xu	Normalized Concentration ( $mg m^{-2}s^{-1}$ )	
U	Enter Line 2	
18 x	CO Concentration--"Imaginary Queue"	+ _____ + _____ + _____ + _____
19 x	CO ( $mg m^{-3}$ ) Total	<u>4.3</u>
20 x	CO Concentration (ppm)-- Total	<u>3.7</u>
OPTIONAL z-CORRECTION (Heights Other than 1.8m Above the Ground)		
21 z	Height of Receptor (m)	_____
22	z-Correction Factor	_____
23 $x^z$	CO Concentration at Height z ( $mg m^{-3}$ )	_____
24 $x^z$	CO Concentration at Height z (ppm)	_____

3.7ppm

WORKSHEET 5 - INTERSECTION CO DISPERSION ANALYSIS

Intersection Purchase St. and I. P. Access Drive  
 Case # 2 Year 1990 Averaging Time 1 Hour

Line No. Symbol	Input/Units	PS	Traffic Stream			
1 SC	Stability Class	D				
2 U	Wind Speed ( $m s^{-1}$ )	1.0				
3 $\theta$	Wind-Road Angle (deg)	4				
4 x	Lateral Distance (m)	12				
5 Yu	Maximum Longitudinal Distance (m)	N/A				
6 Yd	Minimum Longitudinal Distance (m)	N/A				
7 $\sigma_{zo}$	Initial Dispersion (m)	5				
8 Qe	Excess Emissions Rate ( $gm^{-1}s^{-1}$ )	0				
9 Qf	Free Flow Emissions Rate ( $gm^{-1}s^{-1}$ )	.0184				
9a	Street Canyon? Yes or No	NO				
DISPERSION ANALYSIS						
10 $xUQ^{-1}$	Normalized Concentration ( $10^{-3}m^{-1}$ ) Free Flow	8.00				
Qf	Enter Line 9	x	x	x	x	
11 XU	Normalized Concentration ( $mg m^{-2}s^{-1}$ )					
U	Enter Line 2	+	+	+	+	
12 X	CO Concentration ( $mg m^{-3}$ ) Through Emissions	14.7				
13 $xUQ^{-1}$	Normalized Concentration (For Yu)	N/A				
Qe	Enter Line 8					
14 XU	Normalized Concentration ( $mg m^{-2}s^{-1}$ )					
U	Enter Line 2					
15 X	CO Concentration-"Maximum Queue"					
16 $xUQ^{-1}$	Normalized Concentration (For Yd)	N/A				
Qe	Enter Line 8	x	x	x	x	
17 XU	Normalized Concentration ( $mg m^{-2}s^{-1}$ )					
U	Enter Line 2					
18 X	CO Concentration-"Imaginary Queue"	+	+	+	+	
19 X	CO ( $mg m^{-3}$ ) Total	14.7				
20 X	CO Concentration (ppm)-- Total	12.8				
OPTIONAL z-CORRECTION (Heights Other than 1.8m Above the Ground)						
21 z	Height of Receptor (m)					
22	z-Correction Factor					
23 $x'$	CO Concentration at Height z ( $mg m^{-3}$ )					
24 $x'$	CO Concentration at Height z (ppm)					

12.8 ppm

WORKSHEET 5 - INTERSECTION CO DISPERSION ANALYSIS

Intersection Purchase St. and I.P. Access Drive  
 Case # 2 Year 1990 Averaging Time 8 Hour

Line No. Symbol	Input/Units	Traffic Stream
1 SC	Stability Class	PS
2 U	Wind Speed ( $m s^{-1}$ )	D
3 $\theta$	Wind-Road Angle (deg)	1.6
4 x	Lateral Distance (m)	4
5 Yu	Maximum Longitudinal Distance (m)	12
6 Yd	Minimum Longitudinal Distance (m)	N/A
7 $\sigma_{z0}$	Initial Dispersion (m)	N/A
8 Qe	Excess Emissions Rate ( $gm^{-1}s^{-1}$ )	5
9 Qf	Free Flow Emissions Rate ( $gm^{-1}s^{-1}$ )	0
9a	Street Canyon? Yes or No	.0077
		No
DISPERSION ANALYSIS		
10 $xUQ^{-1}$	Normalized Concentration ( $10^{-3}m^{-1}$ ) Free Flow	800
Qf	Enter Line 9	x x x x
11 XU	Normalized Concentration ( $mg m^{-2}s^{-1}$ )	
U	Enter Line 2	÷ 1.6 ÷ ÷ ÷
12 X	CO Concentration ( $mg m^{-3}$ ) Through Emissions	3.9
13 $xUQ^{-1}$	Normalized Concentration (For Yu)	N/A
Qe	Enter Line 8	
14 XU	Normalized Concentration ( $mg m^{-2}s^{-1}$ )	
U	Enter Line 2	
15 X	CO Concentration-"Maximum Queue"	
16 $xUQ^{-1}$	Normalized Concentration (For Yd)	N/A
Qe	Enter Line 8	x x x x
17 XU	Normalized Concentration ( $mg m^{-2}s^{-1}$ )	
U	Enter Line 2	
18 X	CO Concentration-"Imaginary Queue"	÷ ÷ ÷ ÷
19 X	CO ( $mg m^{-3}$ ) Total	3.9
20 X	CO Concentration (ppm)-- Total	3.4
OPTIONAL z-CORRECTION (Heights Other than 1.8m Above the Ground)		
21 z	Height of Receptor (m)	
22	z-Correction Factor	
23 $x^-$	CO Concentration at Height z ( $mg m^{-3}$ )	
24 $x^-$	CO Concentration at Height z (ppm)	

3.4ppm



WORKSHEET 5 - INTERSECTION CO DISPERSION ANALYSIS

Intersection Purchase St. and I.P. Access Drive  
 Case # 3 Year 1990 Averaging Time 1 Hour

Line No. Symbol	Input/Units	PS	AE
1 SC	Stability Class	D	
2 U	Wind Speed ( $m s^{-1}$ )	1.0	
3 $\theta$	Wind-Road Angle (deg)	81	9
4 x	Lateral Distance (m)	12	10
5 Yu	Maximum Longitudinal Distance (m)	N/A	161
6 Yd	Minimum Longitudinal Distance (m)	N/A	20
7 $\sigma_{z0}$	Initial Dispersion (m)	5	
8 Qe	Excess Emissions Rate ( $gm^{-1}s^{-1}$ )	0	.0340
9 Qf	Free Flow Emissions Rate ( $gm^{-1}s^{-1}$ )	.0184	.0083
9a	Street Canyon? Yes or No	No	
DISPERSION ANALYSIS			
10 XUQ <sup>-1</sup>	Normalized Concentration ( $10^{-3}m^{-1}$ ) Free Flow	160	650
Qf	Enter Line 9	x	x
11 XU	Normalized Concentration ( $mg m^{-2}s^{-1}$ )		
U	Enter Line 2	÷	÷
12 x	CO Concentration ( $mg m^{-3}$ ) Through Emissions	2.9	5.4
13 XUQ <sup>-1</sup>	Normalized Concentration (For Yu)	N/A	490
Qe	Enter Line 8		
14 XU	Normalized Concentration ( $mg m^{-2}s^{-1}$ )		
U	Enter Line 2		
15 x	CO Concentration-"Maximum Queue"		16.7
16 XUQ <sup>-1</sup>	Normalized Concentration (For Yd)	N/A	0
Qe	Enter Line 8	x	x
17 XU	Normalized Concentration ( $mg m^{-2}s^{-1}$ )		
U	Enter Line 2		
18 x	CO Concentration-"Imaginary Queue"	÷	0
19 x	CO ( $mg m^{-3}$ ) Total	2.9	22.1
20 x	CO Concentration (ppm)-- Total	2.5	19.2
OPTIONAL z-CORRECTION (Heights Other than 1.8m Above the Ground)			
21 z	Height of Receptor (m)		
22	z-Correction Factor		
23 x'	CO Concentration at Height z ( $mg m^{-3}$ )		
24 x'	CO Concentration at Height z (ppm)		

21.7ppm

WORKSHEET 1 - TRAFFIC INFORMATION

Intersection Oliver And Purchase Streets  
 Case # 1 Year 1984

1. Road segment or intersection approach identification	PS	OS
2. Observed 1-hr volume (vph)	1179	130
Observed 8-hr volume (vph)	884	77
Projected 1-hr peak demand (vph)		
Projected 8-hr peak demand (vph)		
3. Percentage cold starts	50/20.6	
4. Percentage trucks and buses	5.8	
5. Metropolitan population		
6. Slope		
7. Free-flow parameters		
Number of lanes	3	1
Average lane width (ft)	12	20
Design speed (mph) (1Hr/8Hr)	28/35	28/30
Highway type (see Figures 2-5)	Urban Artery	
8. Intersection parameters		
Intersection designation		
Approach width (ft)	36	20
Percentage right turns	2	100
Percentage left turns	0	0
Type control and description of signal controller	STOP SIGN	
9. Area source parameters		
Parking lot gate designation		
Projected 1-hr peak entrance demand (vph)		
Projected 1-hr peak exit demand (vph)		
Projected 8-hr peak entrance demand (vph)		
Projected 8-hr peak exit demand (vph)		
Parking lot area (m <sup>2</sup> )		
Parking lot capacity (veh)		
Running time required to access auxiliary parking (s)		
Facility emptying time		
Average cars per stall		
Average area per stall (m <sup>2</sup> )		

WORKSHEET 5 - INTERSECTION CO DISPERSION ANALYSIS

Intersection Purchase St. and I.P. Access Drive  
 Case # 3 Year 1990 Averaging Time 8 Hour

Line No. Symbol	Input/Units	DS	AE	Traffic Stream
1 SC	Stability Class	D		
2 U	Wind Speed ( $m s^{-1}$ )	1.6		
3 $\theta$	Wind-Road Angle (deg)	4	86	
4 x	Lateral Distance (m)	12	10	
5 Yu	Maximum Longitudinal Distance (m)	N/A	60	
6 Yd	Minimum Longitudinal Distance (m)	N/A	20	
7 $\sigma_{z0}$	Initial Dispersion (m)	5		
8 Qe	Excess Emissions Rate ( $gm^{-1}s^{-1}$ )	0	-0.0013	
9 Qf	Free Flow Emissions Rate ( $gm^{-1}s^{-1}$ )	0.0077	0.0018	
9a	Street Canyon? Yes or No	No		
DISPERSION ANALYSIS				
10 $xUQ^{-1}$	Normalized Concentration ( $10^{-3}m^{-1}$ ) Free Flow	800	160	
Qf	Enter Line 9	x	x	x
11 XU	Normalized Concentration ( $mg m^{-2}s^{-1}$ )			
U	Enter Line 2	+ 1.6	+	+
12 X	CO Concentration ( $mg m^{-3}$ ) Through Emissions	3.9	0.2	
13 $xUQ^{-1}$	Normalized Concentration (For Yu)	N/A	150	
Qe	Enter Line 8			
14 XU	Normalized Concentration ( $mg m^{-2}s^{-1}$ )			
U	Enter Line 2	1.6		
15 X	CO Concentration--"Maximum Queue"		-0.12	
16 $xUQ^{-1}$	Normalized Concentration (For Yd)	N/A	60	
Qe	Enter Line 8	x	x	x
17 XU	Normalized Concentration ( $mg m^{-2}s^{-1}$ )			
U	Enter Line 2	1.6		
18 X	CO Concentration--"Imaginary Queue"	+	-0.05	+
19 X	CO ( $mg m^{-3}$ ) Total	3.9	0.1	
20 X	CO Concentration (ppm)-- Total	3.4	0.1	
OPTIONAL z-CORRECTION (Heights Other than 1.8m Above the Ground)				
21 z	Height of Receptor (m)			
22	z-Correction Factor			
23 $x^z$	CO Concentration at Height z ( $mg m^{-3}$ )			
24 $x^z$	CO Concentration at Height z (ppm)			

3.5 ppm

WORKSHEET 1 - TRAFFIC INFORMATION

Intersection Oliver And Purchase Streets  
 Case # 2 Year 1990

1. Road segment or intersection approach identification	<u>PS</u>	<u>OS</u>
2. Observed 1-hr volume (vph)	_____	_____
Observed 8-hr volume (vph)	_____	_____
Projected 1-hr peak demand (vph)	<u>2468</u>	<u>20</u>
Projected 8-hr peak demand (vph)	<u>1851</u>	<u>12</u>
3. Percentage cold starts	<u>50/20.6</u>	_____
4. Percentage trucks and buses	<u>58</u>	_____
5. Metropolitan population	_____	_____
6. Slope	_____	_____
7. Free-flow parameters	_____	_____
Number of lanes	<u>3</u>	<u>2</u>
Average lane width (ft)	<u>12</u>	<u>19</u>
Design speed (mph)	<u>28/35</u>	<u>28/30</u>
Highway type (see Figures 2-5)	<u>Urban Artery</u>	_____
8. Intersection parameters	_____	_____
Intersection designation	_____	_____
Approach width (ft)	<u>36</u>	<u>38</u>
Percentage right turns	<u>0</u>	<u>100</u>
Percentage left turns	<u>0</u>	<u>0</u>
Type control and description of signal controller	_____	_____
9. Area source parameters	_____	_____
Parking lot gate designation	_____	_____
Projected 1-hr peak entrance demand (vph)	_____	_____
Projected 1-hr peak exit demand (vph)	_____	_____
Projected 8-hr peak entrance demand (vph)	_____	_____
Projected 8-hr peak exit demand (vph)	_____	_____
Parking lot area (m <sup>2</sup> )	_____	_____
Parking lot capacity (veh)	_____	_____
Running time required to access auxiliary parking (s)	_____	_____
Facility emptying time	_____	_____
Average cars per stall	_____	_____
Average area per stall (m <sup>2</sup> )	_____	_____

WORKSHEET 1 - TRAFFIC INFORMATION

Intersection Oliver And Purchase Streets  
 Case # 3 Year 1990

1. Road segment or intersection approach identification	<u>PS</u>	<u>OS</u>
2. Observed 1-hr volume (vph)	---	---
Observed 8-hr volume (vph)	---	---
Projected 1-hr peak demand (vph)	<u>2628</u>	<u>50</u>
Projected 8-hr peak demand (vph)	<u>1971</u>	<u>30</u>
3. Percentage cold starts	<u>50/20.6</u>	---
4. Percentage trucks and buses	<u>5.8</u>	---
5. Metropolitan population	---	---
6. Slope	---	---
7. Free-flow parameters		
Number of lanes	<u>3</u>	<u>2</u>
Average lane width (ft)	<u>12</u>	<u>19</u>
Design speed (mph) (1Hr/8Hr)	<u>28/35</u>	<u>28/30</u>
Highway type (see Figures 2-5)	<u>Urban Artery</u>	
8. Intersection parameters		
Intersection designation	---	---
Approach width (ft)	<u>36</u>	<u>38</u>
Percentage right turns	<u>0</u>	<u>100</u>
Percentage left turns	<u>0</u>	<u>0</u>
Type control and description of signal controller	---	---
9. Area source parameters		
Parking lot gate designation	---	---
Projected 1-hr peak entrance demand (vph)	---	---
Projected 1-hr peak exit demand (vph)	---	---
Projected 8-hr peak entrance demand (vph)	---	---
Projected 8-hr peak exit demand (vph)	---	---
Parking lot area (m <sup>2</sup> )	---	---
Parking lot capacity (veh)	---	---
Running time required to access auxiliary parking (s)	---	---
Facility emptying time	---	---
Average cars per stall	---	---
Average area per stall (m <sup>2</sup> )	---	---



WORKSHEET B - CAPACITY ANALYSIS

Intersection

Oliver And Purchase Streets

Case # 1

Year 1984

Step	Symbol	Input/Units	PS	OS
1	$i$	Road segment (or approach) designation	<u>PS</u>	<u>OS</u>
2		Free flow capacity computation:		
2.1	$M_i$	Number of lanes	<u>3</u>	<u>1</u>
2.2	$W_p$	Adjustment for lane width (Table B-1)		
2.3	$T_i$	Adjustment for trucks (Table B-2)		
2.4	$C_i$	Free flow capacity		
3		Signalized intersection capacity:		
3.1	$j$	Green signal phase identification		
3.2	$wa_i$	Approach width with parking (ft)		
3.3		Percent right turners		
3.4		Percent left turners		
3.5		Metropolitan area size		
3.6	$Cs_{i,j}$	Capacity service volume (vph or green)		
4		Signalized intersection green phase and cycle length:		
4.1	$V_{i,j}$	Demand Volume for approach and phase		
4.2	$V_{i,j}/Cs_{i,j}$	Volume to green capacity ratio		
4.3	approx G/Cy	Approximate G/Cy		
4.4	$\sum_j \max(V_{i,j}/Cs_{i,j})$	Sum of the maximum V/C ratios for each signal phase		
4.5	$Cy$	Signal cycle time (sec)		
4.6	$G_j$	Green phase length		
4.7	$G_j/Cy$	Green phase to cycle time ratio		
4.8	$C_{i,j}$	Capacity for approach i phase j		
5		Two-way stop, two-way yield or uncontrolled intersection:		
5.1	$V_m + V_n$	Major street two-way volume (1Hr/8Hr)	<u>1179/884</u>	
5.2	$C_i$	Cross street capacity		<u>541/599</u>
6		Four-way stop intersections:		
6.1	$V_i$	Approach volume		
6.2	$Sp_i$	Demand split on cross streets		
6.3	$C_i$	Capacity of approach		
7	$C_i$	Approach capacity $\begin{cases} C_{i,j} \\ 5.2 \text{ for a four-way stop or} \\ 6.3 \text{ for a two-way stop} \end{cases}$		

WORKSHEET B - CAPACITY ANALYSIS

Intersection Oliver And Purchase Streets

Case # 2 Year 1990

Step	Symbol	Input/Units	PS	OS
1	$i$	Road segment (or approach) designation	<u>PS</u>	<u>OS</u>
2		<u>Free flow capacity computation:</u>		
2.1	$M_i$	Number of lanes	<u>3</u>	<u>2</u>
2.2	$W_f$	Adjustment for lane width (Table B-1)		
2.3	$T_i$	Adjustment for trucks (Table B-2)		
2.4	$C_i$	Free flow capacity		
3		<u>Signalized intersection capacity:</u>		
3.1	$j$	Green signal phase identification		
3.2	$W_{a_i}$	Approach width with parking (ft)		
3.3		Percent right turners		
3.4		Percent left turners		
3.5		Metropolitan area size		
3.6	$C_{s_{i,j}}$	Capacity service volume (vph or green)		
4		<u>Signalized intersection green phase and cycle length:</u>		
4.1	$V_{i,j}$	Demand Volume for approach and phase		
4.2	$V_{i,j}/C_{s_{i,j}}$	Volume to green capacity ratio		
4.3	approx G/Cy	Approximate G/Cy		
4.4	$\sum_j \max(V_{i,j}, C_{s_{i,j}})$	Sum of the maximum V/C ratios for each signal phase		
4.5	$C_y$	Signal cycle time (sec)		
4.6	$G_j$	Green phase length		
4.7	$G_j/C_y$	Green phase to cycle time ratio		
4.8	$C_{i,j}$	Capacity for approach i phase j		
5		<u>Two-way stop, two-way yield or uncontrolled intersection:</u>		
5.1	$V_m + V_n$	Major street two-way volume	<u>2468/1851</u>	
5.2	$C_i$	Cross street capacity		<u>336/425</u>
6		<u>Four-way stop intersections:</u>		
6.1	$V_i$	Approach volume		
6.2	$S_{pi}$	Demand split on cross streets		
6.3	$C_i$	Capacity of approach		
7	$C_i$	Approach capacity $\sum_j C_{i,j}$		
		5.2 for a four-way stop or		
		6.3 for a two-way stop		

WORKSHEET B - CAPACITY ANALYSIS

Intersection Oliver And Purchase Streets  
 Case # 3 Year 1990

Step	Symbol	Input/Units		
1	i	Road segment (or approach) designation	<u>PS</u>	<u>OS</u>
2		<u>Free flow capacity computation:</u>		
2.1	$M_i$	Number of lanes	<u>3</u>	<u>2</u>
2.2	$W_p$	Adjustment for lane width (Table B-1)		
2.3	$T_i$	Adjustment for trucks (Table B-2)		
2.4	$C_i$	Free flow capacity		
3		<u>Signalized intersection capacity:</u>		
3.1	j	Green signal phase identification		
3.2	$W_{a_i}$	Approach width with parking (ft)		
3.3		Percent right turners		
3.4		Percent left turners		
3.5		Metropolitan area size		
3.6	$C_{s_{i,j}}$	Capacity service volume (vph or green)		
4		<u>Signalized intersection green phase and cycle length:</u>		
4.1	$V_{i,j}$	Demand Volume for approach and phase		
4.2	$V_{i,j}/C_{s_{i,j}}$	Volume to green capacity ratio		
4.3	approx G/Cy	Approximate G/Cy		
4.4	$\sum_j \max(V_{i,j}/C_{s_{i,j}})$	Sum of the maximum V/C ratios for each signal phase		
4.5	Cy	Signal cycle time (sec)		
4.6	Gj	Green phase length		
4.7	Gj/Cy	Green phase to cycle time ratio		
4.8	$C_{i,j}$	Capacity for approach i phase j		
5		<u>Two-way stop, two-way yield or uncontrolled intersection:</u>		
5.1	$V_m + V_n$	Major street two-way volume (1Hr/8Hr)	<u>2628/1971</u>	
5.2	$C_i$	Cross street capacity		<u>315/406</u>
6		<u>Four-way stop intersections:</u>		
6.1	$V_i$	Approach volume		
6.2	Sp1	Demand split on cross streets		
6.3	$C_i$	Capacity of approach		
7	$C_i$	Approach capacity $\sum_j C_{i,j}$ 5.2 for a four-way stop or 6.3 for a two-way stop		

## EPA VOLUME 9 (REVISED) INDIRECT SOURCE GUIDELINE MODEL - WORKSHEET #2

INTERSECTION: OLIVER STREET & PURCHASE STREET  
CASE # 1 YEAR: 1984 AVERAGING TIME: 1-HOUR

LINE		PS	QS
LINE 1	ROAD SEGMENT ID		
LINE 2	DEMAND VOLUME (VPH)	1179	130
LINE 4	CRUISE SPEED (MPH)	28	28
LINE 5	FREE-FLOW EMISSIONS (G-VEH/M)	0.0409	0.0409
LINE 6 1	NUMBER OF LANES	3	1
LINE 6 3	CAPACITY SERVICE VOLUME (VPH OF GREEN)	0	0
LINE 6 4	DEMAND VOLUME (VPH)	0	0
LINE 6 5	SIGNAL CYCLE LENGTH (S)	0	
LINE 6 6	GREEN PHASE LENGTH (S)	0	0
LINE 6 7	CAPACITY (VPH)	0	541
LINE 6 8	PROPORTION OF VEHICLES THAT STOP	0.0	0.0
LINE 6 9	NUMBER OF VEHICLES THAT STOP PER CYCLE	0.0	0.0
LINE 7 0	AVERAGE NUMBER OF VEHICLES IN QUEUE	0.0	0.32
LINE 8 0	LENGTH OF QUEUE (M/LANE)	0.0	1.38
LINE 9 0	AVERAGE EXCESS RUNNING TIME (S/VEH)	0.0	2.10
LINE 10	EMISSIONS FROM ACCELERATION (G/VEH-M)	0.0	0.103
LINE 11	EMISSIONS FROM DECELERATION (G/VEH-M)	0.0	0.034
LINE 12	EMISSION RATE FOR ACC. AND DEC. (G/M-S)	0.0	0.005
LINE 13	LENGTH OF ACC. AND DEC. (M)	0.0	70.1
LINE 14	LENGTH FOR EXCESS EMISSIONS (M)	0.0	140.2
LINE 15	IDLING EMISSION RATE (G/S)	0.0	-0.032
LINE 16	AVERAGE EMISSION RATE (G/S-M)	0.0	0.0022
LINE 17	ADJUSTED EXCESS EMISSION RATE (G/S-M)	0.0	0.0023
LINE 18	FREE-FLOW EMISSION RATE (G/S-M)	0.0134	0.0015

## EPA VOLUME 9 (REVISED) INDIRECT SOURCE GUIDELINE MODEL - WORKSHEET #2

INTERSECTION: OLIVER STREET & PURCHASE STREET  
CASE # 1 YEAR 1984 AVERAGING TIME 8-HOUR

LINE		PS	OS
LINE 1	ROAD SEGMENT ID		
LINE 2	DEMAND VOLUME (VPH)	884	77
LINE 4	CRUISE SPEED (MPH)	35	30
LINE 5	FREE-FLOW EMISSIONS (G-VEH/M)	0.0215	0.0256
LINE 6.1	NUMBER OF LANES	3	1
LINE 6.3	CAPACITY SERVICE VOLUME (VPH OF GREEN)	0.	0.
LINE 6.4	DEMAND VOLUME (VPH)	0	0
LINE 6.5	SIGNAL CYCLE LENGTH (S)	0.	
LINE 6.6	GREEN PHASE LENGTH (S)	0	0
LINE 6.7	CAPACITY (VPH)	0	599
LINE 6.8	PROPORTION OF VEHICLES THAT STOP	0.0	0.0
LINE 6.9	NUMBER OF VEHICLES THAT STOP PER CYCLE	0.0	0.0
LINE 7.0	AVERAGE NUMBER OF VEHICLES IN QUEUE	0.0	0.15
LINE 8.0	LENGTH OF QUEUE (M/LANE)	0.0	0.64
LINE 9.0	AVERAGE EXCESS RUNNING TIME (S/VEH)	0.0	0.89
LINE 10.	EMISSIONS FROM ACCELERATION (G/VEH-M)	0.0	0.100
LINE 11.	EMISSIONS FROM DECELERATION (G/VEH-M)	0.0	0.031
LINE 12.	EMISSION RATE FOR ACC. AND DEC. (G/M-S)	0.0	0.003
LINE 13.	LENGTH OF ACC. AND DEC. (M)	0.0	80.5
LINE 14.	LENGTH FOR EXCESS EMISSIONS (M)	0.0	160.9
LINE 15.	IDLING EMISSION RATE (G/S)	0.0	-0.028
LINE 16.	AVERAGE EMISSION RATE (G/S-M)	0.0	0.0012
LINE 17	ADJUSTED EXCESS EMISSION RATE (G/S-M)	0.0	0.0008
LINE 18.	FREE-FLOW EMISSION RATE (G/S-M)	0.0053	0.0005



## EPA VOLUME 9 (REVISED) INDIRECT SOURCE GUIDELINE MODEL - WORKSHEET #2

INTERSECTION: OLIVER STREET & PURCHASE STREET  
 CASE # 2 YEAR: 1990 AVERAGING TIME: 1-HOUR

LINE	ROAD SEGMENT ID	PS	OS
LINE 2	DEMAND VOLUME (VPH)	2468	20.
LINE 4	CRUISE SPEED (MPH)	28	28
LINE 5	FREE-FLOW EMISSIONS (G-VEH/M)	0.0198	0.0198
LINE 6.1	NUMBER OF LANES	3	2
LINE 6.3	CAPACITY SERVICE VOLUME (VPH OF GREEN)	0.	0
LINE 6.4	DEMAND VOLUME (VPH)	0.	0.
LINE 6.5	SIGNAL CYCLE LENGTH (S)	0	
LINE 6.6	GREEN PHASE LENGTH (S)	0.	0.
LINE 6.7	CAPACITY (VPH)	0	336
LINE 6.8	PROPORTION OF VEHICLES THAT STOP	0 0	0.0
LINE 6.9	NUMBER OF VEHICLES THAT STOP PER CYCLE	0.0	0.0
LINE 7.0	AVERAGE NUMBER OF VEHICLES IN QUEUE	0 0	0 06
LINE 8.0	LENGTH OF QUEUE (M/LANE)	0 0	0 14
LINE 9.0	AVERAGE EXCESS RUNNING TIME (S/VEH)	0 0	0 68
LINE 10.	EMISSIONS FROM ACCELERATION (G/VEH-M)	0.0	0 103
LINE 11.	EMISSIONS FROM DECELERATION (G/VEH-M)	0 0	0 034
LINE 12.	EMISSION RATE FOR ACC. AND DEC. (G/M-S)	0 0	0 001
LINE 13.	LENGTH OF ACC AND DEC. (M)	0.0	70 1
LINE 14.	LENGTH FOR EXCESS EMISSIONS (M)	0 0	140 2
LINE 15.	IDLING EMISSION RATE (G/S)	0.0	-0 007
LINE 16.	AVERAGE EMISSION RATE (G/S-M)	0 0	0 0003
LINE 17.	ADJUSTED EXCESS EMISSION RATE (G/S-M)	0 0	0 0001
LINE 18.	FREE-FLOW EMISSION RATE (G/S-M)	0.0136	0 0001

## EPA VOLUME 9 (REVISED) INDIRECT SOURCE GUIDELINE MODEL - WORKSHEET #2

INTERSECTION OLIVER STREET & PURCHASE STREET  
CASE # 2 YEAR 1990 AVERAGING TIME 8-HOUR

LINE	ROAD SEGMENT ID	PS	DS
LINE 2	DEMAND VOLUME (VPH)	1851	12
LINE 4	CRUISE SPEED (MPH)	35	30
LINE 5	FREE-FLOW EMISSIONS (G-VEH/M)	0.0111	0.0132
LINE 6.1	NUMBER OF LANES	3	2
LINE 6.3	CAPACITY SERVICE VOLUME (VPH OF GREEN)	0	0
LINE 6.4	DEMAND VOLUME (VPH)	0	0
LINE 6.5	SIGNAL CYCLE LENGTH (S)	0	0
LINE 6.6	GREEN PHASE LENGTH (S)	0	0
LINE 6.7	CAPACITY (VPH)	0	425
LINE 6.8	PROPORTION OF VEHICLES THAT STOP	0.0	0.0
LINE 6.9	NUMBER OF VEHICLES THAT STOP PER CYCLE	0.0	0.0
LINE 7.0	AVERAGE NUMBER OF VEHICLES IN QUEUE	0.0	0.03
LINE 8.0	LENGTH OF QUEUE (M/LANE)	0.0	0.06
LINE 9.0	AVERAGE EXCESS RUNNING TIME (S/VEH)	0.0	0.25
LINE 10.	EMISSIONS FROM ACCELERATION (G/VEH-M)	0.0	0.100
LINE 11.	EMISSIONS FROM DECELERATION (G/VEH-M)	0.0	0.031
LINE 12	EMISSION RATE FOR ACC AND DEC. (G/M-S)	0.0	0.000
LINE 13.	LENGTH OF ACC AND DEC. (M)	0.0	80.5
LINE 14.	LENGTH FOR EXCESS EMISSIONS (M)	0.0	160.9
LINE 15.	IDLING EMISSION RATE (G/S)	0.0	-0.005
LINE 16.	AVERAGE EMISSION RATE (G/S-M)	0.0	0.0002
LINE 17	ADJUSTED EXCESS EMISSION RATE (G/S-M)	0.0	0.0001
LINE 18	FREE-FLOW EMISSION RATE (G/S-M)	0.0057	0.0000

## EPA VOLUME 9 (REVISED) INDIRECT SOURCE GUIDELINE MODEL - WORKSHEET #2

INTERSECTION: OLIVER STREET & PURCHASE STREET  
CASE # 3 YEAR: 1990 AVERAGING TIME: 1-HOUR

LINE		PS	OS
LINE 1	ROAD SEGMENT ID		
LINE 2	DEMAND VOLUME (VPH)	2628	50
LINE 4	CRUISE SPEED (MPH)	28	28
LINE 5	FREE-FLOW EMISSIONS (G/VEH/M)	0.0198	0.0198
LINE 6.1	NUMBER OF LANES	3	2
LINE 6.3	CAPACITY SERVICE VOLUME (VPH OF GREEN)	0	0
LINE 6.4	DEMAND VOLUME (VPH)	0	0
LINE 6.5	SIGNAL CYCLE LENGTH (S)	0	
LINE 6.6	GREEN PHASE LENGTH (S)	0	0
LINE 6.7	CAPACITY (VPH)	0	315
LINE 6.8	PROPORTION OF VEHICLES THAT STOP	0.0	0.0
LINE 6.9	NUMBER OF VEHICLES THAT STOP PER CYCLE	0.0	0.0
LINE 7.0	AVERAGE NUMBER OF VEHICLES IN QUEUE	0.0	0.19
LINE 8.0	LENGTH OF QUEUE (M/LANE)	0.0	0.41
LINE 9.0	AVERAGE EXCESS RUNNING TIME (S/VEH)	0.0	2.16
LINE 10.	EMISSIONS FROM ACCELERATION (G/VEH-M)	0.0	0.103
LINE 11	EMISSIONS FROM DECELERATION (G/VEH-M)	0.0	0.034
LINE 12.	EMISSION RATE FOR ACC. AND DEC. (G/M-S)	0.0	0.002
LINE 13.	LENGTH OF ACC. AND DEC. (M)	0.0	70.1
LINE 14.	LENGTH FOR EXCESS EMISSIONS (M)	0.0	140.2
LINE 15.	IDLING EMISSION RATE (G/S)	0.0	-0.012
LINE 16	AVERAGE EMISSION RATE (G/S-M)	0.0	0.0009
LINE 17	ADJUSTED EXCESS EMISSION RATE (G/S-M)	0.0	0.0004
LINE 18.	FREE-FLOW EMISSION RATE (G/S-M)	0.0145	0.0003

## EPA VOLUME 9 (REVISED) INDIRECT SOURCE GUIDELINE MODEL - WORKSHEET #2

INTERSECTION: OLIVER STREET & PURCHASE STREET  
CASE # 3 YEAR 1990 AVERAGING TIME 8-HOUR

LINE 1	ROAD SEGMENT ID	PS	DS
LINE 2	DEMAND VOLUME (VPH)	1917	30
LINE 4	CRUISE SPEED (MPH)	35	30
LINE 5	FREE-FLOW EMISSIONS (G/VEH-M)	0 0111	0 0132
LINE 6.1	NUMBER OF LANES	3	2
LINE 6.3	CAPACITY SERVICE VOLUME (VPH OF GREEN)	0	0.
LINE 6.4	DEMAND VOLUME (VPH)	0	0
LINE 6.5	SIGNAL CYCLE LENGTH (S)	■	
LINE 6.6	GREEN PHASE LENGTH (S)	0	0
LINE 6.7	CAPACITY (VPH)	0	406
LINE 6.8	PROPORTION OF VEHICLES THAT STOP	0 0	0 0
LINE 6.9	NUMBER OF VEHICLES THAT STOP PER CYCLE	0 0	0.0
LINE 7.0	AVERAGE NUMBER OF VEHICLES IN QUEUE	0.0	0.08
LINE 8.0	LENGTH OF QUEUE (M/LANE)	0.0	0.17
LINE 9.0	AVERAGE EXCESS RUNNING TIME (S/VEH)	0.0	0.71
LINE 10	EMISSIONS FROM ACCELERATION (G/VEH-M)	0 0	0 100
LINE 11.	EMISSIONS FROM DECELERATION (G/VEH-M)	0 0	0 031
LINE 12	EMISSION RATE FOR ACC AND DEC. (G/M-S)	0 0	0 001
LINE 13	LENGTH OF ACC AND DEC. (M)	0 0	80.5
LINE 14	LENGTH FOR EXCESS EMISSIONS (M)	0 0	160.9
LINE 15	IDLING EMISSION RATE (G/S)	0 0	-0.011
LINE 16	AVERAGE EMISSION RATE (G/S-M)	0 0	0 0005
LINE 17	ADJUSTED EXCESS EMISSION RATE (G/S-M)	0 0	0 0001
LINE 18	FREE-FLOW EMISSION RATE (G/S-M)	0 0059	0 0001

WORKSHEET 5 - INTERSECTION CO DISPERSION ANALYSIS

Intersection Oliver And Purchase Street  
 Case # 1 Year 1984 Averaging Time 1 Hour

Line No. Symbol	Input/Units	Traffic Stream	
		<u>PS</u>	<u>OS</u>
1 SC	Stability Class	<u>D</u>	
2 U	Wind Speed ( $m s^{-1}$ )	<u>1.0</u>	
3 $\theta$	Wind-Road Angle (deg)	<u>4</u>	<u>86</u>
4 x	Lateral Distance (m)	<u>15</u>	<u>10</u>
5 Yu	Maximum Longitudinal Distance (m)	<u>NA</u>	<u>29</u>
6 Yd	Minimum Longitudinal Distance (m)	<u>NA</u>	<u>0</u>
7 $\sigma_{z0}$	Initial Dispersion (m)	<u>5.0</u>	
8 Qe	Excess Emissions Rate ( $gm^{-1}s^{-1}$ )	<u>.0000</u>	<u>.0023</u>
9 Qf	Free Flow Emissions Rate ( $gm^{-1}s^{-1}$ )	<u>.0134</u>	<u>.0015</u>
9a	Street Canyon? Yes or No	<u>NO</u>	
DISPERSION ANALYSIS			
10 $xUQ^{-1}$	Normalized Concentration ( $10^{-3}m^{-1}$ ) Free Flow	<u>690</u>	<u>145</u>
Qf	Enter Line 9	$\times .0134$	$\times .0015$
11 XU	Normalized Concentration ( $mg m^{-2}s^{-1}$ )		
U	Enter Line 2	$\div 1.0$	$\div$
12 X	CO Concentration ( $mg m^{-3}$ ) Through Emissions	<u>9.2</u>	<u>0.2</u>
13 $xUQ^{-1}$	Normalized Concentration (For Yu)	<u>NA</u>	<u>90</u>
Qe	Enter Line 8	<u>.0000</u>	<u>.0023</u>
14 XU	Normalized Concentration ( $mg m^{-2}s^{-1}$ )		
U	Enter Line 2	<u>1.0</u>	
15 X	CO Concentration-"Maximum Queue"	<u>0.0</u>	<u>0.2</u>
16 $xUQ^{-1}$	Normalized Concentration (For Yd)	<u>NA</u>	<u>0</u>
Qe	Enter Line 8	$\times .0000$	$\times .0023$
17 XU	Normalized Concentration ( $mg m^{-2}s^{-1}$ )		
U	Enter Line 2	<u>1.0</u>	
18 X	CO Concentration-"Imaginary Queue"	$\div 0.0$	$\div 0.0$
19 X	CO ( $mg m^{-3}$ ) Total	<u>9.2</u>	<u>0.4</u>
20 X	CO Concentration (ppm)-- Total	<u>8.0</u>	<u>0.3</u>
OPTIONAL z-CORRECTION (Heights Other than 1.8m Above the Ground)			
21 z	Height of Receptor (m)		
22	z-Correction Factor		
23 $x'$	CO Concentration at Height z ( $mg m^{-3}$ )		
24 $x'$	CO Concentration at Height z (ppm)		

**8.3 ppm**



WORKSHEET 5 - INTERSECTION CO DISPERSION ANALYSIS

Intersection Oliver And Purchase Street

Case # 1 Year 1984 Averaging Time 8 Hour

Line No. Symbol	Input/Units	PS	Traffic Stream
1 SC	Stability Class	<u>D</u>	<u>05</u>
2 U	Wind Speed ( $m s^{-1}$ )	<u>1.6</u>	
3 $\theta$	Wind-Road Angle (deg)	<u>4</u>	<u>86</u>
4 x	Lateral Distance (m)	<u>15</u>	<u>10</u>
5 Yu	Maximum Longitudinal Distance (m)	<u>NA</u>	<u>29</u>
6 Yd	Minimum Longitudinal Distance (m)	<u>NA</u>	<u>0</u>
7 $\sigma_{z0}$	Initial Dispersion (m)	<u>5.0</u>	
8 Qe	Excess Emissions Rate ( $gm^{-1}s^{-1}$ )	<u>.0000</u>	<u>.0008</u>
9 Qf	Free Flow Emissions Rate ( $gm^{-1}s^{-1}$ )	<u>.0053</u>	<u>.0005</u>
9a	Street Canyon? Yes or No	<u>NO</u>	
DISPERSION ANALYSIS			
10 $xUQ^{-1}$	Normalized Concentration ( $10^{-3}m^{-1}$ ) Free Flow	<u>640</u>	<u>145</u>
Qf	Enter Line 9	$\times .0053$	$\times .0005$
11 XU	Normalized Concentration ( $mg m^{-2}s^{-1}$ )		
U	Enter Line 2	$\div 1.6$	$\div$
12 X	CO Concentration ( $mg m^{-3}$ ) Through Emissions	<u>2.3</u>	<u>0.05</u>
13 $xUQ^{-1}$	Normalized Concentration (For Yu)	<u>NA</u>	<u>90</u>
Qe	Enter Line 8	$\times .0000$	$\times .0008$
14 XU	Normalized Concentration ( $mg m^{-2}s^{-1}$ )		
U	Enter Line 2	<u>1.6</u>	
15 X	CO Concentration--"Maximum Queue"	<u>0.0</u>	<u>0.04</u>
16 $xUQ^{-1}$	Normalized Concentration (For Yd)	<u>NA</u>	<u>0</u>
Qe	Enter Line 8	$\times .0000$	$\times .0008$
17 XU	Normalized Concentration ( $mg m^{-2}s^{-1}$ )		
U	Enter Line 2	<u>1.6</u>	
18 X	CO Concentration--"Imaginary Queue"	$\div 0.0$	$\div 0.0$
19 X	CO ( $mg m^{-3}$ ) Total	<u>2.3</u>	<u>0.09</u>
20 X	CO Concentration (ppm)-- Total	<u>2.0</u>	<u>0.08</u>
OPTIONAL z-CORRECTION (Heights Other than 1.8m Above the Ground)			
21 z	Height of Receptor (m)		
22	z-Correction Factor		
23 $x'$	CO Concentration at Height z ( $mg m^{-3}$ )		
24 $x'$	CO Concentration at Height z (ppm)		

2.1 ppm

WORKSHEET 5 - INTERSECTION CO DISPERSION ANALYSIS

Intersection Oliver And Purchase Street  
 Case # 2 Year 1990 Averaging Time 1 Hour

Line No. Symbol	Input/Units	PS	Traffic Stream OS
1 SC	Stability Class	D	
2 U	Wind Speed ( $m s^{-1}$ )	1.0	
3 $\theta$	Wind-Road Angle (deg)	4	86
4 x	Lateral Distance (m)	15	7
5 Yu	Maximum Longitudinal Distance (m)	NA	29
6 Yd	Minimum Longitudinal Distance (m)	NA	0
7 $\sigma_{z0}$	Initial Dispersion (m)	5.0	
8 Qe	Excess Emissions Rate ( $gm^{-1}s^{-1}$ )	.0000	.0001
9 Qf	Free Flow Emissions Rate ( $gm^{-1}s^{-1}$ )	.0136	.0001
9a	Street Canyon? Yes or No	NO	
DISPERSION ANALYSIS			
10 $xuQ^{-1}$	Normalized Concentration ( $10^{-3}m^{-1}$ ) Free Flow	690	150
Qf	Enter Line 9	$\times .0136$	$\times .0001$
11 XU	Normalized Concentration ( $mg m^{-2}s^{-1}$ )		
U	Enter Line 2	$\div 1.0$	$\div$
12 x	CO Concentration ( $mg m^{-3}$ ) Through Emissions	9.4	0.02
13 $xuQ^{-1}$	Normalized Concentration (For Yu)	NA	100
Qe	Enter Line 8	.0000	.0001
14 XU	Normalized Concentration ( $mg m^{-2}s^{-1}$ )		
U	Enter Line 2	1.0	
15 x	CO Concentration-"Maximum Queue"	0	0.01
16 $xuQ^{-1}$	Normalized Concentration (For Yd)	NA	0
Qe	Enter Line 8	$\times$	$\times$
17 XU	Normalized Concentration ( $mg m^{-2}s^{-1}$ )		
U	Enter Line 2	1.0	
18 x	CO Concentration-"Imaginary Queue"	$\div 0$	$\div 0$
19 x	CO ( $mg m^{-3}$ ) Total	9.4	0.03
20 x	CO Concentration (ppm)-- Total	8.2	0.03
OPTIONAL z-CORRECTION (Heights Other than 1.8m Above the Ground)			
21 z	Height of Receptor (m)		
22	z-Correction Factor		
23 $x''$	CO Concentration at Height z ( $mg m^{-3}$ )		
24 $x''$	CO Concentration at Height z (ppm)		

8.2 ppm

WORKSHEET 5 - INTERSECTION CO DISPERSION ANALYSIS

Intersection Oliver And Purchase Street  
 Case # 2 Year 1990 Averaging Time 8 Hour

Line No. Symbol	Input/Units	TS	Traffic Stream OS
1 SC	Stability Class	D	
2 U	Wind Speed ( $m s^{-1}$ )	1.6	
3 $\theta$	Wind-Road Angle (deg)	4	86
4 x	Lateral Distance (m)	15	7
5 Yu	Maximum Longitudinal Distance (m)	NA	29
6 Yd	Minimum Longitudinal Distance (m)	NA	0
7 $\sigma_{zo}$	Initial Dispersion (m)	5.0	
8 Qe	Excess Emissions Rate ( $gm^{-1}s^{-1}$ )	0.0000	0.0001
9 Qf	Free Flow Emissions Rate ( $gm^{-1}s^{-1}$ )	0.0057	0.0000
9a	Street Canyon? Yes or No	NO	
DISPERSION ANALYSIS			
10 $xUQ^{-1}$	Normalized Concentration ( $10^{-3}m^{-1}$ ) Free Flow	690	150
Qf	Enter Line 9	$\times 0.0057 \times$	$\times 0.0000 \times$
11 XU	Normalized Concentration ( $mg m^{-2}s^{-1}$ )		
U	Enter Line 2	$\div 1.6 \div$	$\div \div$
12 x	CO Concentration ( $mg m^{-3}$ ) Through Emissions	2.5	0.0
13 $xUQ^{-1}$	Normalized Concentration (For Yu)	NA	100
Qe	Enter Line 8	0.0000	0.0001
14 XU	Normalized Concentration ( $mg m^{-2}s^{-1}$ )		
U	Enter Line 2	1.6	
15 x	CO Concentration--"Maximum Queue"	0	0.01
16 $xUQ^{-1}$	Normalized Concentration (For Yd)	NA	0
Qe	Enter Line 8	$\times$	$\times$
17 XU	Normalized Concentration ( $mg m^{-2}s^{-1}$ )		
U	Enter Line 2	1.6	
18 x	CO Concentration--"Imaginary Queue"	$\div 0 \div$	$\div 0 \div$
19 x	CO ( $mg m^{-3}$ ) Total	2.5	0.01
20 x	CO Concentration (ppm)-- Total	2.2	0.01
OPTIONAL z-CORRECTION (Heights Other than 1.8m Above the Ground)			
21 z	Height of Receptor (m)		
22	z-Correction Factor		
23 x'	CO Concentration at Height z ( $mg m^{-3}$ )		
24 x'	CO Concentration at Height z (ppm)		

2.2 ppm

WORKSHEET 5 - INTERSECTION CO DISPERSION ANALYSIS

Intersection Oliver And Purchase Street  
 Case # 3 Year 1990 Averaging Time 1 Hour

Line No. Symbol	Input/Units	Traffic Stream	
		<u>PS</u>	<u>OS</u>
1 SC	Stability Class	<u>D</u>	
2 U	Wind Speed ( $m s^{-1}$ )	<u>1.0</u>	
3 $\theta$	Wind-Road Angle (deg)	<u>4</u>	<u>86</u>
4 x	Lateral Distance (m)	<u>15</u>	<u>7</u>
5 Yu	Maximum Longitudinal Distance (m)	<u>NA</u>	<u>29</u>
6 Yd	Minimum Longitudinal Distance (m)	<u>NA</u>	<u>0</u>
7 $\sigma_{z0}$	Initial Dispersion (m)	<u>5.0</u>	
8 Qe	Excess Emissions Rate ( $gm^{-1}s^{-1}$ )	<u>.0000</u>	<u>.0004</u>
9 Qf	Free Flow Emissions Rate ( $gm^{-1}s^{-1}$ )	<u>.0145</u>	<u>.0003</u>
9a	Street Canyon? Yes or No	<u>NO</u>	
DISPERSION ANALYSIS			
10 $XUQ^{-1}$	Normalized Concentration ( $10^{-3}m^{-1}$ ) Free Flow	<u>690</u>	<u>150</u>
Qf	Enter Line 9	$\times .0145$	$\times .0003$
11 XU	Normalized Concentration ( $mg m^{-2}s^{-1}$ )		
U	Enter Line 2	$\div 1.0$	$\div$
12 X	CO Concentration ( $mg m^{-3}$ ) Through Emissions	<u>10.0</u>	<u>0.05</u>
13 $XUQ^{-1}$	Normalized Concentration (For Yu)	<u>NA</u>	<u>100</u>
Qe	Enter Line 8	<u>.0000</u>	<u>.0004</u>
14 XU	Normalized Concentration ( $mg m^{-2}s^{-1}$ )		
U	Enter Line 2	<u>1.0</u>	
15 X	CO Concentration-"Maximum Queue"	<u>0.0</u>	<u>0.04</u>
16 $XUQ^{-1}$	Normalized Concentration (For Yd)	<u>NA</u>	<u>0</u>
Qe	Enter Line 8	$\times .0000$	$\times .0004$
17 XU	Normalized Concentration ( $mg m^{-2}s^{-1}$ )		
U	Enter Line 2	<u>1.0</u>	
18 X	CO Concentration-"Imaginary Queue"	$\div 0.0$	$\div 0.0$
19 X	CO ( $mg m^{-3}$ ) Total	<u>10.0</u>	<u>0.09</u>
20 X	CO Concentration (ppm)-- Total	<u>8.7</u>	<u>0.08</u>
OPTIONAL z-CORRECTION (Heights Other than 1.8m Above the Ground)			
21 z	Height of Receptor (m)		
22	z-Correction Factor		
23 $X^z$	CO Concentration at Height z ( $mg m^{-3}$ )		
24 $X^z$	CO Concentration at Height z (ppm)		

8.8ppm

WORKSHEET 5 - INTERSECTION CO DISPERSION ANALYSIS

Intersection Oliver And Purchase Streets  
 Case # 3 Year 1990 Averaging Time 8 Hour

Line No. Symbol	Input/Units	Traffic Stream	
		<u>PS</u>	<u>OS</u>
1 SC	Stability Class	<u>D</u>	
2 U	Wind Speed ( $m s^{-1}$ )	<u>1.6</u>	
3 $\theta$	Wind-Road Angle (deg)	<u>4</u>	<u>86</u>
4 x	Lateral Distance (m)	<u>15</u>	<u>9</u>
5 Yu	Maximum Longitudinal Distance (m)	<u>NA</u>	<u>29</u>
6 Yd	Minimum Longitudinal Distance (m)	<u>NA</u>	<u>0</u>
7 $\sigma_{z0}$	Initial Dispersion (m)	<u>5.0</u>	
8 Qe	Excess Emissions Rate ( $gm^{-1}s^{-1}$ )	<u>.0000</u>	<u>.0001</u>
9 Qf	Free Flow Emissions Rate ( $gm^{-1}s^{-1}$ )	<u>.0059</u>	<u>.0001</u>
9a	Street Canyon? Yes or No	<u>NO</u>	
DISPERSION ANALYSIS			
10 $xUQ^{-1}$	Normalized Concentration ( $10^{-3}m^{-1}$ ) Free Flow	<u>690</u>	<u>150</u>
Qf	Enter Line 9	$\times .0059$	$\times .0001$
11 XU	Normalized Concentration ( $mg m^{-2}s^{-1}$ )		
U	Enter Line 2	$\div 1.6$	$\div$
12 x	CO Concentration ( $mg m^{-3}$ ) Through Emissions	<u>2.5</u>	<u>0.02</u>
13 $xUQ^{-1}$	Normalized Concentration (For Yu)	<u>NA</u>	<u>100</u>
Qe	Enter Line 8	<u>.0000</u>	<u>.0001</u>
14 XU	Normalized Concentration ( $mg m^{-2}s^{-1}$ )		
U	Enter Line 2	<u>1.6</u>	
15 x	CO Concentration--"Maximum Queue"	<u>0.0</u>	<u>0.01</u>
16 $xUQ^{-1}$	Normalized Concentration (For Yd)	<u>NA</u>	<u>0</u>
Qe	Enter Line 8	$\times .0000$	$\times .0001$
17 XU	Normalized Concentration ( $mg m^{-2}s^{-1}$ )		
U	Enter Line 2	<u>1.6</u>	
18 x	CO Concentration--"Imaginary Queue"	$\div 0.0$	$\div 0.0$
19 x	CO ( $mg m^{-3}$ ) Total	<u>2.5</u>	<u>0.03</u>
20 x	CO Concentration (ppm)-- Total	<u>2.2</u>	<u>0.03</u>
OPTIONAL z-CORRECTION (Heights Other than 1.8m Above the Ground)			
21 z	Height of Receptor (m)		
22	z-Correction Factor		
23 $x'$	CO Concentration at Height z ( $mg m^{-3}$ )		
24 $x'$	CO Concentration at Height z (ppm)		

2.2ppm



WORKSHEET 1 - TRAFFIC INFORMATION

Intersection Northern Ave And Atlantic Ave  
 Case # 1 Year 1984

1. Road segment or intersection approach identification	AN	NW	
2. Observed 1-hr volume (vph)	2022	1478	
Observed 8-hr volume (vph)	1597	1079	
Projected 1-hr peak demand (vph)			
Projected 8-hr peak demand (vph)			
3. Percentage cold starts	50/20.6		
4. Percentage trucks and buses	3.8		
5. Metropolitan population			
6. Slope			
7. Free-flow parameters			
Number of lanes	3	4	
Average lane width (ft)	18	12	
Design speed (mph) (14r/84r)	24/29	21/33	
Highway type (see Figures 2-5)	Urban Artery		
8. Intersection parameters			
Intersection designation			
Approach width (ft)			
Percentage right turns	15	100	
Percentage left turns	0	0	
Type control and description of signal controller		STOP SIGN	
9. Area source parameters			
Parking lot gate designation			
Projected 1-hr peak entrance demand (vph)			
Projected 1-hr peak exit demand (vph)			
Projected 8-hr peak entrance demand (vph)			
Projected 8-hr peak exit demand (vph)			
Parking lot area (m <sup>2</sup> )			
Parking lot capacity (veh)			
Running time required to access auxiliary parking (s)			
Facility emptying time			
Average cars per stall			
Average area per stall (m <sup>2</sup> )			

Note: The AN volumes contain the expressway off-ramp traffic which merges into Atlantic Ave. before the intersection.

WORKSHEET 1 - TRAFFIC INFORMATION

Intersection Northern Ave And Atlantic Ave  
 Case # 2 Year 1990

1. Road segment or intersection approach identification	AN	NN	RE
2. Observed 1-hr volume (vph)	---	---	---
Observed 8-hr volume (vph)	---	---	---
Projected 1-hr peak demand (vph)	1784	1825	643
Projected 8-hr peak demand (vph)	1409	1332	508
3. Percentage cold starts	50/20.6	---	---
4. Percentage trucks and buses	3.8	---	---
5. Metropolitan population	---	---	---
6. Slope	---	---	---
7. Free-flow parameters			
Number of lanes	4	3	2
Average lane width (ft)	12	15	20
Design speed (mph)	24/29	21/33	24/29
Highway type (see Figures 2-5)	Urban Arterial		
8. Intersection parameters			
Intersection designation	---	---	---
Approach width (ft)	---	---	---
Percentage right turns	17	100	0
Percentage left turns	0	0	0
Type control and description of signal controller	Signal		
9. Area source parameters			
Parking lot gate designation	---	---	---
Projected 1-hr peak entrance demand (vph)	---	---	---
Projected 1-hr peak exit demand (vph)	---	---	---
Projected 8-hr peak entrance demand (vph)	---	---	---
Projected 8-hr peak exit demand (vph)	---	---	---
Parking lot area (m <sup>2</sup> )	---	---	---
Parking lot capacity (veh)	---	---	---
Running time required to access auxiliary parking (s)	---	---	---
Facility emptying time	---	---	---
Average cars per stall	---	---	---
Average area per stall (m <sup>2</sup> )	---	---	---

Ramp left turn  
has no conflicts

WORKSHEET 1 - TRAFFIC INFORMATION

Intersection Northern Ave And Atlantic Ave  
 Case # 3 Year 1990

1. Road segment or intersection approach identification	AN	NW	RE
2. Observed 1-hr volume (vph)	---	---	---
Observed 8-hr volume (vph)	---	---	---
Projected 1-hr peak demand (vph)	1863	1825	643
Projected 8-hr peak demand (vph)	1472	1332	508
3. Percentage cold starts	50/20.6	---	---
4. Percentage trucks and buses	3.8	---	---
5. Metropolitan population	---	---	---
6. Slope	---	---	---
7. Free-flow parameters			
Number of lanes	4	3	2
Average lane width (ft)	12	15	20
Design speed (mph)	24/29	21/33	24/29
Highway type (see Figures 2-5)	Urban	Arterial	---
8. Intersection parameters			
Intersection designation	---	---	---
Approach width (ft)	---	---	---
Percentage right turns	17	100	0
Percentage left turns	0	0	0
Type control and description of signal controller	---	---	---
9. Area source parameters			
Parking lot gate designation	---	---	---
Projected 1-hr peak entrance demand (vph)	---	---	---
Projected 1-hr peak exit demand (vph)	---	---	---
Projected 8-hr peak entrance demand (vph)	---	---	---
Projected 8-hr peak exit demand (vph)	---	---	---
Parking lot area (m <sup>2</sup> )	---	---	---
Parking lot capacity (veh)	---	---	---
Running time required to access auxiliary parking (s)	---	---	---
Facility emptying time	---	---	---
Average cars per stall	---	---	---
Average area per stall (m <sup>2</sup> )	---	---	---

WORKSHEET B - CAPACITY ANALYSIS

Intersection Northern Ave And Atlantic Ave  
 Case # 1 year 1984

Step	Symbol	Input/Units		
1	1	Road segment (or approach) designation	<u>AN</u>	<u>NW</u>
2		Free flow capacity computation:		
2.1	$M_i$	Number of lanes		
2.2	$W_p$	Adjustment for lane width (Table B-1)		
2.3	$T_i$	Adjustment for trucks (Table B-2)		
2.4	$C_i$	Free flow capacity		
3		Signalized intersection capacity:		
3.1	$j$	Green signal phase identification		
3.2	$wa_i$	Approach width with parking (ft)		
3.3		Percent right turners		
3.4		Percent left turners		
3.5		Metropolitan area size		
3.6	$Cs_{i,j}$	Capacity service volume (vph or green)		
4		Signalized intersection green phase and cycle length:		
4.1	$V_{i,j}$	Demand Volume for approach and phase		
4.2	$V_{i,j}/Cs_{i,j}$	Volume to green capacity ratio		
4.3	approx $G/Cy$	Approximate $G/Cy$		
4.4	$\sum \max(V_{i,j}/Cs_{i,j})_j$	Sum of the maximum $V/C$ ratios for each signal phase		
4.5	$Cy$	Signal cycle time (sec)		
4.6	$Gj$	Green phase length		
4.7	$Gj/Cy$	Green phase to cycle time ratio		
4.8	$C_{i,j}$	Capacity for approach $i$ phase $j$		
5		Two-way stop, two-way yield or uncontrolled intersection:		
5.1	$V_m + V_n$	Major street two-way volume (excl. right turn)	<u>1710/1351</u>	
5.2	$C_i$	Cross street capacity (14/18 ft)		<u>1857/2194</u>
6		Four-way stop intersections:		
6.1	$V_i$	Approach volume		
6.2	$Sp_i$	Demand split on cross streets		
6.3	$C_i$	Capacity of approach		
7	$C_i$	Approach capacity $\sum C_{i,j}$ 5.2 for a four-way stop or 6.3 for a two-way stop		

Northern Ave  
Lane No.

1-Hour

8-Hour

	<u><math>V_m + V_n</math></u>	<u><math>C_i</math></u>		<u><math>V_m + V_n</math></u>	<u><math>C_i</math></u>
1	1120	568		885	622
2	1378	489		1089	578
3	1710	400		1351	497
4	1710	400		1351	497

Intersection Northern Ave And Atlantic Ave  
Case # 2, 3 Year 1990

Intersection Northern Ave And Atlantic Ave  
Case # 2, 3 Year 1990

Case # 23 Year 1990

ΦA Atlantic Ave 30 s.

QB Off-ramp and Atlantic Right Turn 25 s.

Φ c Northern Ave. 35 s  
and Atlantic  
Right Turn

Total 90 s.

Signal times assume traffic moves on amber

$$\phi_D = \phi_A + \phi_B \rightarrow \phi_C = 90^\circ.$$

Parking on east side of Atlantic Ave. Reduces Approach Capacity For Right Turns.



## EPA VOLUME 9 (REVISED) INDIRECT SOURCE GUIDELINE MODEL - WORKSHEET #2

INTERSECTION: NORTHERN AVE AND ATLANTIC AVE  
CASE # 1 YEAR 1984 AVERAGING TIME 1-HOUR

LINE	ROAD SEGMENT ID	AN	NW
LINE 2	DEMAND VOLUME (VPH)	2022	1478
LINE 4	CRUISE SPEED (MPH)	24	21
LINE 5	FREE-FLOW EMISSIONS (G-VEH/M)	0 0480	0 0541
LINE 6 1	NUMBER OF LANES	3	4
LINE 6 3	CAPACITY SERVICE VOLUME (VPH OF GREEN)	0	0
LINE 6 4	DEMAND VOLUME (VPH)	0	0
LINE 6 5	SIGNAL CYCLE LENGTH (S)	0	
LINE 6 6	GREEN PHASE LENGTH (S)	0	0
LINE 6 7	CAPACITY (VPH)	0	1857
LINE 6 8	PROPORTION OF VEHICLES THAT STOP	0 0	0 0
LINE 6 9	NUMBER OF VEHICLES THAT STOP PER CYCLE	0 0	0 0
LINE 7 0	AVERAGE NUMBER OF VEHICLES IN QUEUE	0 0	3 90
LINE 8 0	LENGTH OF QUEUE (M/LANE)	0 0	4 24
LINE 9 0	AVERAGE EXCESS RUNNING TIME (S/VEH)	0 0	7 56
LINE 10	EMISSIONS FROM ACCELERATION (G/VEH-M)	0 0	0 125
LINE 11	EMISSIONS FROM DECELERATION (G/VEH-M)	0 0	0 044
LINE 12	EMISSION RATE FOR ACC AND DEC. (G/M-S)	0 0	0 069
LINE 13	LENGTH OF ACC AND DEC. (M)	0 0	39 4
LINE 14	LENGTH FOR EXCESS EMISSIONS (M)	0 0	78 9
LINE 15	IDLING EMISSION RATE (G/S)	0 0	0 350
LINE 16	AVERAGE EMISSION RATE (G/S-M)	0 0	0 0391
LINE 17	ADJUSTED EXCESS EMISSION RATE (G/S-M)	0 0	0 0431
LINE 18	FREE-FLOW EMISSION RATE (G/S-M)	0 0270	0 0222

## EPA VOLUME 9 (REVISED) INDIRECT SOURCE GUIDELINE MODEL - WORKSHEET #2

INTERSECTION: NORTHERN AVE AND ATLANTIC AVE  
CASE # 1 YEAR: 1984 AVERAGING TIME: 8-HOUR

LINE	ROAD SEGMENT ID	AN	NW
LINE 2	DEMAND VOLUME (VPH)	1597	1079
LINE 4	CRUISE SPEED (MPH)	29	33
LINE 5	FREE-FLOW EMISSIONS (G/VEH/M)	0.0266	0.0229
LINE 6 1	NUMBER OF LANES	3	4
LINE 6.3	CAPACITY SERVICE VOLUME (VPH OF GREEN)	0.	0.
LINE 6 4	DEMAND VOLUME (VPH)	0	0.
LINE 6.5	SIGNAL CYCLE LENGTH (S)	0	
LINE 6 6	GREEN PHASE LENGTH (S)	0	0.
LINE 6 7	CAPACITY (VPH)	0.	2194
LINE 6 8	PROPORTION OF VEHICLES THAT STOP	0 0	0 0
LINE 6 9	NUMBER OF VEHICLES THAT STOP PER CYCLE	0.0	0.0
LINE 7 0	AVERAGE NUMBER OF VEHICLES IN QUEUE	0 0	0.97
LINE 8 0	LENGTH OF QUEUE (M/LANE)	0 0	1.05
LINE 9 0	AVERAGE EXCESS RUNNING TIME (S/VEH)	0.0	1.59
LINE 10.	EMISSIONS FROM ACCELERATION (G/VEH-M)	0.0	0.096
LINE 11	EMISSIONS FROM DECELERATION (G/VEH-M)	0 0	0.029
LINE 12	EMISSION RATE FOR ACC. AND DEC. (G/M-S)	0 0	0.037
LINE 13	LENGTH OF ACC AND DEC (M)	0 0	97.4
LINE 14	LENGTH FOR EXCESS EMISSIONS (M)	0 0	194.7
LINE 15	IDLING EMISSION RATE (G/S)	0.0	-0.382
LINE 16	AVERAGE EMISSION RATE (G/S-M)	0 0	0.0168
LINE 17	ADJUSTED EXCESS EMISSION RATE (G/S-M)	0 0	0.0121
LINE 18	FREE-FLOW EMISSION RATE (G/S-M)	0.0118	0.0069

## EPA VOLUME 9 (REVISED) INDIRECT SOURCE GUIDELINE MODEL - WORKSHEET #2

INTERSECTION: NORTHERN AVE AND ATLANTIC AVE  
CASE # 2 YEAR: 1990 AVERAGING TIME 1-HOUR

LINE	ROAD SEGMENT ID	AN	NW	RE
LINE 2	DEMAND VOLUME (VPH)	1784	1825	643
LINE 4	CRUISE SPEED (MPH)	24	21	24
LINE 5	FREE-FLOW EMISSIONS (G-VEH/M)	0 0232	0 0261	0 0232
LINE 6.1	NUMBER OF LANES	4	3	2
LINE 6.3	CAPACITY SERVICE VOLUME (VPH OF GREEN)	4800	5800	5400
LINE 6.3	CAPACITY SERVICE VOLUME (VPH OF GREEN)	1000	0	0
LINE 6.4	DEMAND VOLUME (VPH)	1476	1825	643
LINE 6.4	DEMAND VOLUME (VPH)	308	0	0
LINE 6.5	SIGNAL CYCLE LENGTH (S)	90		
LINE 6.6	GREEN PHASE LENGTH (S)	30	35	25
LINE 6.6	GREEN PHASE LENGTH (S)	90	0	0
LINE 6.7	CAPACITY (VPH)	2600	2256	1500
LINE 6.8	PROPORTION OF VEHICLES THAT STOP	0 963	0 892	0 820
LINE 6.8	PROPORTION OF VEHICLES THAT STOP	0 0	0 0	0 0
LINE 6.9	NUMBER OF VEHICLES THAT STOP PER CYCLE	35 523	40 683	13 179
LINE 6.9	NUMBER OF VEHICLES THAT STOP PER CYCLE	0 0	0 0	0 0
LINE 7.0	AVERAGE NUMBER OF VEHICLES IN QUEUE	2.19	4.24	0.75
LINE 8.0	LENGTH OF QUEUE (M/LANE)	41.01	65.14	30.30
LINE 9.0	AVERAGE EXCESS RUNNING TIME (S/VEH)	26.92	31.29	28.45
LINE 10	EMISSIONS FROM ACCELERATION (G/VEH-M)	0 113	0 125	0 113
LINE 11	EMISSIONS FROM DECELERATION (G/VEH-M)	0 039	0 044	0 039
LINE 12	EMISSION RATE FOR ACC AND DEC (G/M-S)	0 060	0 076	0 022
LINE 13	LENGTH OF ACC AND DEC (M)	51.5	39.4	51.5
LINE 14	LENGTH FOR EXCESS EMISSIONS (M)	103.0	78.9	103.0
LINE 15	IDLING EMISSION RATE (G/S)	2.784	3.488	1.073
LINE 16	AVERAGE EMISSION RATE (G/S-M)	0 0570	0 0824	0 0215
LINE 17	ADJUSTED EXCESS EMISSION RATE (G/S-M)	0 0330	0 0492	0 0125
LINE 18	FREE-FLOW EMISSION RATE (G/S-M)	0 0115	0 0132	0 0041

## EPA VOLUME 9 (REVISED) INDIRECT SOURCE GUIDELINE MODEL - WORKSHEET #2

INTERSECTION: NORTHERN AVE AND ATLANTIC AVE  
CASE # 2 YEAR: 1990 AVERAGING TIME: 8-HOUR

LINE	ROAD SEGMENT ID	AN	NW	RE
LINE 2	DEMAND VOLUME (VPH)	1409	1332	508
LINE 4	CRUISE SPEED (MPH)	29	33	29
LINE 5	FREE-FLOW EMISSIONS (G/VEH-M)	0.0137	0.0118	0.0137
LINE 6 1	NUMBER OF LANES	4	3	2
LINE 6 3	CAPACITY SERVICE VOLUME (VPH OF GREEN)	4800	5800	5400
LINE 6 3	CAPACITY SERVICE VOLUME (VPH OF GREEN)	1000	0	0
LINE 6 4	DEMAND VOLUME (VPH)	1166	1332	508
LINE 6 4	DEMAND VOLUME (VPH)	243	0	0
LINE 6 5	SIGNAL CYCLE LENGTH (S)	90		
LINE 6 6	GREEN PHASE LENGTH (S)	30	35	25
LINE 6 6	GREEN PHASE LENGTH (S)	90	0	0
LINE 6 7	CAPACITY (VPH)	2600	2256	1500
LINE 6 8	PROPORTION OF VEHICLES THAT STOP	0.881	0.793	0.797
LINE 6 8	PROPORTION OF VEHICLES THAT STOP	0.0	0.0	0.0
LINE 6 9	NUMBER OF VEHICLES THAT STOP PER CYCLE	25 669	26 417	10 125
LINE 6 9	NUMBER OF VEHICLES THAT STOP PER CYCLE	0.0	0.0	0.0
LINE 7 0	AVERAGE NUMBER OF VEHICLES IN QUEUE	1 18	1 44	0.51
LINE 8 0	LENGTH OF QUEUE (M/LANE)	29.20	40.40	23.13
LINE 9 0	AVERAGE EXCESS RUNNING TIME (S/VEH)	23.50	24.12	27.14
LINE 10	EMISSIONS FROM ACCELERATION (G/VEH-M)	0.101	0.096	0.101
LINE 11	EMISSIONS FROM DECELERATION (G/VEH-M)	0.032	0.029	0.032
LINE 12	EMISSION RATE FOR ACC AND DEC (G/M-S)	0.038	0.037	0.015
LINE 13	LENGTH OF ACC AND DEC (M)	75.2	97.4	75.2
LINE 14	LENGTH FOR EXCESS EMISSIONS (M)	150.4	194.7	150.4
LINE 15	IDLING EMISSION RATE (G/S)	1.760	1.646	0.765
LINE 16	AVERAGE EMISSION RATE (G/S-M)	0.0307	0.0268	0.0126
LINE 17	ADJUSTED EXCESS EMISSION RATE (G/S-M)	0.0123	0.0107	0.0051
LINE 18	FREE-FLOW EMISSION RATE (G/S-M)	0.0054	0.0044	0.0019

## EPA VOLUME 9 (REVISED) INDIRECT SOURCE GUIDELINE MODEL - WORKSHEET #2

INTERSECTION: NORTHERN AVE AND ATLANTIC AVE  
CASE # 3 YEAR: 1990 AVERAGING TIME: 1-HOUR

LINE	ROAD SEGMENT ID	AN	NW	RE
LINE 2	DEMAND VOLUME (VPH)	1863	1825	643
LINE 4	CRUISE SPEED (MPH)	24	21	24
LINE 5	FREE-FLOW EMISSIONS (G-VEH/M)	0 0232	0 0261	0 0232
LINE 6 1	NUMBER OF LANES	4	3	2
LINE 6 3	CAPACITY SERVICE VOLUME (VPH OF GREEN)	4800	5800	5400
LINE 6 3	CAPACITY SERVICE VOLUME (VPH OF GREEN)	1000	0	0
LINE 6 4	DEMAND VOLUME (VPH)	1555	1825	643
LINE 6 4	DEMAND VOLUME (VPH)	308	0	0
LINE 6 5	SIGNAL CYCLE LENGTH (S)	90		
LINE 6 6	GREEN PHASE LENGTH (S)	30	35	25
LINE 6 6	GREEN PHASE LENGTH (S)	90	0	0
LINE 6 7	CAPACITY (VPH)	2600	2255	1500
LINE 6 8	PROPORTION OF VEHICLES THAT STOP	0 986	0 892	0 820
LINE 6 8	PROPORTION OF VEHICLES THAT STOP	0 0	0 0	0 0
LINE 6 9	NUMBER OF VEHICLES THAT STOP PER CYCLE	38 336	40 683	13 179
LINE 6 9	NUMBER OF VEHICLES THAT STOP PER CYCLE	0 0	0 0	0 0
LINE 7 0	AVERAGE NUMBER OF VEHICLES IN QUEUE	2 53	4 24	0 75
LINE 8 0	LENGTH OF QUEUE (M/LANE)	44 44	65 14	30 30
LINE 9 0	AVERAGE EXCESS RUNNING TIME (S/VEH)	28 19	31 29	28 45
LINE 10	EMISSIONS FROM ACCELERATION (G/VEH-M)	0 113	0 125	0 113
LINE 11	EMISSIONS FROM DECELERATION (G/VEH-M)	0 039	0 044	0 039
LINE 12	EMISSION RATE FOR ACC. AND DEC. (G/M-S)	0 065	0 076	0 022
LINE 13	LENGTH OF ACC AND DEC (M)	51 5	39 4	51 5
LINE 14	LENGTH FOR EXCESS EMISSIONS (M)	103 0	78 9	103 0
LINE 15	IDLING EMISSION RATE (G/S)	3 075	3 488	1 073
LINE 16	AVERAGE EMISSION RATE (G/S-M)	0 0622	0 0824	0 0215
LINE 17	ADJUSTED EXCESS EMISSION RATE (G/S-M)	0 0362	0 0492	0 0125
LINE 18	FREE-FLOW EMISSION RATE (G/S-M)	0 0120	0 0132	0 0041



## EPA VOLUME 9 (REVISED) INDIRECT SOURCE GUIDELINE MODEL - WORKSHEET #2

INTERSECTION: NORTHERN AVE AND ATLANTIC AVE  
CASE # 3 YEAR: 1990 AVERAGING TIME: 8-HOUR

LINE	ROAD SEGMENT ID	AN	NW	RE
LINE 2	DEMAND VOLUME (VPH)	1472	1332	508
LINE 4	CRUISE SPEED (MPH)	29	33	29
LINE 5	FREE-FLOW EMISSIONS (G-VEH/M)	0.0137	0.0118	0.0137
LINE 6.1	NUMBER OF LANES	4	3	2
LINE 6.3	CAPACITY SERVICE VOLUME (VPH OF GREEN)	4800	5800	5400
LINE 6.3	CAPACITY SERVICE VOLUME (VPH OF GREEN)	1000	0	0
LINE 6.4	DEMAND VOLUME (VPH)	1229	1332	508
LINE 6.4	DEMAND VOLUME (VPH)	243	0	0
LINE 6.5	SIGNAL CYCLE LENGTH (S)	90		
LINE 6.6	GREEN PHASE LENGTH (S)	30	35	25
LINE 6.6	GREEN PHASE LENGTH (S)	90	0	0
LINE 6.7	CAPACITY (VPH)	2600	2256	1500
LINE 6.8	PROPORTION OF VEHICLES THAT STOP	0.896	0.793	0.797
LINE 6.8	PROPORTION OF VEHICLES THAT STOP	0.0	0.0	0.0
LINE 6.9	NUMBER OF VEHICLES THAT STOP PER CYCLE	27.533	26.417	10.125
LINE 6.9	NUMBER OF VEHICLES THAT STOP PER CYCLE	0.0	0.0	0.0
LINE 7.0	AVERAGE NUMBER OF VEHICLES IN QUEUE	1.30	1.44	0.51
LINE 8.0	LENGTH OF QUEUE (M/LANE)	31.36	40.40	23.13
LINE 9.0	AVERAGE EXCESS RUNNING TIME (S/VEH)	24.25	24.12	27.14
LINE 10.	EMISSIONS FROM ACCELERATION (G/VEH-M)	0.101	0.096	0.101
LINE 11.	EMISSIONS FROM DECELERATION (G/VEH-M)	0.032	0.029	0.032
LINE 12.	EMISSION RATE FOR ACC AND DEC. (G/M-S)	0.041	0.037	0.015
LINE 13.	LENGTH OF ACC AND DEC (M)	75.2	97.4	75.2
LINE 14	LENGTH FOR EXCESS EMISSIONS (M)	150.4	194.7	150.4
LINE 15.	IDLING EMISSION RATE (G/S)	1.916	1.646	0.765
LINE 16.	AVERAGE EMISSION RATE (G/S-M)	0.0331	0.0268	0.0126
LINE 17.	ADJUSTED EXCESS EMISSION RATE (G/S-M)	0.0133	0.0107	0.0051
LINE 18	FREE-FLOW EMISSION RATE (G/S-M)	0.0056	0.0044	0.0019

WORKSHEET 5 - INTERSECTION CO DISPERSION ANALYSIS

Intersection Northern Ave And Atlantic Ave  
 Case # 1 Year 1984 Averaging Time 1 Hour

Line No. Symbol	Input/Units	AN	Traffic Stream NW
1 SC	Stability Class	D	
2 U	Wind Speed ( $m s^{-1}$ )	1.0	
3 $\theta$	Wind-Road Angle (deg)		
4 x	Lateral Distance (m)	38	32
5 Yu	Maximum Longitudinal Distance (m)	NA	50
6 Yd	Minimum Longitudinal Distance (m)	NA	0
7 $\sigma_{z0}$	Initial Dispersion (m)	5	
8 Qe	Excess Emissions Rate ( $gm^{-1}s^{-1}$ )	0.0	.0431
9 Qf	Free Flow Emissions Rate ( $gm^{-1}s^{-1}$ )	.0270	.0222
9a	Street Canyon? Yes or No	No	
DISPERSION ANALYSIS			
10 $xUQ^{-1}$	Normalized Concentration ( $10^{-3}m^{-1}$ ) Free Flow	195	140
Qf	Enter Line 9	$\times .0270$	$\times .0222$
11 XU	Normalized Concentration ( $mg m^{-2}s^{-1}$ )		
U	Enter Line 2	$\div 1.0$	$\div$
12 x	CO Concentration ( $mg m^{-3}$ ) Through Emissions	5.3	3.1
13 $xUQ^{-1}$	Normalized Concentration (For Yu)	0	124
Qe	Enter Line 8	0	.0431
14 XU	Normalized Concentration ( $mg m^{-2}s^{-1}$ )		
U	Enter Line 2	1.0	
15 x	CO Concentration--"Maximum Queue"	0	5.3
16 $xUQ^{-1}$	Normalized Concentration (For Yd)	0	0
Qe	Enter Line 8	$\times 0$	$\times .0431$
17 XU	Normalized Concentration ( $mg m^{-2}s^{-1}$ )		
U	Enter Line 2	1.0	
18 x	CO Concentration--"Imaginary Queue"	$\div 0$	$\div 0$
19 x	CO ( $mg m^{-3}$ ) Total	5.3	8.4
20 x	CO Concentration (ppm)-- Total	4.6	7.3
OPTIONAL z-CORRECTION (Heights Other than 1.8m Above the Ground)			
21 z	Height of Receptor (m)		
22	z-Correction Factor		
23 $x'$	CO Concentration at Height z ( $mg m^{-3}$ )		
24 $x'$	CO Concentration at Height z (ppm)		

11.9 ppm

WORKSHEET 5 - INTERSECTION CO DISPERSION ANALYSIS

Intersection Northern Ave And Atlantic Ave  
 Case # 1 Year 1984 Averaging Time 8 Hour

Line No. Symbol	Input/Units	Traffic Stream	
		AN	NW
1 SC	Stability Class	D	
2 U	Wind Speed ( $m s^{-1}$ )	1.6	
3 B	Wind-Road Angle (deg)	30	60
4 x	Lateral Distance (m)	38	32
5 Yu	Maximum Longitudinal Distance (m)	NA	50
6 Yd	Minimum Longitudinal Distance (m)	NA	0
7 $\sigma_{z0}$	Initial Dispersion (m)	5.0	
8 Qe	Excess Emissions Rate ( $gm^{-1}s^{-1}$ )	0.0	.0121
9 Qf	Free Flow Emissions Rate ( $gm^{-1}s^{-1}$ )	.0118	.0069
9a	Street Canyon? Yes or No	NO	
DISPERSION ANALYSIS			
10 $xUQ^{-1}$	Normalized Concentration ( $10^{-3}m^{-1}$ ) Free Flow	195	140
Qf	Enter Line 9	$\times .0118$	$\times .0069$
11 XU	Normalized Concentration ( $mg m^{-2}s^{-1}$ )		
U	Enter Line 2	$\div 1.6$	$\div$
12 x	CO Concentration ( $mg m^{-3}$ ) Through Emissions	1.4	0.6
13 $xUQ^{-1}$	Normalized Concentration (For Yu)	0	129
Qe	Enter Line 8	.0	.0121
14 XU	Normalized Concentration ( $mg m^{-2}s^{-1}$ )		
U	Enter Line 2	1.6	
15 x	CO Concentration-"Maximum Queue"	0	0.9
16 $xUQ^{-1}$	Normalized Concentration (For Yd)	0	0
Qe	Enter Line 8	$\times .0$	$\times .0121$
17 XU	Normalized Concentration ( $mg m^{-2}s^{-1}$ )		
U	Enter Line 2	1.6	
18 x	CO Concentration-"Imaginary Queue"	$\div 0$	$\div 0$
19 x	CO ( $mg m^{-3}$ ) Total	1.4	1.5
20 x	CO Concentration (ppm)-- Total	1.2	1.3
OPTIONAL z-CORRECTION (Heights Other than 1.8m Above the Ground)			
21 z	Height of Receptor (m)		
22	z-Correction Factor		
23 $x'$	CO Concentration at Height z ( $mg m^{-3}$ )		
24 $x'$	CO Concentration at Height z (ppm)		

2.5ppm

WORKSHEET 5 - INTERSECTION CO DISPERSION ANALYSIS

Intersection

Northern Ave And Atlantic Ave

Case # 2

Year 1990

Averaging Time 1 Hour

Line No. Symbol	Input/Units	AN	Traffic Stream NN	RE
1 SC	Stability Class	D		
2 U	Wind Speed ( $m s^{-1}$ )	1.0		
3 $\theta$	Wind-Road Angle (deg)	30	60	5
4 x	Lateral Distance (m)	50	30	34
5 Yu	Maximum Longitudinal Distance (m)	165	50	178
6 Yd	Minimum Longitudinal Distance (m)	62	0	75
7 $\sigma_{zo}$	Initial Dispersion (m)	5.0		
8 Qe	Excess Emissions Rate ( $gm^{-1}s^{-1}$ )	.0330	.0492	.0125
9 Qf	Free Flow Emissions Rate ( $gm^{-1}s^{-1}$ )	.0115	.0132	.0041
9a	Street Canyon? Yes or No	NO		
DISPERSION ANALYSIS				
10 $xUQ^{-1}$	Normalized Concentration ( $10^{-3}m^{-1}$ ) Free Flow	180	150	410
Qf	Enter Line 9	x .0115	x .0132	x .0041
11 XU	Normalized Concentration ( $mg m^{-2}s^{-1}$ )			
U	Enter Line 2	÷ 1.0	÷	÷
12 x	CO Concentration ( $mg m^{-3}$ ) Through Emissions	2.1	2.0	1.7
13 $xUQ^{-1}$	Normalized Concentration (For Yu)	190	110	40
Qe	Enter Line 8	.0330	.0492	.0125
14 XU	Normalized Concentration ( $mg m^{-2}s^{-1}$ )			
U	Enter Line 2	1.0		
15 x	CO Concentration--"Maximum Queue"	6.3	5.4	0.5
16 $xUQ^{-1}$	Normalized Concentration (For Yd)	0	0	0
Qe	Enter Line 8	x	x	x
17 XU	Normalized Concentration ( $mg m^{-2}s^{-1}$ )			
U	Enter Line 2	1.0		
18 x	CO Concentration--"Imaginary Queue"	÷ 0	÷ 0	÷ 0
19 x	CO ( $mg m^{-3}$ ) Total	8.4	7.4	2.2
20 x	CO Concentration (ppm)-- Total	7.3	6.4	1.9
OPTIONAL z-CORRECTION (Heights Other than 1.8m Above the Ground)				
21 z	Height of Receptor (m)			
22	z-Correction Factor			
23 $x^-$	CO Concentration at Height z ( $mg m^{-3}$ )			
24 $x^-$	CO Concentration at Height z (ppm)			

15.6 ppm

WORKSHEET 5 - INTERSECTION CO DISPERSION ANALYSIS

Intersection Northern Ave And Atlantic Ave  
 Case # 2 Year 1990 Averaging Time 8 Hour

Line No. Symbol	Input/Units	AN	Traffic Stream NW RE	
1 SC	Stability Class	D		
2 U	Wind Speed ( $m s^{-1}$ )	1.6		
3 $\theta$	Wind-Road Angle (deg)	30	60	5
4 x	Lateral Distance (m)	50	30	34
5 Yu	Maximum Longitudinal Distance (m)	212	50	225
6 Yd	Minimum Longitudinal Distance (m)	62	0	75
7 $\sigma_{z0}$	Initial Dispersion (m)	5.0		
8 Qe	Excess Emissions Rate ( $gm^{-1}s^{-1}$ )	.0123	.0107	.0051
9 Qf	Free Flow Emissions Rate ( $gm^{-1}s^{-1}$ )	.0054	.0044	.0019
9a	Street Canyon? Yes or No	NO		
DISPERSION ANALYSIS				
10 $xUQ^{-1}$	Normalized Concentration ( $10^{-3}m^{-1}$ ) Free Flow	180	150	40
Qf	Enter Line 9	$\times .0054$	$\times .0044$	$\times .0019$
11 xU	Normalized Concentration ( $mg m^{-2}s^{-1}$ )			
U	Enter Line 2	$\div 1.6$	$\div$	$\div$
12 x	CO Concentration ( $mg m^{-3}$ ) Through Emissions	0.6	0.4	0.5
13 $xUQ^{-1}$	Normalized Concentration (For Yu)	190	110	60
Qe	Enter Line 8	.0123	.0107	.0051
14 xU	Normalized Concentration ( $mg m^{-2}s^{-1}$ )			
U	Enter Line 2	1.6		
15 x	CO Concentration--"Maximum Queue"	1.5	0.7	0.2
16 $xUQ^{-1}$	Normalized Concentration (For Yd)	0	0	0
Qe	Enter Line 8	$\times$	$\times$	$\times$
17 xU	Normalized Concentration ( $mg m^{-2}s^{-1}$ )			
U	Enter Line 2	1.6		
18 x	CO Concentration--"Imaginary Queue"	$\div 0$	$\div 0$	$\div 0$
19 x	CO ( $mg m^{-3}$ ) Total	2.1	1.1	0.7
20 x	CO Concentration (ppm)-- Total	1.8	1.0	0.6
OPTIONAL z-CORRECTION (Heights Other than 1.8m Above the Ground)				
21 z	Height of Receptor (m)			
22	z-Correction Factor			
23 $x'$	CO Concentration at Height z ( $mg m^{-3}$ )			
24 $x'$	CO Concentration at Height z (ppm)			

3.4 ppm



WORKSHEET 5 - INTERSECTION CO DISPERSION ANALYSIS

Intersection Northern Ave And Atlantic Ave.  
 Case # 3 Year 1990 Averaging Time 1 Hour

Line No.	Symbol	Input/Units	AN	Traffic Stream	
				NN	RE
1	SC	Stability Class	D		
2	U	Wind Speed ( $m s^{-1}$ )	1.0		
3	$\theta$	Wind-Road Angle (deg)	30	60	5
4	x	Lateral Distance (m)	50	30	34
5	Yu	Maximum Longitudinal Distance (m)	165	50	178
6	Yd	Minimum Longitudinal Distance (m)	62	0	75
7	$\sigma_{z0}$	Initial Dispersion (m)	5.0		
8	Qe	Excess Emissions Rate ( $gm^{-1}s^{-1}$ )	.0362	.0492	.0125
9	Qf	Free Flow Emissions Rate ( $gm^{-1}s^{-1}$ )	.0120	.0132	.0041
9a		Street Canyon? Yes or No	No		
DISPERSION ANALYSIS					
10	$xUQ^{-1}$	Normalized Concentration ( $10^{-3}m^{-1}$ ) Free Flow	180	150	410
	Qf	Enter Line 9	$\times .0120$	$\times .0132$	$\times .0041$
11	$xU$	Normalized Concentration ( $mg m^{-2}s^{-1}$ )			
	U	Enter Line 2	$\div 1.0$	$\div$	$\div$
12	x	CO Concentration ( $mg m^{-3}$ ) Through Emissions	2.2	2.0	1.7
13	$xUQ^{-1}$	Normalized Concentration (For Yu)	190	110	40
	Qe	Enter Line 8	.0362	.0492	.0125
14	$xU$	Normalized Concentration ( $mg m^{-2}s^{-1}$ )			
	U	Enter Line 2	1.0		
15	x	CO Concentration-"Maximum Queue"	6.9	5.4	0.5
16	$xUQ^{-1}$	Normalized Concentration (For Yd)	0	0	0
	Qe	Enter Line 8	$\times$	$\times$	$\times$
17	$xU$	Normalized Concentration ( $mg m^{-2}s^{-1}$ )			
	U	Enter Line 2	1.0		
18	x	CO Concentration-"Imaginary Queue"	$\div 0$	$\div 0$	$\div 0$
19	x	CO ( $mg m^{-3}$ ) Total	9.1	7.4	2.2
20	x	CO Concentration (ppm)-- Total	7.9	6.4	1.9
OPTIONAL z-CORRECTION (Heights Other than 1.8m Above the Ground)					
21	z	Height of Receptor (m)			
22		z-Correction Factor			
23	$x''$	CO Concentration at Height z ( $mg m^{-3}$ )			
24	$x''$	CO Concentration at Height z (ppm)			

16.2 ppm

WORKSHEET 5 - INTERSECTION CO DISPERSION ANALYSIS

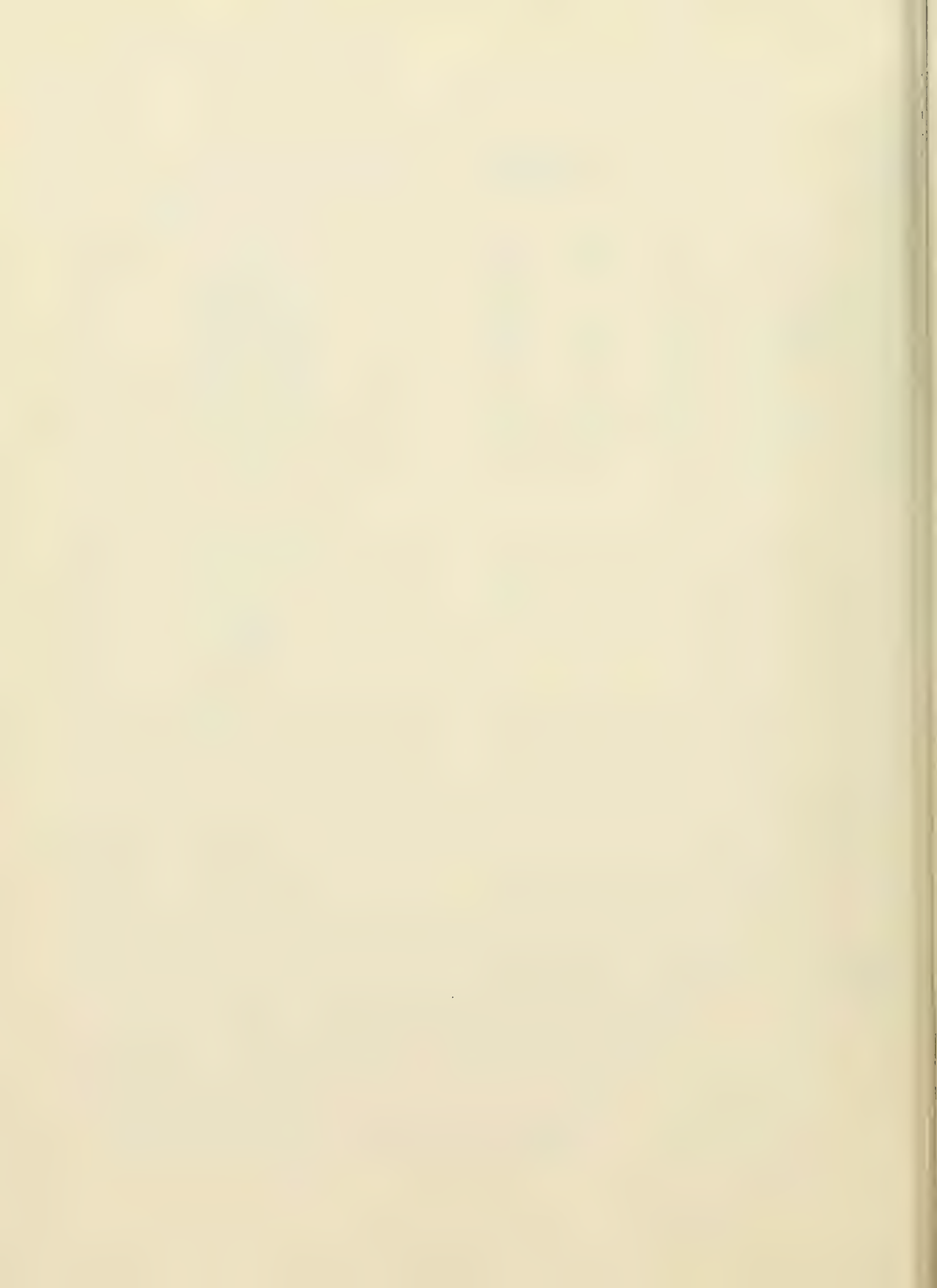
Intersection Northern Ave And Atlantic Ave  
 Case # 3 Year 1990 Averaging Time 8 Hour

Line No. Symbol	Input/Units	Traffic Stream		
		AN	NW	RE
1 SC	Stability Class	D		
2 U	Wind Speed ( $m s^{-1}$ )	1.6		
3 $\theta$	Wind-Road Angle (deg)	30	60	5
4 x	Lateral Distance (m)	50	30	34
5 Yu	Maximum Longitudinal Distance (m)	212	50	225
6 Yd	Minimum Longitudinal Distance (m)	62	0	75
7 $\sigma_{z0}$	Initial Dispersion (m)	5		
8 Qe	Excess Emissions Rate ( $gm^{-1}s^{-1}$ )	.0133	.0107	.0051
9 Qf	Free Flow Emissions Rate ( $gm^{-1}s^{-1}$ )	.0056	.0044	.0019
9a	Street Canyon? Yes or No	No		
DISPERSION ANALYSIS				
10 $xUQ^{-1}$	Normalized Concentration ( $10^{-3}m^{-1}$ ) Free Flow	180	150	410
Qf	Enter Line 9	$\times .0056$	$\times .0044$	$\times .0019$
11 XU	Normalized Concentration ( $mg m^{-2}s^{-1}$ )			
U	Enter Line 2	$\div 1.6$		
12 x	CO Concentration ( $mg m^{-3}$ ) Through Emissions	0.6	0.4	0.5
13 $xUQ^{-1}$	Normalized Concentration (For Yu)	190	110	60
Qe	Enter Line 8	.0133	.0107	.0051
14 XU	Normalized Concentration ( $mg m^{-2}s^{-1}$ )			
U	Enter Line 2	1.6		
15 x	CO Concentration-"Maximum Queue"	1.6	0.7	0.2
16 $xUQ^{-1}$	Normalized Concentration (For Yd)	0	0	0
Qe	Enter Line 8	$\times$	$\times$	$\times$
17 XU	Normalized Concentration ( $mg m^{-2}s^{-1}$ )			
U	Enter Line 2	1.6		
18 x	CO Concentration-"Imaginary Queue"	$\div 0$	$\div 0$	$\div 0$
19 x	CO ( $mg m^{-3}$ ) Total	2.2	1.1	0.7
20 x	CO Concentration (ppm)-- Total	1.9	1.0	0.6
OPTIONAL z-CORRECTION (Heights Other than 1.8m Above the Ground)				
21 z	Height of Receptor (m)			
22	z-Correction Factor			
23 $x^-$	CO Concentration at Height z ( $mg m^{-3}$ )			
24 $x^-$	CO Concentration at Height z (ppm)			

3.5 ppm

AQ APPENDIX C

PARKING FACILITY WORKSHEETS



WORKSHEET 3 - AREA SOURCE EMISSIONS COMPUTATION

Area Source Existing Parking Lot  
 Case # 1 Year 1984 Averaging Time 1 Hour

Step	Symbol	Input/Units	Traffic Stream			
1	Brt	Base running time	<u>In</u>	<u>Out</u>		
1.1		Base approach time(s)	<u>0.7</u>			
1.2		Base entrance time(s)	<u>5</u>			
1.3		Base movement-in time(s)	<u>18.8</u>			
1.4		Base stop, base start time(s)	<u>10</u>			
1.5		Base movement-out time(s)	<u>18.8</u>			
1.6		Base exit time(s)	<u>10</u>			
1.7		Base departure time(s)	<u>0.7</u>			
1.8		Total base running time(s)	<u>64</u>			
2	A	Area of parking lot (m <sup>2</sup> )	<u>2865</u>			
3	i	Entrance approach identification	<u>In</u>			
4	Ve <sub>1</sub>	Entrance demand volume (vph)	<u>20</u>			
5	Ce <sub>1</sub>	Entrance approach capacities (vph)	<u>360*</u>			
6	i	Exit approach identification		<u>Out</u>		
7	Vx <sub>1</sub>	Exit demand volume (vph)		<u>100</u>		
8	Cx <sub>1</sub>	Exit approach capacities (vph)		<u>417**</u>		
9		Number of parking spaces occupied				
10	F	Emissions (g/s-veh)	<u>.212</u>	<u>.750</u>		
11	Pc	Capacity of parking lot (veh)	<u>167</u>			
12	Rmi	Excess movement-in time(s)	<u>0</u>			
13	Fet	Facility emptying time(s)	<u>1442</u>			
14		Excess running time				
14.1	Ve <sub>1</sub> /Ce <sub>1</sub>	Entering volume-to-capacity ratio	<u>.05</u>			
14.2	Vx <sub>1</sub> /Cx <sub>1</sub>	Exiting volume-to-capacity ratio		<u>.24</u>		
14.3	Re <sub>1</sub>	Excess running time entering parking lot	<u>0.6</u>			
14.4	Rx <sub>1</sub>	Excess running time exiting parking lot		<u>2.7</u>		
15	Te <sub>1</sub>	Total entering running time (s/veh)	<u>32.6</u>			
16	Rmo	Excess running time moving out of parking stalls (s/veh)		<u>120</u>		
17	Tx <sub>1</sub>	Total exiting running time (s/veh)		<u>155</u>		
18	Qa	Total emission rate from a parking lot (g/m <sup>2</sup> - s)	<u>1.14</u>	<u>(10<sup>-3</sup>)</u>		
19	Qa'	Area source emission rate without the emissions from internal road segment. i				

\* Assumes a capacity consistent with an entrance time of 10 seconds per vehicle.

\*\* Cross Street capacity assuming a 4.5s critical gap.



WORKSHEET 3 - AREA SOURCE EMISSIONS COMPUTATION

Area Source Existing Parking Lot  
 Case # 1 Year 1984 Averaging Time 8 Hour

Step	Symbol	Input/Units	Traffic Stream			
			In	Out		
1	Brt	Base running time	<u>In</u>	<u>Out</u>		
1.1		Base approach time(s)	<u>0.7</u>			
1.2		Base entrance time(s)	<u>5</u>			
1.3		Base movement-in time(s)	<u>18.8</u>			
1.4		Base stop, base start time(s)	<u>10</u>			
1.5		Base movement-out time(s)	<u>18.8</u>			
1.6		Base exit time(s)	<u>10</u>			
1.7		Base departure time(s)	<u>0.7</u>			
1.8		Total base running time(s)	<u>64</u>			
2	A	Area of parking lot (m <sup>2</sup> )	<u>2865</u>			
3	i	Entrance approach identification	<u>In</u>			
4	Ve <sub>i</sub>	Entrance demand volume (vph)	<u>20</u>			
5	Ce <sub>i</sub>	Entrance approach capacities (vph)	<u>360</u>			
6	i	Exit approach identification		<u>Out</u>		
7	Vx <sub>i</sub>	Exit demand volume (vph)		<u>20</u>		
8	Cx <sub>i</sub>	Exit approach capacities (vph)		<u>496</u>		
9		Number of parking spaces occupied				
10	F	Emissions	<u>.212</u>	<u>.750</u>		
11	Pc	Capacity of parking lot (veh)	<u>167</u>			
12	Rmi	Excess movement-in time(s)	<u>0</u>			
13	Fet	Facility emptying time(s)	<u>1442</u>			
14		Excess running time				
14.1	Ve <sub>i</sub> /Ce <sub>i</sub>	Entering volume-to-capacity ratio	<u>0.06</u>			
14.2	Vx <sub>i</sub> /Cx <sub>i</sub>	Exiting volume-to-capacity ratio		<u>0.04</u>		
14.3	Re <sub>i</sub>	Excess running time entering parking lot	<u>0.6</u>			
14.4	Rx <sub>i</sub>	Excess running time exiting parking lot		<u>0.3</u>		
15	Te <sub>i</sub>	Total entering running time (s/veh)	<u>32.6</u>			
16	Rmo	Excess running time moving out of parking stalls (s/veh)		<u>120</u>		
17	Tx <sub>i</sub>	Total exiting running time (s/veh)		<u>152</u>		
18	Qa	Total emission rate from a parking lot (g/m <sup>2</sup> - s)	<u>2.35</u>	<u>(10<sup>-4</sup>)</u>		
19	Qa'	Area source emission rate without the emissions from internal road segment. i				

WORKSHEET 3 - AREA SOURCE EMISSIONS COMPUTATION

Area Source Existing Parking Lot  
 Case # 2 Year 1990 Averaging Time 1 Hour

Step	Symbol	Input/Units	Traffic Stream			
			In	Out		
1	Brt	Base running time				
1.1		Base approach time(s)	<u>0.7</u>			
1.2		Base entrance time(s)	<u>5</u>			
1.3		Base movement-in time(s)	<u>18.8</u>			
1.4		Base stop, base start time(s)	<u>10</u>			
1.5		Base movement-out time(s)	<u>18.8</u>			
1.6		Base exit time(s)	<u>10</u>			
1.7		Base departure time(s)	<u>0.7</u>			
1.8		Total base running time(s)	<u>64</u>			
2	A	Area of parking lot (m <sup>2</sup> )	<u>2865</u>			
3	i	Entrance approach identification	<u>In</u>			
4	Ve <sub>i</sub>	Entrance demand volume (vph)	<u>20</u>			
5	Ce <sub>i</sub>	Entrance approach capacities (vph)	<u>360</u>			
6	i	Exit approach identification		<u>Out</u>		
7	Vx <sub>i</sub>	Exit demand volume (vph)		<u>100</u>		
8	Cx <sub>i</sub>	Exit approach capacities (vph)		<u>236</u>		
9		Number of parking spaces occupied				
10	F	Emissions	<u>.109</u>	<u>.312</u>		
11	Pc	Capacity of parking lot (veh)	<u>167</u>			
12	Rmi	Excess movement-in time(s)	<u>0</u>			
13	Fet	Facility emptying time(s)	<u>2547</u>			
14		Excess running time				
14.1	Ve <sub>i</sub> /Ce <sub>i</sub>	Entering volume-to-capacity ratio	<u>.05</u>			
14.2	Vx <sub>i</sub> /Cx <sub>i</sub>	Exiting volume-to-capacity ratio		<u>.42</u>		
14.3	Re <sub>i</sub>	Excess running time entering parking lot	<u>0.6</u>			
14.4	Rx <sub>i</sub>	Excess running time exiting parking lot		<u>11.2</u>		
15	Te <sub>i</sub>	Total entering running time (s/veh)	<u>32.6</u>			
16	Rmo	Excess running time moving out of parking stalls (s/veh)		<u>211</u>		
17	Tx <sub>i</sub>	Total exiting running time (s/veh)		<u>254</u>		
18	Qa	Total emission rate from a parking lot (g/m <sup>2</sup> - s)	<u>7.75</u>	<u>(10<sup>4</sup>)</u>		
19	Qa'	Area source emission rate without the emissions from internal road segment. 1				

WORKSHEET 3 - AREA SOURCE EMISSIONS COMPUTATION

Area Source Existing Parking Lot  
 Case # 2 Year 1990 Averaging Time 8 Hour

Step	Symbol	Input/Units	Traffic Stream			
1	Brt	Base running time	<u>In</u>	<u>Out</u>		
1.1		Base approach time(s)	<u>0.7</u>			
1.2		Base entrance time(s)	<u>5</u>			
1.3		Base movement-in time(s)	<u>18.8</u>			
1.4		Base stop, base start time(s)	<u>10</u>			
1.5		Base movement-out time(s)	<u>18.8</u>			
1.6		Base exit time(s)	<u>10</u>			
1.7		Base departure time(s)	<u>0.7</u>			
1.8		Total base running time(s)	<u>64</u>			
2	A	Area of parking lot (m <sup>2</sup> )	<u>2865</u>			
3	i	Entrance approach identification	<u>In</u>			
4	Ve <sub>i</sub>	Entrance demand volume (vph)	<u>20</u>			
5	Ce <sub>i</sub>	Entrance approach capacities (vph)	<u>360</u>			
6	i	Exit approach identification		<u>Out</u>		
7	Vx <sub>i</sub>	Exit demand volume (vph)		<u>20</u>		
8	Cx <sub>i</sub>	Exit approach capacities (vph)		<u>330</u>		
9		Number of parking spaces occupied				
10	F	Emissions	<u>.109</u>	<u>.312</u>		
11	Pc	Capacity of parking lot (veh)	<u>167</u>			
12	Rmi	Excess movement-in time(s)	<u>0</u>			
13	Fet	Facility emptying time(s)	<u>2547</u>			
14		Excess running time				
14.1	Ve <sub>i</sub> /Ce <sub>i</sub>	Entering volume-to-capacity ratio	<u>.05</u>			
14.2	Vx <sub>i</sub> /Cx <sub>i</sub>	Exiting volume-to-capacity ratio		<u>.06</u>		
14.3	Re <sub>i</sub>	Excess running time entering parking lot	<u>0.6</u>			
14.4	Rx <sub>i</sub>	Excess running time exiting parking lot		<u>0.7</u>		
15	Te <sub>i</sub>	Total entering running time (s/veh)	<u>32.6</u>			
16	Rmo	Excess running time moving out of parking stalls (s/veh)		<u>211</u>		
17	Tx <sub>i</sub>	Total exiting running time (s/veh)		<u>244</u>		
18	Qa	Total emission rate from a parking lot (g/m <sup>2</sup> - s)	<u>1.54</u>	<u>(10<sup>-4</sup>)</u>		
19	Qa'	Area source emission rate without the emissions from internal road segment. i				

WORKSHEET 3 - AREA SOURCE EMISSIONS COMPUTATION

Area Source IP Parking Garage  
 Case # 3 Year 1990 Averaging Time 1 Hour

Step	Symbol	Input/Units	Traffic Stream			
1	Brt	Base running time	<u>IN</u>	<u>OUT</u>		
1.1		Base approach time(s)	<u>0.7</u>			
1.2		Base entrance time(s)	<u>5</u>			
1.3		Base movement-in time(s)	<u>109</u>			
1.4		Base stop, base start time(s)	<u>10</u>			
1.5		Base movement-out time(s)	<u>93</u>			
1.6		Base exit time(s)	<u>10</u>			
1.7		Base departure time(s)	<u>0.7</u>			
1.8		Total base running time(s)	<u>228</u>			
2	A	Area of parking lot (m <sup>2</sup> )				
3	i	Entrance approach identification	<u>In</u>			
4	Ve <sub>1</sub>	Entrance demand volume (vph)	<u>85</u>			
5	Ce <sub>1</sub>	Entrance approach capacities (vph)	<u>720*</u>			
6	i	Exit approach identification		<u>Out</u>		
7	Vx <sub>1</sub>	Exit demand volume (vph)		<u>357</u>		
8	Cx <sub>1</sub>	Exit approach capacities (vph)		<u>368**</u>		
9		Number of parking spaces occupied				
10	F	Emissions	<u>.109</u>	<u>.312</u>		
11	Pc	Capacity of parking lot (veh)	<u>800</u>			
12	Rmi	Excess movement-in time(s)	<u>0.</u>			
13	Fet	Facility emptying time(s)	<u>8000</u>			
14		Excess running time				
14.1	Ve <sub>1</sub> /Ce <sub>1</sub>	Entering volume-to-capacity ratio	<u>.12</u>			
14.2	Vx <sub>1</sub> /Cx <sub>1</sub>	Exiting volume-to-capacity ratio		<u>.97</u>		
14.3	Re <sub>1</sub>	Excess running time entering parking lot	<u>.67</u>			
14.4	Rx <sub>1</sub>	Excess running time exiting parking lot		<u>196</u>		
15	Te <sub>1</sub>	Total entering running time (s/veh)	<u>115</u>			
16	Rmo	Excess running time moving out of parking stalls (s/veh)		<u>0</u>		
17	Tx <sub>1</sub>	Total exiting running time (s/veh)		<u>310</u>		
18	Qa	Total emission rate from a parking lot (g/m <sup>2</sup> -s) garage vent	<u>9.89 g/s</u>			
19	Qa'	Area source emission rate without the emissions from internal road segment. 1				

\* Assumes an entrance capacity consistent with a gate rate of 5 seconds per vehicle

\*\* Cross Street capacity assuming a 4.5s critical gap.

WORKSHEET 3 - AREA SOURCE EMISSIONS COMPUTATION

Area Source IP Parking Garage  
 Case # 3 Year 1990 Averaging Time 8 Hour

Step	Symbol	Input/Units	Traffic Stream			
1	Brt	Base running time	<u>In</u>	<u>Out</u>		
1.1		Base approach time(s)	<u>0.7</u>			
1.2		Base entrance time(s)	<u>5</u>			
1.3		Base movement-in time(s)	<u>109</u>			
1.4		Base stop, base start time(s)	<u>10</u>			
1.5		Base movement-out time(s)	<u>93</u>			
1.6		Base exit time(s)	<u>10</u>			
1.7		Base departure time(s)	<u>0.7</u>			
1.8		Total base running time(s)	<u>228</u>			
2	A	Area of parking lot (m <sup>2</sup> )				
3	i	Entrance approach identification	<u>In</u>			
4	Ve <sub>1</sub>	Entrance demand volume (vph)	<u>110</u>			
5	Ce <sub>1</sub>	Entrance approach capacities (vph)	<u>720</u>			
6	i	Exit approach identification		<u>Out</u>		
7	Vx <sub>1</sub>	Exit demand volume (vph)		<u>110</u>		
8	Cx <sub>1</sub>	Exit approach capacities (vph)		<u>453</u>		
9		Number of parking spaces occupied				
10	F	Emissions	<u>109</u>	<u>312</u>		
11	Pc	Capacity of parking lot (veh)	<u>800</u>			
12	Rmi	Excess movement-in time(s)	<u>0</u>			
13	Fet	Facility emptying time(s)	<u>8000</u>			
14		Excess running time				
14.1	Ve <sub>1</sub> /Ce <sub>1</sub>	Entering volume-to-capacity ratio	<u>.15</u>			
14.2	Vx <sub>1</sub> /Cx <sub>1</sub>	Exiting volume-to-capacity ratio		<u>.24</u>		
14.3	Re <sub>1</sub>	Excess running time entering parking lot	<u>0.90</u>			
14.4	Rx <sub>1</sub>	Excess running time exiting parking lot		<u>2.55</u>		
15	Te <sub>1</sub>	Total entering running time (s/veh)	<u>115</u>			
16	Rmo	Excess running time moving out of parking stalls (s/veh)		<u>0</u>		
17	Tx <sub>1</sub>	Total exiting running time (s/veh)		<u>117</u>		
18	Qa	Total emission rate from a parking lot (g/m <sup>2</sup> -s) <u>garage vent</u>	<u>1.50 g/s</u>			
19	Qa'	Area source emission rate without the emissions from internal road segment. i				



WORKSHEET 6 - CO AREA SOURCE DISPERSION ANALYSIS

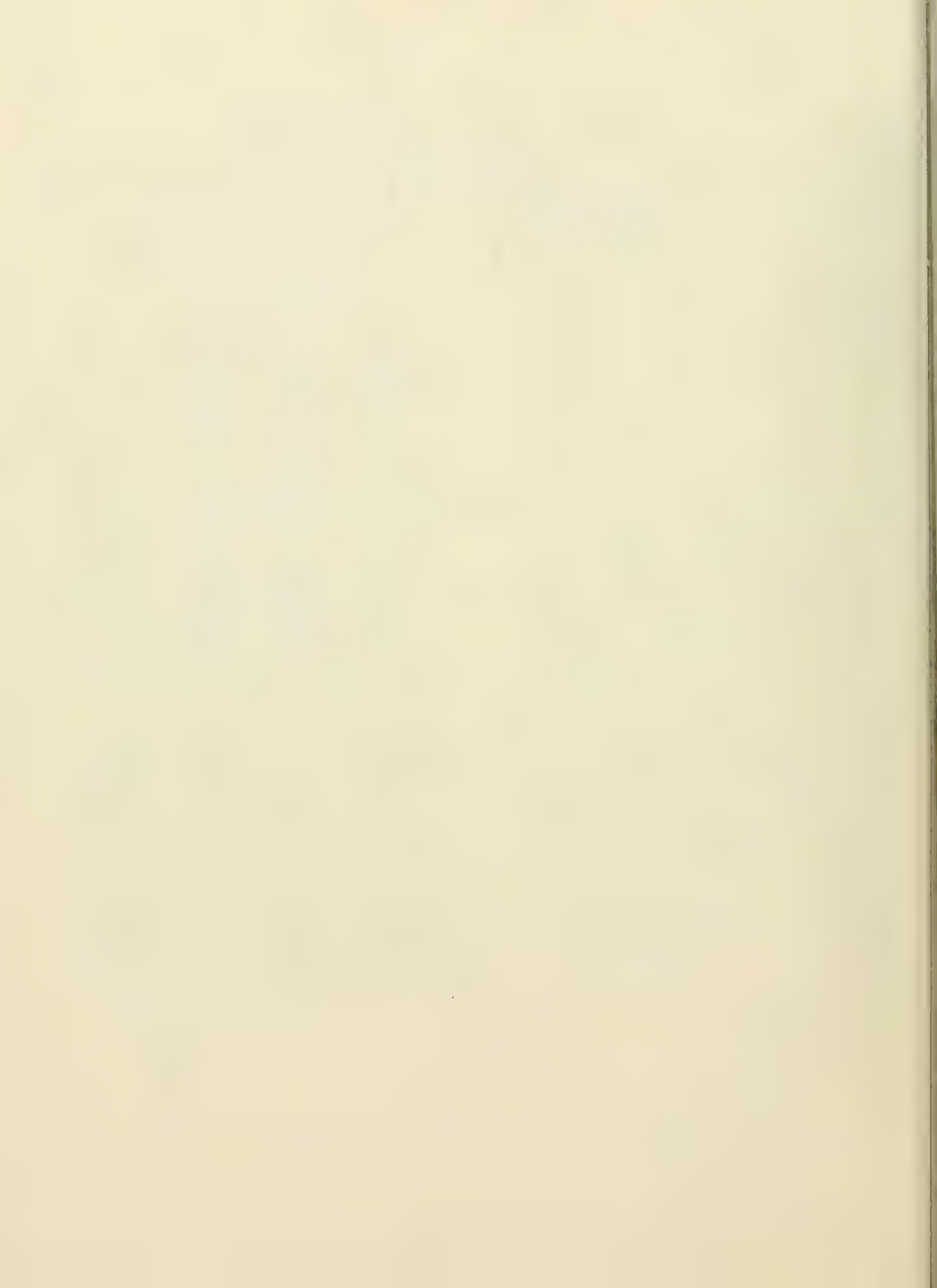
Area Source Existing Parking Lot  
 Case # 1 Year 1984 Averaging Time 1 Hour

Step Symbol Input/Units

Basic Inputs		Traffic Stream			
		Case 1	Case 1	Case 2	Case 2
		1-Hr	8-Hr	1-Hr	8-Hr
1	Source ID	<u>D</u>	<u>D</u>	<u>D</u>	<u>D</u>
2	SC Stability class	<u>D</u>	<u>D</u>	<u>D</u>	<u>D</u>
3	U Wind speed ( $\text{m s}^{-1}$ )	<u>1.0</u>	<u>1.6</u>	<u>1.0</u>	<u>1.6</u>
4	$\sigma_{z_0}$ Initial dispersion (m)	<u>5.0</u>	<u>5.0</u>	<u>5.0</u>	<u>5.0</u>
5	$x_0$ Virtual dispersion distance (m)	<u>19.9</u>	<u>19.9</u>	<u>19.9</u>	<u>19.9</u>
6	$x_u$ Actual upwind distance (m)	<u>41.1</u>	<u>41.1</u>	<u>41.1</u>	<u>41.1</u>
7	$r_u = x_u + x_0$ Effective upwind distance (m)	<u>61.0</u>	<u>61.0</u>	<u>61.0</u>	<u>61.0</u>
8	$x_d$ Actual downwind distance (m)	<u>1.0</u>	<u>1.0</u>	<u>1.0</u>	<u>1.0</u>
9	$r_d = x_d + x_0$ Effective downwind distance (m)	<u>20.9</u>	<u>20.9</u>	<u>20.9</u>	<u>20.9</u>
10	$Q_a$ Emission rate ( $\text{g m}^{-2} \text{s}^{-1}$ )	<u>.00114</u>	<u>.000235</u>	<u>.000775</u>	<u>.000154</u>

Dispersion Computation

11	$(xU/Q_a)_u$ Upwind normalized concentration	<u>17,000</u>	<u>17,000</u>	<u>17,000</u>	<u>17,000</u>
12	$(xU/Q_a)_d$ Downwind normalized concentration	<u>- 13,500</u>	<u>- 13,500</u>	<u>- 13,500</u>	<u>- 13,500</u>
13	$xU/Q_a$ Normalized CO concentration	<u>3,500</u>	<u>3,500</u>	<u>3,500</u>	<u>3,500</u>
14	$Q_a$ Emission rate ( $\text{g m}^{-2} \text{s}^{-1}$ )	<u>x .00114</u>	<u>x .000235</u>	<u>x .000775</u>	<u>x .000154</u>
15	$xU$	<u>4.0</u>	<u>0.8</u>	<u>2.7</u>	<u>0.5</u>
	Enter Line 3	<u>+ 1.0</u>	<u>+ 1.6</u>	<u>+ 1.0</u>	<u>+ 1.6</u>
16	$x$ CO concentration ( $\text{mg m}^{-3}$ )	<u>4.0</u>	<u>0.5</u>	<u>2.7</u>	<u>0.3</u>
17	$x$ CO concentration (ppm)	<u>3.5</u>	<u>0.4</u>	<u>2.3</u>	<u>0.3</u>

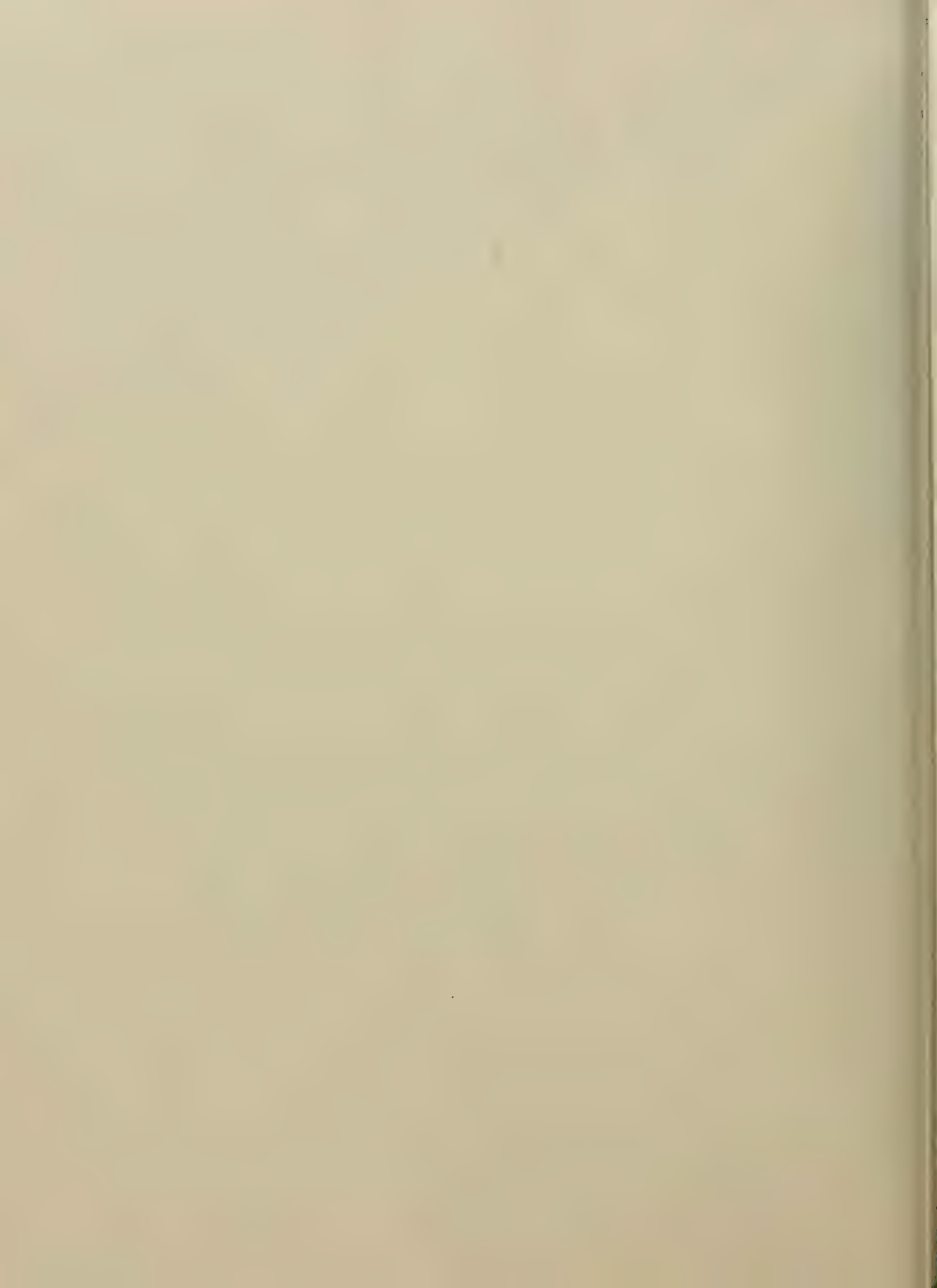


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# Pedestrian Wind Analysis





APPENDIX B

EXPERIMENTAL MEASUREMENTS



Figure B1 Approach and Site Velocity Profiles for Approach A

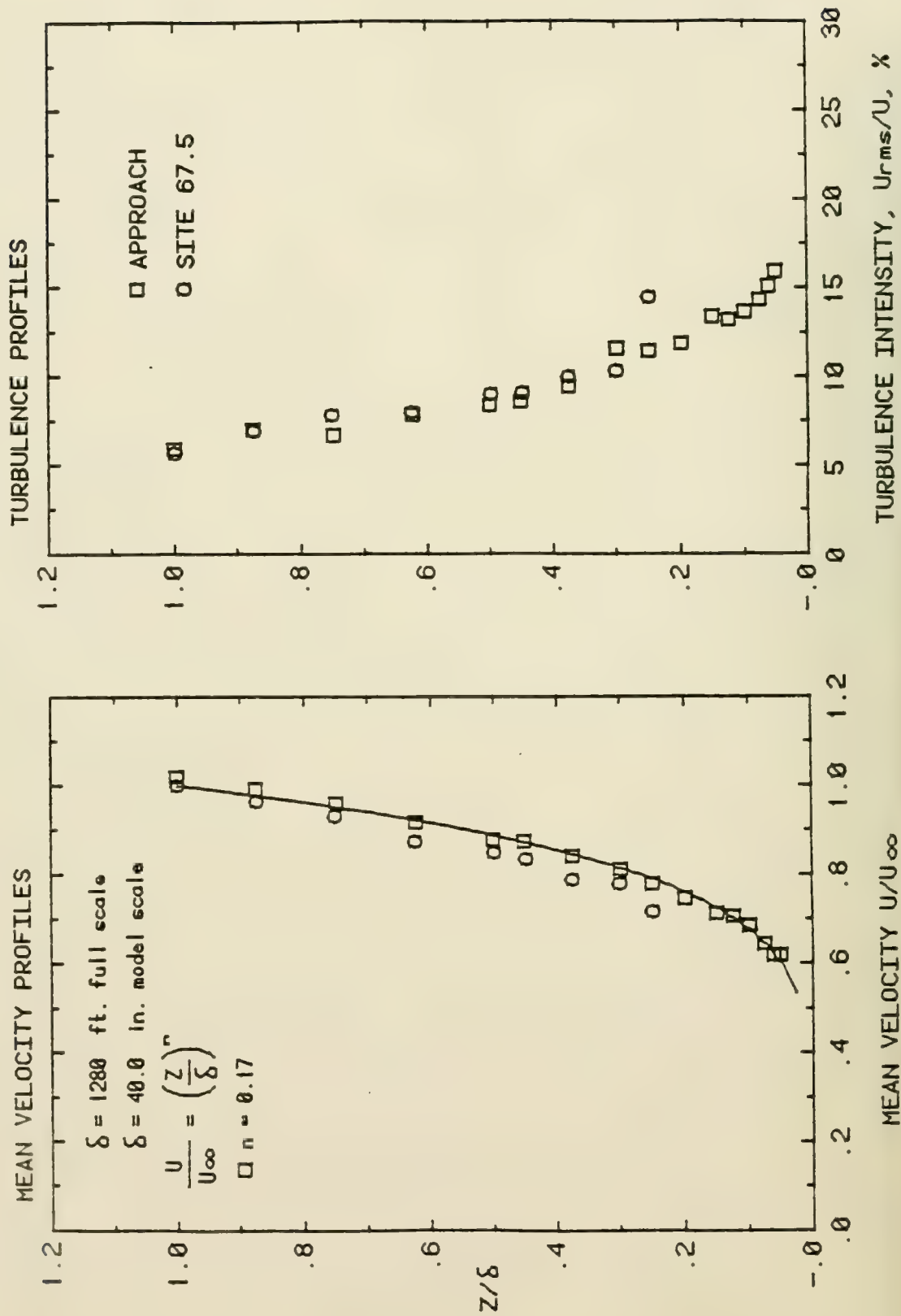


Figure B2 Approach and Site Velocity Profiles for Approach B

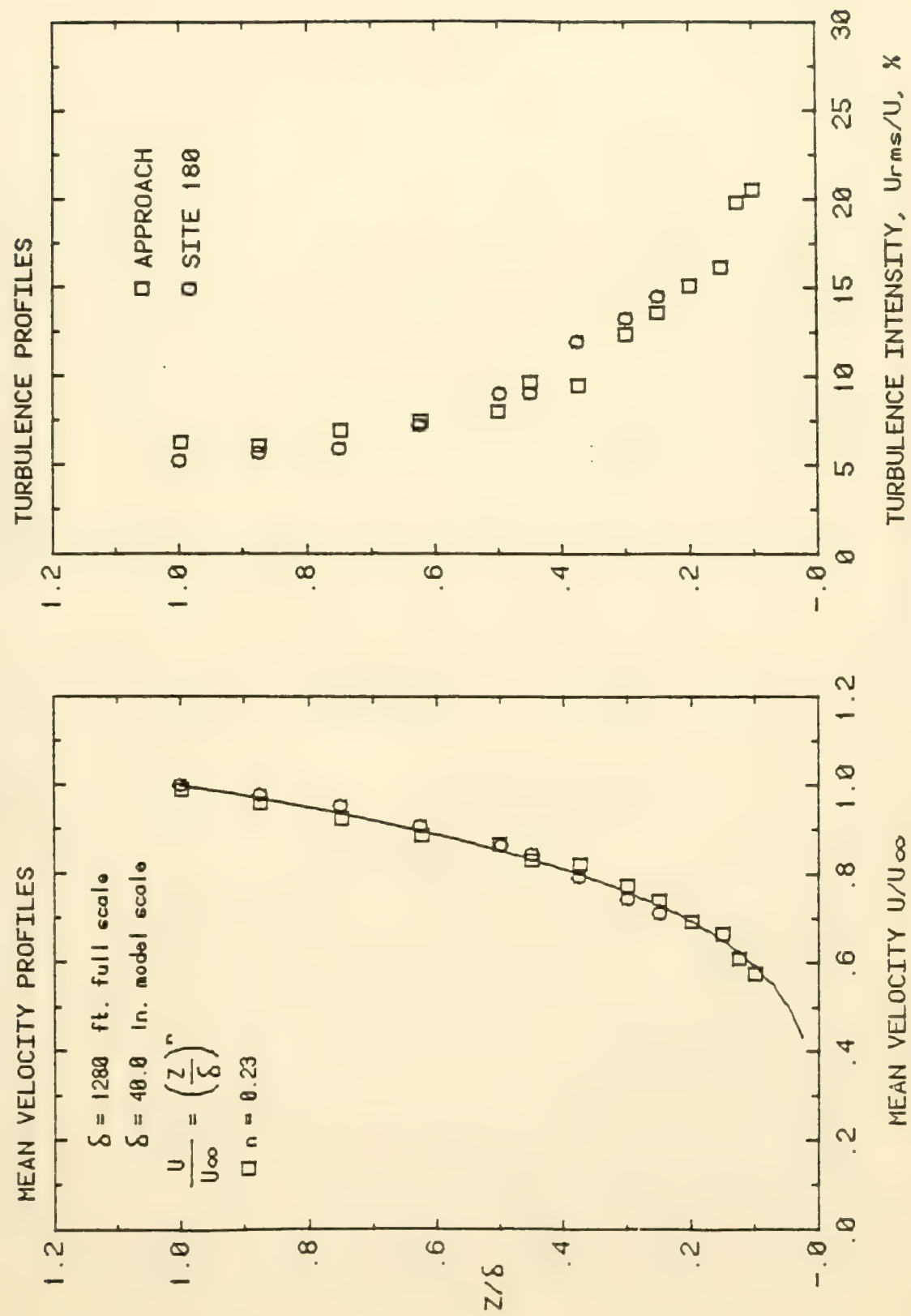
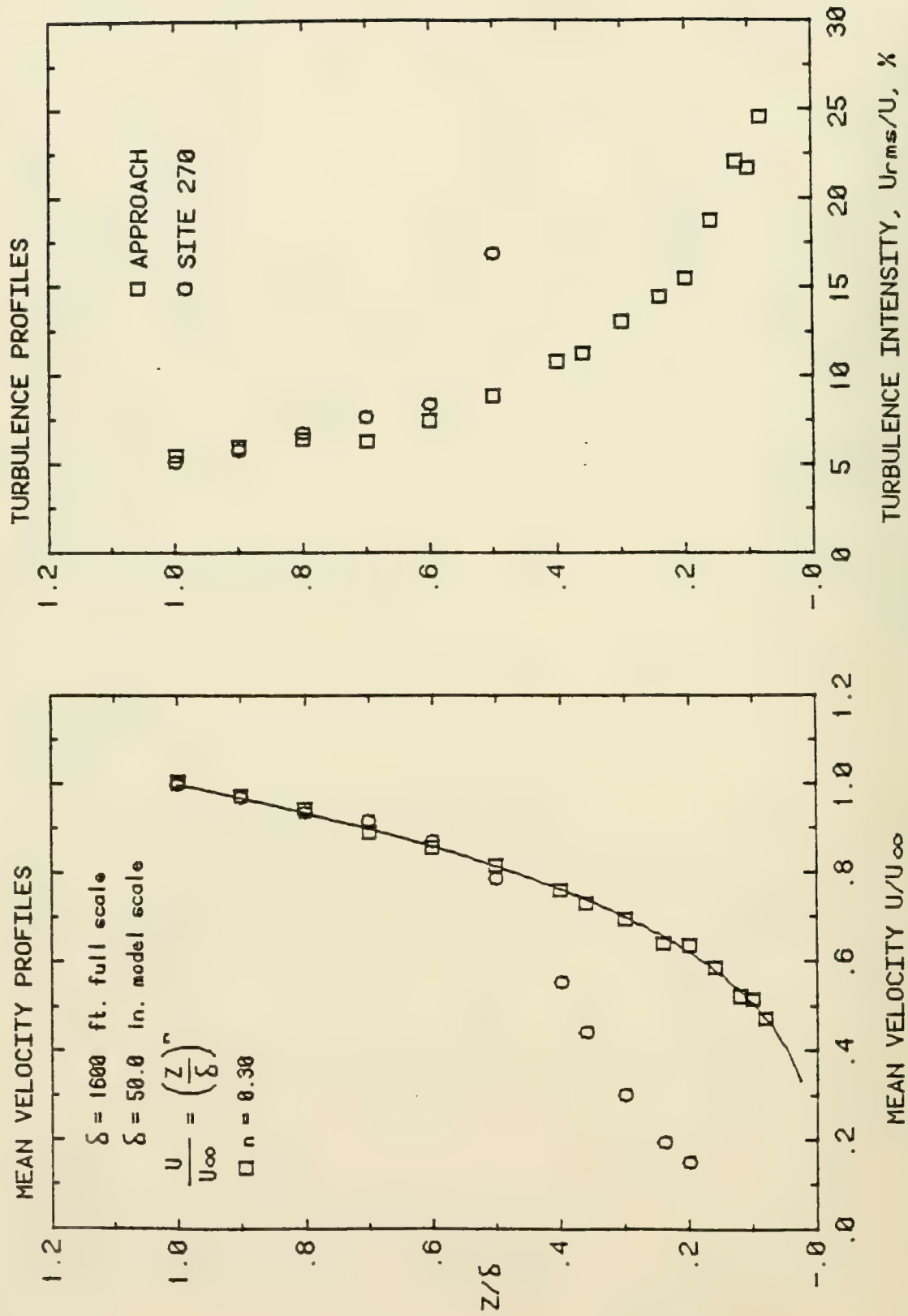


Figure B3 Approach and Site Velocity Profiles for Approach C



APPENDIX C

POLAR PLOTS OF PEDESTRIAN WINDS

#### POLAR PLOTS OF PEDESTRIAN WINDS

The graphs included in this appendix show the directional variation of measured wind speeds normalized by the wind speed at an elevation of 900 feet.



# Configuration PRE

Location 1

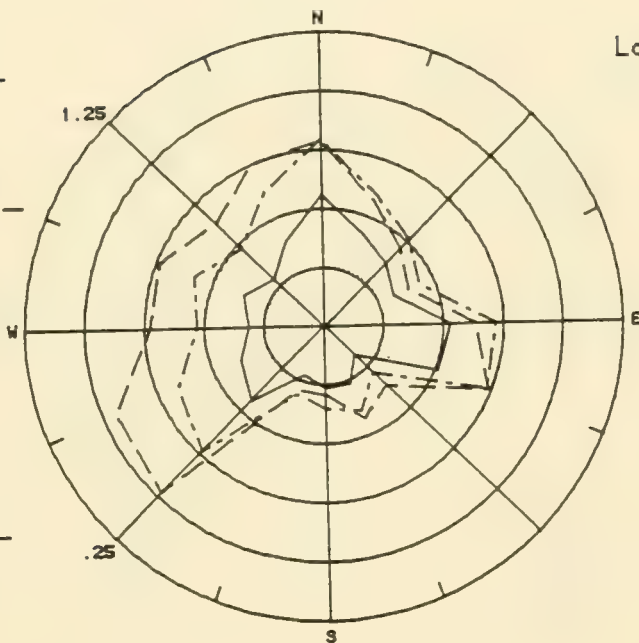
$\frac{U_{mean}}{U_{inf}}$  ———

$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}}$  - - -

.25/Div

$\frac{U_{rms}}{U_{inf}}$  - - -

.05/Div



Location 2

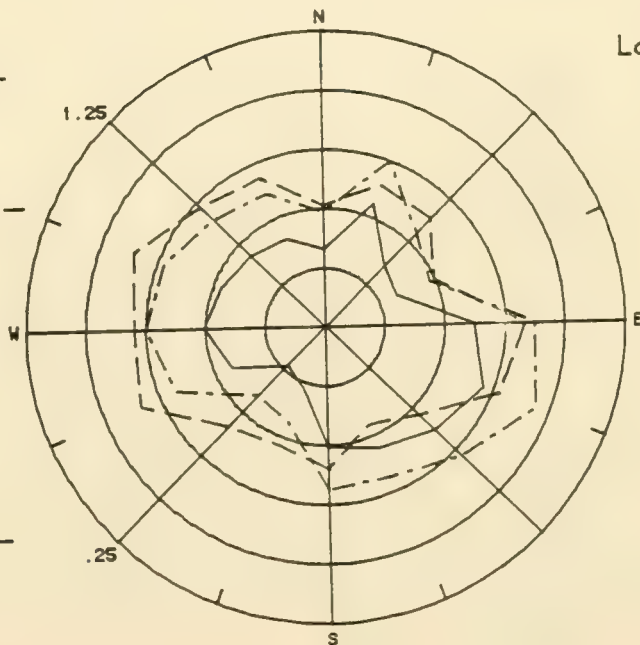
$\frac{U_{mean}}{U_{inf}}$  ———

$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}}$  - - -

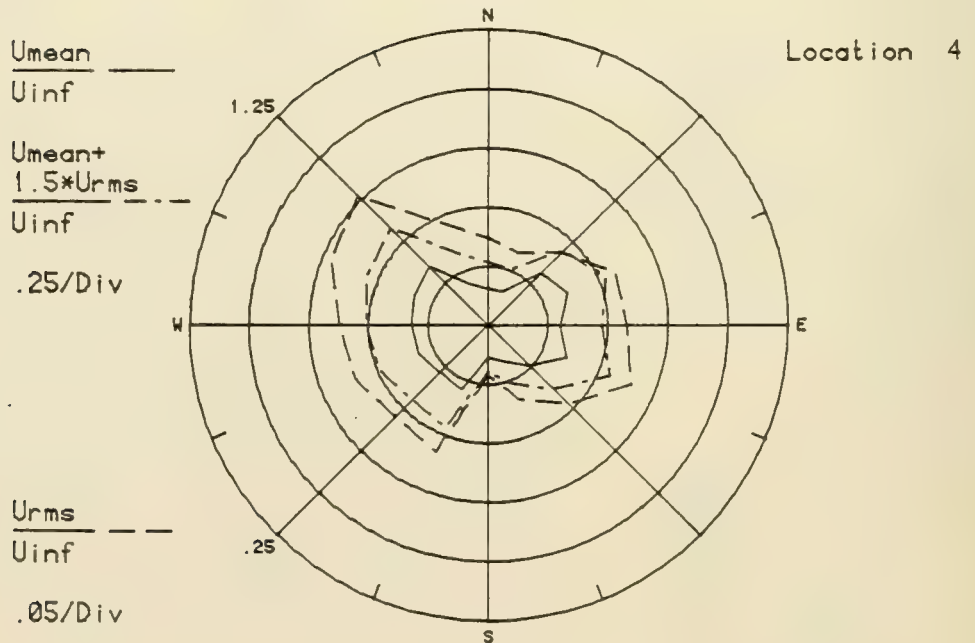
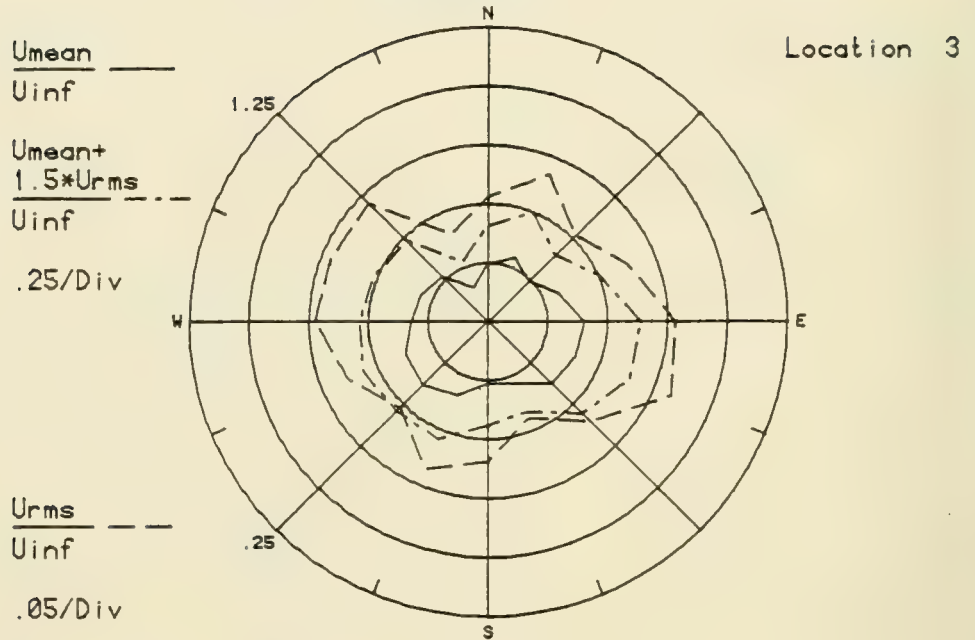
.25/Div

$\frac{U_{rms}}{U_{inf}}$  - - -

.05/Div



# Configuration PRE



# Configuration PRE

Location 5

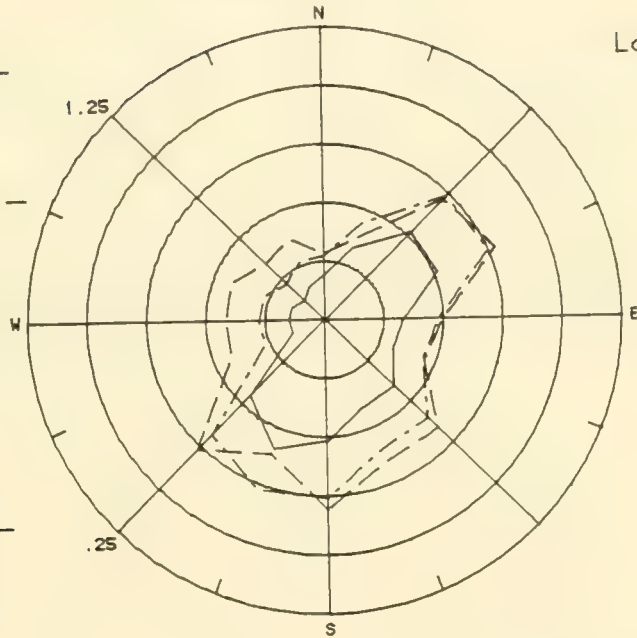
$\frac{U_{mean}}{U_{inf}}$  ———

$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}}$  - - -

.25/Div

$\frac{U_{rms}}{U_{inf}}$  - - -

.05/Div



Location 6

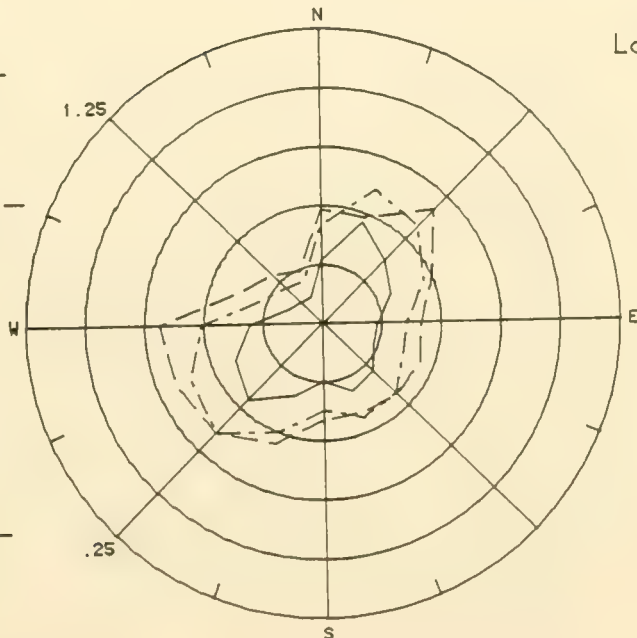
$\frac{U_{mean}}{U_{inf}}$  ———

$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}}$  - - -

.25/Div

$\frac{U_{rms}}{U_{inf}}$  - - -

.05/Div



# Configuration PRE

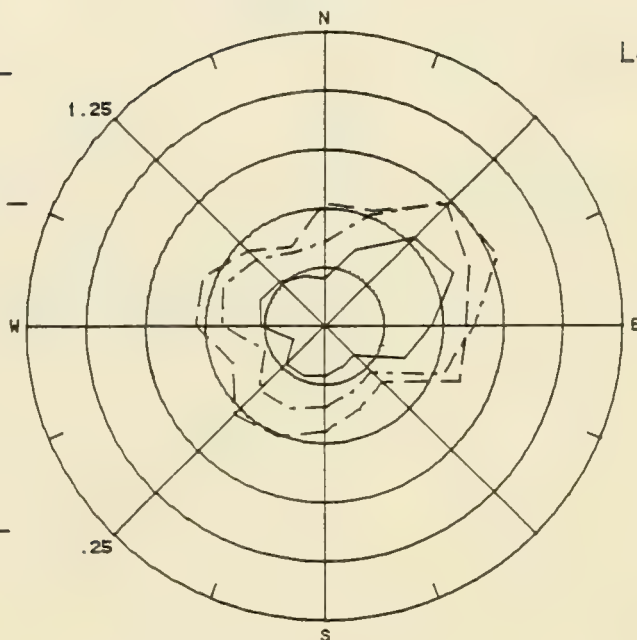
$\frac{U_{mean}}{U_{inf}}$  ———

$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}}$  - - -

.25/Div

$\frac{U_{rms}}{U_{inf}}$  - - -

.05/Div



Location 7

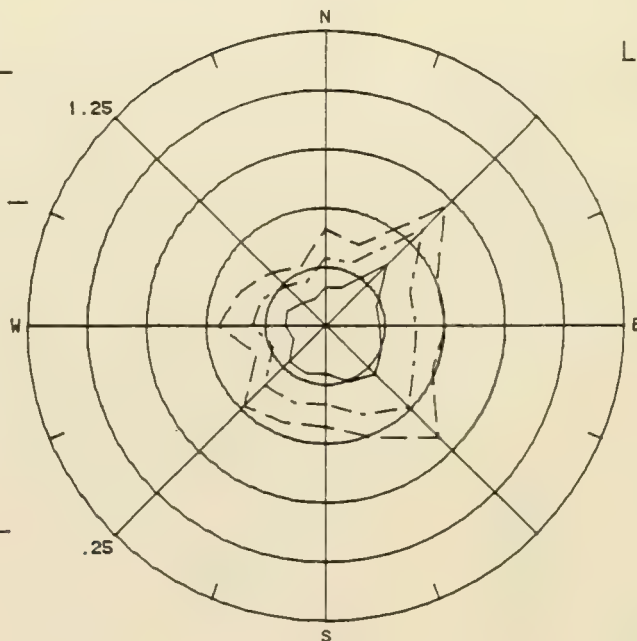
$\frac{U_{mean}}{U_{inf}}$  ———

$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}}$  - - -

.25/Div

$\frac{U_{rms}}{U_{inf}}$  - - -

.05/Div



Location 8

# Configuration PRE

Location 9

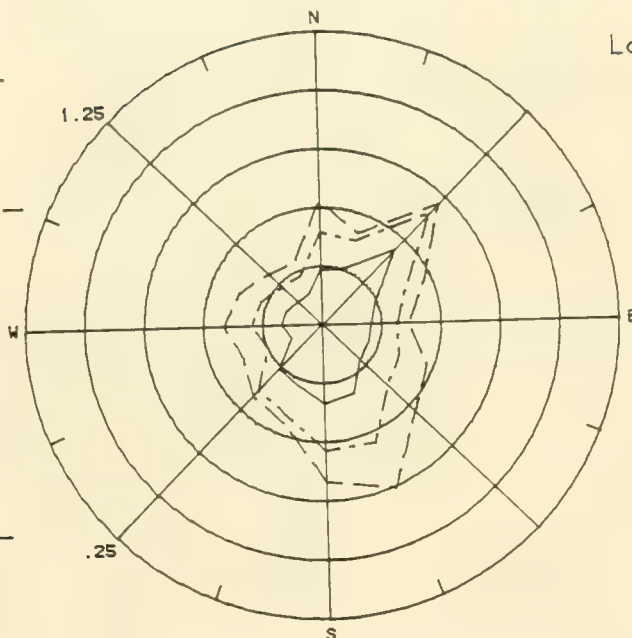
$\frac{U_{mean}}{U_{inf}}$  ———

$\frac{U_{mean} + 1.5 \times U_{rms}}{U_{inf}}$  - - -

.25/Div

$\frac{U_{rms}}{U_{inf}}$  - - -

.05/Div



Location 10

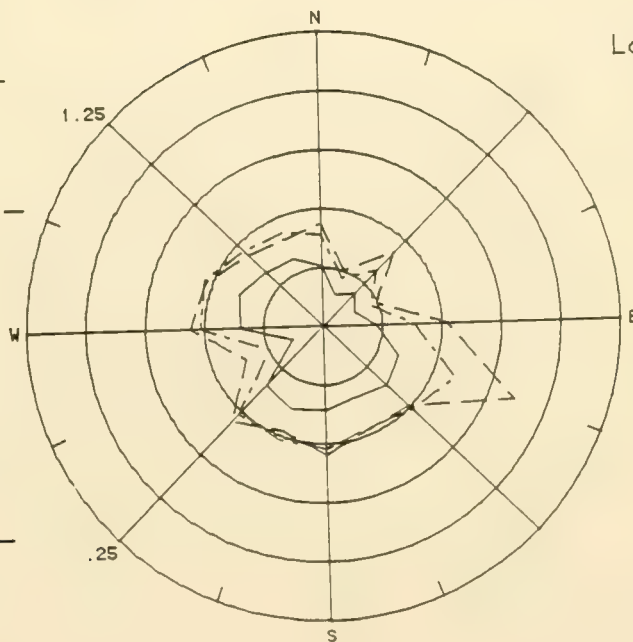
$\frac{U_{mean}}{U_{inf}}$  ———

$\frac{U_{mean} + 1.5 \times U_{rms}}{U_{inf}}$  - - -

.25/Div

$\frac{U_{rms}}{U_{inf}}$  - - -

.05/Div





# Configuration PRE

$$\frac{U_{mean}}{U_{inf}} \text{ ———}$$

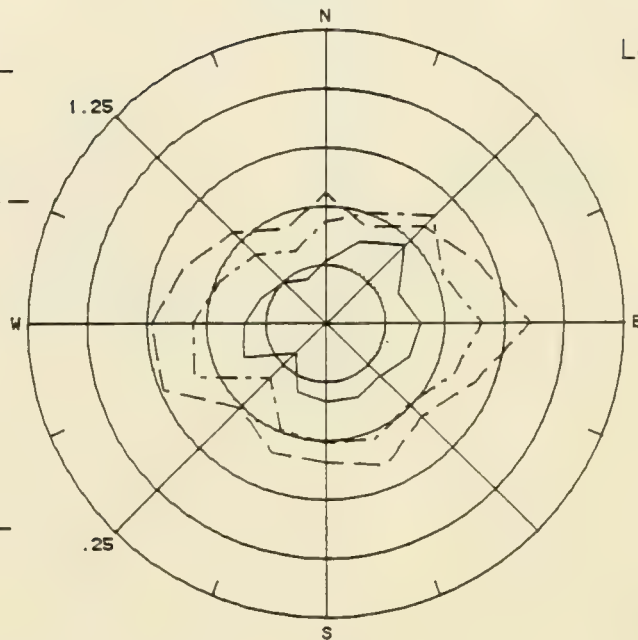
$$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}} \text{ - - -}$$

.25/Div

$$\frac{U_{rms}}{U_{inf}} \text{ - - -}$$

.05/Div

Location 11



$$\frac{U_{mean}}{U_{inf}} \text{ ———}$$

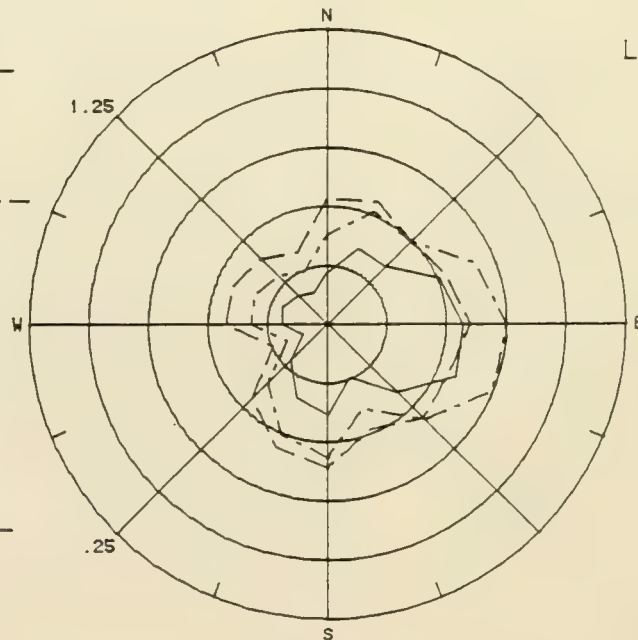
$$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}} \text{ - - -}$$

.25/Div

$$\frac{U_{rms}}{U_{inf}} \text{ - - -}$$

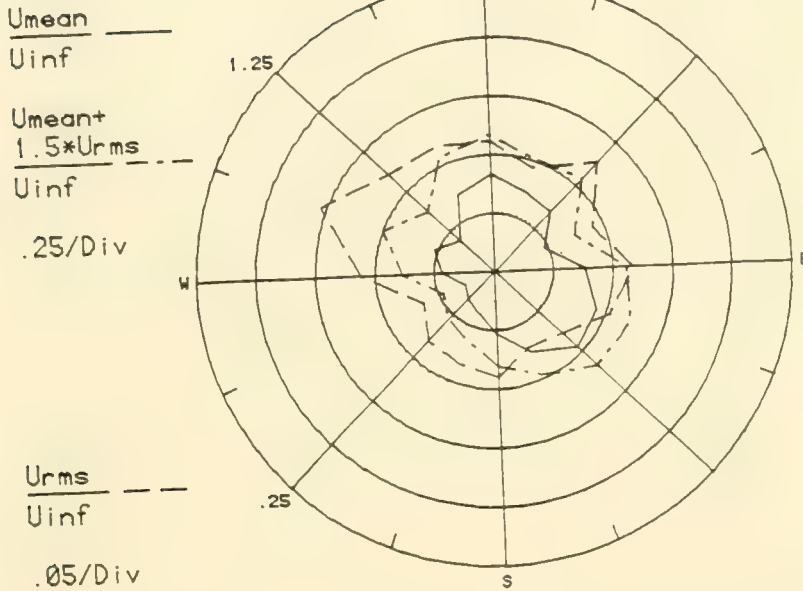
.05/Div

Location 12

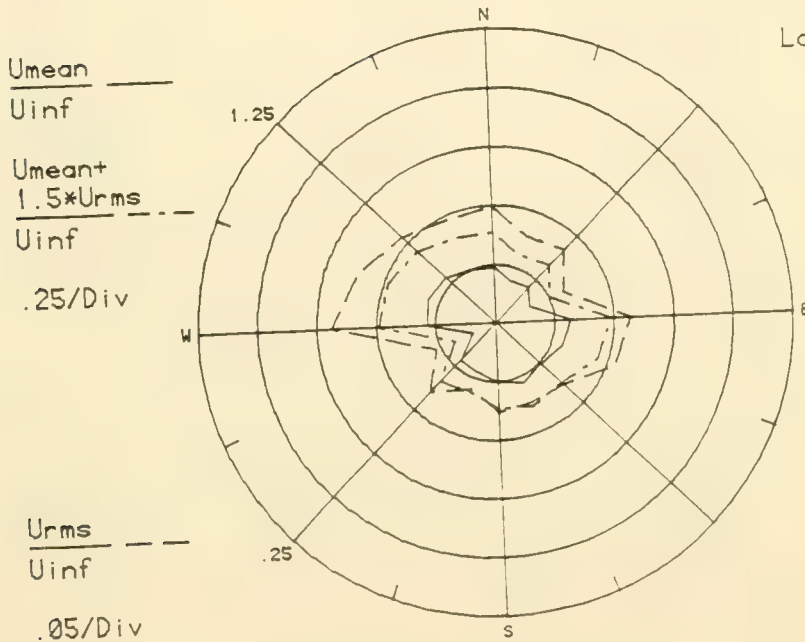


# Configuration PRE

Location 13



Location 14



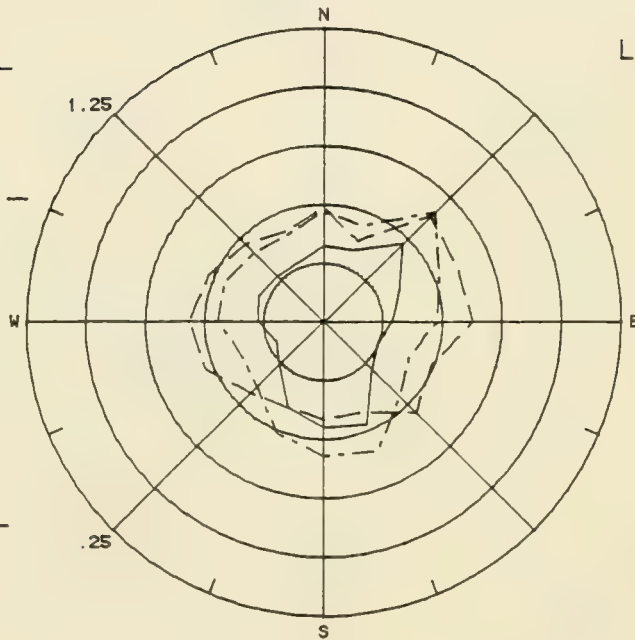
# Configuration PRE

$\frac{U_{mean}}{U_{inf}}$  \_\_\_\_\_

Location 15

$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}}$  - - - -

.25/Div



$\frac{U_{rms}}{U_{inf}}$  - - - -

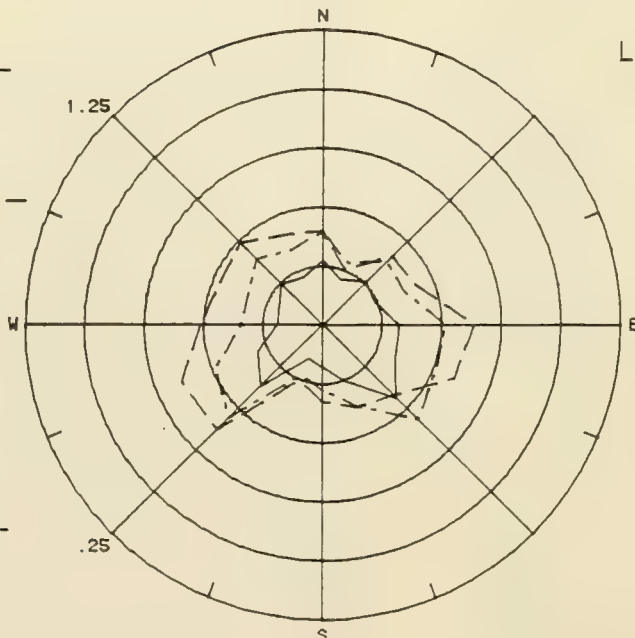
.05/Div

$\frac{U_{mean}}{U_{inf}}$  \_\_\_\_\_

Location 16

$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}}$  - - - -

.25/Div



$\frac{U_{rms}}{U_{inf}}$  - - - -

.05/Div

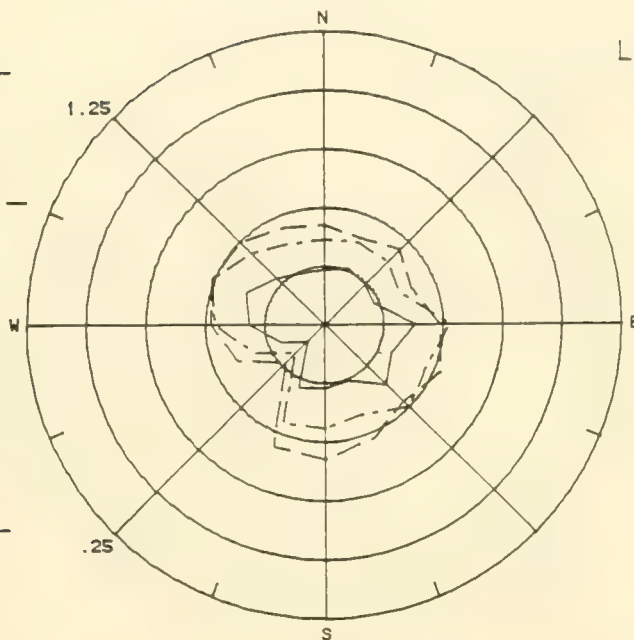
# Configuration PRE

$\frac{U_{mean}}{U_{inf}}$  ———

Location 17

$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}}$  - - -

.25/Div



$\frac{U_{rms}}{U_{inf}}$  - - -

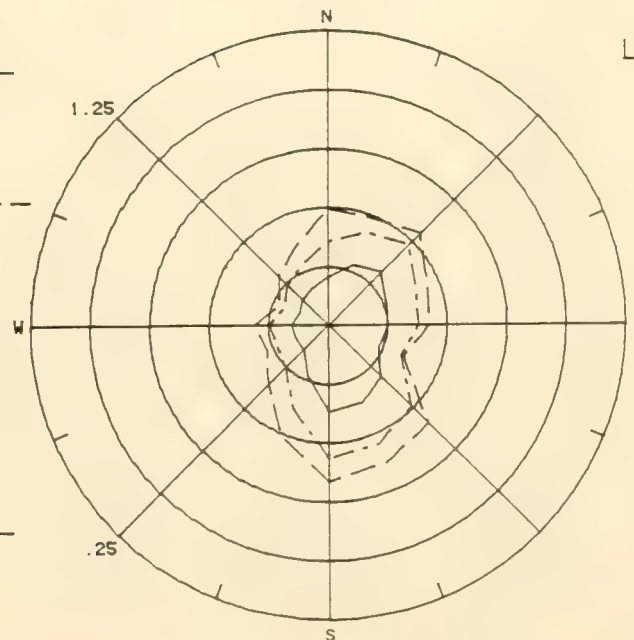
.05/Div

$\frac{U_{mean}}{U_{inf}}$  ———

Location 18

$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}}$  - - -

.25/Div



$\frac{U_{rms}}{U_{inf}}$  - - -

.05/Div

# Configuration PRE

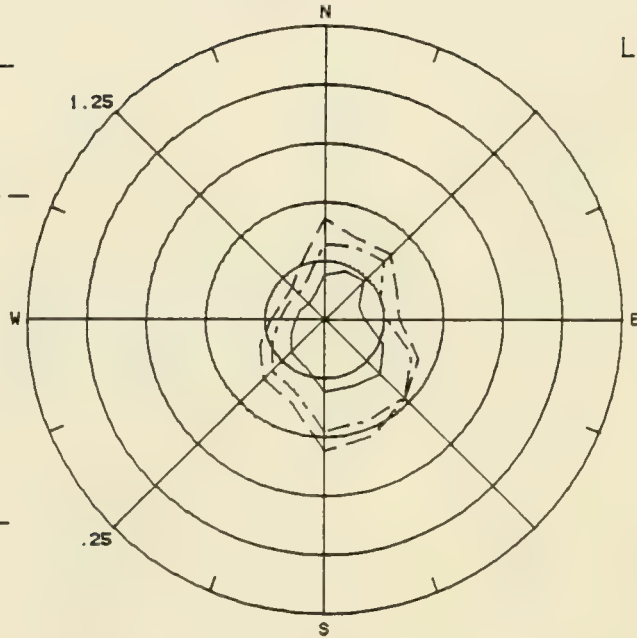
$$\frac{U_{mean}}{U_{inf}} \text{ ---}$$

$$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}} \text{ ---}$$

.25/Div

$$\frac{U_{rms}}{U_{inf}} \text{ ---}$$

.05/Div



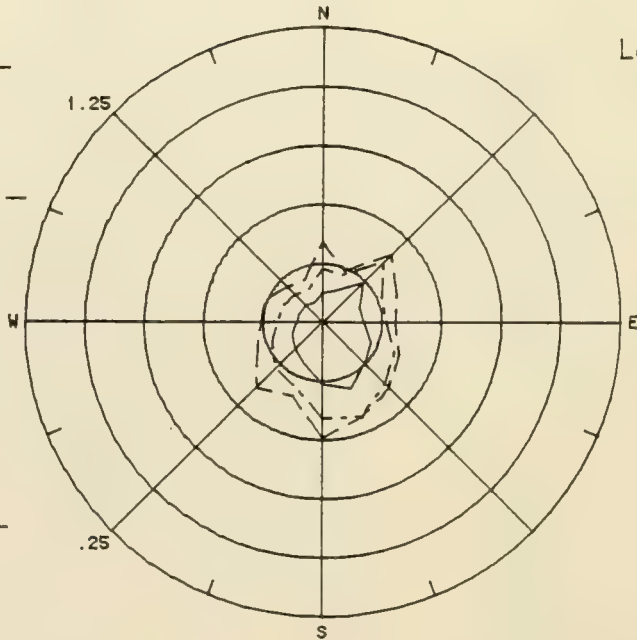
$$\frac{U_{mean}}{U_{inf}} \text{ ---}$$

$$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}} \text{ ---}$$

.25/Div

$$\frac{U_{rms}}{U_{inf}} \text{ ---}$$

.05/Div





# Configuration PRE

Location 21

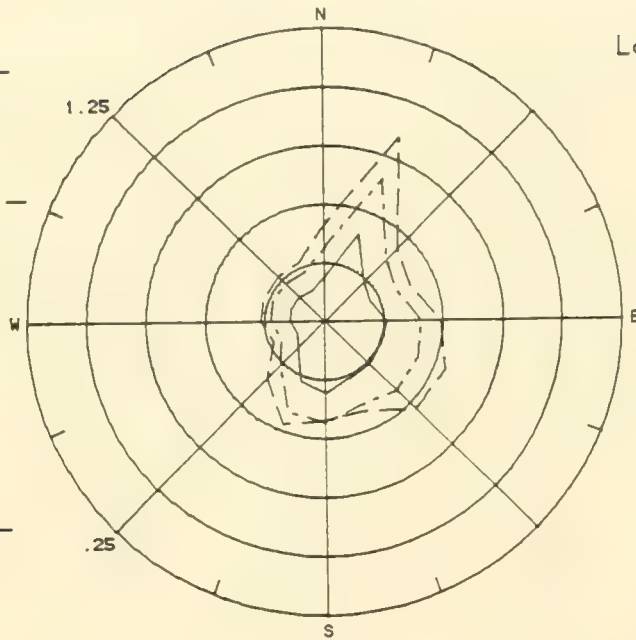
$$\frac{U_{mean}}{U_{inf}} \text{ ---}$$

$$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}} \text{ ---}$$

.25/Div

$$\frac{U_{rms}}{U_{inf}} \text{ ---}$$

.05/Div



Location 22

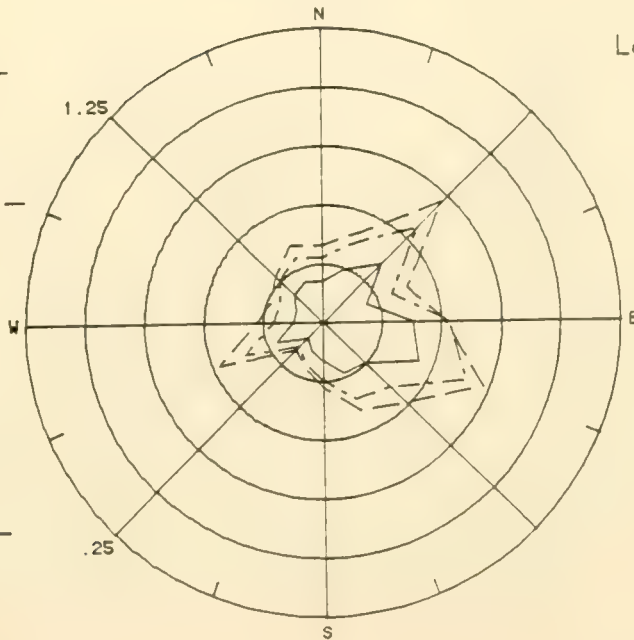
$$\frac{U_{mean}}{U_{inf}} \text{ ---}$$

$$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}} \text{ ---}$$

.25/Div

$$\frac{U_{rms}}{U_{inf}} \text{ ---}$$

.05/Div



# Configuration PRE

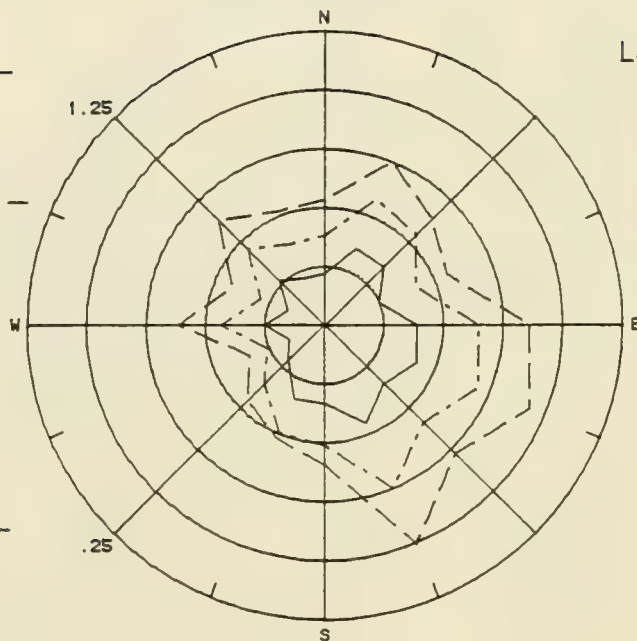
$\frac{U_{mean}}{U_{inf}}$  ———

$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}}$  - - -

.25/Div

$\frac{U_{rms}}{U_{inf}}$  - - -

.05/Div



Location 23

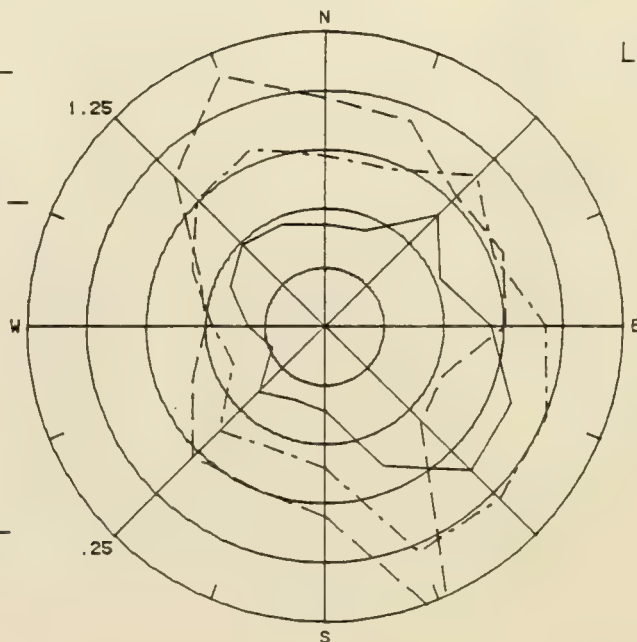
$\frac{U_{mean}}{U_{inf}}$  ———

$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}}$  - - -

.25/Div

$\frac{U_{rms}}{U_{inf}}$  - - -

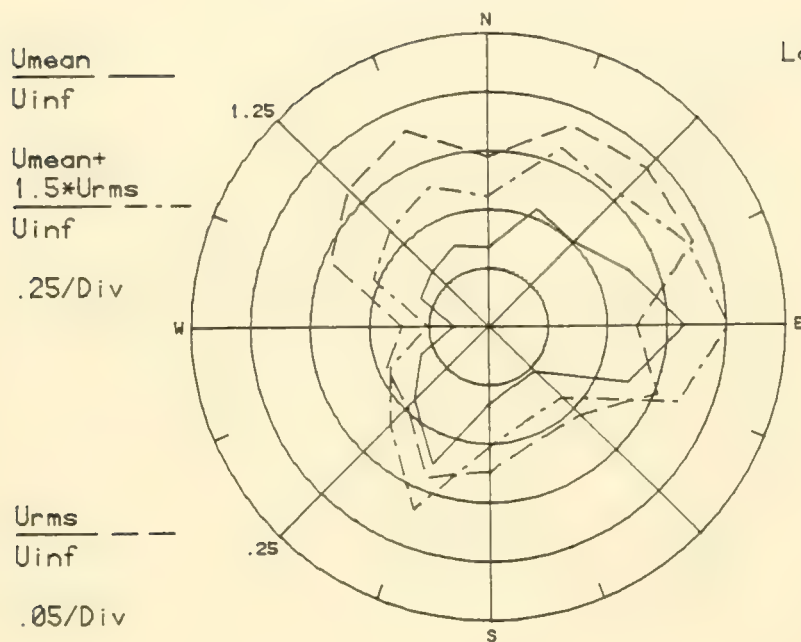
.05/Div



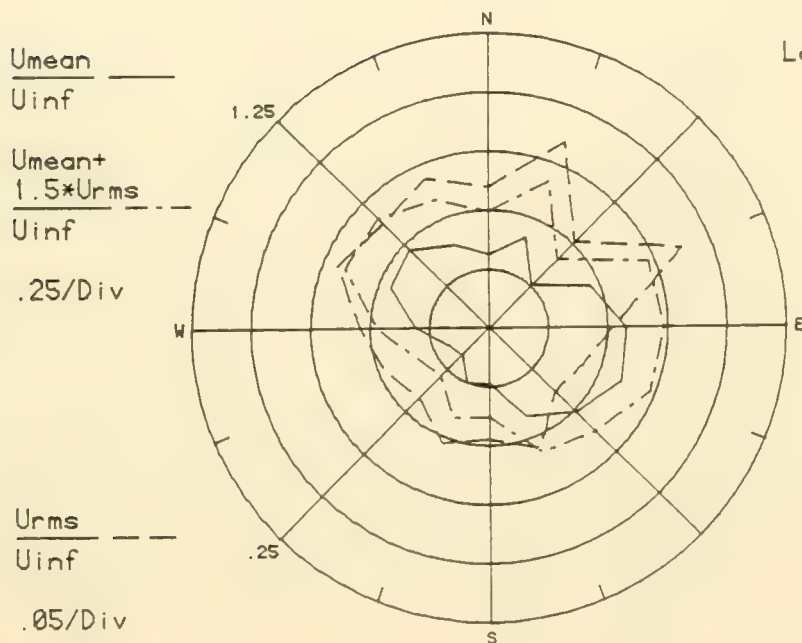
Location 24

# Configuration PRE

Location 25



Location 26



# Configuration PRE

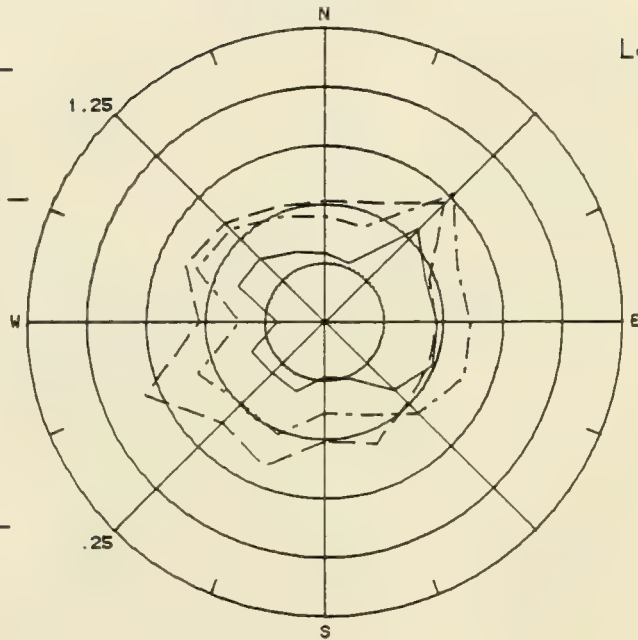
$\frac{U_{mean}}{U_{inf}}$  ———

$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}}$  - - -

.25/Div

$\frac{U_{rms}}{U_{inf}}$  - - -

.05/Div



Location 27

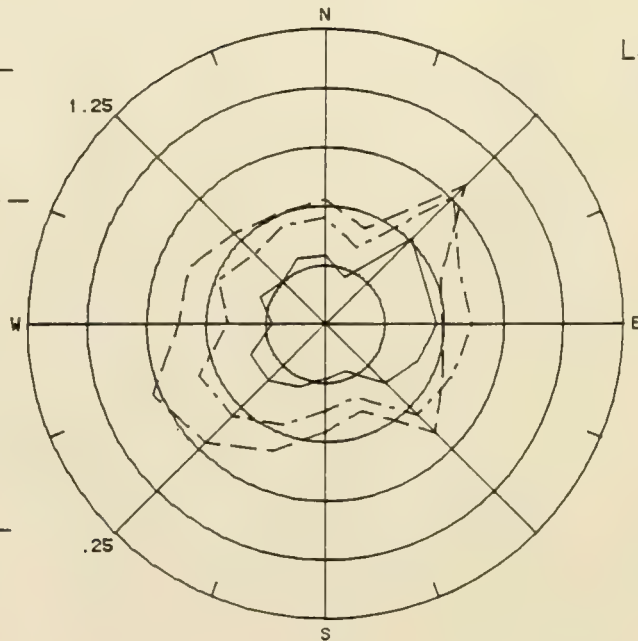
$\frac{U_{mean}}{U_{inf}}$  ———

$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}}$  - - -

.25/Div

$\frac{U_{rms}}{U_{inf}}$  - - -

.05/Div



Location 28

# Configuration PRE

Location 29

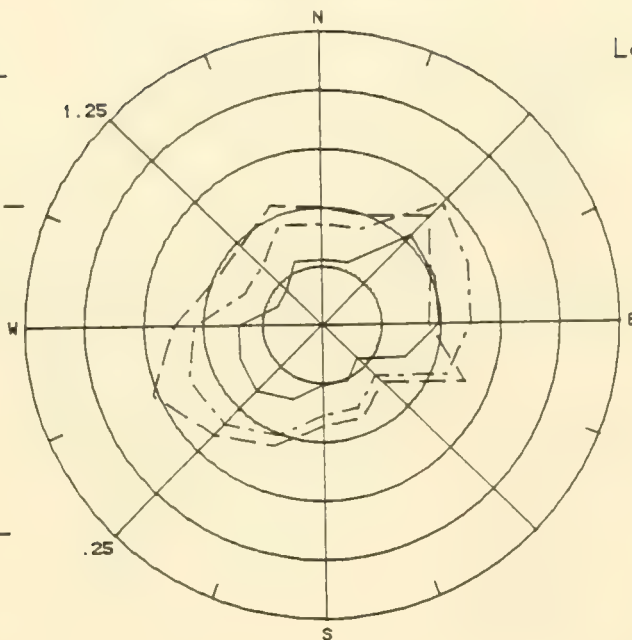
$$\frac{U_{mean}}{U_{inf}} \text{ ———}$$

$$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}} \text{ - - -}$$

.25/Div

$$\frac{U_{rms}}{U_{inf}} \text{ - - -}$$

.05/Div



Location 30

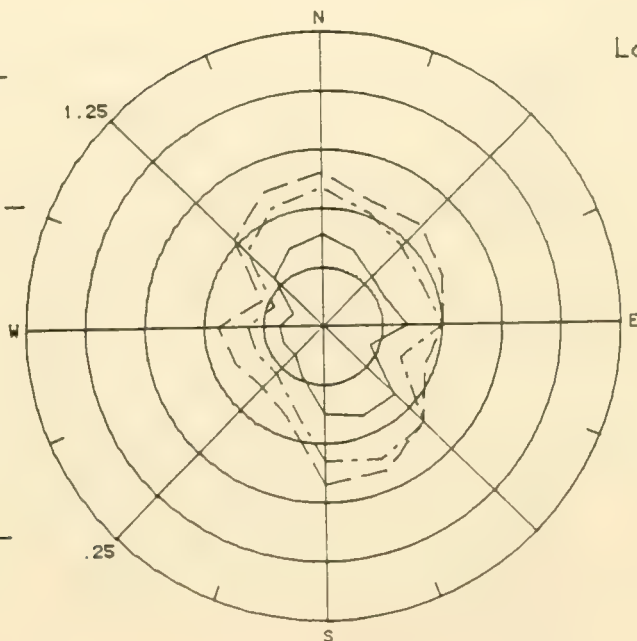
$$\frac{U_{mean}}{U_{inf}} \text{ ———}$$

$$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}} \text{ - - -}$$

.25/Div

$$\frac{U_{rms}}{U_{inf}} \text{ - - -}$$

.05/Div



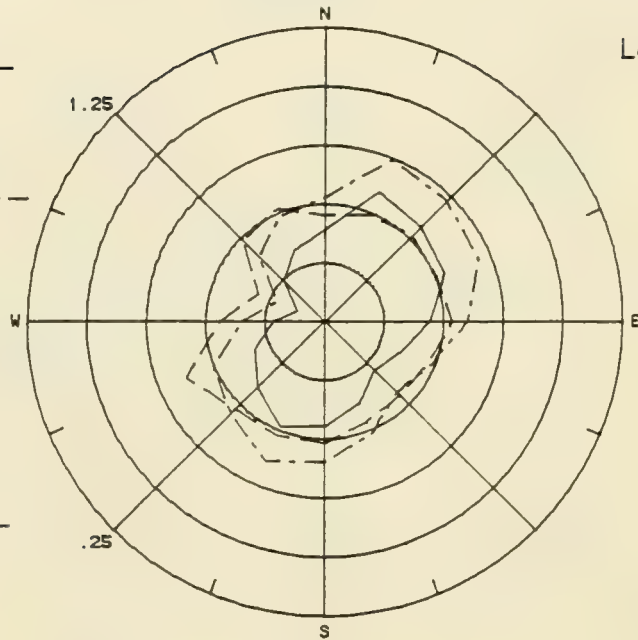


# Configuration PRE

$\frac{U_{mean}}{U_{inf}}$  ———

$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}}$  - - -  
 .25/Div

$\frac{U_{rms}}{U_{inf}}$  - - -  
 .05/Div

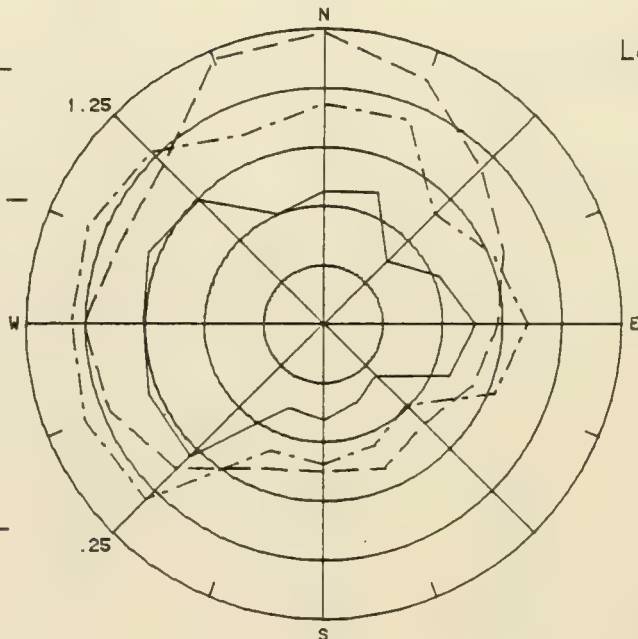


Location 31

$\frac{U_{mean}}{U_{inf}}$  ———

$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}}$  - - -  
 .25/Div

$\frac{U_{rms}}{U_{inf}}$  - - -  
 .05/Div



Location 32

# Configuration PRE

Location 33

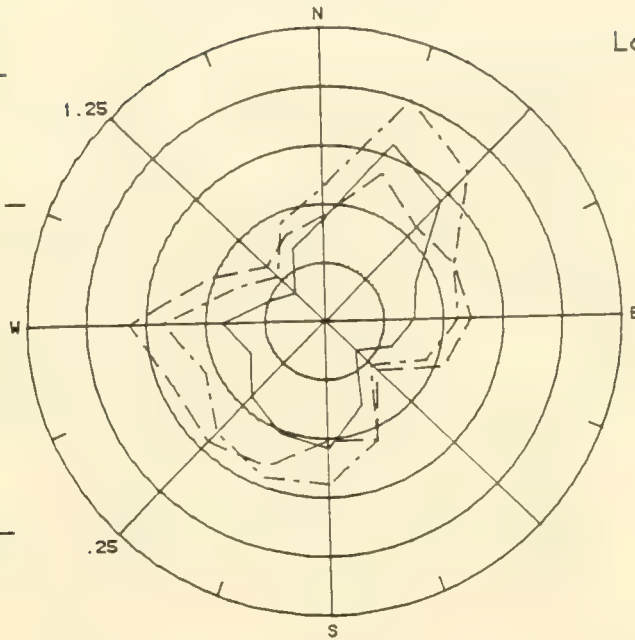
$\frac{U_{mean}}{U_{inf}}$  ———

$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}}$  - - -

.25/Div

$\frac{U_{rms}}{U_{inf}}$  - - -

.05/Div



Location 34

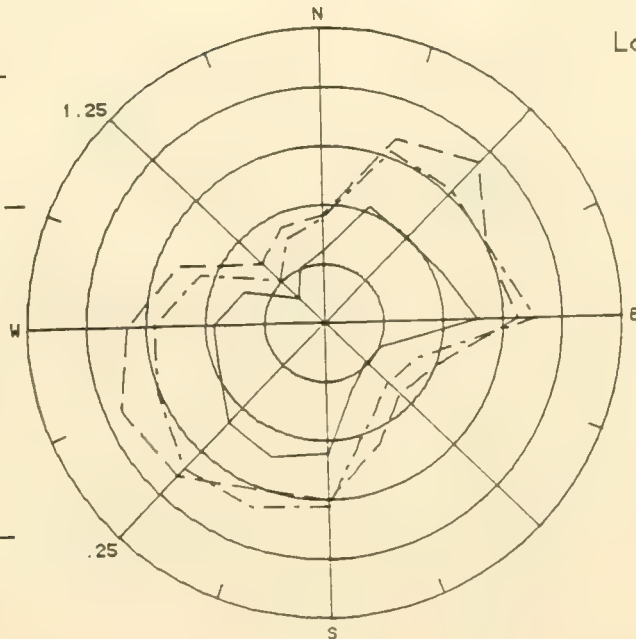
$\frac{U_{mean}}{U_{inf}}$  ———

$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}}$  - - -

.25/Div

$\frac{U_{rms}}{U_{inf}}$  - - -

.05/Div



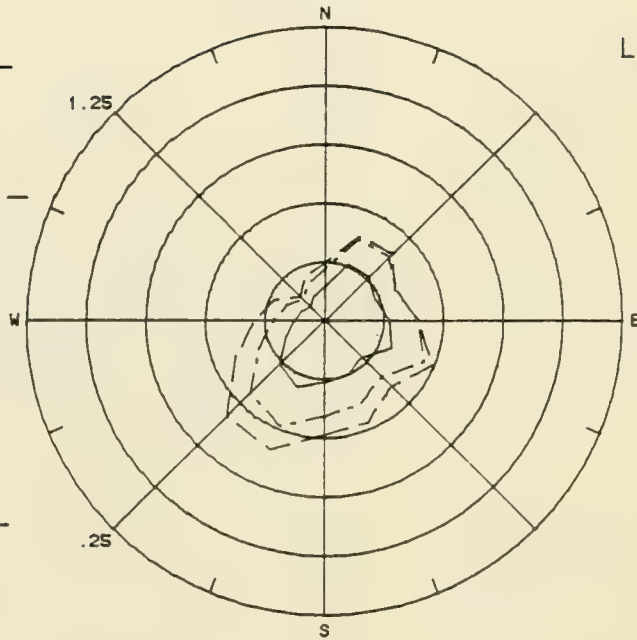
# Configuration PRE

$$\frac{U_{mean}}{U_{inf}} \text{ ———}$$

Location 35

$$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}} \text{ - - -}$$

.25/Div



$$\frac{U_{rms}}{U_{inf}} \text{ - - -}$$

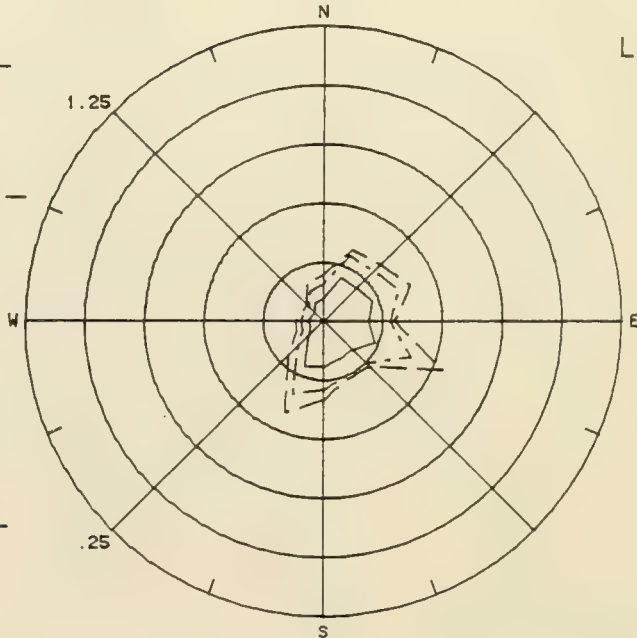
.05/Div

$$\frac{U_{mean}}{U_{inf}} \text{ ———}$$

Location 36

$$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}} \text{ - - -}$$

.25/Div



$$\frac{U_{rms}}{U_{inf}} \text{ - - -}$$

.05/Div

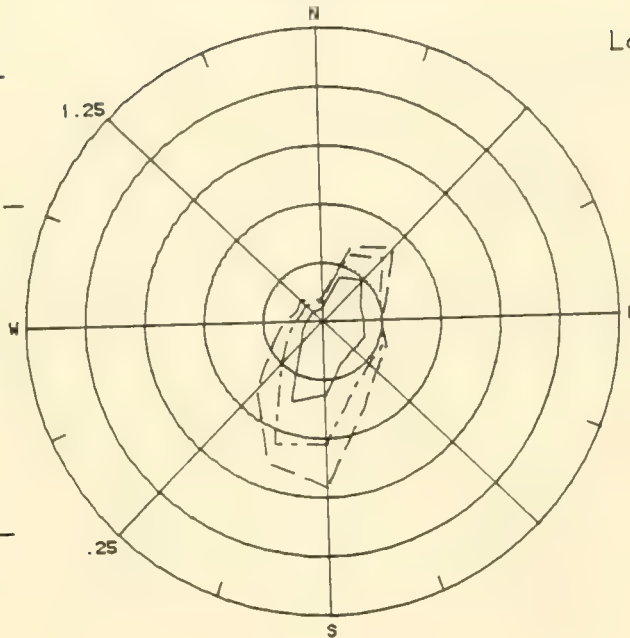
# Configuration PRE

Location 37

$$\frac{U_{mean}}{U_{inf}} \text{ ———}$$

$$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}} \text{ - - -}$$

.25/Div



$$\frac{U_{rms}}{U_{inf}} \text{ - - -}$$

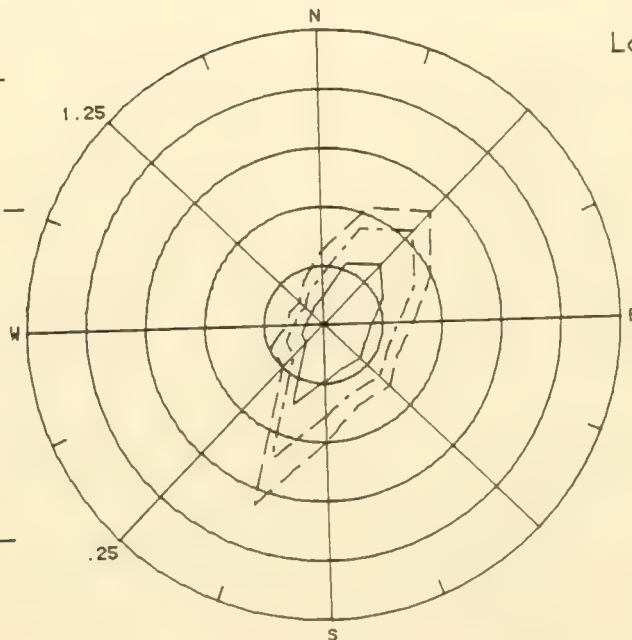
.05/Div

Location 38

$$\frac{U_{mean}}{U_{inf}} \text{ ———}$$

$$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}} \text{ - - -}$$

.25/Div



$$\frac{U_{rms}}{U_{inf}} \text{ - - -}$$

.05/Div

# Configuration PRE

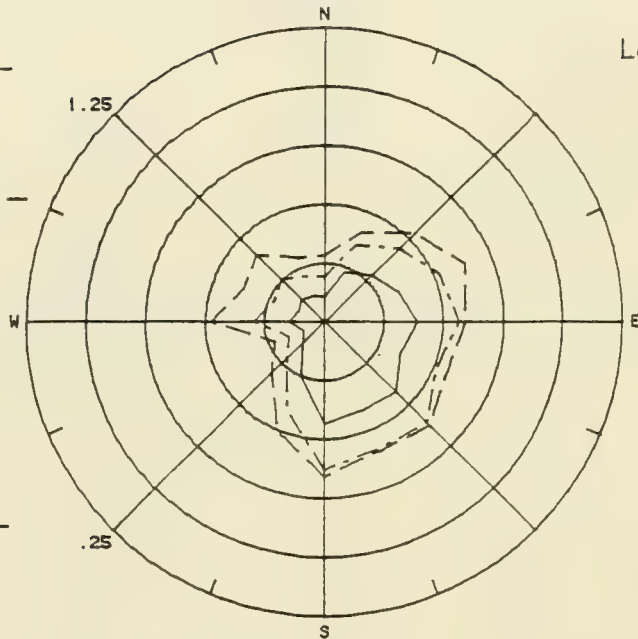
$\frac{U_{mean}}{U_{inf}}$  \_\_\_\_\_

$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}}$  - - - -

.25/Div

$\frac{U_{rms}}{U_{inf}}$  - - - -

.05/Div



Location 39

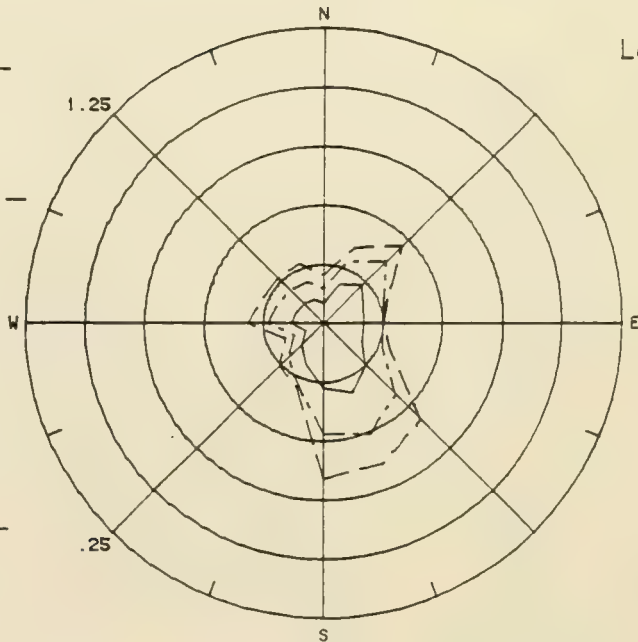
$\frac{U_{mean}}{U_{inf}}$  \_\_\_\_\_

$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}}$  - - - -

.25/Div

$\frac{U_{rms}}{U_{inf}}$  - - - -

.05/Div



Location 40



# Configuration PRE

Location 43

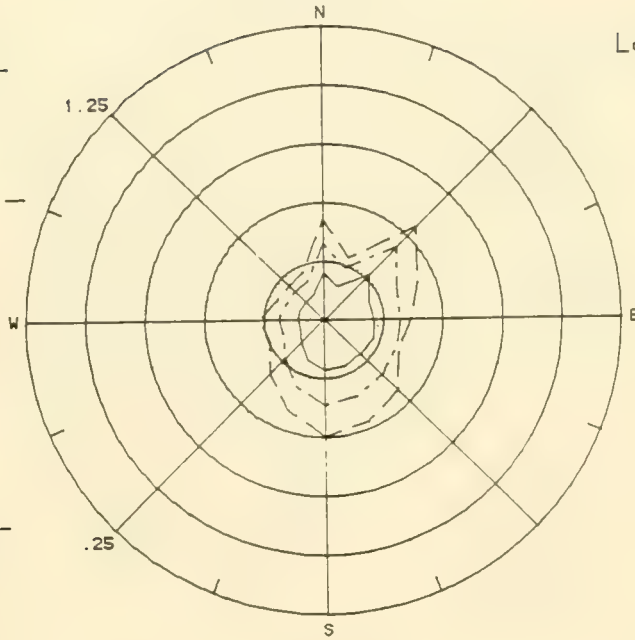
$\frac{U_{mean}}{U_{inf}}$  ———

$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}}$  - - -

.25/Div

$\frac{U_{rms}}{U_{inf}}$  - - -

.05/Div



Location 44

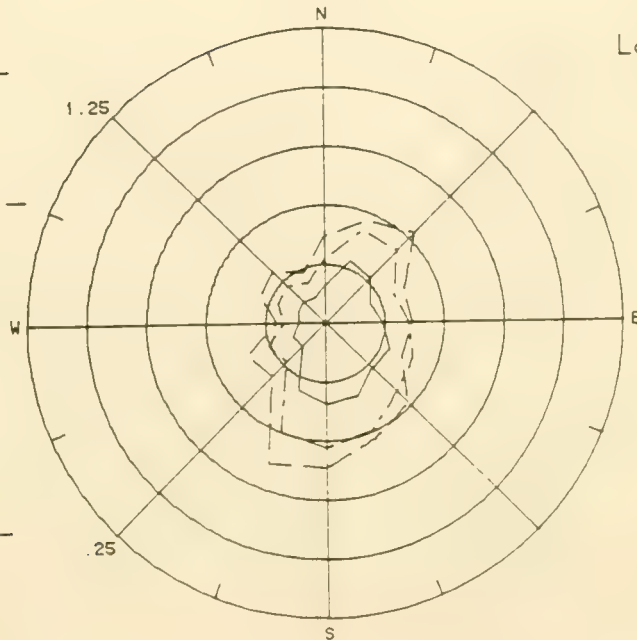
$\frac{U_{mean}}{U_{inf}}$  ———

$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}}$  - - -

.25/Div

$\frac{U_{rms}}{U_{inf}}$  - - -

.05/Div



# Configuration PRE

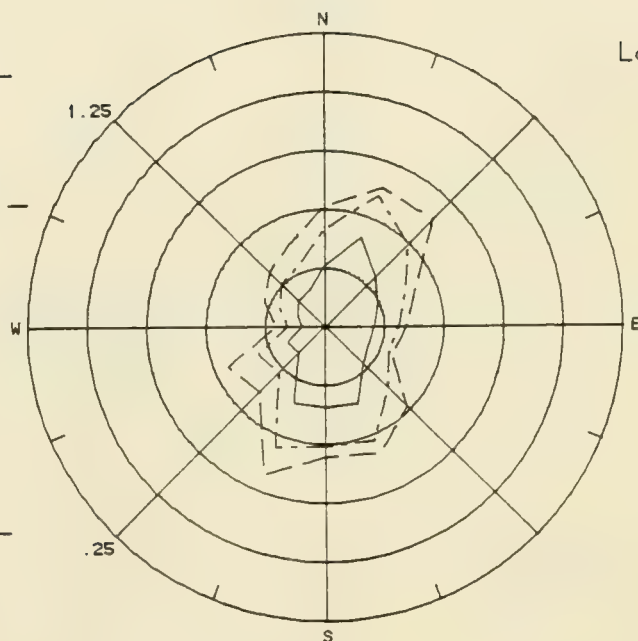
$\frac{U_{mean}}{U_{inf}}$  ———

$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}}$  - - -

.25/Div

$\frac{U_{rms}}{U_{inf}}$  - - -

.05/Div



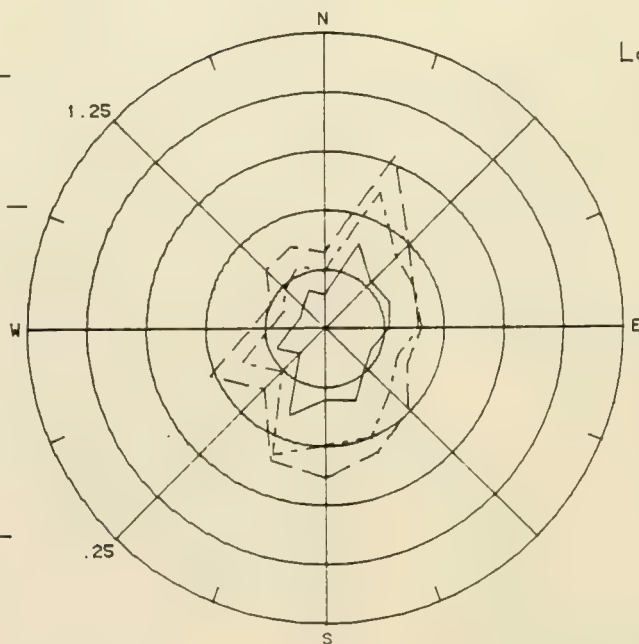
$\frac{U_{mean}}{U_{inf}}$  ———

$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}}$  - - -

.25/Div

$\frac{U_{rms}}{U_{inf}}$  - - -

.05/Div



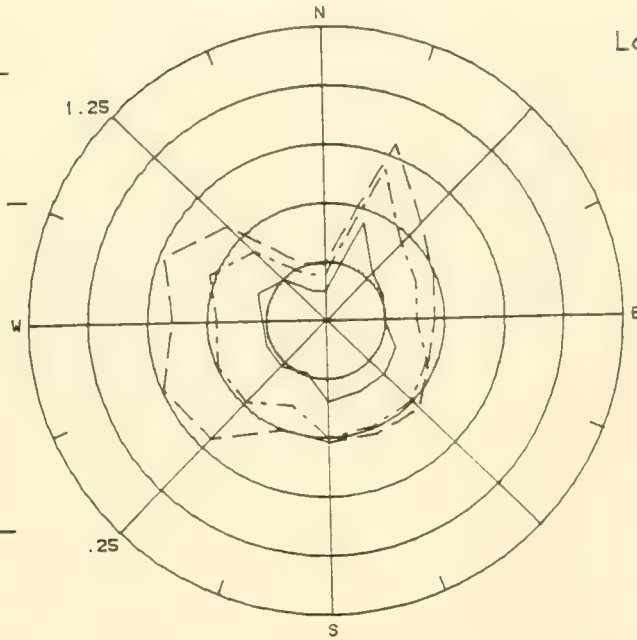
# Configuration PRE

Location 47

$$\frac{U_{mean}}{U_{inf}} \text{ ---}$$

$$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}} \text{ ---}$$

.25/Div



$$\frac{U_{rms}}{U_{inf}} \text{ ---}$$

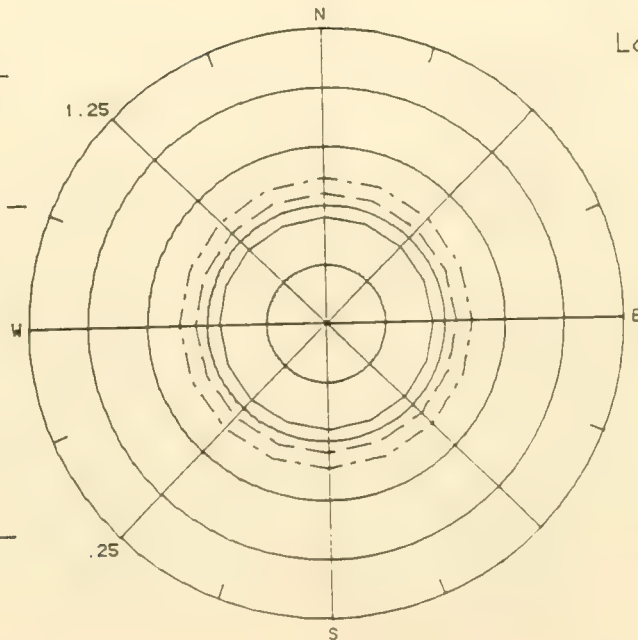
.05/Div

Location 48

$$\frac{U_{mean}}{U_{inf}} \text{ ---}$$

$$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}} \text{ ---}$$

.25/Div



$$\frac{U_{rms}}{U_{inf}} \text{ ---}$$

.05/Div

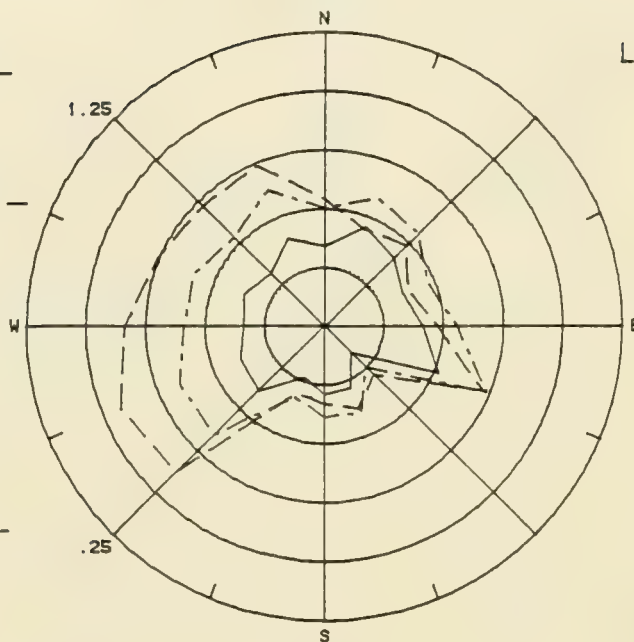
# Configuration PH1

$\frac{U_{mean}}{U_{inf}}$  ———

Location 1

$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}}$  - - -

.25/Div



$\frac{U_{rms}}{U_{inf}}$  - - -

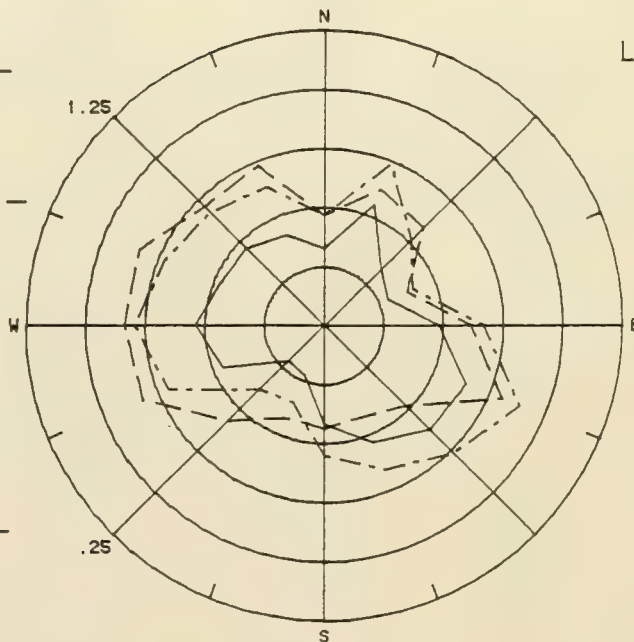
.05/Div

$\frac{U_{mean}}{U_{inf}}$  ———

Location 2

$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}}$  - - -

.25/Div



$\frac{U_{rms}}{U_{inf}}$  - - -

.05/Div

# Configuration PH1

Location 3

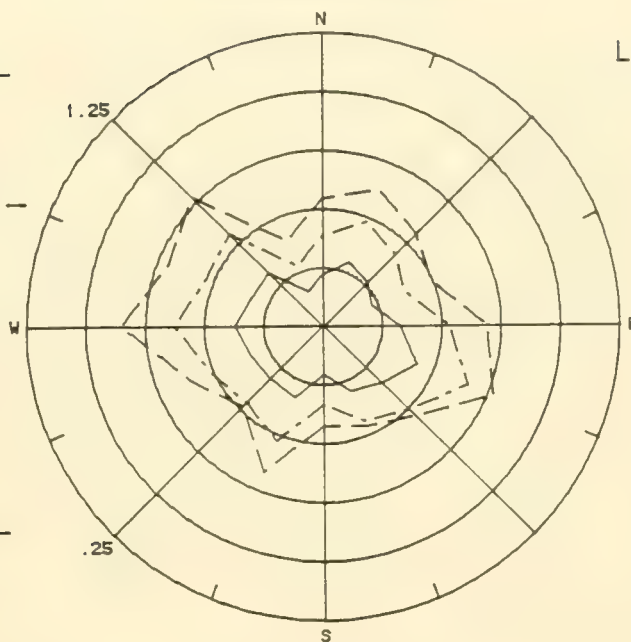
$\frac{U_{mean}}{U_{inf}}$  ———

$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}}$  - - -

.25/Div

$\frac{U_{rms}}{U_{inf}}$  - - -

.05/Div



Location 4

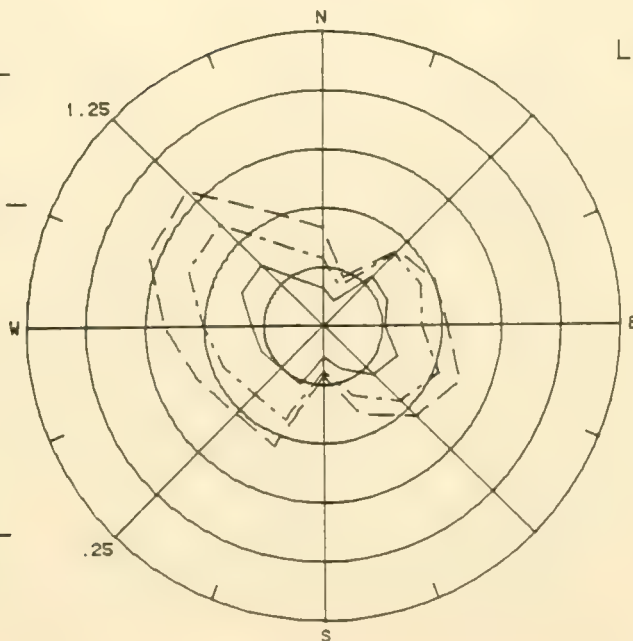
$\frac{U_{mean}}{U_{inf}}$  ———

$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}}$  - - -

.25/Div

$\frac{U_{rms}}{U_{inf}}$  - - -

.05/Div





# Configuration PH1

Location 5

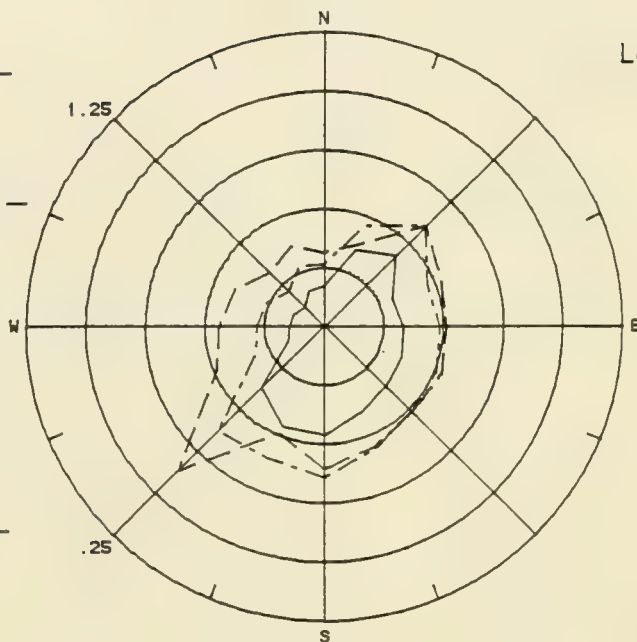
$\frac{U_{mean}}{U_{inf}}$  ———

$\frac{U_{mean} + 1.5 * U_{rms}}{U_{inf}}$  - - -

.25/Div

$\frac{U_{rms}}{U_{inf}}$  - - -

.05/Div



Location 6

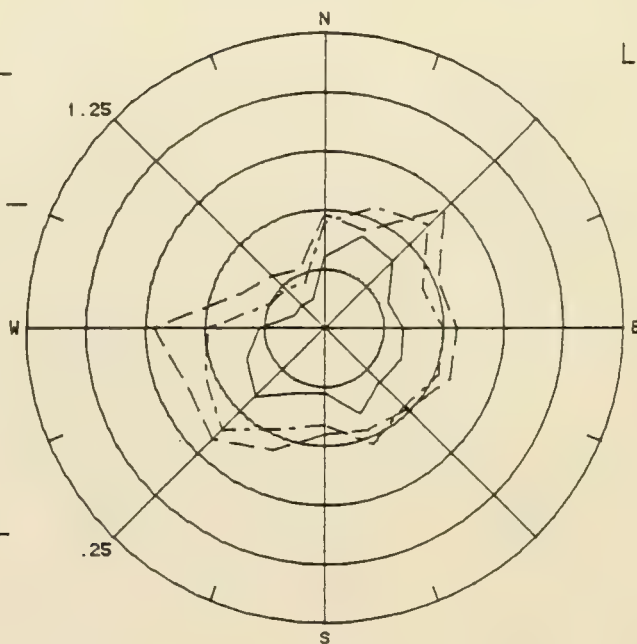
$\frac{U_{mean}}{U_{inf}}$  ———

$\frac{U_{mean} + 1.5 * U_{rms}}{U_{inf}}$  - - -

.25/Div

$\frac{U_{rms}}{U_{inf}}$  - - -

.05/Div

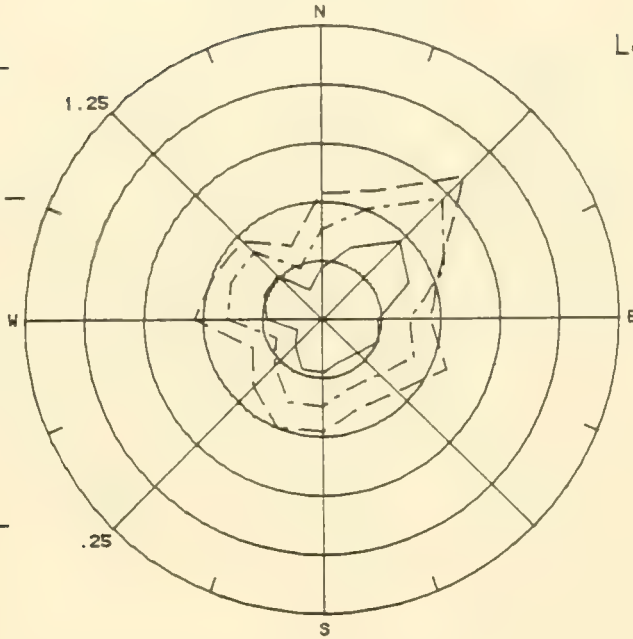


# Configuration PH1

$\frac{U_{mean}}{U_{inf}}$  ———

Location 7

$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}}$  - - -  
 .25/Div

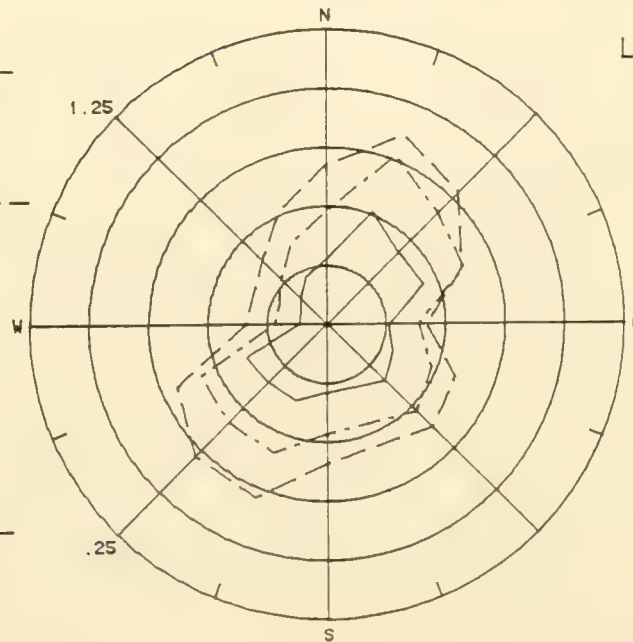


$\frac{U_{rms}}{U_{inf}}$  - - -  
 .05/Div

$\frac{U_{mean}}{U_{inf}}$  ———

Location 8

$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}}$  - - -  
 .25/Div



$\frac{U_{rms}}{U_{inf}}$  - - -  
 .05/Div

# Configuration PH1

$\frac{U_{mean}}{U_{inf}}$  ———

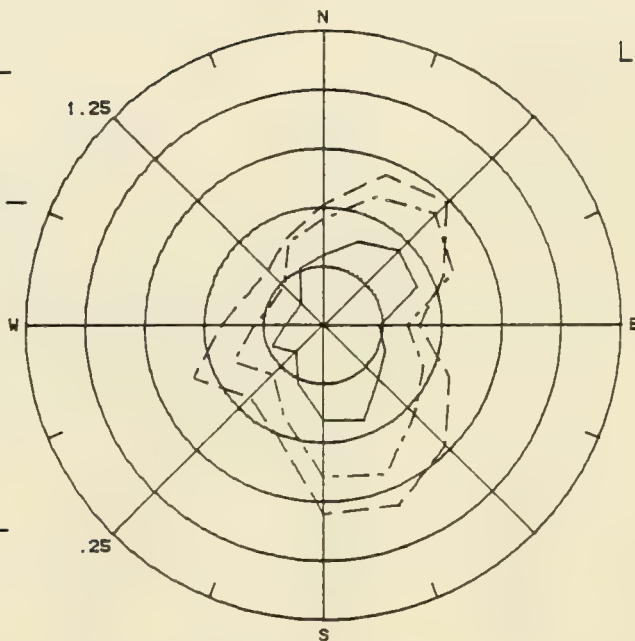
$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}}$  - - -

.25/Div

$\frac{U_{rms}}{U_{inf}}$  - - -

.05/Div

Location 9



$\frac{U_{mean}}{U_{inf}}$  ———

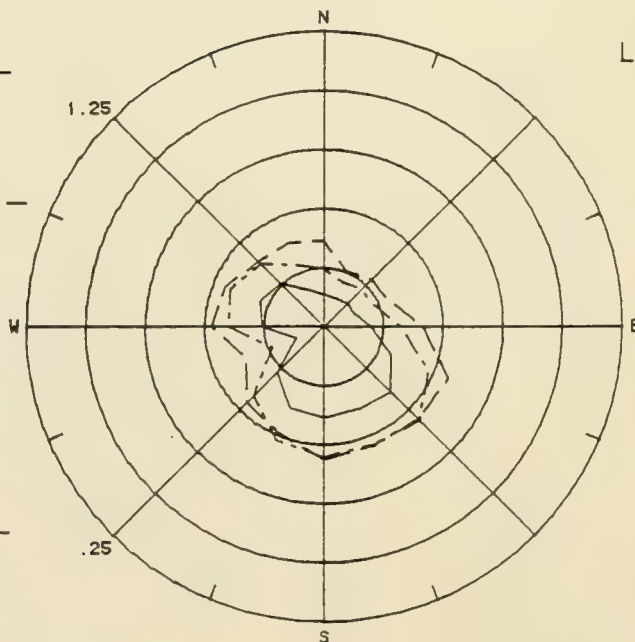
$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}}$  - - -

.25/Div

$\frac{U_{rms}}{U_{inf}}$  - - -

.05/Div

Location 10



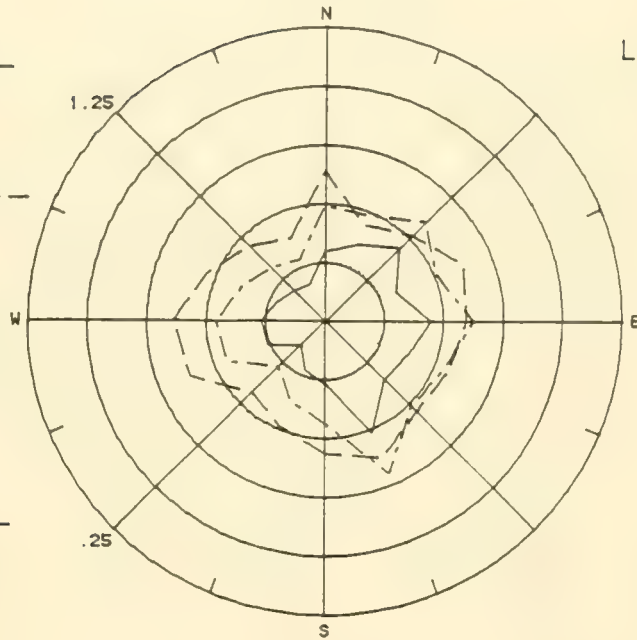
# Configuration PH1

$\frac{U_{mean}}{U_{inf}}$  ———

Location 11

$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}}$  - - -

.25/Div



$\frac{U_{rms}}{U_{inf}}$  - - -

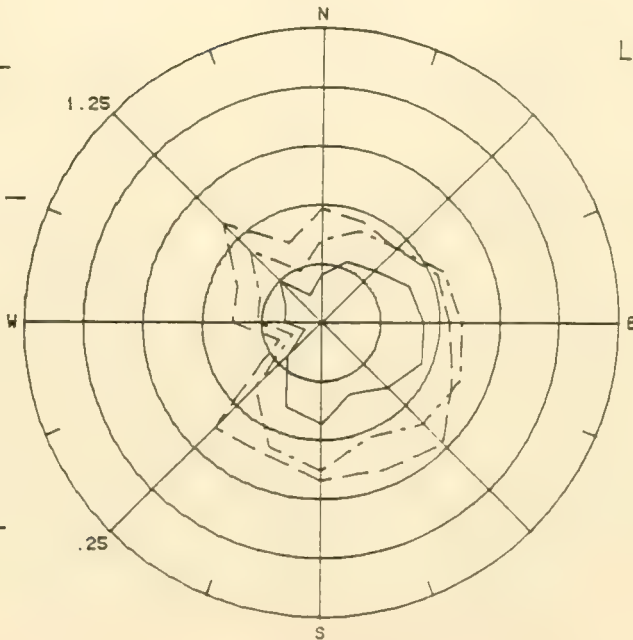
.05/Div

$\frac{U_{mean}}{U_{inf}}$  ———

Location 12

$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}}$  - - -

.25/Div



$\frac{U_{rms}}{U_{inf}}$  - - -

.05/Div

# Configuration PH1

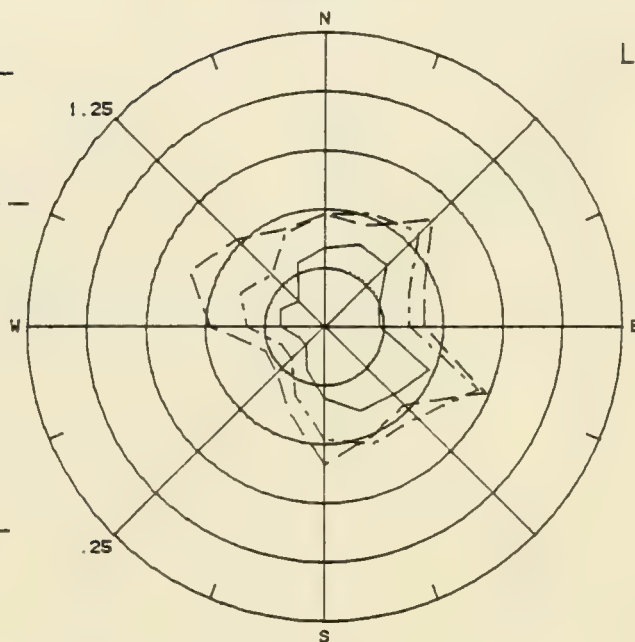
$\frac{U_{mean}}{U_{inf}}$  ———

$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}}$  - - -

.25/Div

$\frac{U_{rms}}{U_{inf}}$  - - -

.05/Div



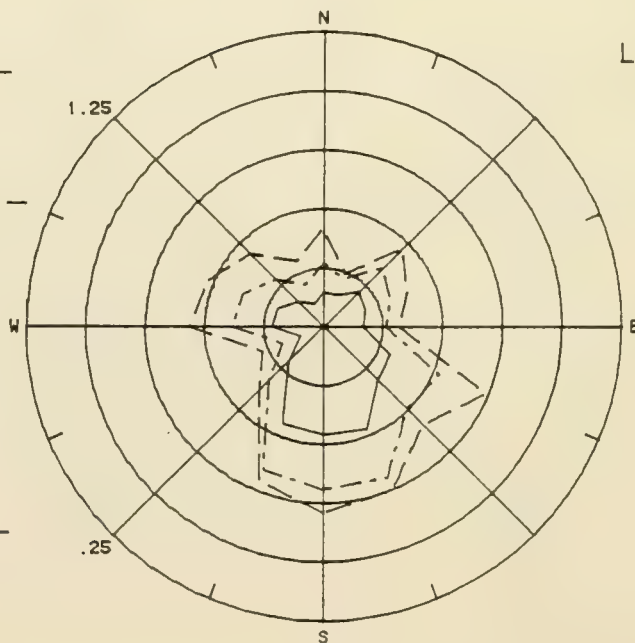
$\frac{U_{mean}}{U_{inf}}$  ———

$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}}$  - - -

.25/Div

$\frac{U_{rms}}{U_{inf}}$  - - -

.05/Div





# Configuration PH1

Location 15

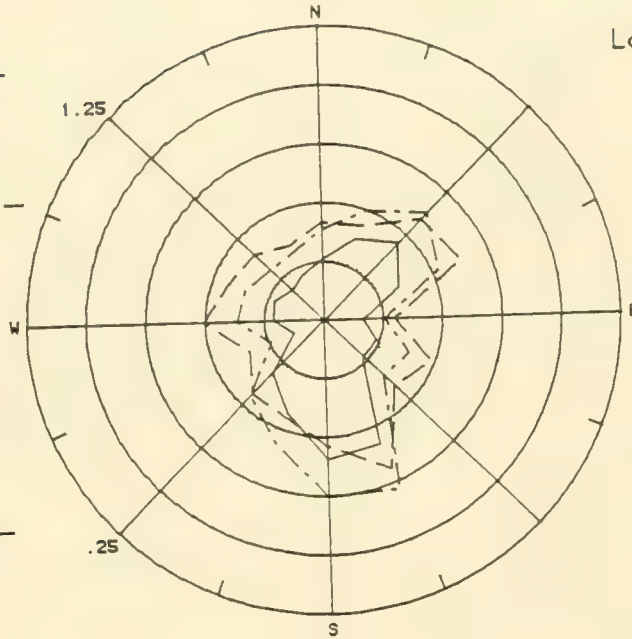
$\frac{U_{mean}}{U_{inf}}$  ———

$\frac{U_{mean} + 1.5 \times U_{rms}}{U_{inf}}$  - - -

.25/Div

$\frac{U_{rms}}{U_{inf}}$  - - -

.05/Div



Location 16

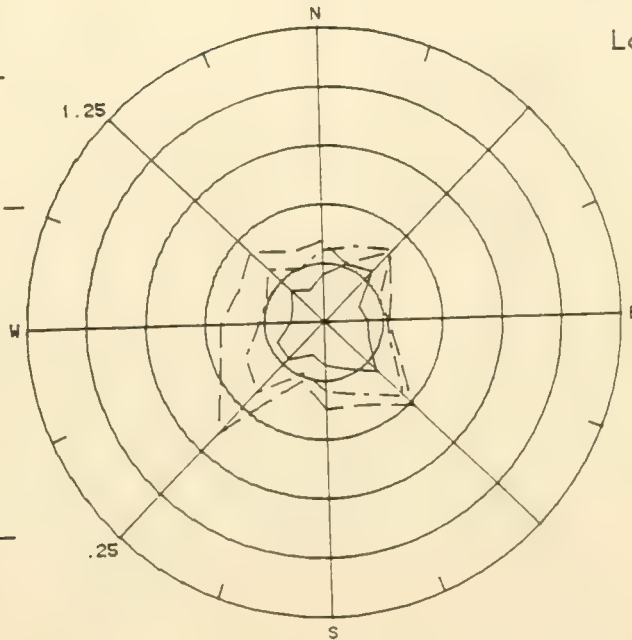
$\frac{U_{mean}}{U_{inf}}$  ———

$\frac{U_{mean} + 1.5 \times U_{rms}}{U_{inf}}$  - - -

.25/Div

$\frac{U_{rms}}{U_{inf}}$  - - -

.05/Div



# Configuration PH1

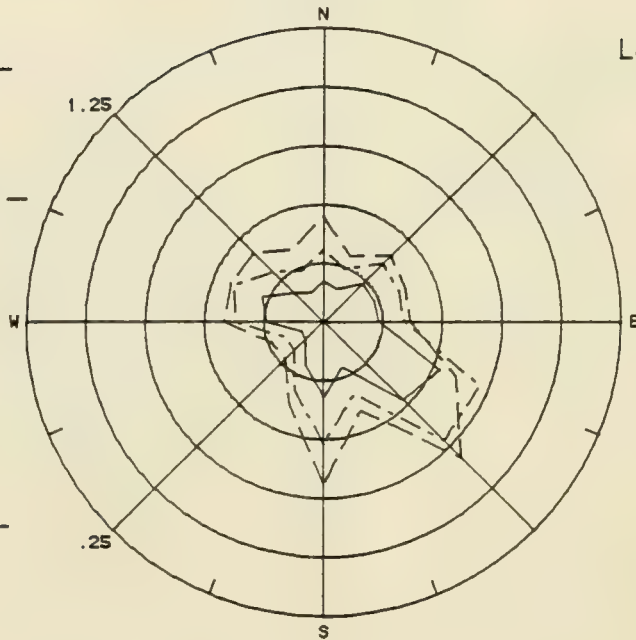
$\frac{U_{mean}}{U_{inf}}$  ———

$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}}$  - - -

.25/Div

$\frac{U_{rms}}{U_{inf}}$  - - -

.05/Div



Location 17

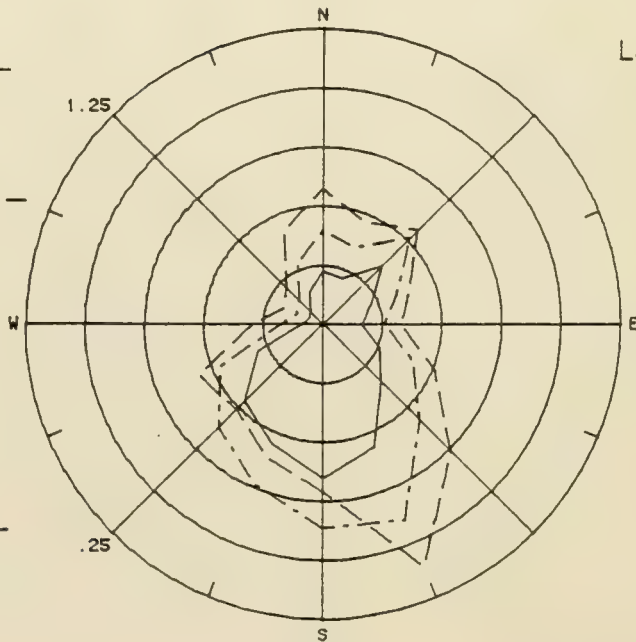
$\frac{U_{mean}}{U_{inf}}$  ———

$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}}$  - - -

.25/Div

$\frac{U_{rms}}{U_{inf}}$  - - -

.05/Div



Location 18

# Configuration PH1

Location 19

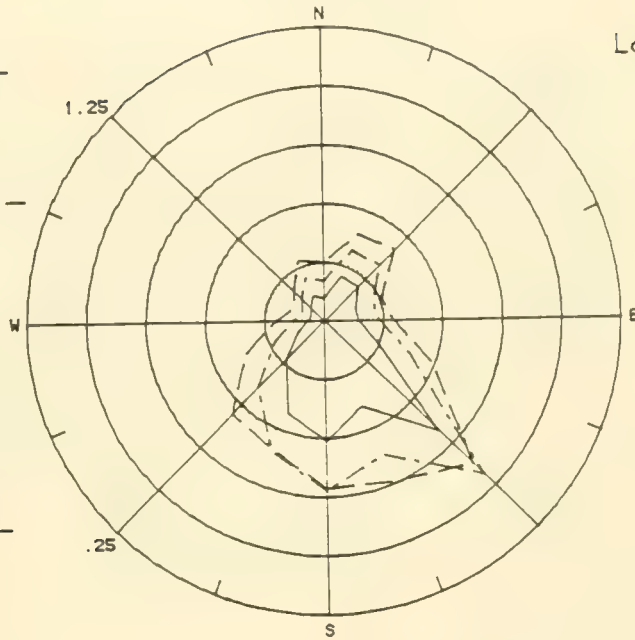
$\frac{U_{mean}}{U_{inf}}$  ———

$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}}$  - - -

.25/Div

$\frac{U_{rms}}{U_{inf}}$  - - -

.05/Div



Location 20

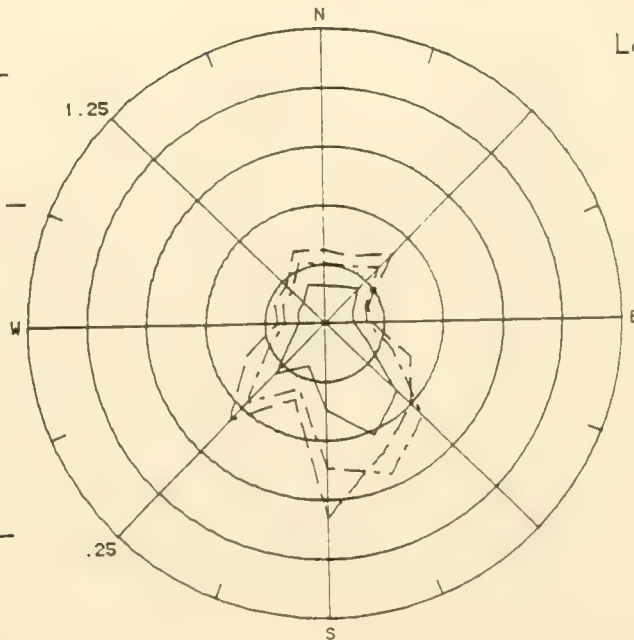
$\frac{U_{mean}}{U_{inf}}$  ———

$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}}$  - - -

.25/Div

$\frac{U_{rms}}{U_{inf}}$  - - -

.05/Div



# Configuration PH1

Location 21

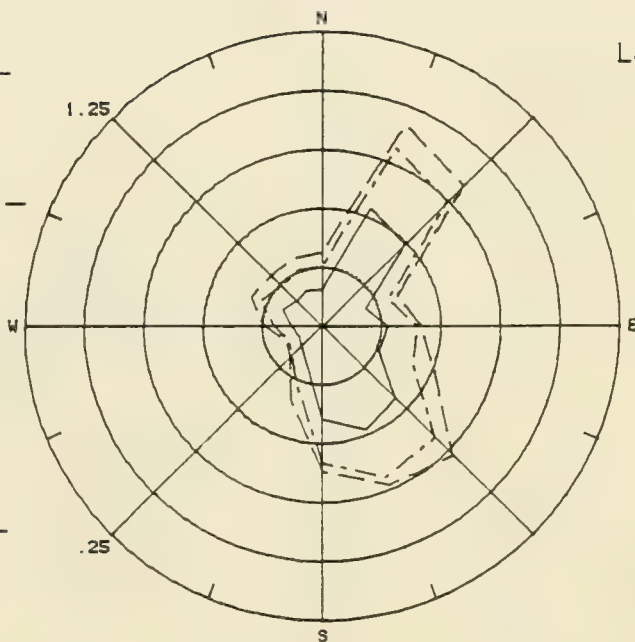
$$\frac{U_{mean}}{U_{inf}} \text{ ---}$$

$$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}} \text{ ---}$$

.25/Div

$$\frac{U_{rms}}{U_{inf}} \text{ ---}$$

.05/Div



Location 22

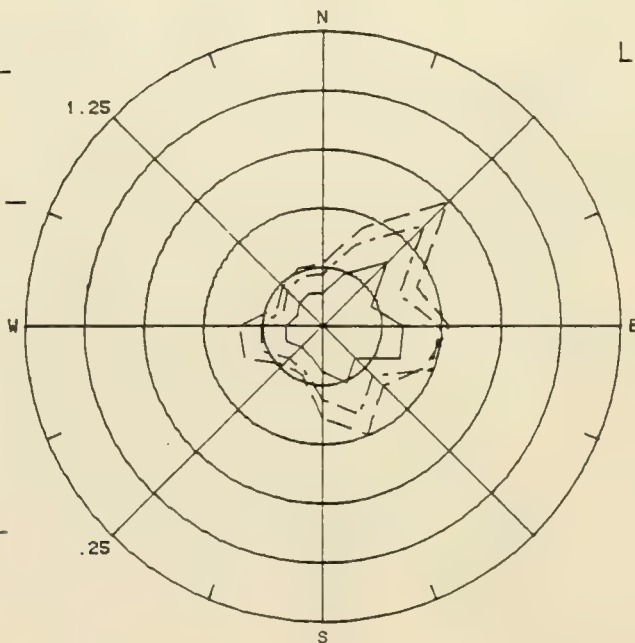
$$\frac{U_{mean}}{U_{inf}} \text{ ---}$$

$$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}} \text{ ---}$$

.25/Div

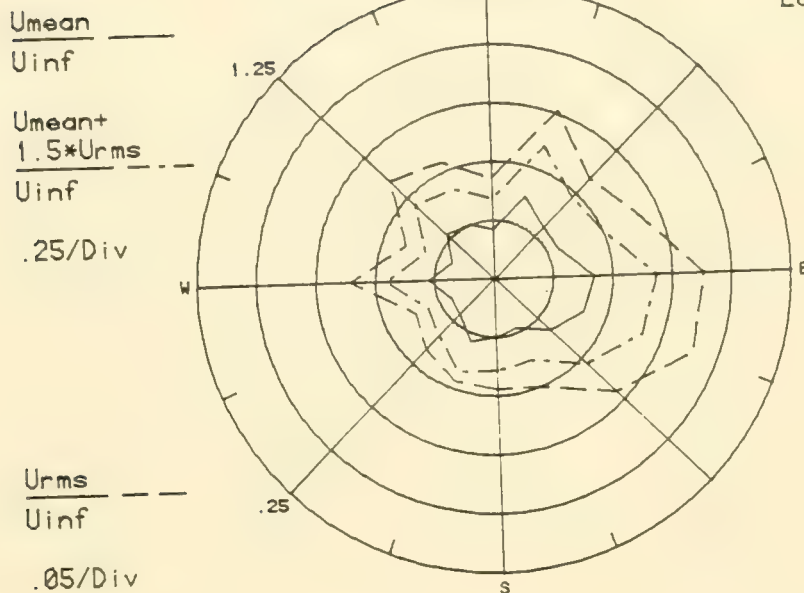
$$\frac{U_{rms}}{U_{inf}} \text{ ---}$$

.05/Div

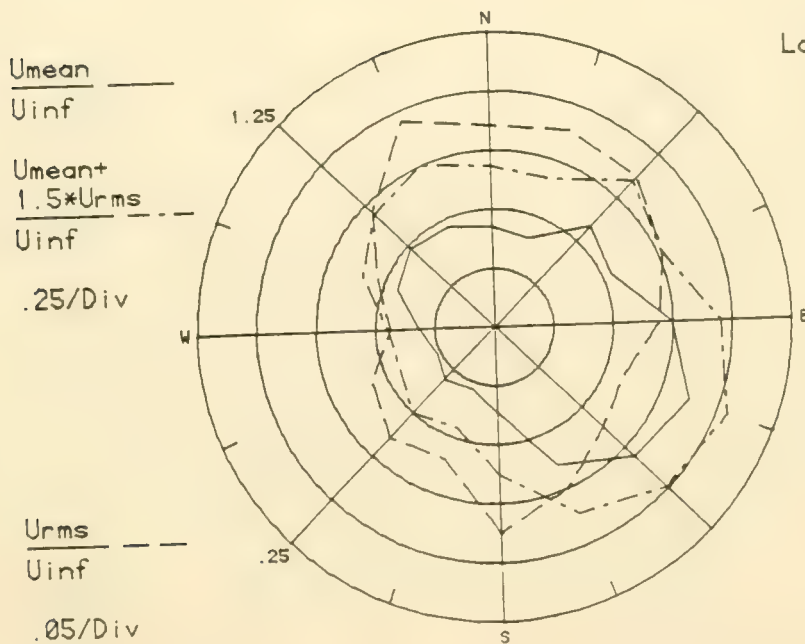


# Configuration PH1

Location 23



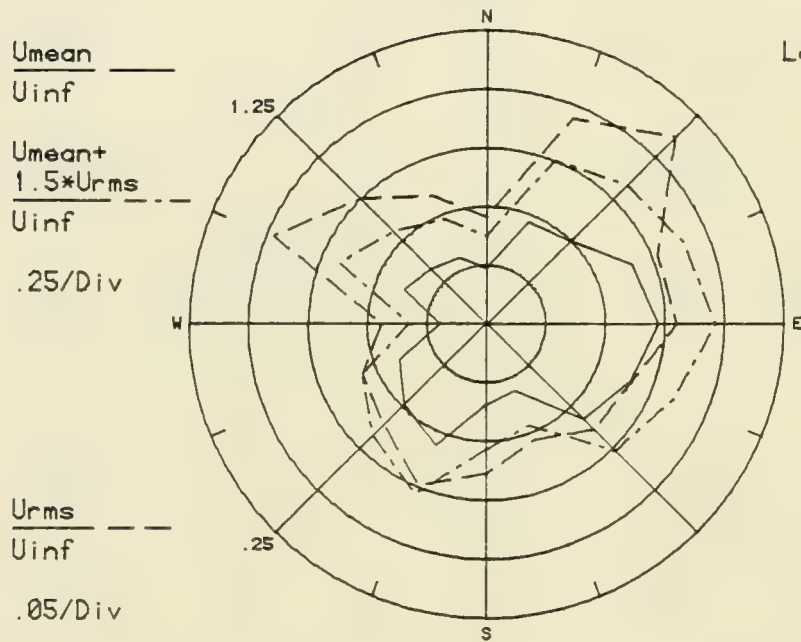
Location 24



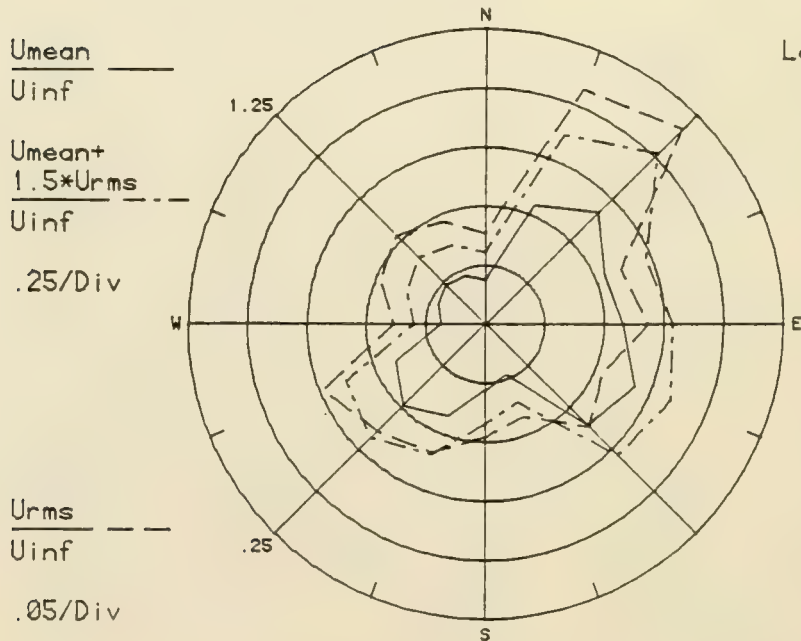


# Configuration PH1

Location 25



Location 26



# Configuration PH1

Location 27

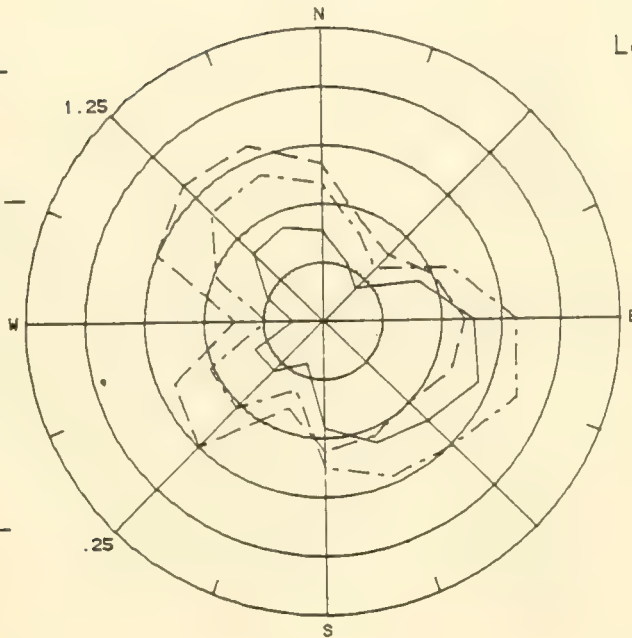
$\frac{U_{mean}}{U_{inf}}$  ———

$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}}$  - - -

.25/Div

$\frac{U_{rms}}{U_{inf}}$  - - -

.05/Div



Location 28

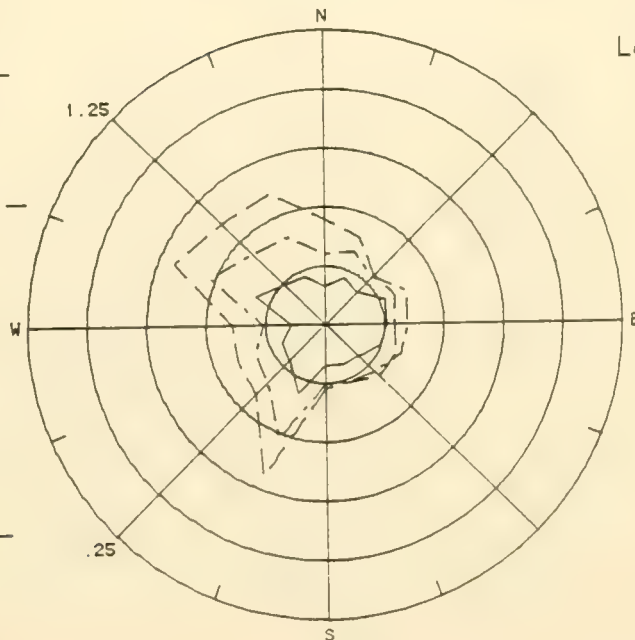
$\frac{U_{mean}}{U_{inf}}$  ———

$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}}$  - - -

.25/Div

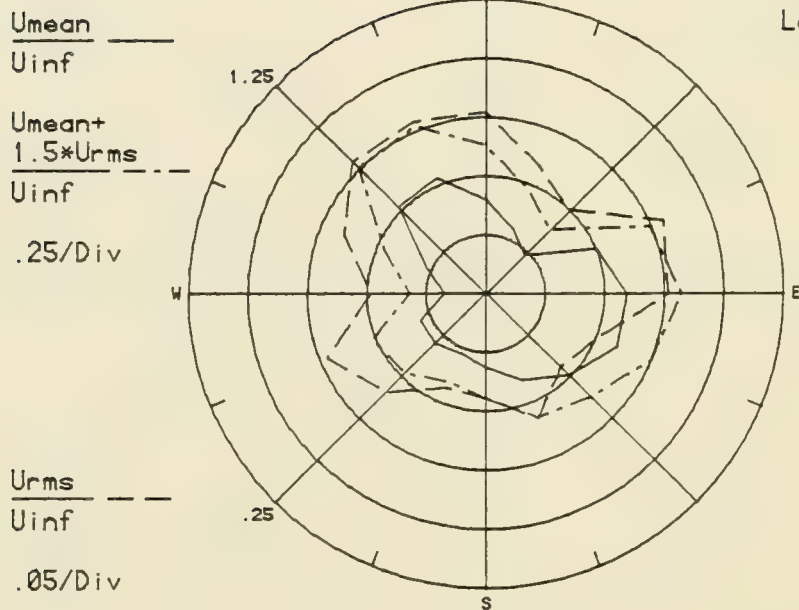
$\frac{U_{rms}}{U_{inf}}$  - - -

.05/Div

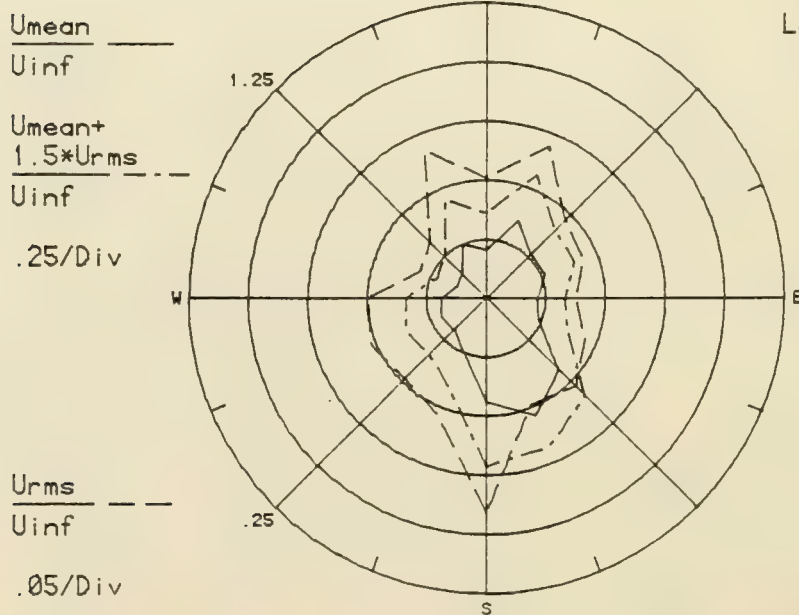


# Configuration PH1

Location 29



Location 30



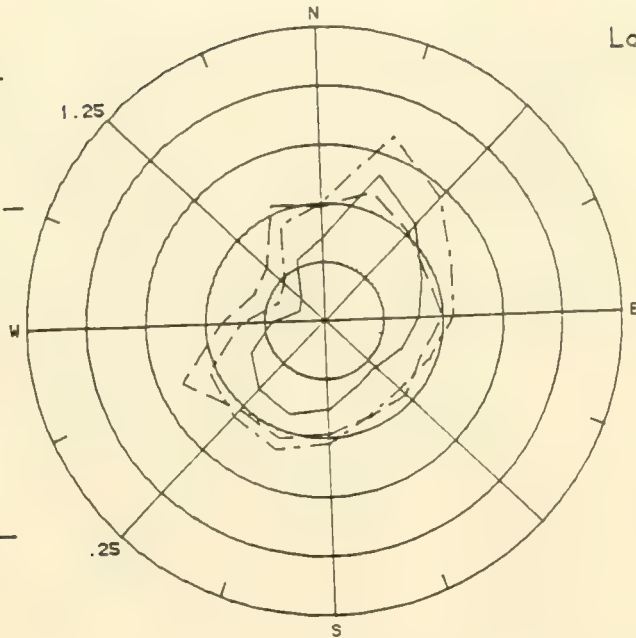
# Configuration PH1

Location 31

$$\frac{U_{mean}}{U_{inf}} \text{ ---}$$

$$\frac{U_{mean} + 1.5 \times U_{rms}}{U_{inf}} \text{ - - -}$$

.25/Div



$$\frac{U_{rms}}{U_{inf}} \text{ - - -}$$

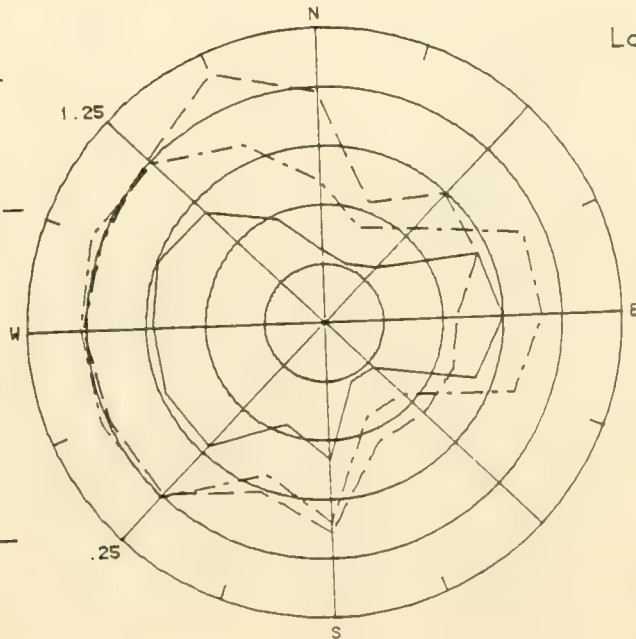
.05/Div

Location 32

$$\frac{U_{mean}}{U_{inf}} \text{ ---}$$

$$\frac{U_{mean} + 1.5 \times U_{rms}}{U_{inf}} \text{ - - -}$$

.25/Div



$$\frac{U_{rms}}{U_{inf}} \text{ - - -}$$

.05/Div

# Configuration PH1

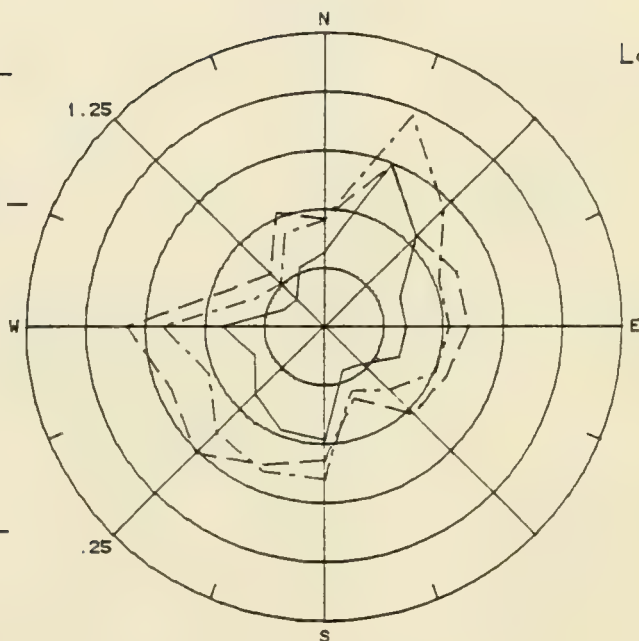
$\frac{U_{mean}}{U_{inf}}$  ———

$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}}$  - - -

.25/Div

$\frac{U_{rms}}{U_{inf}}$  - - -

.05/Div



Location 33

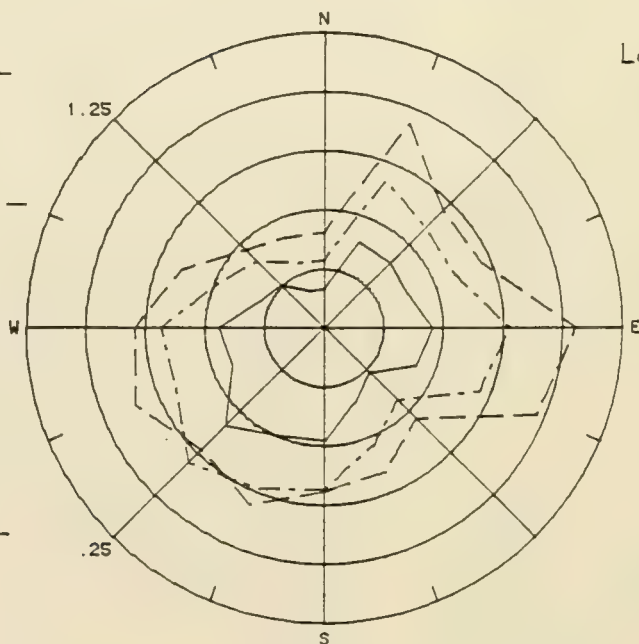
$\frac{U_{mean}}{U_{inf}}$  ———

$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}}$  - - -

.25/Div

$\frac{U_{rms}}{U_{inf}}$  - - -

.05/Div



Location 34



# Configuration PH1

Location 35

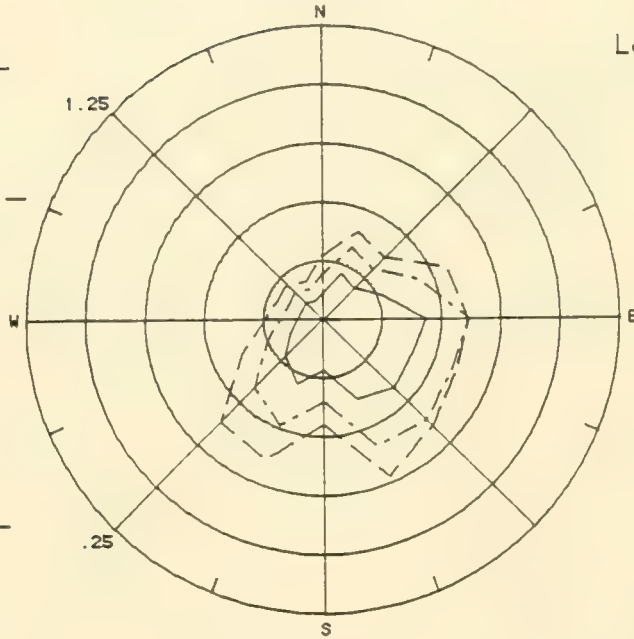
$$\frac{U_{mean}}{U_{inf}} \text{ ———}$$

$$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}} \text{ - - -}$$

.25/Div

$$\frac{U_{rms}}{U_{inf}} \text{ - - -}$$

.05/Div



Location 36

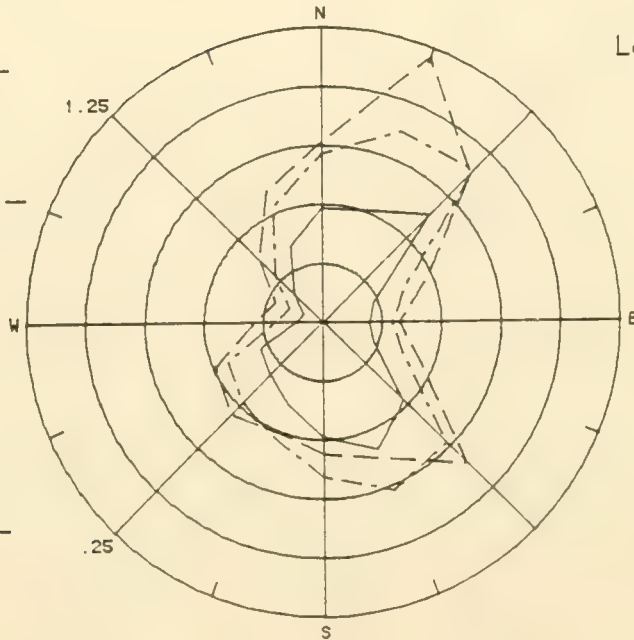
$$\frac{U_{mean}}{U_{inf}} \text{ ———}$$

$$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}} \text{ - - -}$$

.25/Div

$$\frac{U_{rms}}{U_{inf}} \text{ - - -}$$

.05/Div



# Configuration PH1

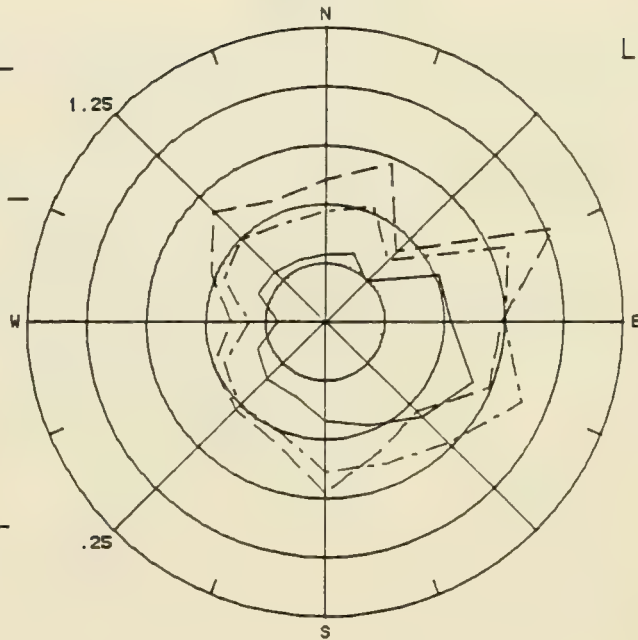
$\frac{U_{mean}}{U_{inf}}$  ———

$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}}$  - - -

.25/Div

$\frac{U_{rms}}{U_{inf}}$  - - -

.05/Div



Location 37

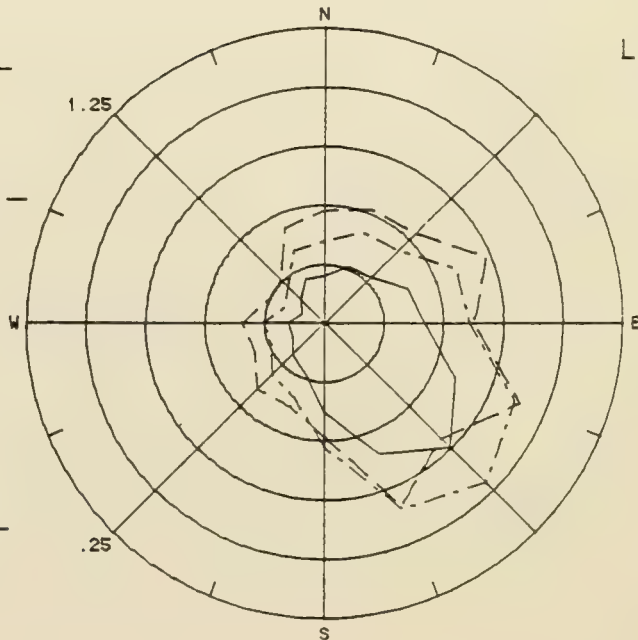
$\frac{U_{mean}}{U_{inf}}$  ———

$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}}$  - - -

.25/Div

$\frac{U_{rms}}{U_{inf}}$  - - -

.05/Div



Location 38

# Configuration PH1

Location 39

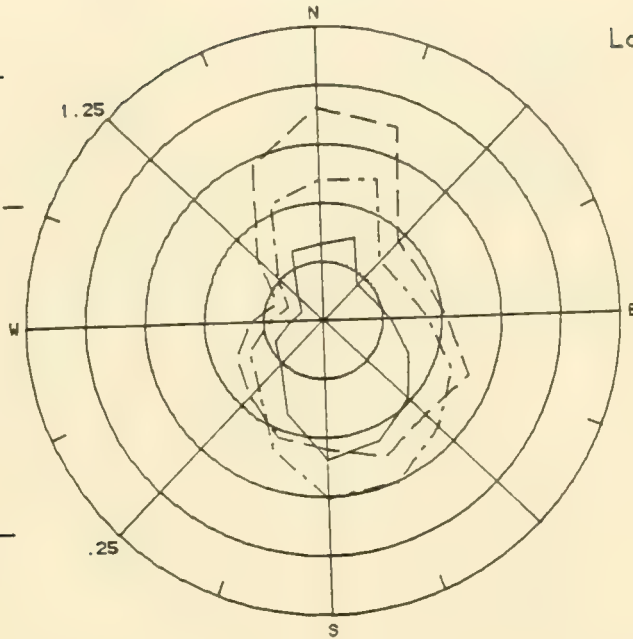
$$\frac{U_{mean}}{U_{inf}} \text{ ———}$$

$$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}} \text{ - - -}$$

.25/Div

$$\frac{U_{rms}}{U_{inf}} \text{ - - -}$$

.05/Div



Location 40

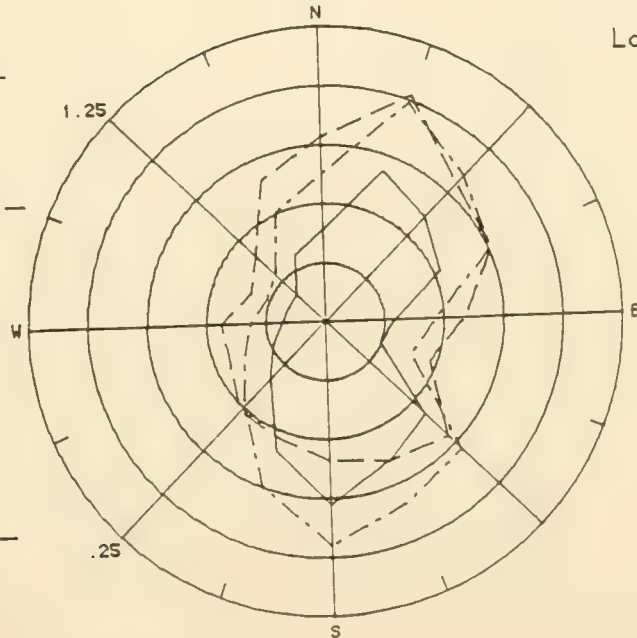
$$\frac{U_{mean}}{U_{inf}} \text{ ———}$$

$$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}} \text{ - - -}$$

.25/Div

$$\frac{U_{rms}}{U_{inf}} \text{ - - -}$$

.05/Div



# Configuration PH1

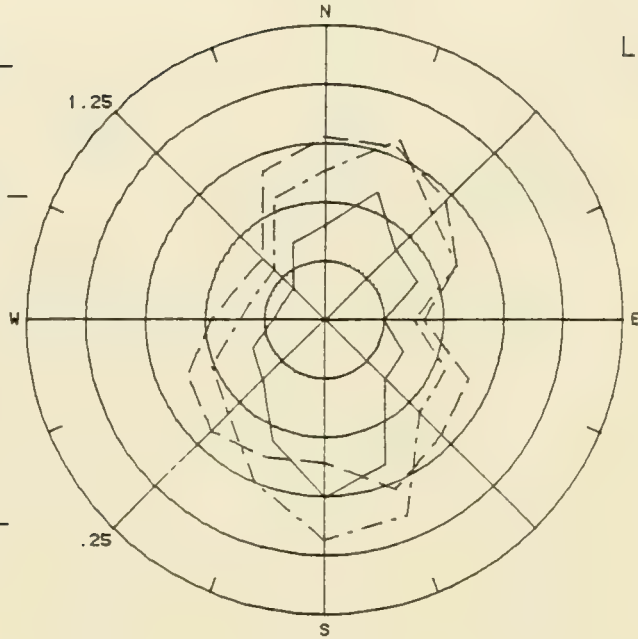
$\frac{U_{mean}}{U_{inf}}$  ———

$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}}$  - - -

.25/Div

$\frac{U_{rms}}{U_{inf}}$  - - -

.05/Div



Location 41

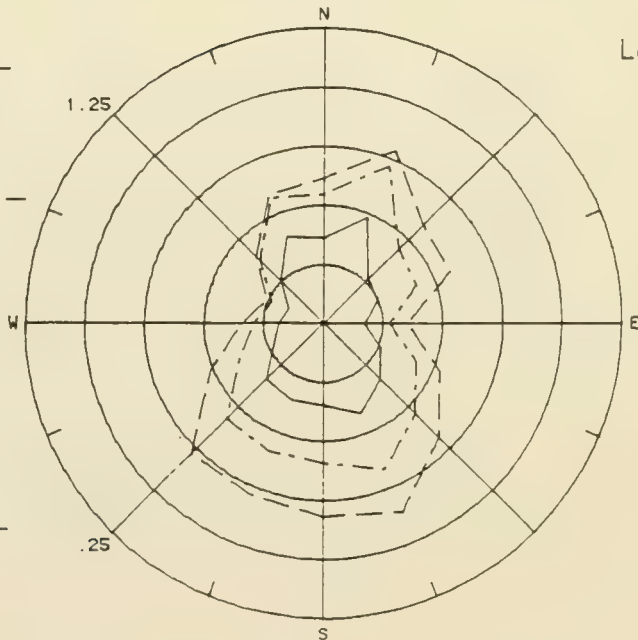
$\frac{U_{mean}}{U_{inf}}$  ———

$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}}$  - - -

.25/Div

$\frac{U_{rms}}{U_{inf}}$  - - -

.05/Div



Location 42

# Configuration PH1

Location 43

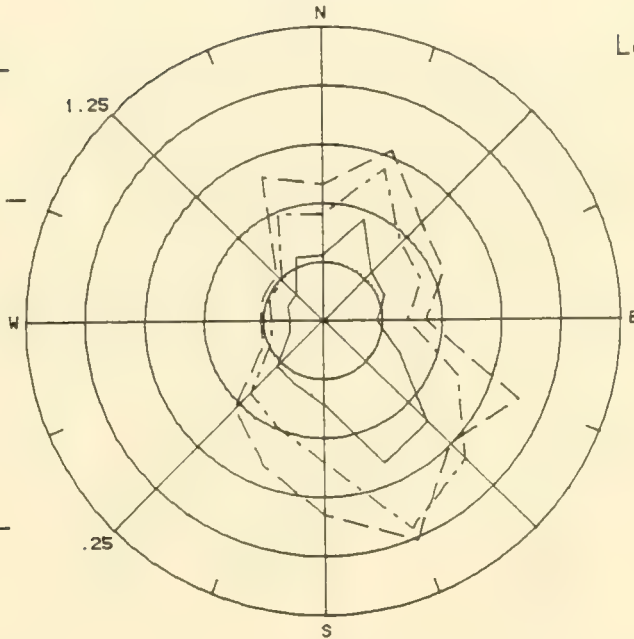
$\frac{U_{mean}}{U_{inf}}$  ———

$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}}$  - - -

.25/Div

$\frac{U_{rms}}{U_{inf}}$  - - -

.05/Div



Location 44

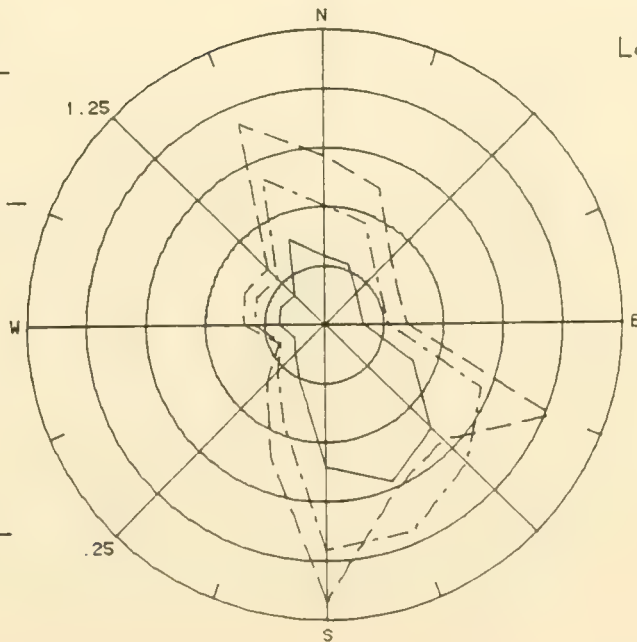
$\frac{U_{mean}}{U_{inf}}$  ———

$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}}$  - - -

.25/Div

$\frac{U_{rms}}{U_{inf}}$  - - -

.05/Div





# Configuration PH1

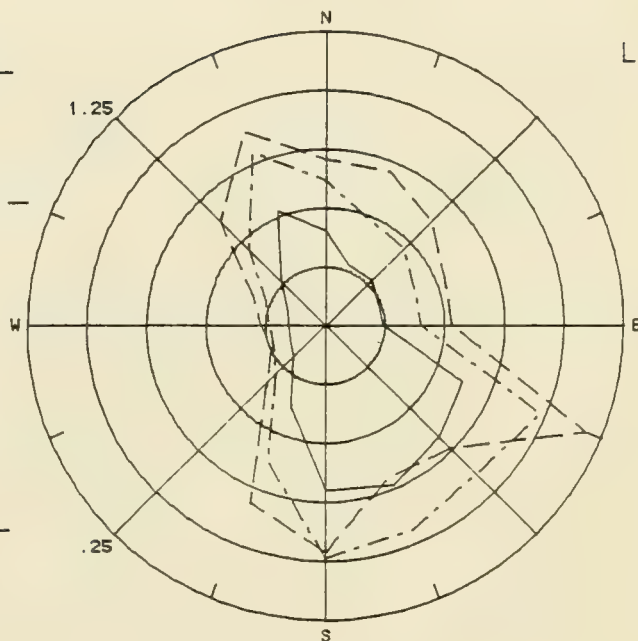
$\frac{U_{mean}}{U_{inf}}$  ———

$\frac{U_{mean} + 1.5 \times U_{rms}}{U_{inf}}$  - - -

.25/Div

$\frac{U_{rms}}{U_{inf}}$  - - -

.05/Div



Location 45

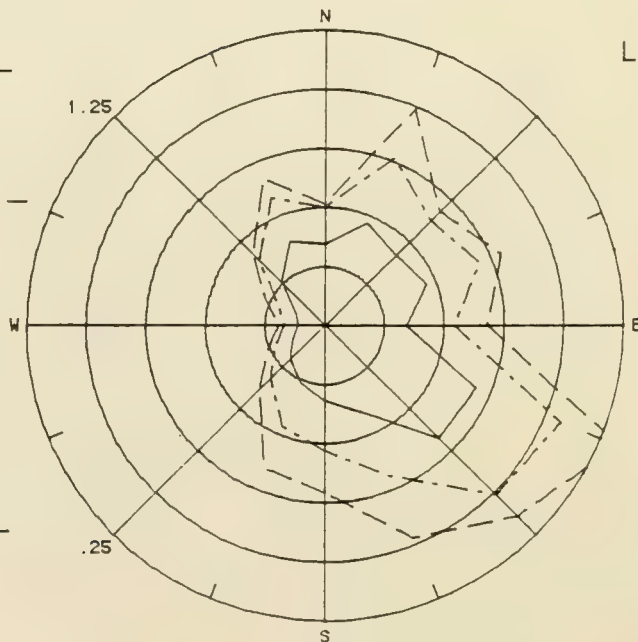
$\frac{U_{mean}}{U_{inf}}$  ———

$\frac{U_{mean} + 1.5 \times U_{rms}}{U_{inf}}$  - - -

.25/Div

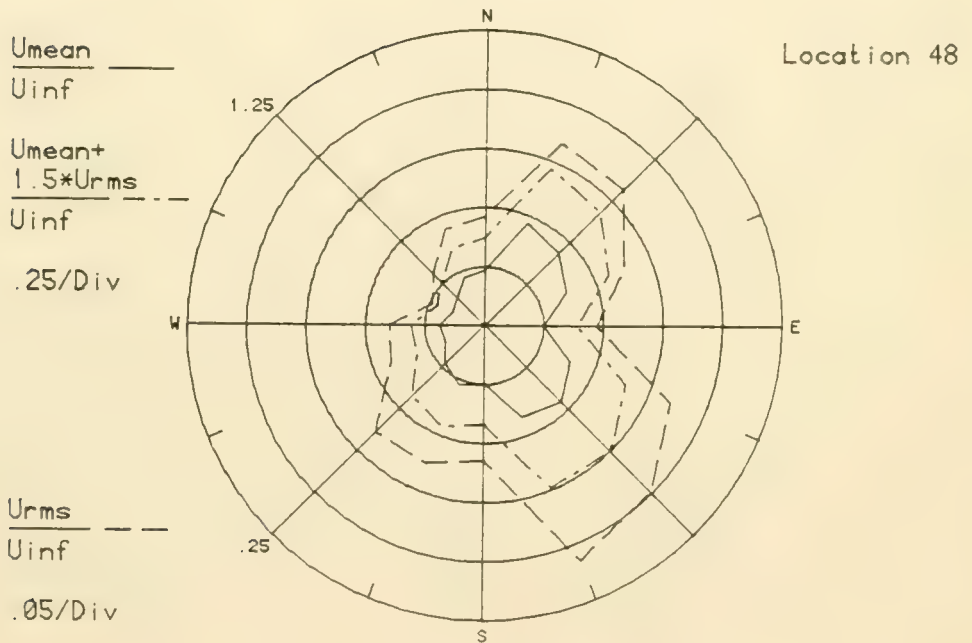
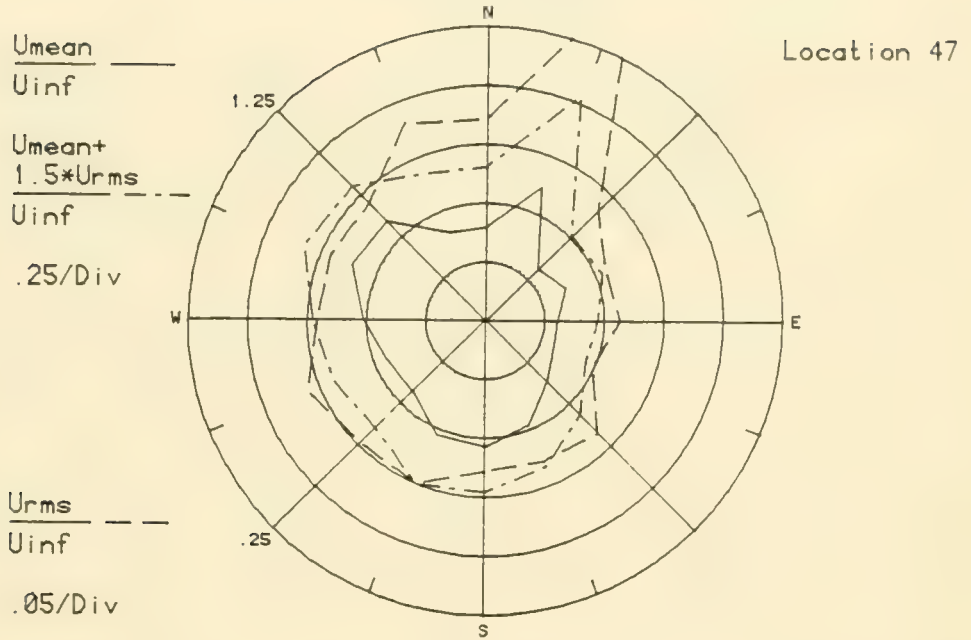
$\frac{U_{rms}}{U_{inf}}$  - - -

.05/Div



Location 46

# Configuration PH1



# Configuration PH1

$$\frac{U_{mean}}{U_{inf}} \text{ ———}$$

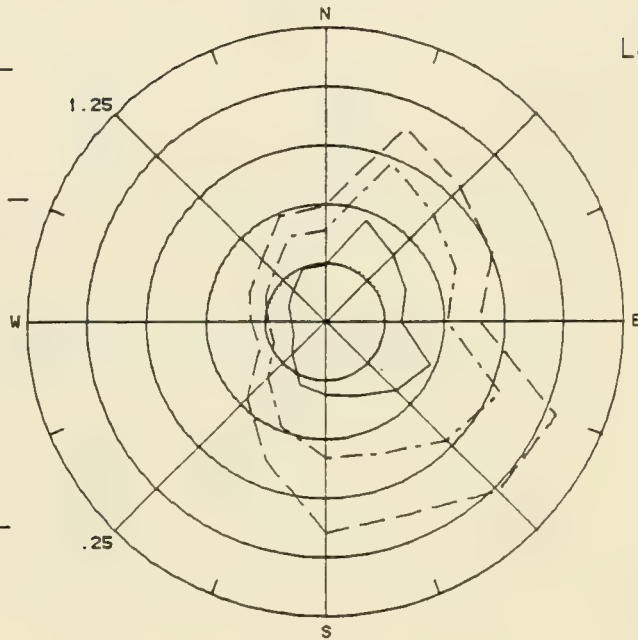
$$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}} \text{ - - -}$$

.25/Div

$$\frac{U_{rms}}{U_{inf}} \text{ - - -}$$

.05/Div

Location 49



$$\frac{U_{mean}}{U_{inf}} \text{ ———}$$

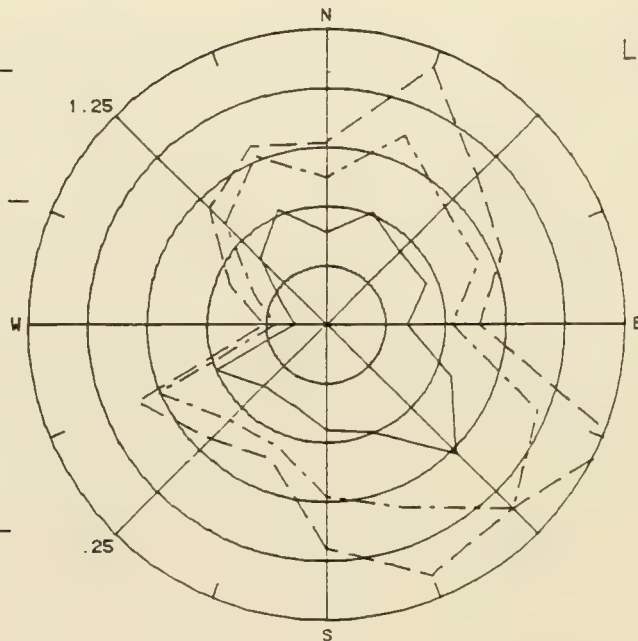
$$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}} \text{ - - -}$$

.25/Div

$$\frac{U_{rms}}{U_{inf}} \text{ - - -}$$

.05/Div

Location 50



# Configuration PH 2

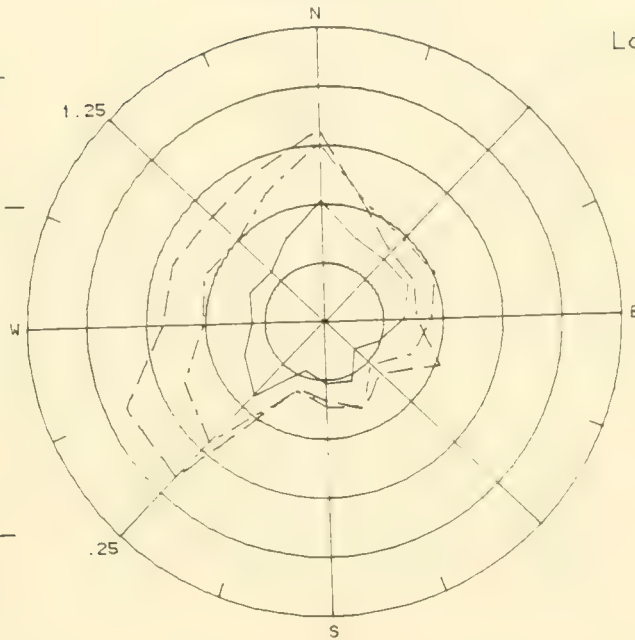
Location 1

$\frac{U_{mean}}{U_{inf}}$  ———

$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}}$  - - -

$\frac{U_{rms}}{U_{inf}}$  - - -

.25/Div



$\frac{U_{rms}}{U_{inf}}$  - - -

.05/Div

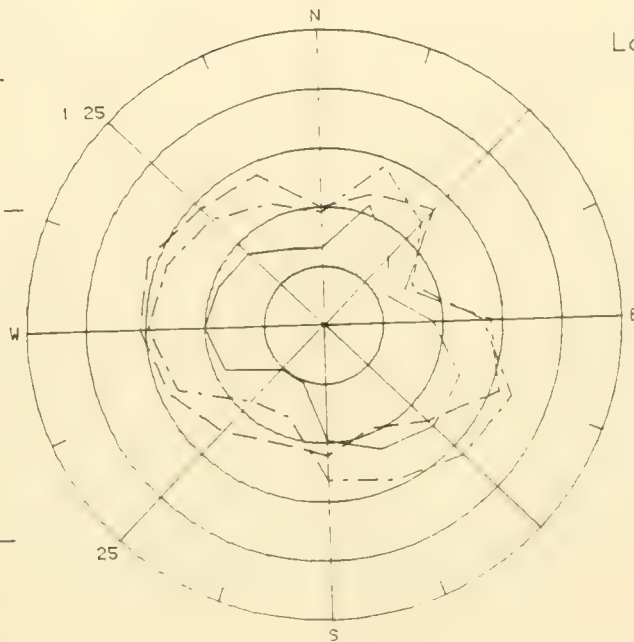
Location 2

$\frac{U_{mean}}{U_{inf}}$  ———

$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}}$  - - -

$\frac{U_{rms}}{U_{inf}}$  - - -

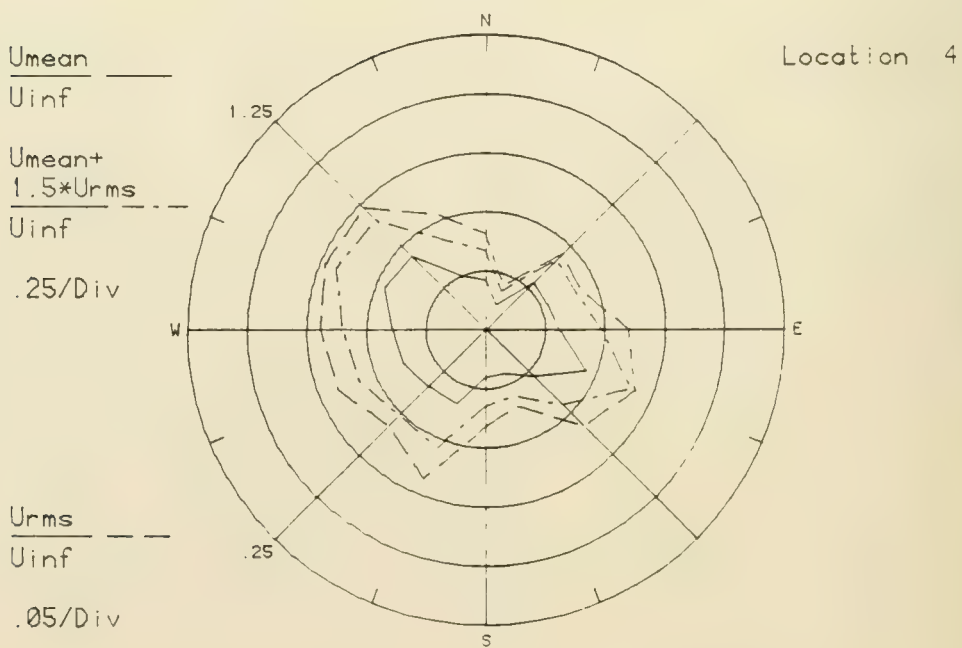
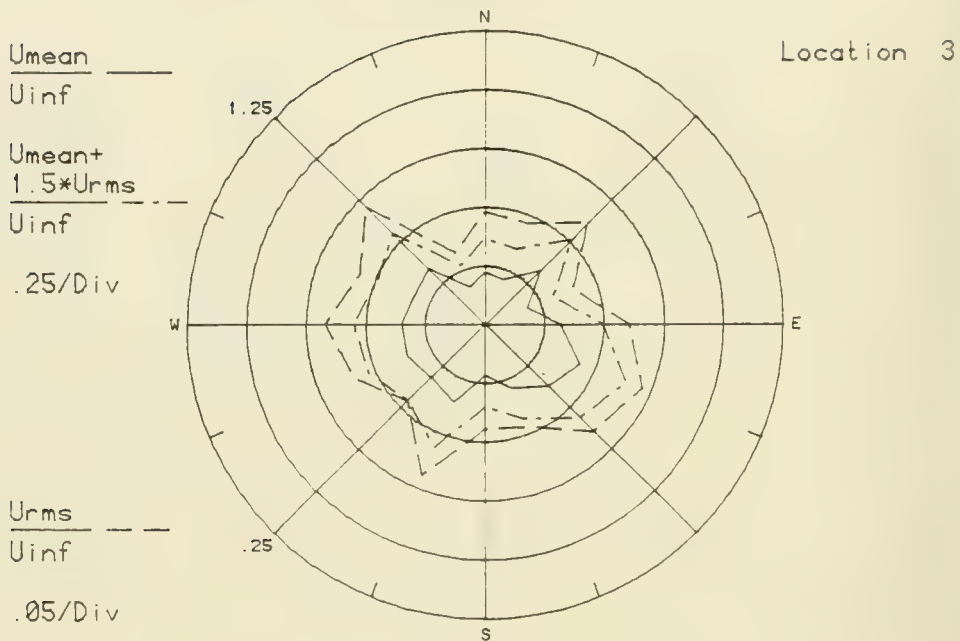
.25/Div



$\frac{U_{rms}}{U_{inf}}$  - - -

.05/Div

# Configuration PH 2





# Configuration PH 2

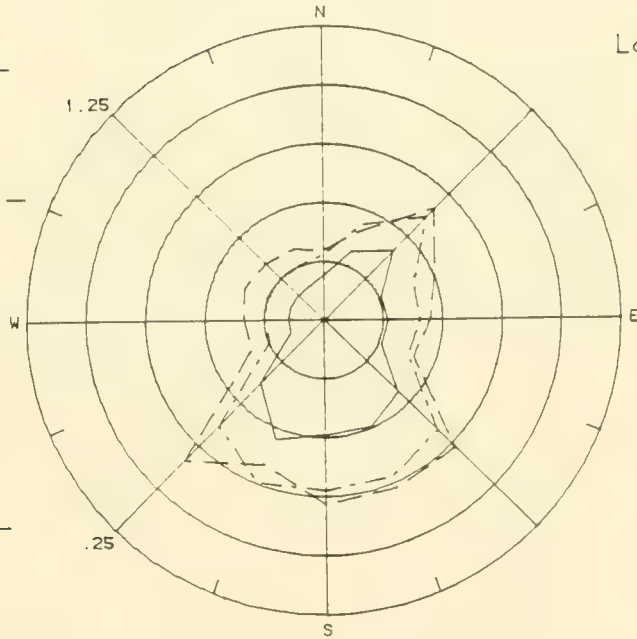
$\frac{U_{mean}}{U_{inf}}$  ———

$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}}$  - - -

.25/Div

$\frac{U_{rms}}{U_{inf}}$  - - -

.05/Div



Location 5

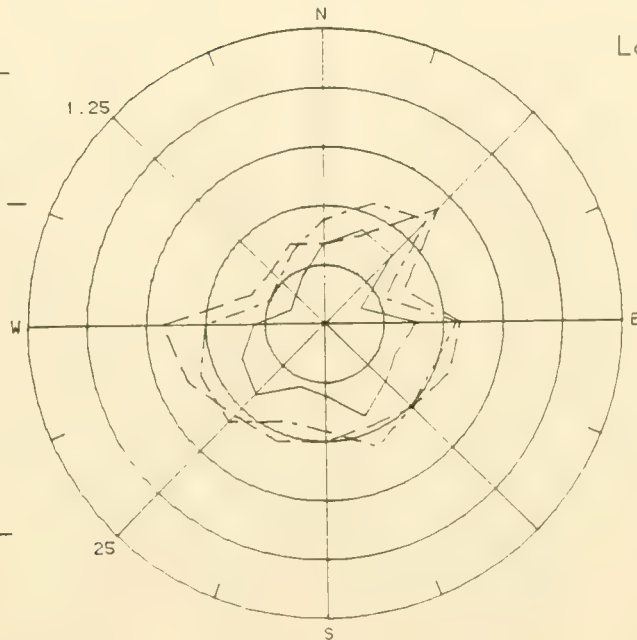
$\frac{U_{mean}}{U_{inf}}$  ———

$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}}$  - - -

.25/Div

$\frac{U_{rms}}{U_{inf}}$  - - -

.05/Div



Location 6

# Configuration PH 2

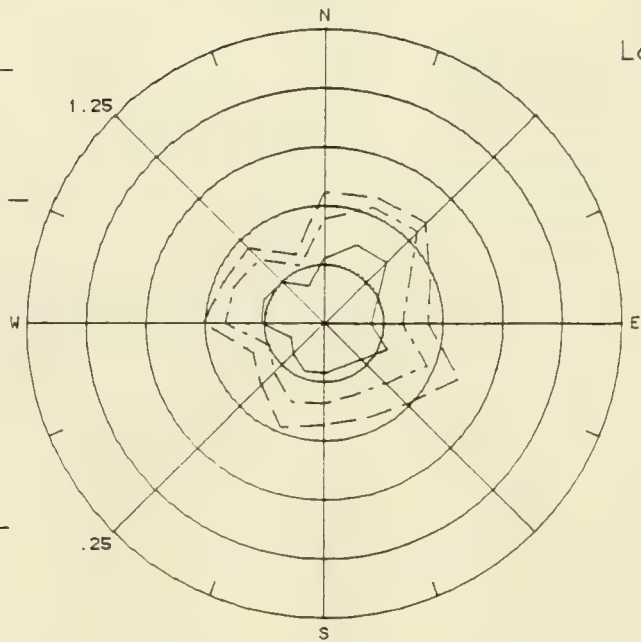
$\frac{U_{mean}}{U_{inf}}$  ———

$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}}$  - - -

.25/Div

$\frac{U_{rms}}{U_{inf}}$  - - -

.05/Div



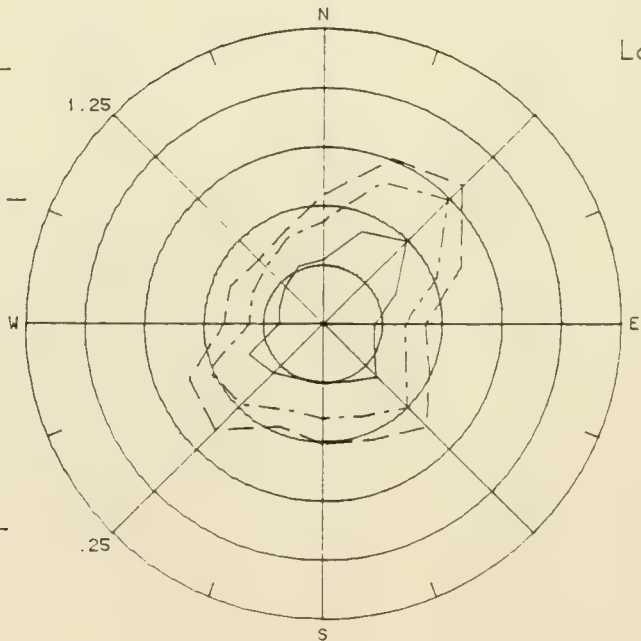
$\frac{U_{mean}}{U_{inf}}$  ———

$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}}$  - - -

.25/Div

$\frac{U_{rms}}{U_{inf}}$  - - -

.05/Div



# Configuration PH 2

Location 9

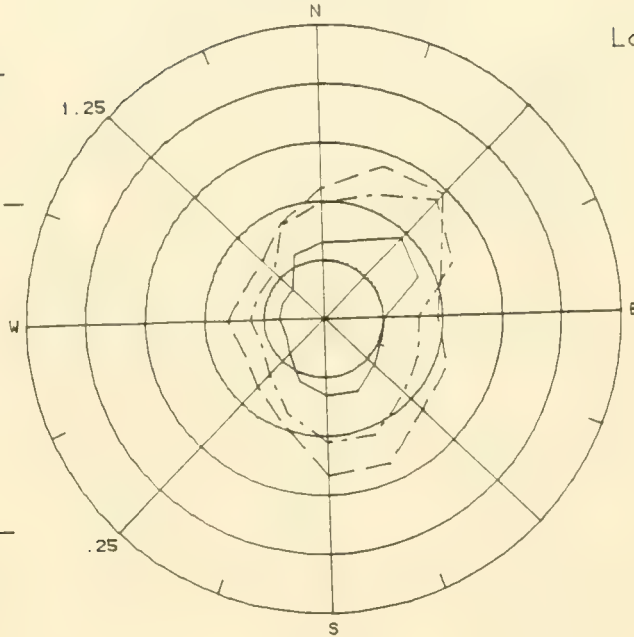
$\frac{U_{mean}}{U_{inf}}$  ———

$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}}$  - - -

.25/Div

$\frac{U_{rms}}{U_{inf}}$  - - -

.05/Div



Location 10

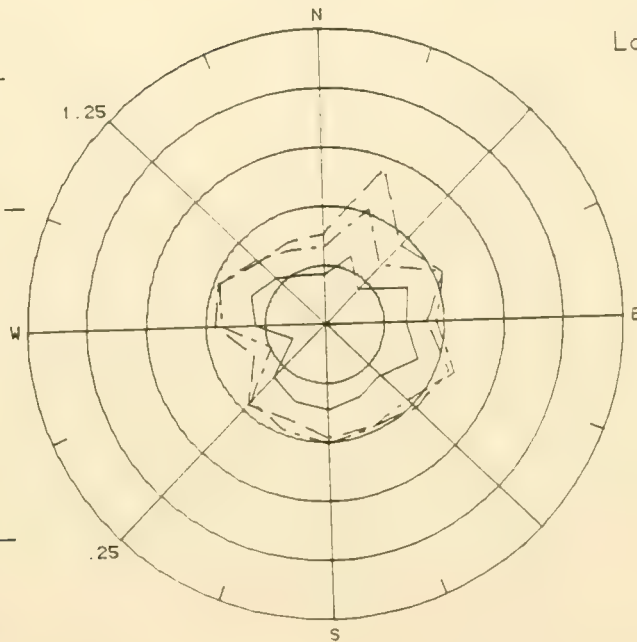
$\frac{U_{mean}}{U_{inf}}$  ———

$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}}$  - - -

.25/Div

$\frac{U_{rms}}{U_{inf}}$  - - -

.05/Div



# Configuration PH 2

$$\frac{U_{mean}}{U_{inf}} \text{ ———}$$

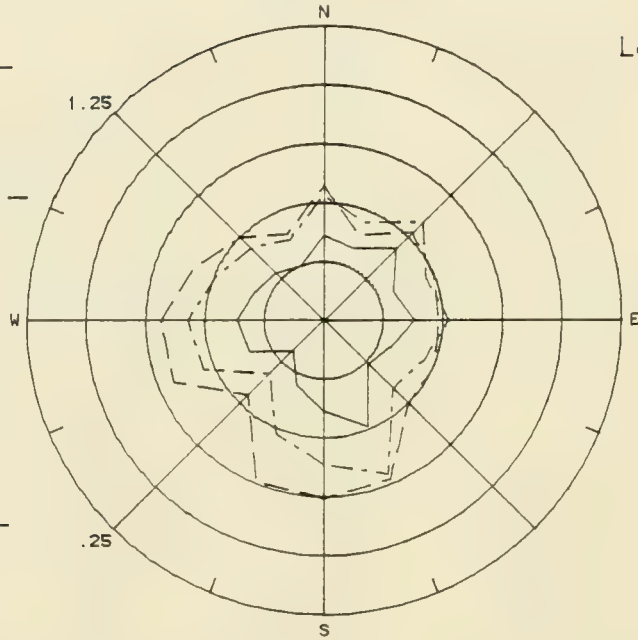
$$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}} \text{ - - -}$$

.25/Div

$$\frac{U_{rms}}{U_{inf}} \text{ - - -}$$

.05/Div

Location 11



$$\frac{U_{mean}}{U_{inf}} \text{ ———}$$

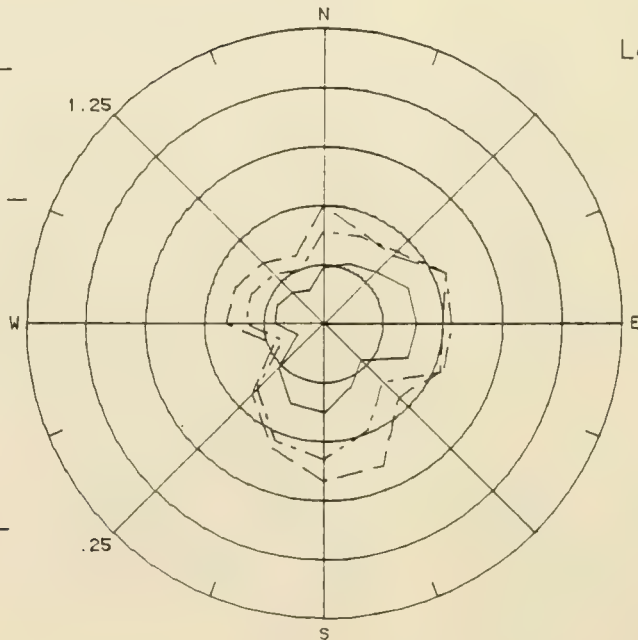
$$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}} \text{ - - -}$$

.25/Div

$$\frac{U_{rms}}{U_{inf}} \text{ - - -}$$

.05/Div

Location 12



# Configuration PH 2

$$\frac{U_{mean}}{U_{inf}} \text{ ———}$$

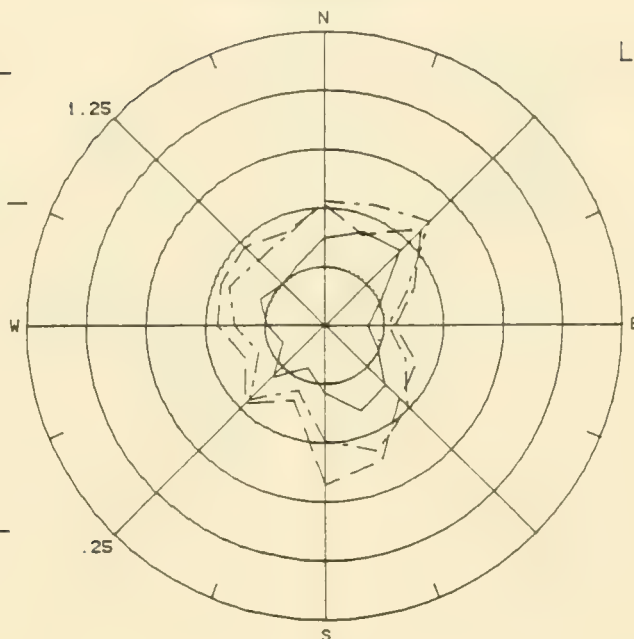
$$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}} \text{ - - -}$$

.25/Div

$$\frac{U_{rms}}{U_{inf}} \text{ - - -}$$

.05/Div

Location 13



$$\frac{U_{mean}}{U_{inf}} \text{ ———}$$

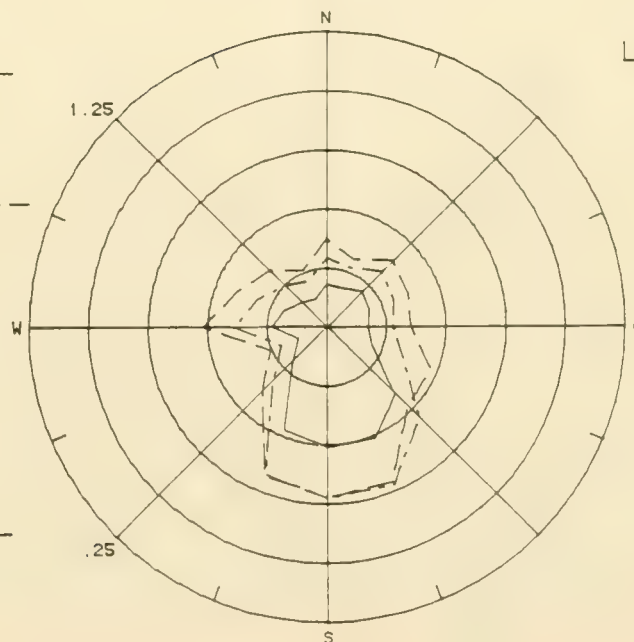
$$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}} \text{ - - -}$$

.25/Div

$$\frac{U_{rms}}{U_{inf}} \text{ - - -}$$

.05/Div

Location 14





# Configuration PH 2

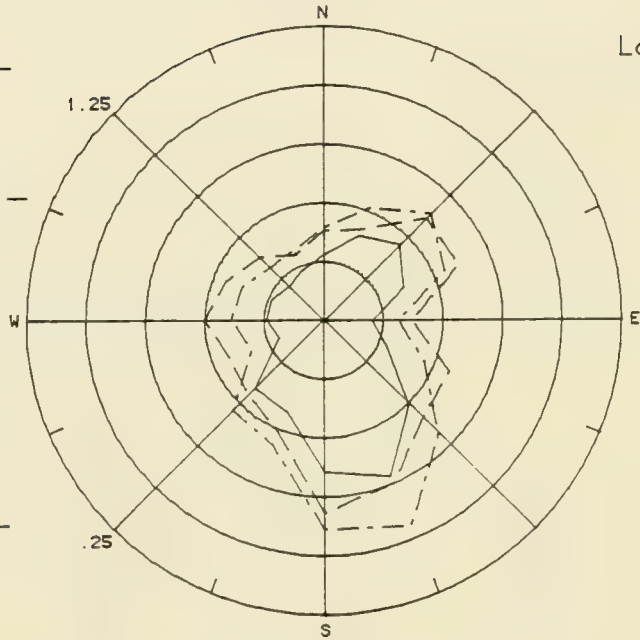
$\frac{U_{mean}}{U_{inf}}$  ———

$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}}$  - - -

.25/Div

$\frac{U_{rms}}{U_{inf}}$  - - -

.05/Div



Location 15

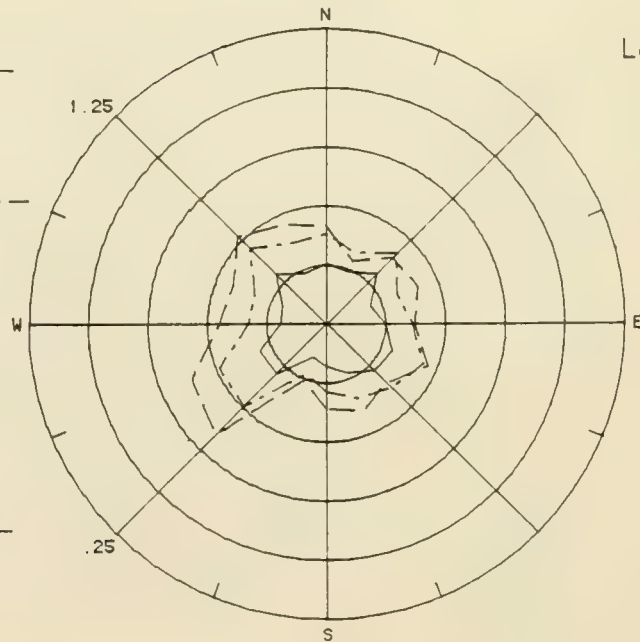
$\frac{U_{mean}}{U_{inf}}$  ———

$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}}$  - - -

.25/Div

$\frac{U_{rms}}{U_{inf}}$  - - -

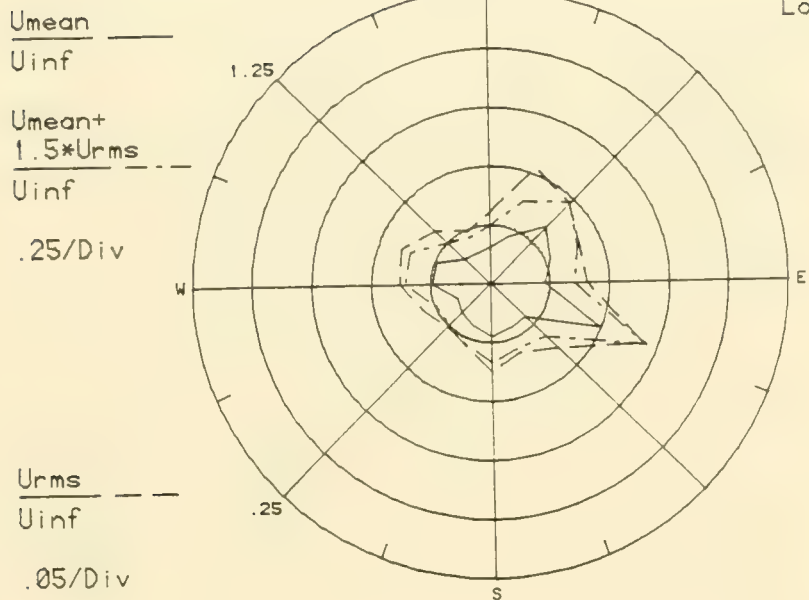
.05/Div



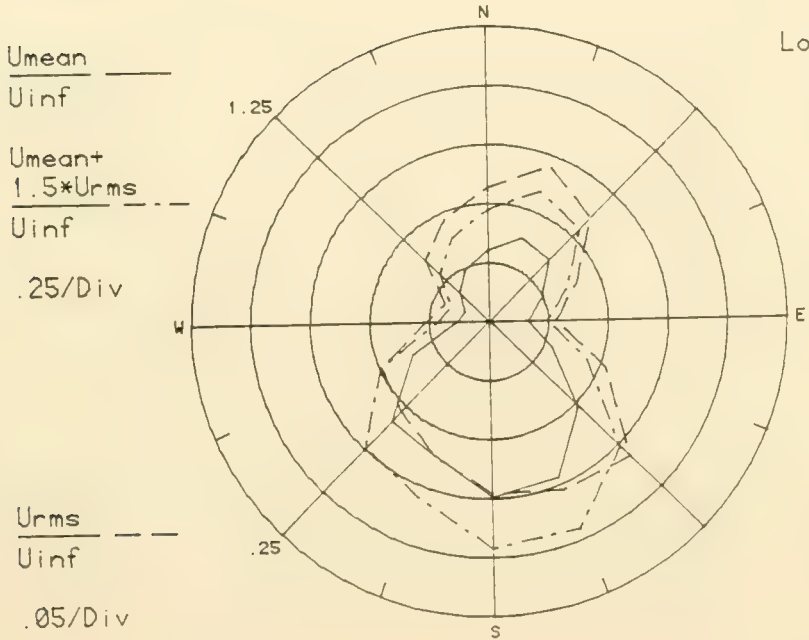
Location 16

# Configuration PH 2

Location 17



Location 18



# Configuration PH 2

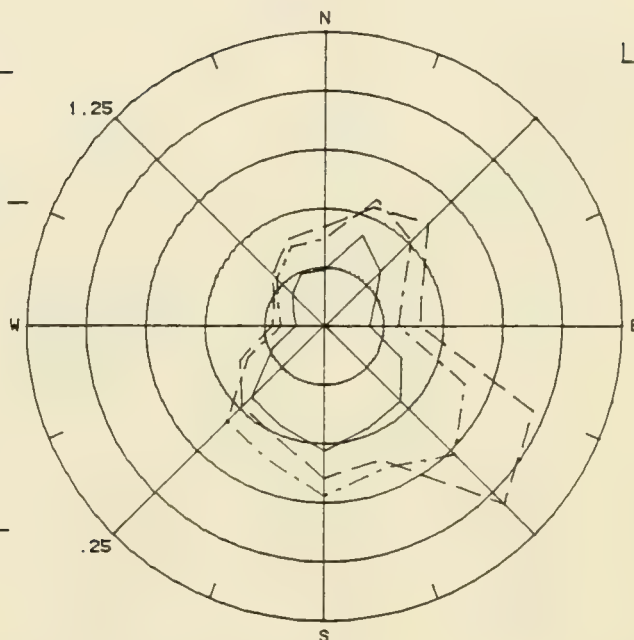
$\frac{U_{mean}}{U_{inf}}$  ———

$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}}$  - - -

.25/Div

$\frac{U_{rms}}{U_{inf}}$  - - -

.05/Div



Location 19

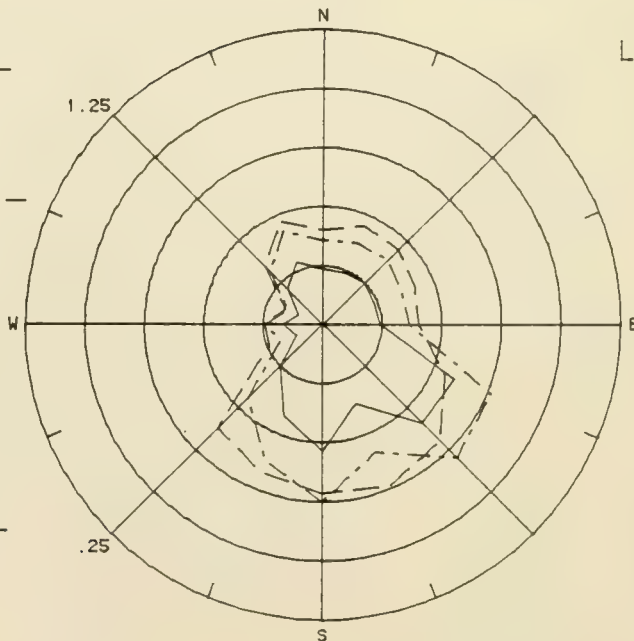
$\frac{U_{mean}}{U_{inf}}$  ———

$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}}$  - - -

.25/Div

$\frac{U_{rms}}{U_{inf}}$  - - -

.05/Div



Location 20

# Configuration PH 2

Location 21

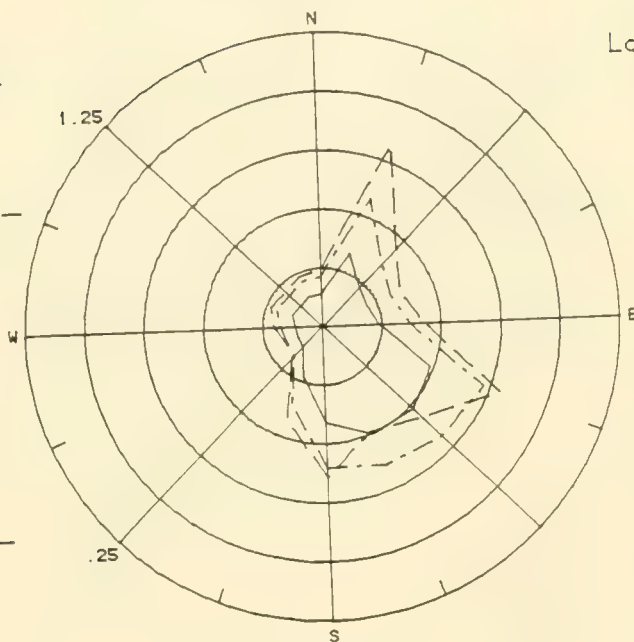
$$\frac{U_{mean}}{U_{inf}} \text{ ———}$$

$$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}} \text{ - - -}$$

.25/Div

$$\frac{U_{rms}}{U_{inf}} \text{ - - -}$$

.05/Div



Location 22

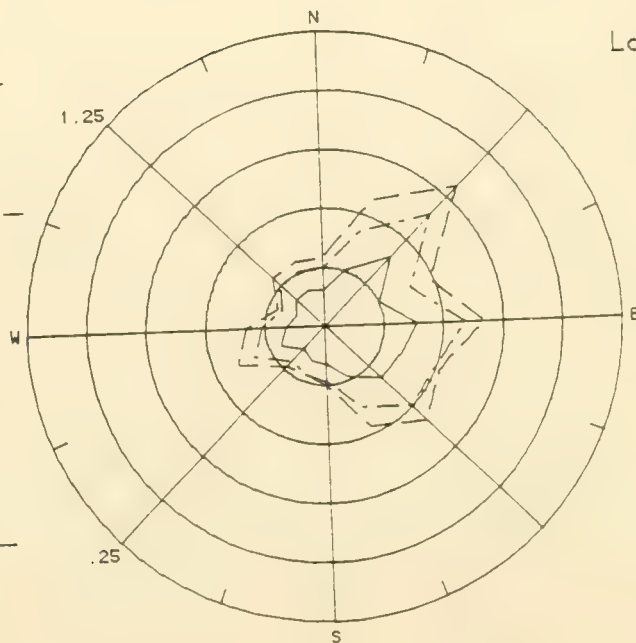
$$\frac{U_{mean}}{U_{inf}} \text{ ———}$$

$$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}} \text{ - - -}$$

.25/Div

$$\frac{U_{rms}}{U_{inf}} \text{ - - -}$$

.05/Div



# Configuration PH 2

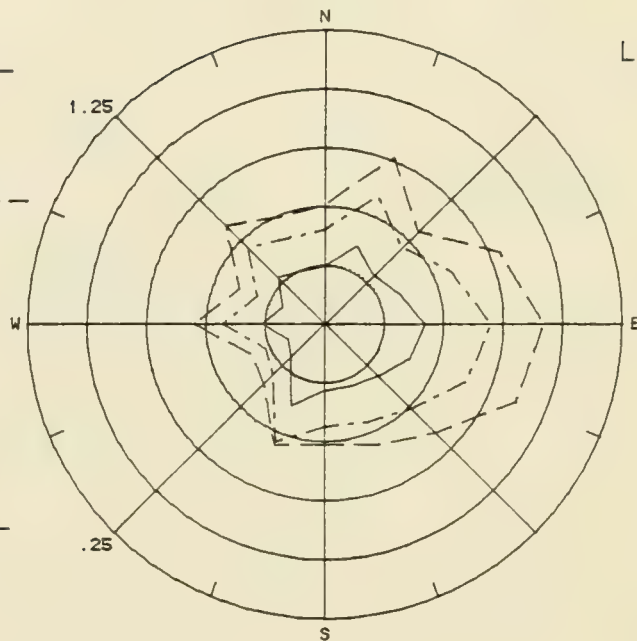
$\frac{U_{mean}}{U_{inf}}$  ———

$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}}$  - - -

.25/Div

$\frac{U_{rms}}{U_{inf}}$  - - -

.05/Div



Location 23

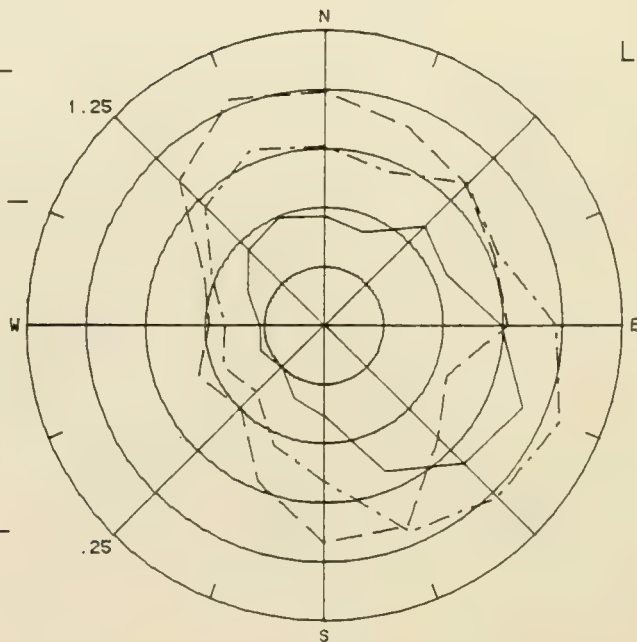
$\frac{U_{mean}}{U_{inf}}$  ———

$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}}$  - - -

.25/Div

$\frac{U_{rms}}{U_{inf}}$  - - -

.05/Div



Location 24



# Configuration PH 2

$\frac{U_{mean}}{U_{inf}}$  ———

$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}}$  - - -

$\frac{U_{rms}}{U_{inf}}$  - - -

$\frac{U_{rms}}{U_{inf}}$  - - -

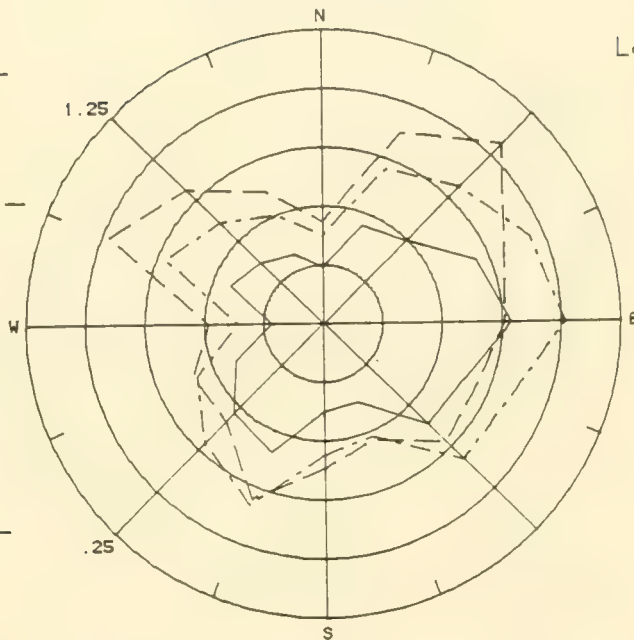
.25/Div

$\frac{U_{rms}}{U_{inf}}$  - - -

$\frac{U_{rms}}{U_{inf}}$  - - -

.05/Div

Location 25



$\frac{U_{mean}}{U_{inf}}$  ———

$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}}$  - - -

$\frac{U_{rms}}{U_{inf}}$  - - -

$\frac{U_{rms}}{U_{inf}}$  - - -

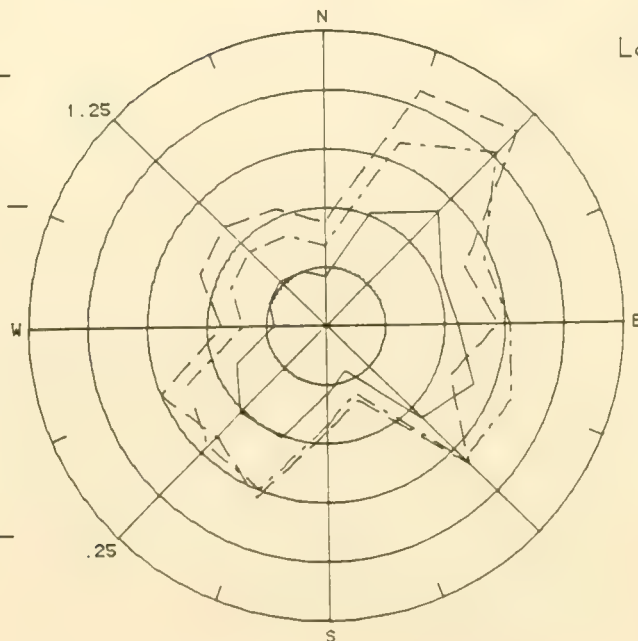
.25/Div

$\frac{U_{rms}}{U_{inf}}$  - - -

$\frac{U_{rms}}{U_{inf}}$  - - -

.05/Div

Location 26



# Configuration PH 2

$\frac{U_{mean}}{U_{inf}}$  ———

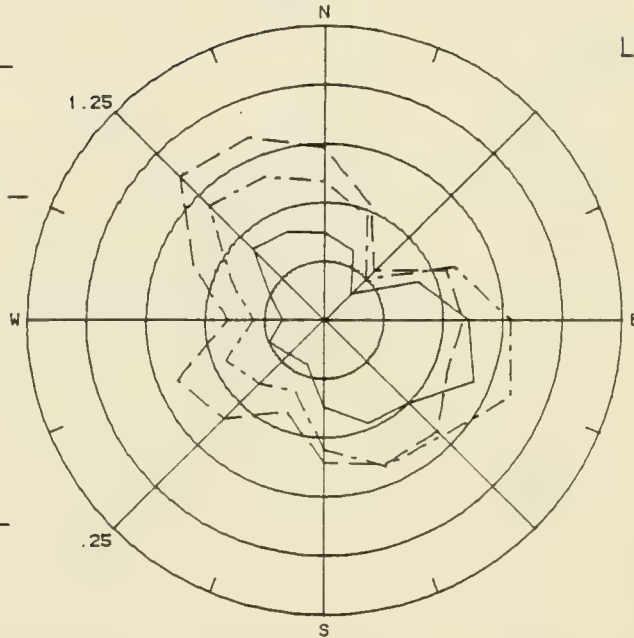
$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}}$  - - -

.25/Div

$\frac{U_{rms}}{U_{inf}}$  - - -

.05/Div

Location 27



$\frac{U_{mean}}{U_{inf}}$  ———

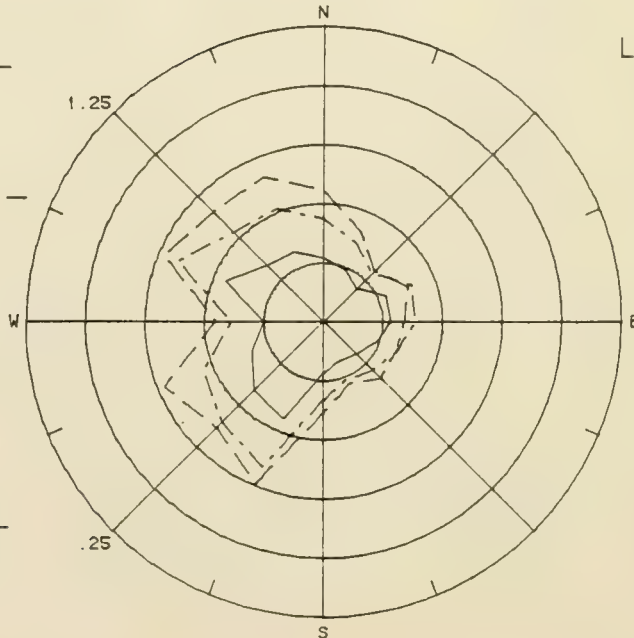
$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}}$  - - -

.25/Div

$\frac{U_{rms}}{U_{inf}}$  - - -

.05/Div

Location 28



# Configuration PH 2

Location 29

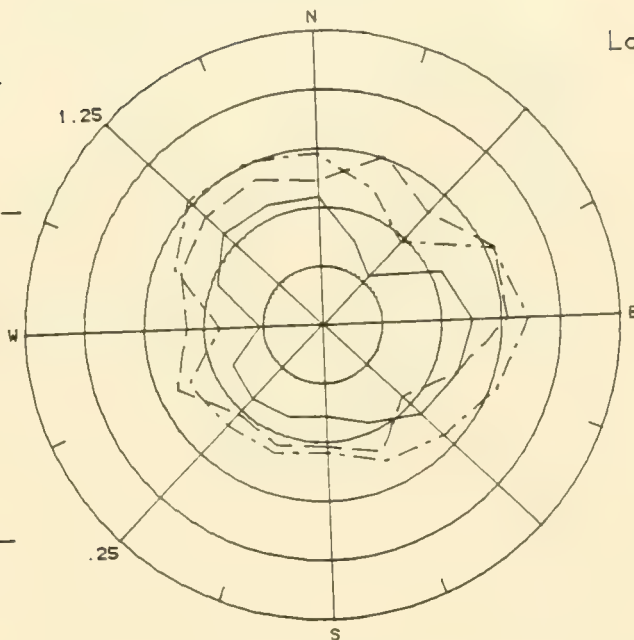
$\frac{U_{mean}}{U_{inf}}$  ———

$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}}$  - - -

.25/Div

$\frac{U_{rms}}{U_{inf}}$  - - -

.05/Div



Location 30

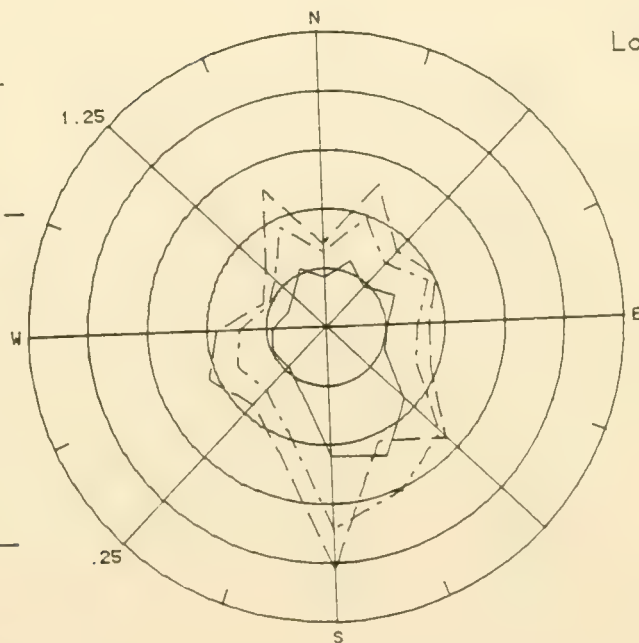
$\frac{U_{mean}}{U_{inf}}$  ———

$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}}$  - - -

.25/Div

$\frac{U_{rms}}{U_{inf}}$  - - -

.05/Div



# Configuration PH 2

$\frac{U_{mean}}{U_{inf}}$  ———

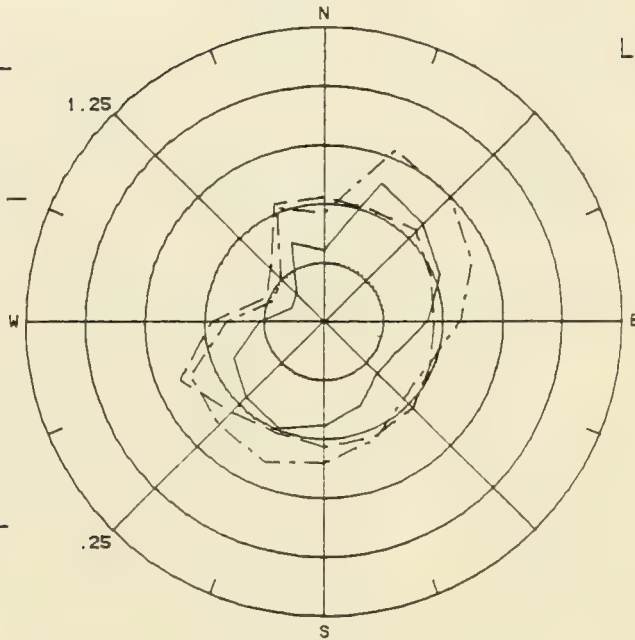
$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}}$  - - -

.25/Div

$\frac{U_{rms}}{U_{inf}}$  - - -

.05/Div

Location 31



$\frac{U_{mean}}{U_{inf}}$  ———

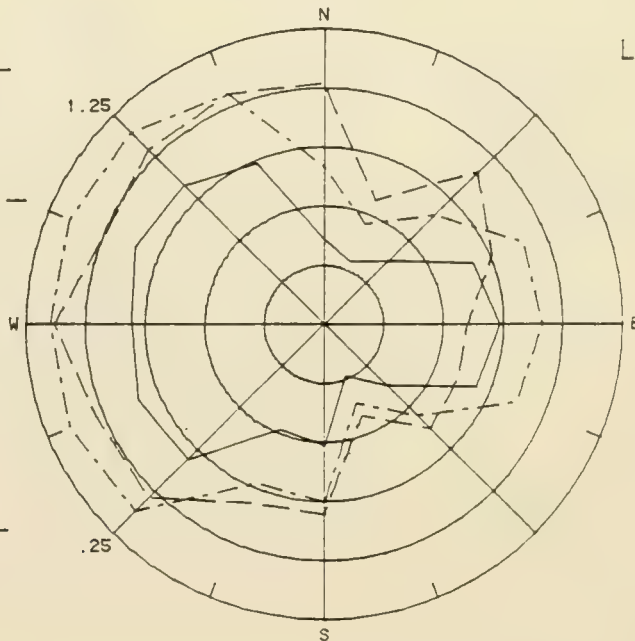
$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}}$  - - -

.25/Div

$\frac{U_{rms}}{U_{inf}}$  - - -

.05/Div

Location 32



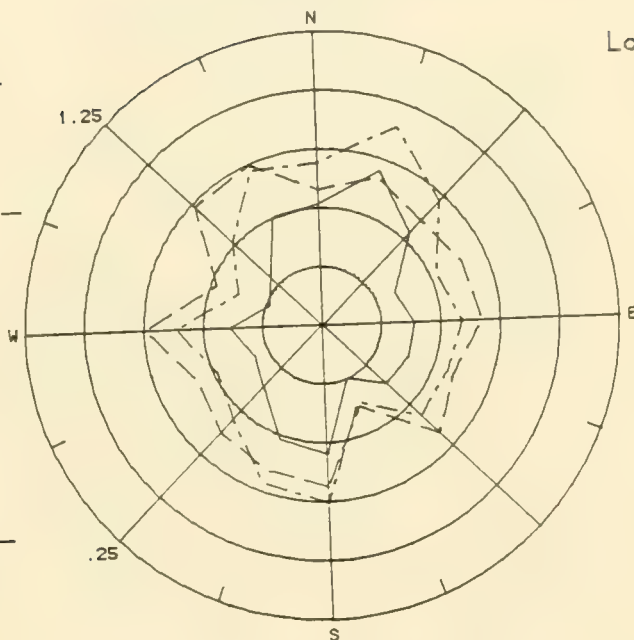
# Configuration PH 2

Location 33

$$\frac{U_{mean}}{U_{inf}} \text{ ———}$$

$$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}} \text{ - - -}$$

.25/Div



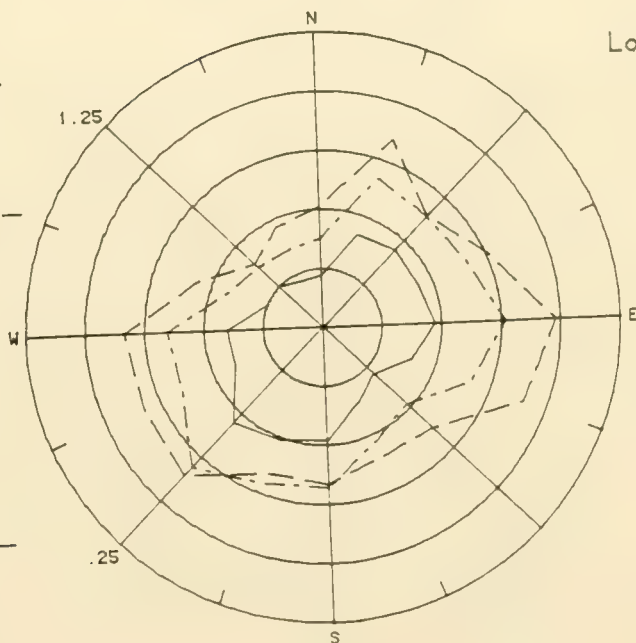
$$\frac{U_{rms}}{U_{inf}} \text{ - - -}$$

.05/Div

$$\frac{U_{mean}}{U_{inf}} \text{ ———}$$

$$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}} \text{ - - -}$$

.25/Div



$$\frac{U_{rms}}{U_{inf}} \text{ - - -}$$

.05/Div



# Configuration PH 2

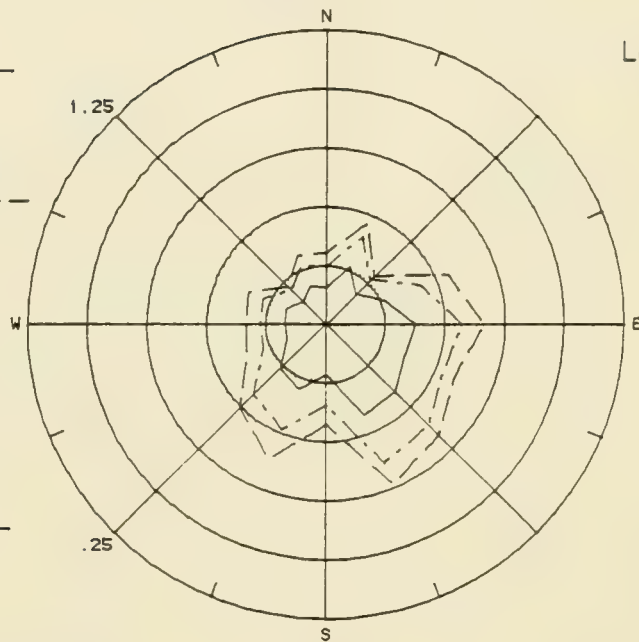
$$\frac{U_{mean}}{U_{inf}} \text{ ---}$$

$$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}} \text{ ---}$$

.25/Div

$$\frac{U_{rms}}{U_{inf}} \text{ ---}$$

.05/Div



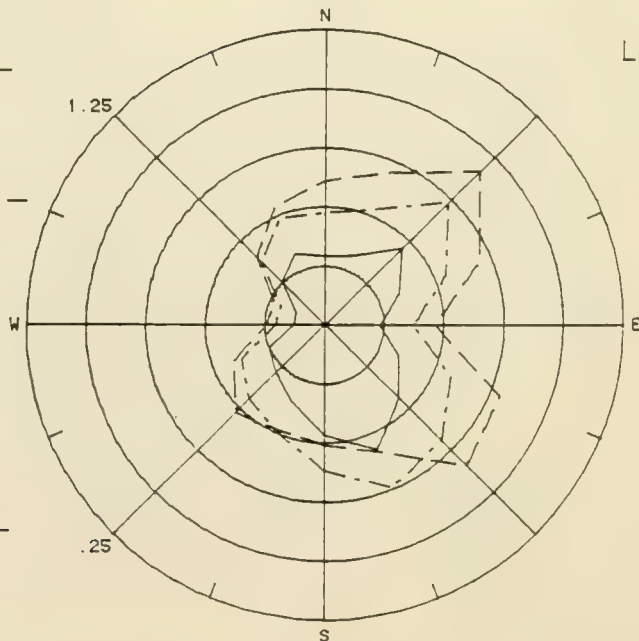
$$\frac{U_{mean}}{U_{inf}} \text{ ---}$$

$$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}} \text{ ---}$$

.25/Div

$$\frac{U_{rms}}{U_{inf}} \text{ ---}$$

.05/Div



# Configuration PH 2

Location 37

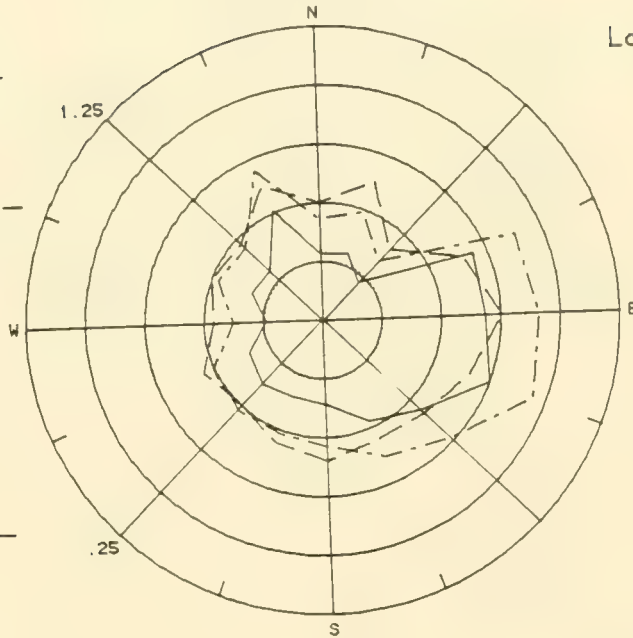
$\frac{U_{mean}}{U_{inf}}$  ———

$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}}$  - - -

.25/Div

$\frac{U_{rms}}{U_{inf}}$  - - -

.05/Div



Location 38

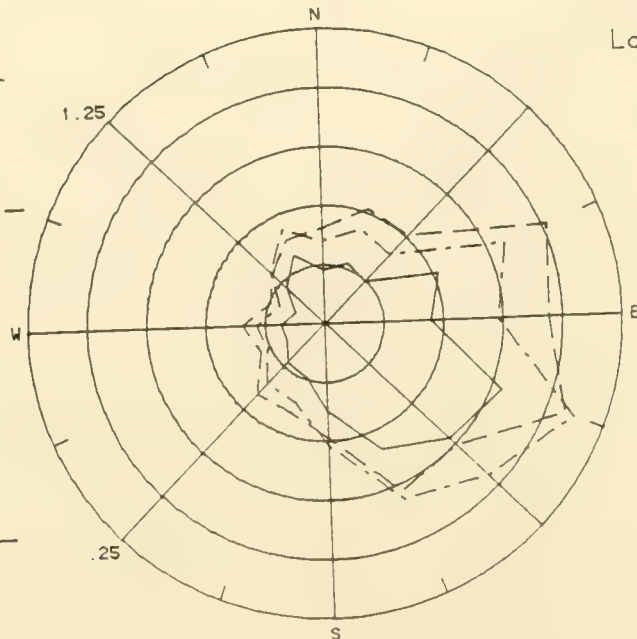
$\frac{U_{mean}}{U_{inf}}$  ———

$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}}$  - - -

.25/Div

$\frac{U_{rms}}{U_{inf}}$  - - -

.05/Div



# Configuration PH 2

$\frac{U_{mean}}{U_{inf}}$  ———

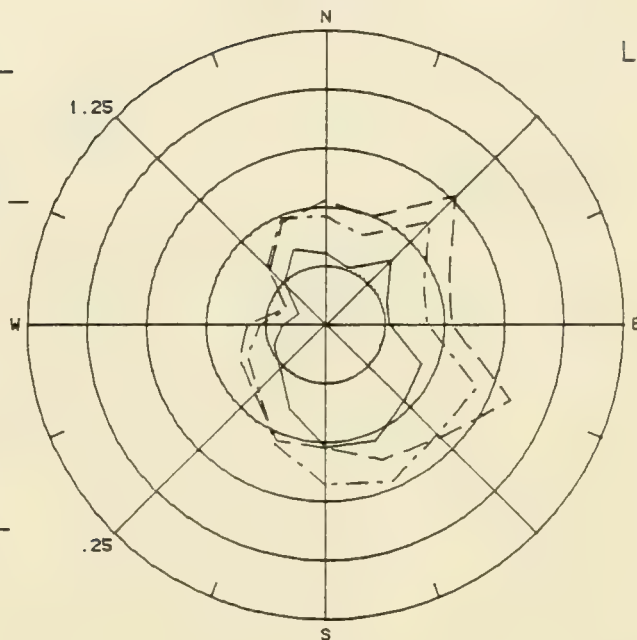
$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}}$  - - -

.25/Div

$\frac{U_{rms}}{U_{inf}}$  - - -

.05/Div

Location 39



$\frac{U_{mean}}{U_{inf}}$  ———

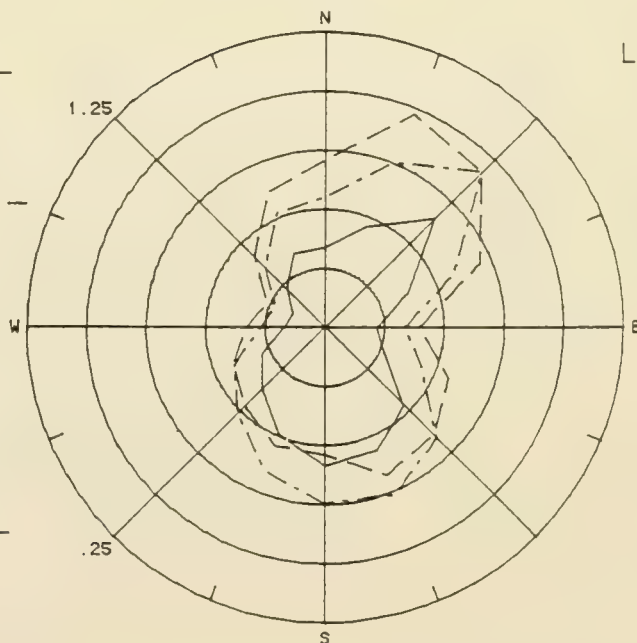
$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}}$  - - -

.25/Div

$\frac{U_{rms}}{U_{inf}}$  - - -

.05/Div

Location 40



# Configuration PH 2

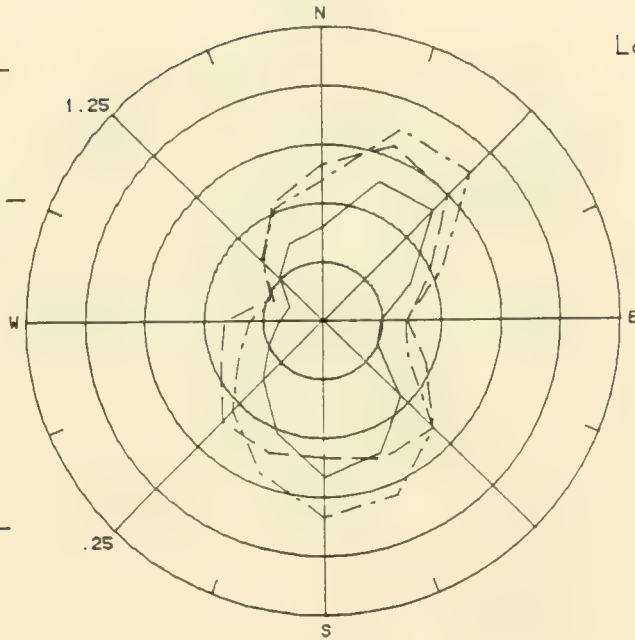
$\frac{U_{mean}}{U_{inf}}$  ———

$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}}$  - - -

.25/Div

$\frac{U_{rms}}{U_{inf}}$  - - -

.05/Div



Location 41

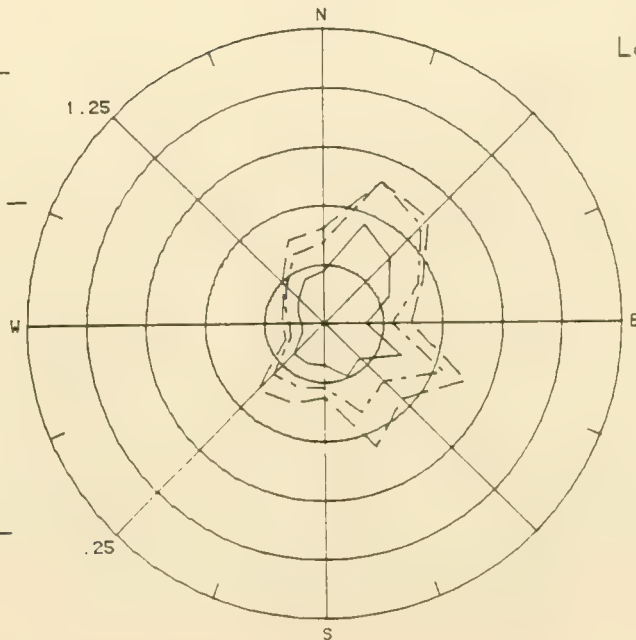
$\frac{U_{mean}}{U_{inf}}$  ———

$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}}$  - - -

.25/Div

$\frac{U_{rms}}{U_{inf}}$  - - -

.05/Div



Location 42

# Configuration PH 2

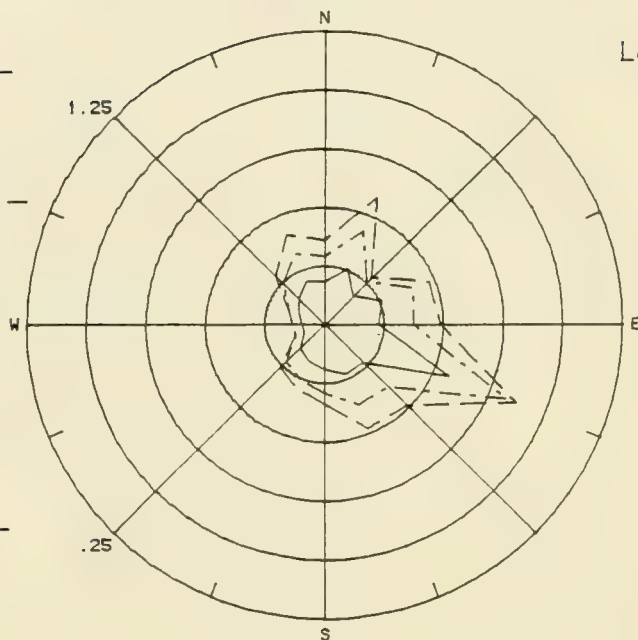
$\frac{U_{mean}}{U_{inf}}$  ———

$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}}$  - - -

.25/Div

$\frac{U_{rms}}{U_{inf}}$  - - -

.05/Div



Location 43

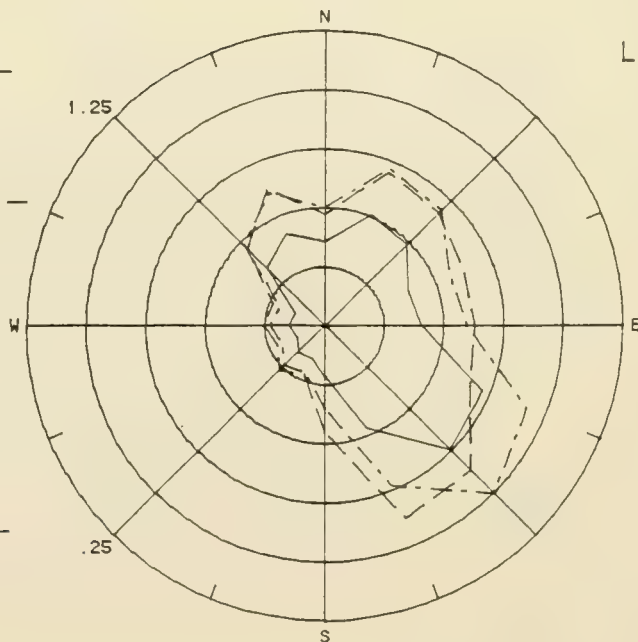
$\frac{U_{mean}}{U_{inf}}$  ———

$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}}$  - - -

.25/Div

$\frac{U_{rms}}{U_{inf}}$  - - -

.05/Div



Location 44



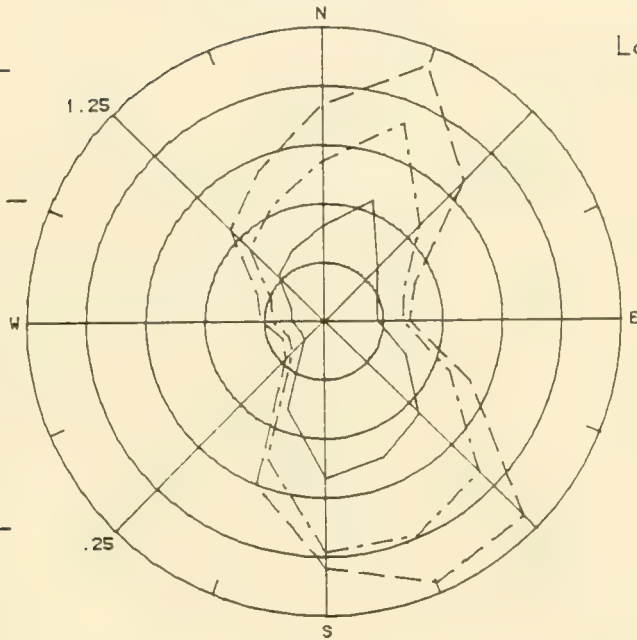
# Configuration PH 2

$\frac{U_{mean}}{U_{inf}}$  ———

$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}}$  - - -

$\frac{U_{rms}}{U_{inf}}$  - - -

.25/Div



Location 45

$\frac{U_{rms}}{U_{inf}}$  - - -

$\frac{U_{rms}}{U_{inf}}$  - - -

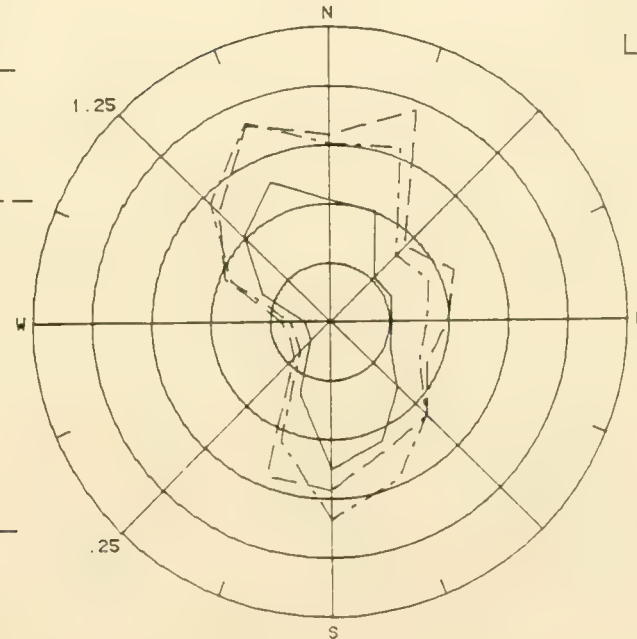
.05/Div

$\frac{U_{mean}}{U_{inf}}$  ———

$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}}$  - - -

$\frac{U_{rms}}{U_{inf}}$  - - -

.25/Div



Location 46

# Configuration PH 2

Location 47

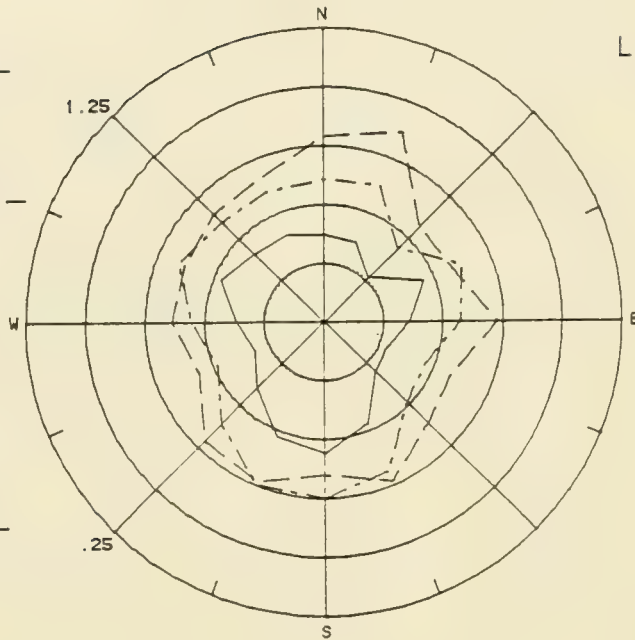
$\frac{U_{mean}}{U_{inf}}$  ———

$\frac{U_{mean} + 1.5 \cdot U_{rms}}{U_{inf}}$  - - -

.25/Div

$\frac{U_{rms}}{U_{inf}}$  - - -

.05/Div

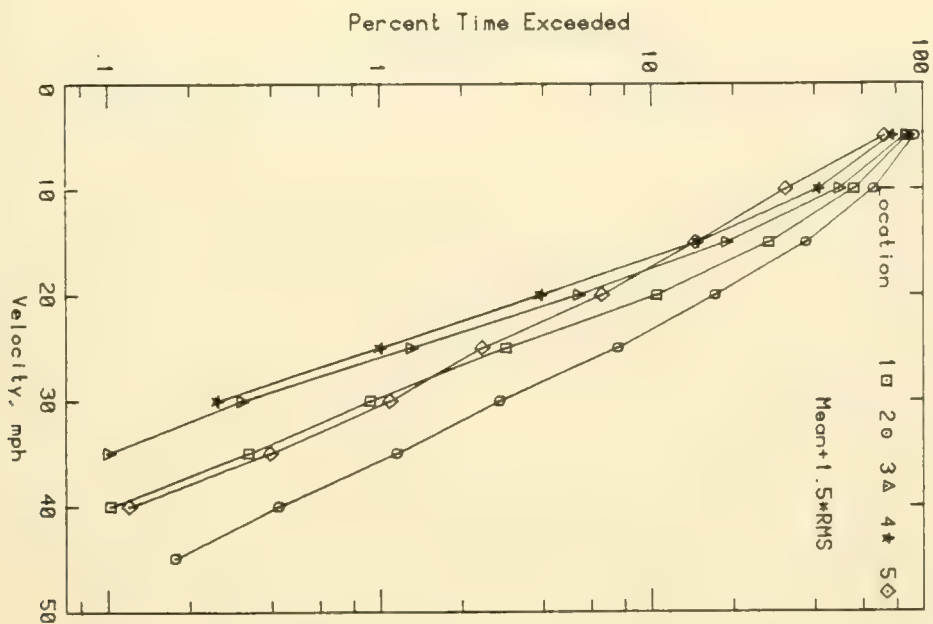
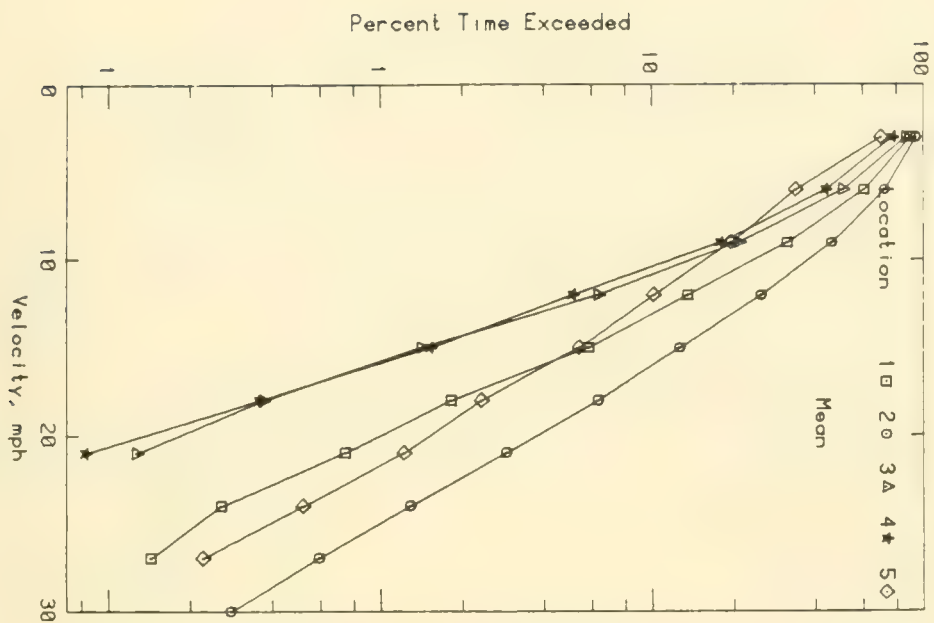


APPENDIX D

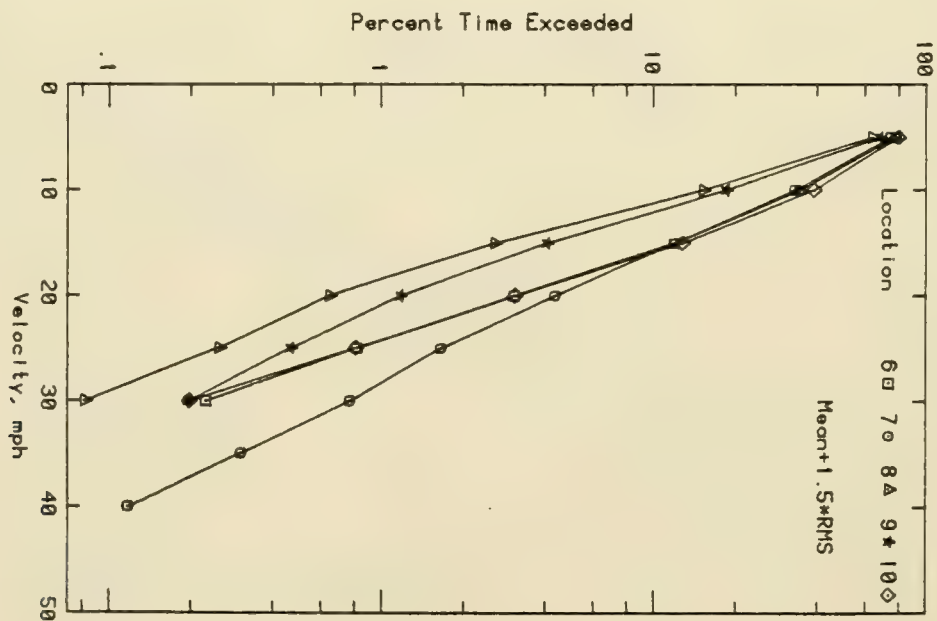
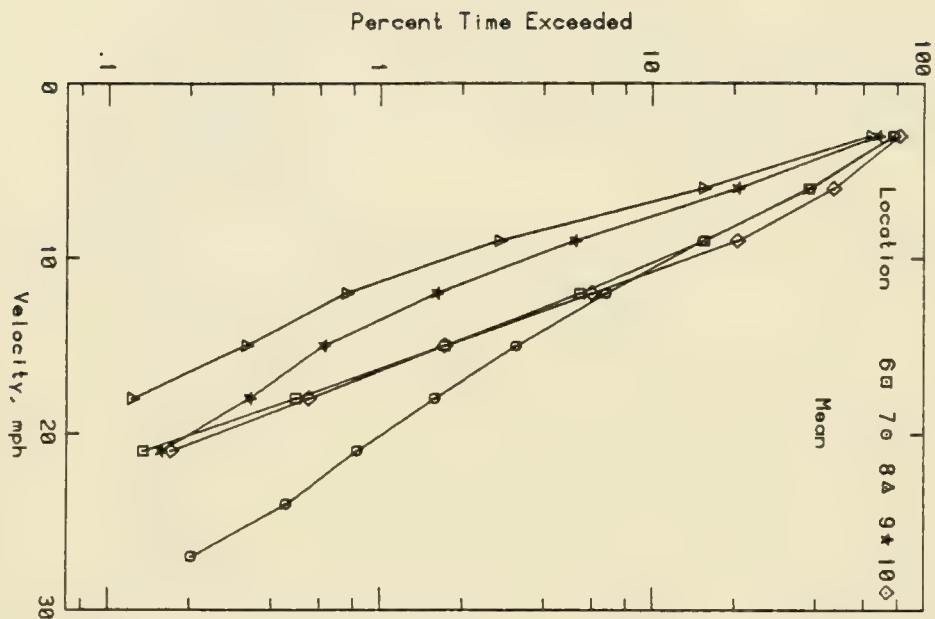
PERCENT TIME EXCEEDED PLOTS

#### PERCENT TIME EXCEEDED PLOTS

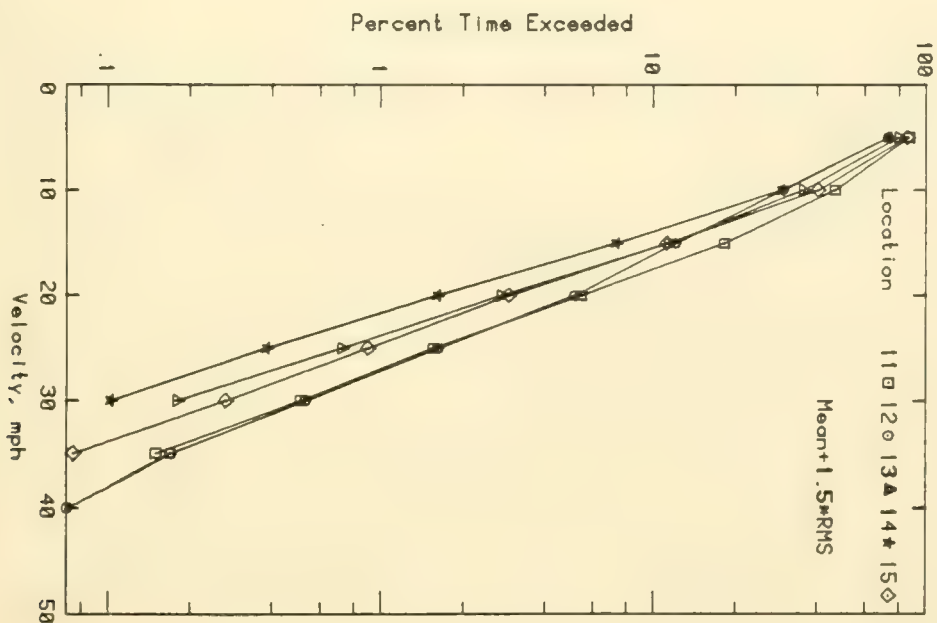
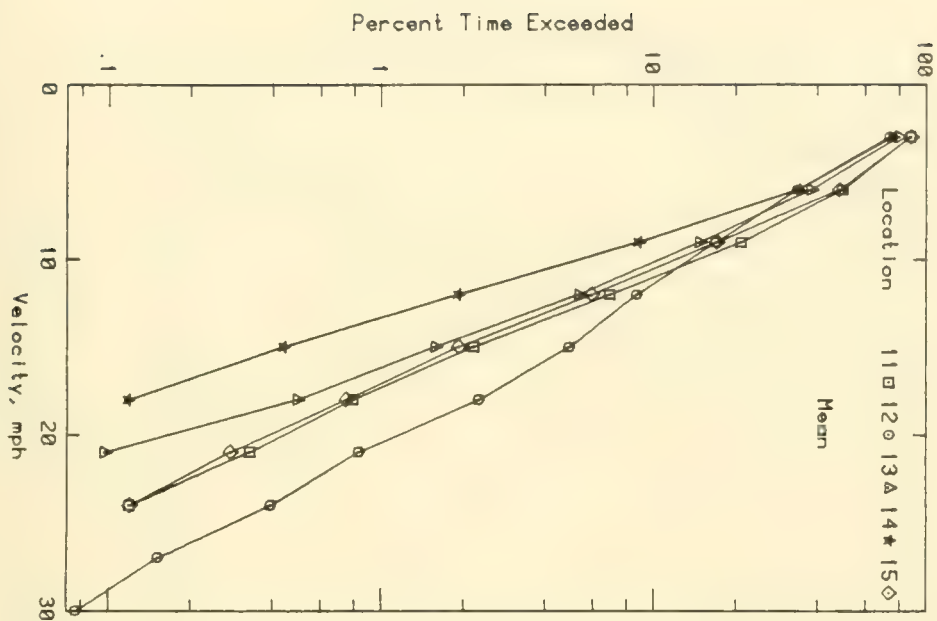
The graphs included in this appendix show the percent of time for which a given mean or gust velocity is exceeded for each pedestrian location for each configuration.

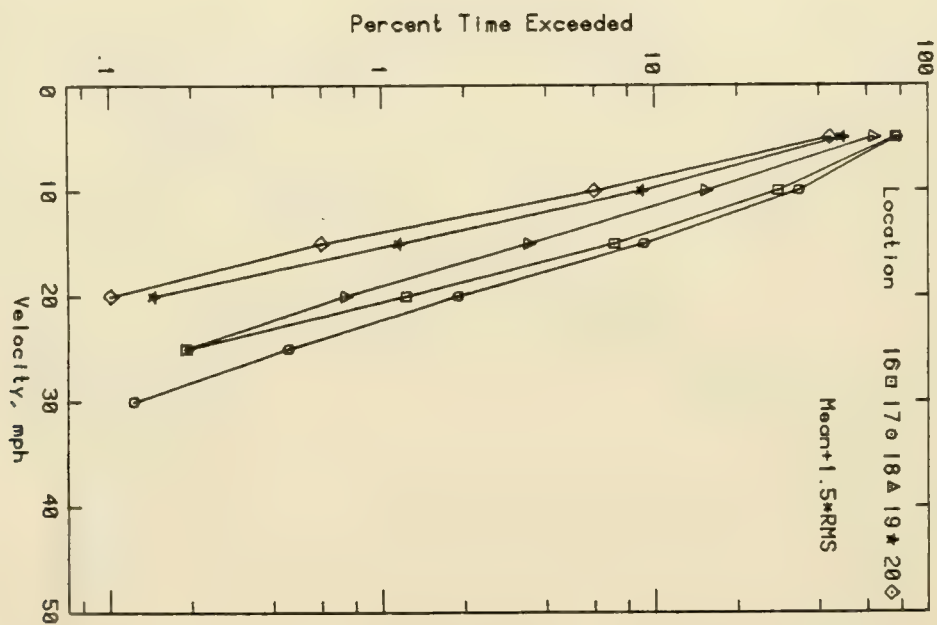
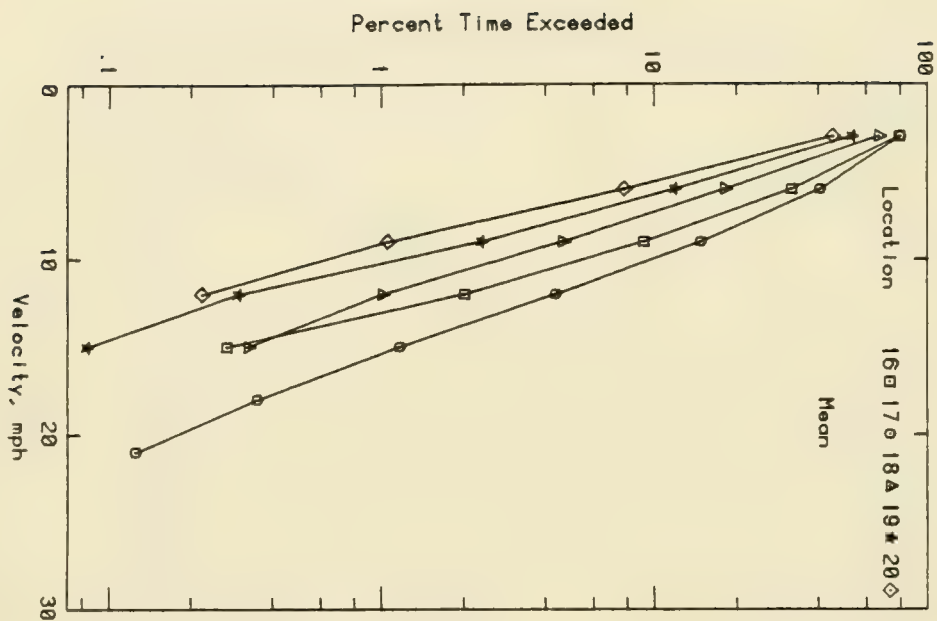




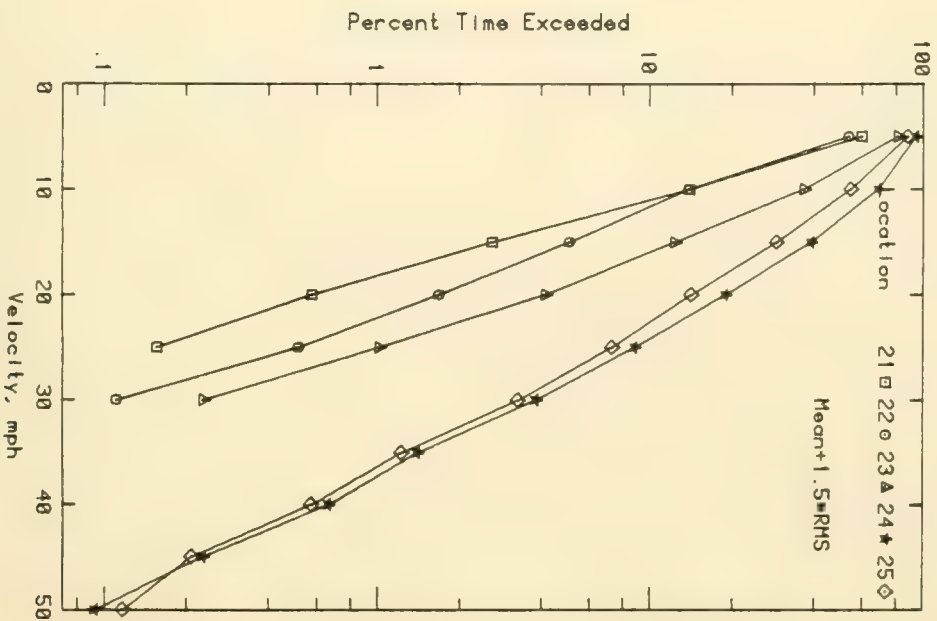
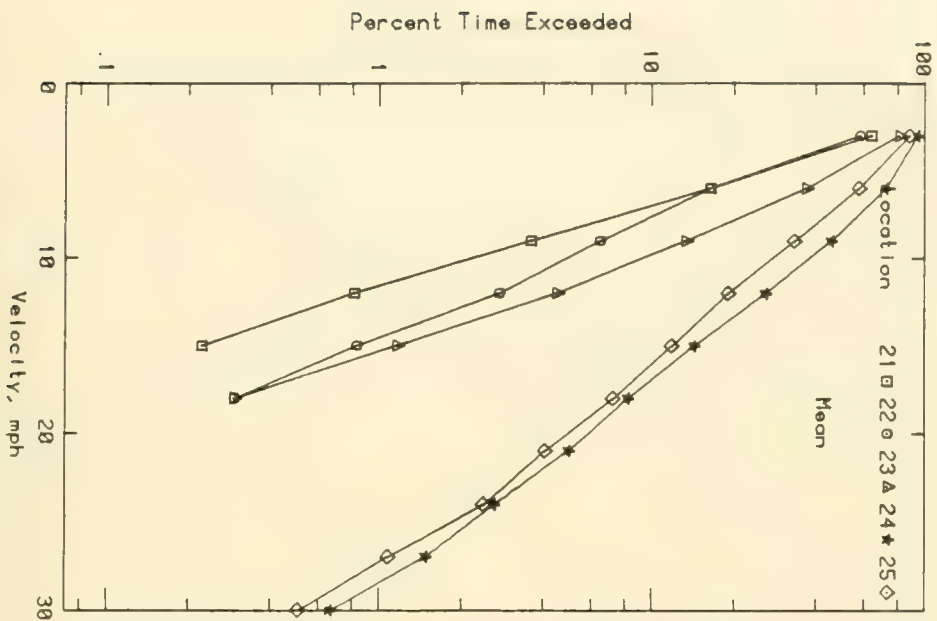


Percent Time Exceeded for PRE Configuration

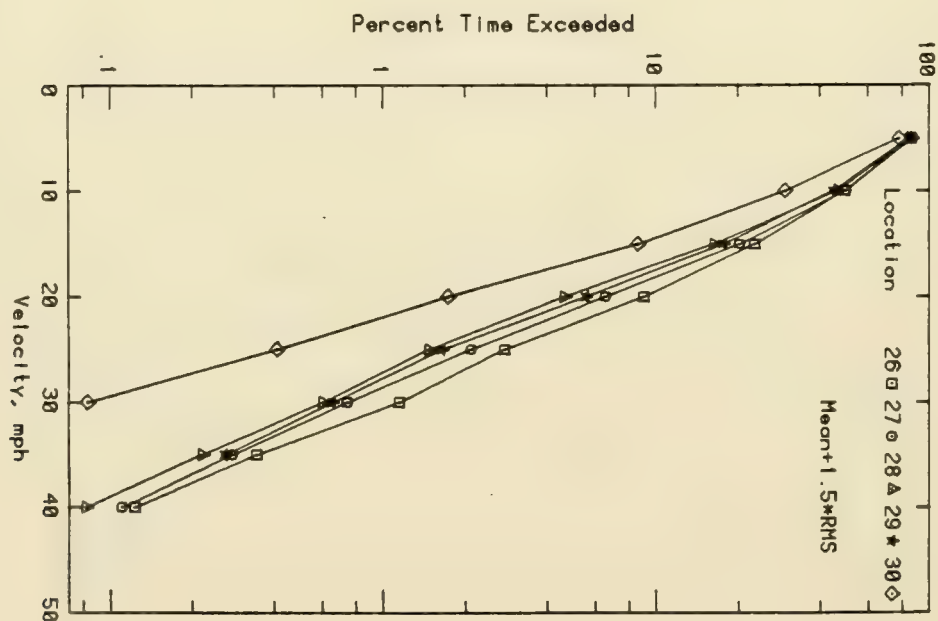
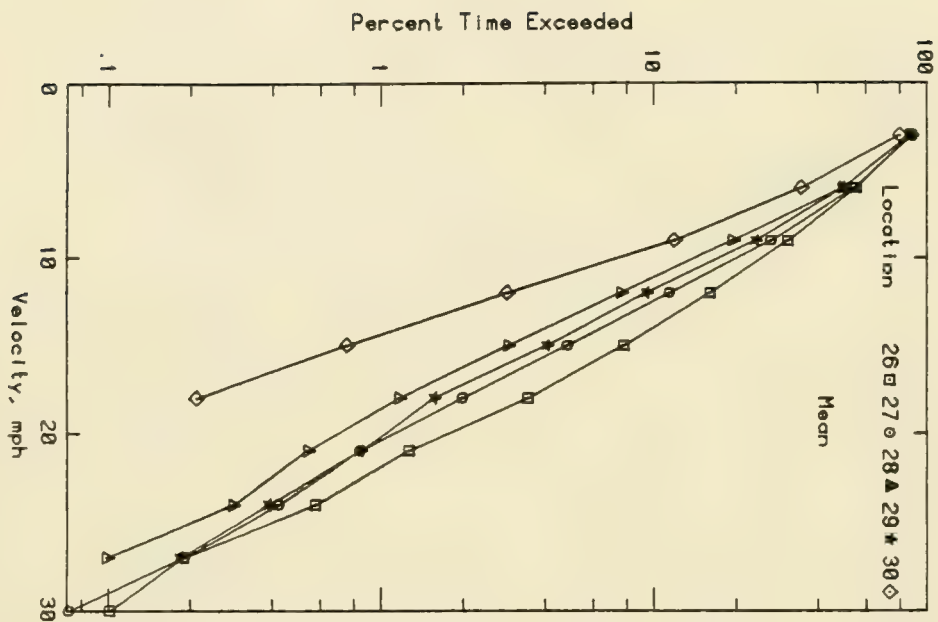




Percent Time Exceeded for PRE Configuration

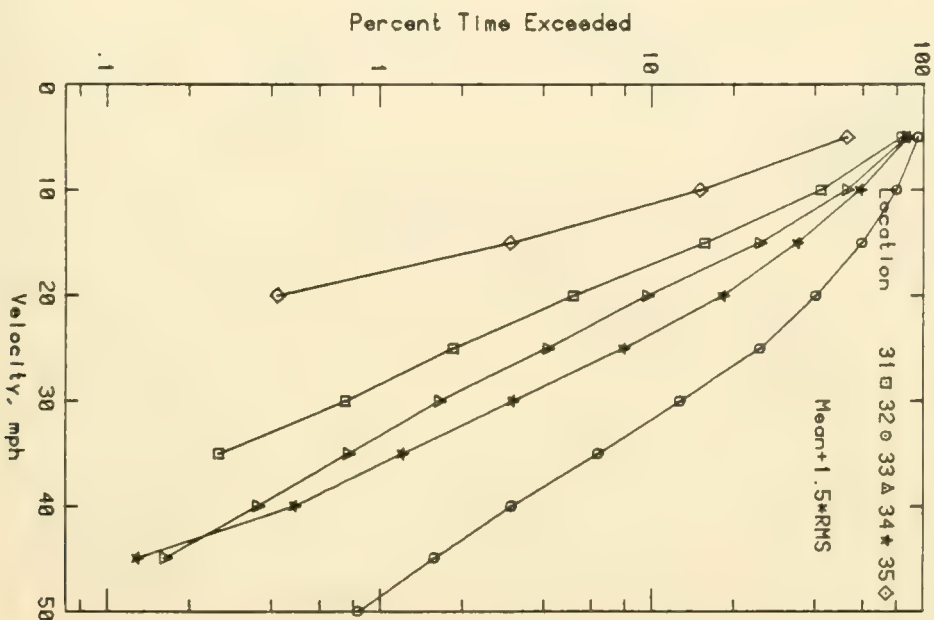
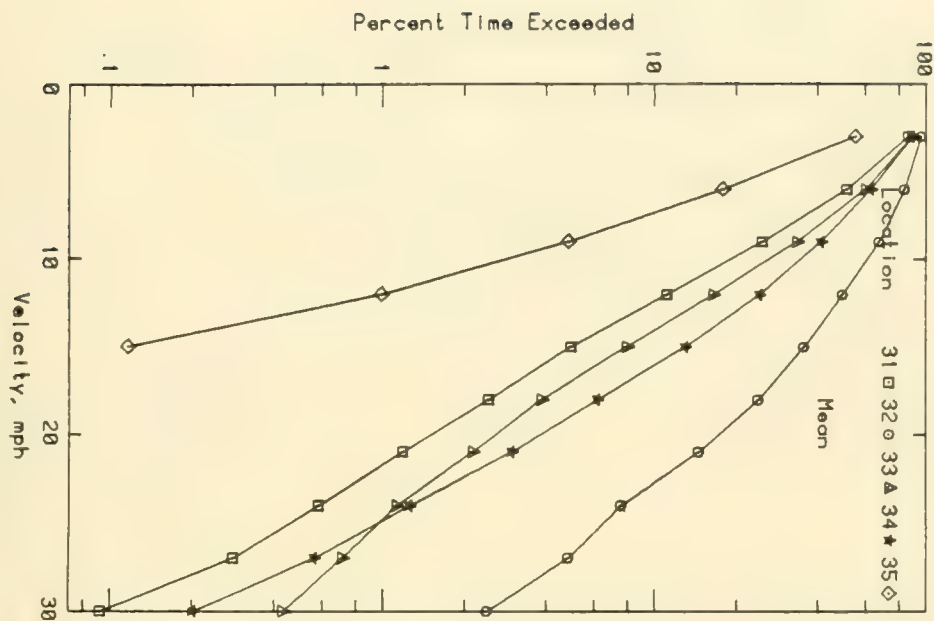


Percent Time Exceeded for PRE Configuration

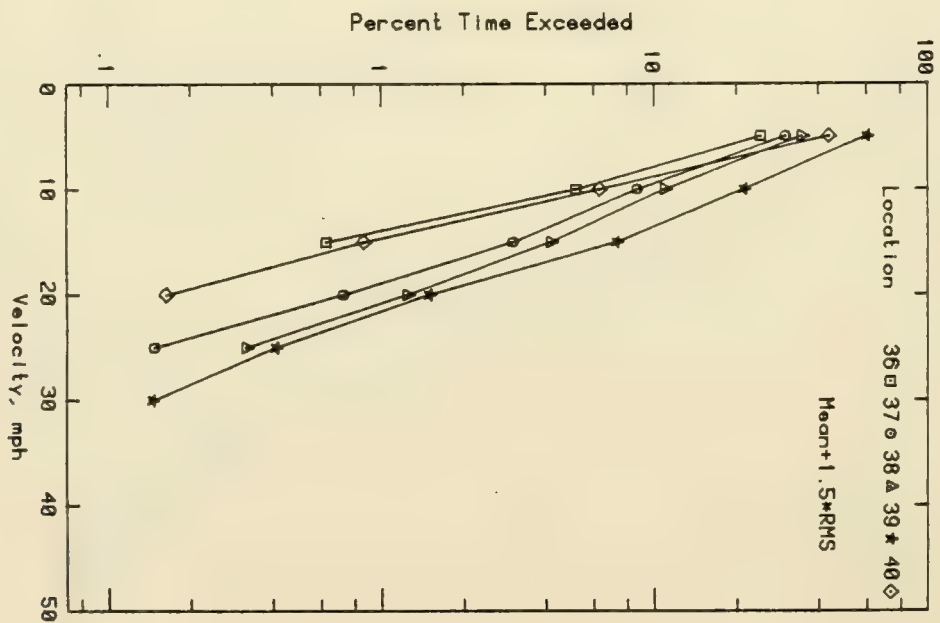
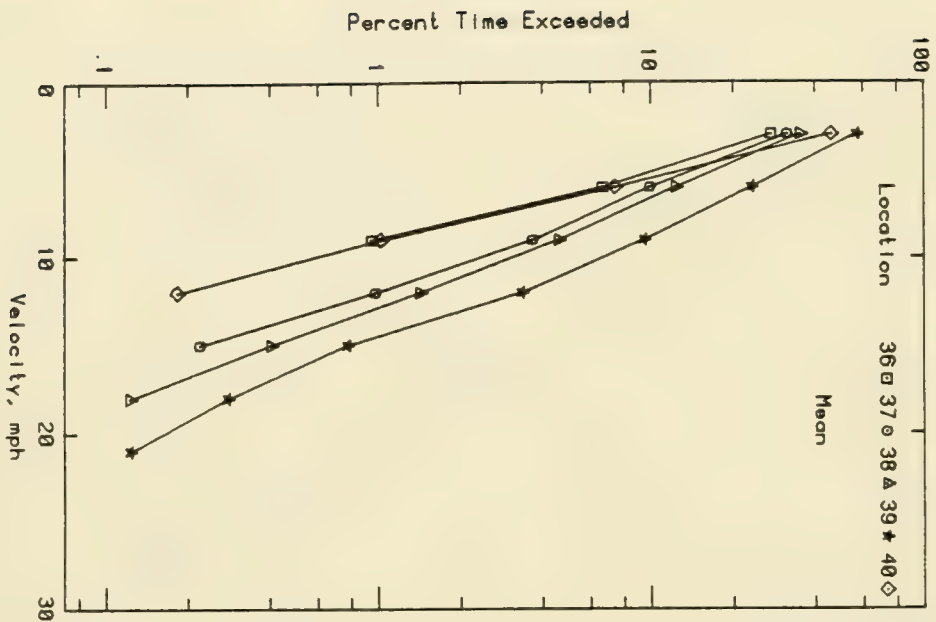


Percent Time Exceeded for PRE Configuration

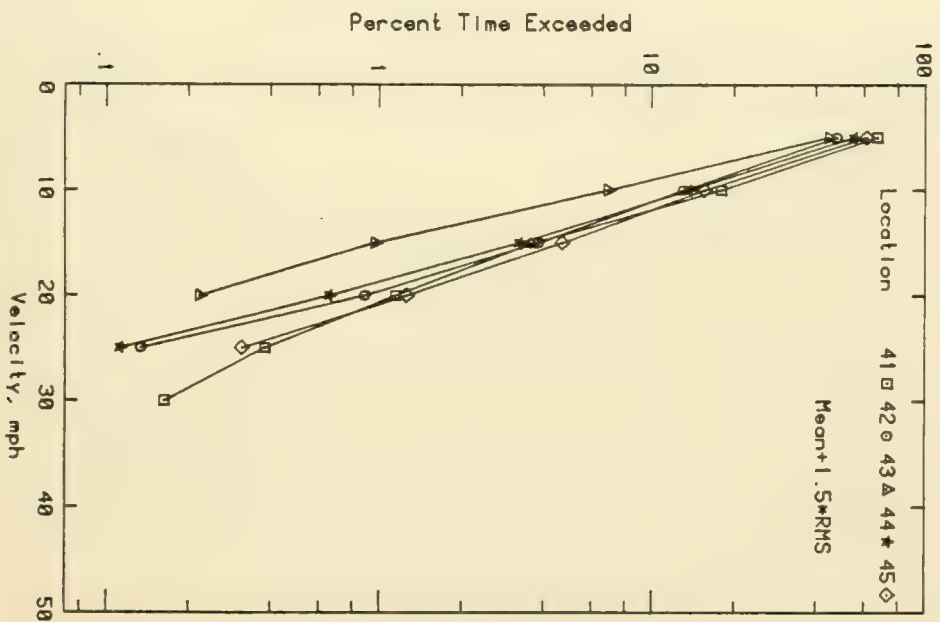
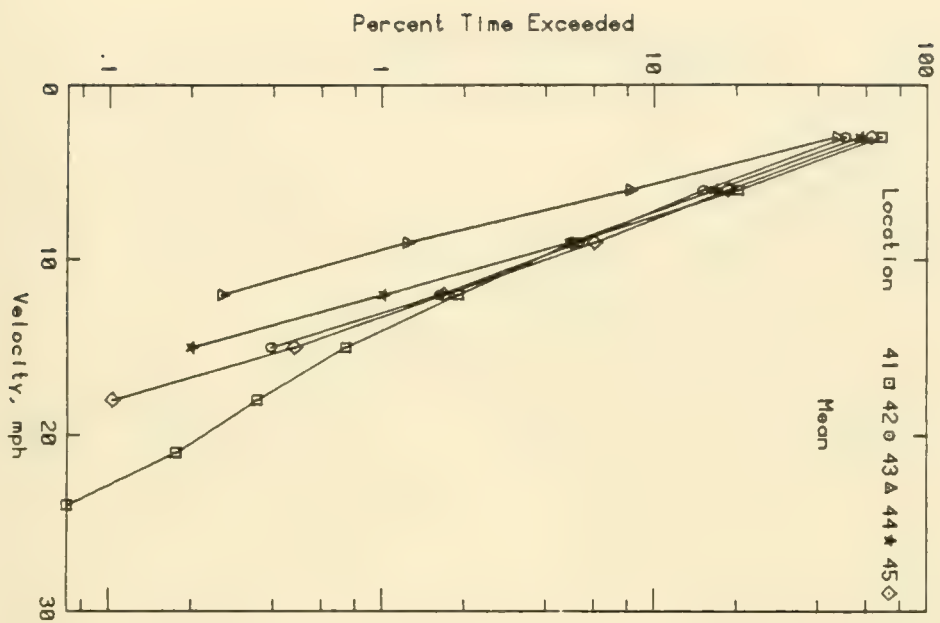


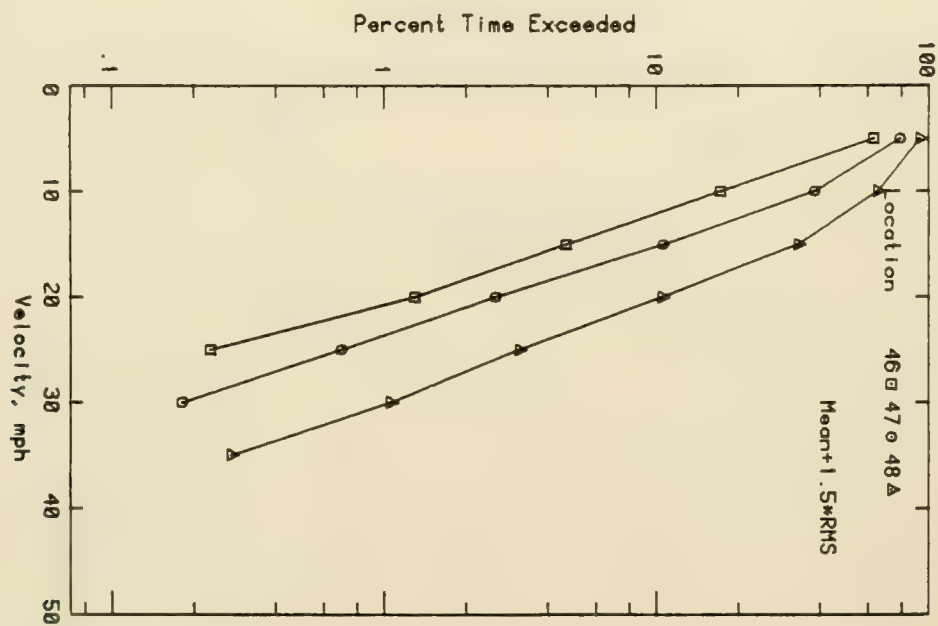
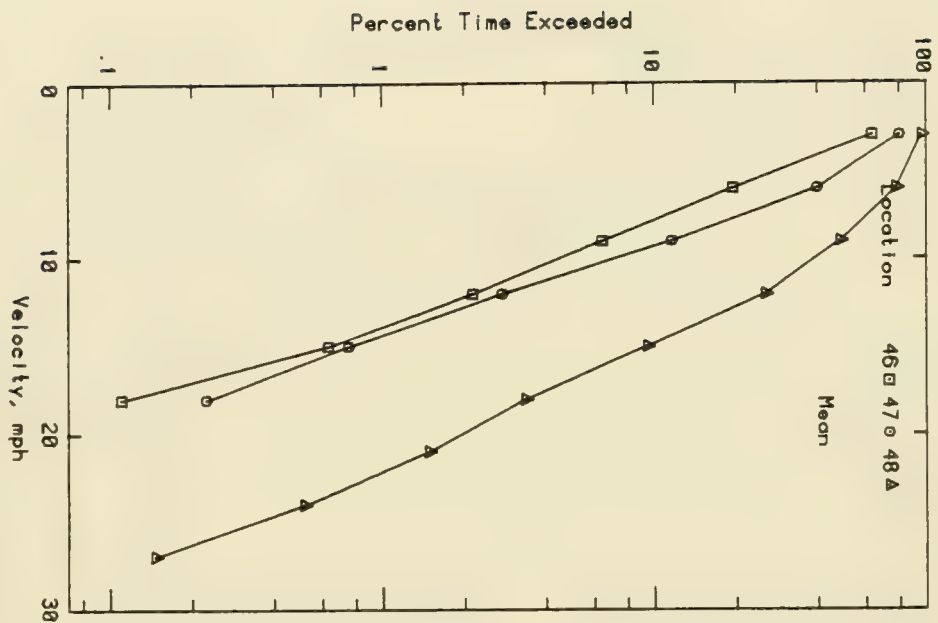


Percent Time Exceeded for PRE Configuration

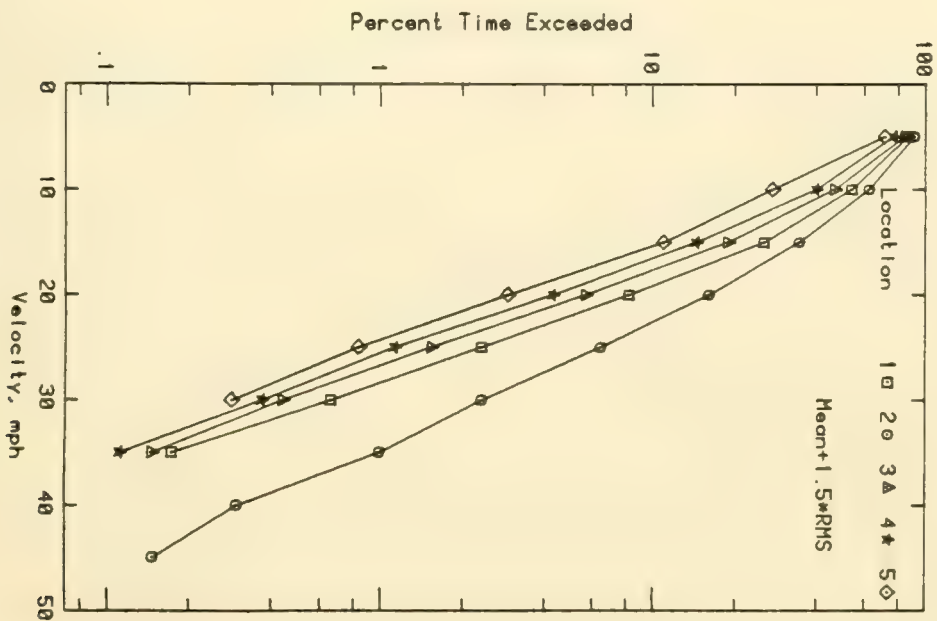
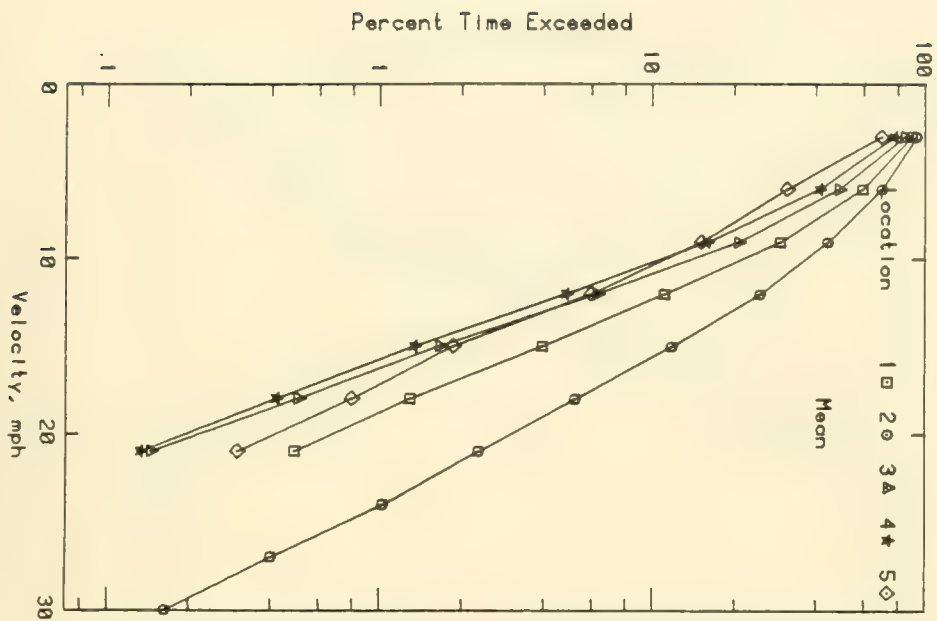


Percent Time Exceeded for PRE Configuration

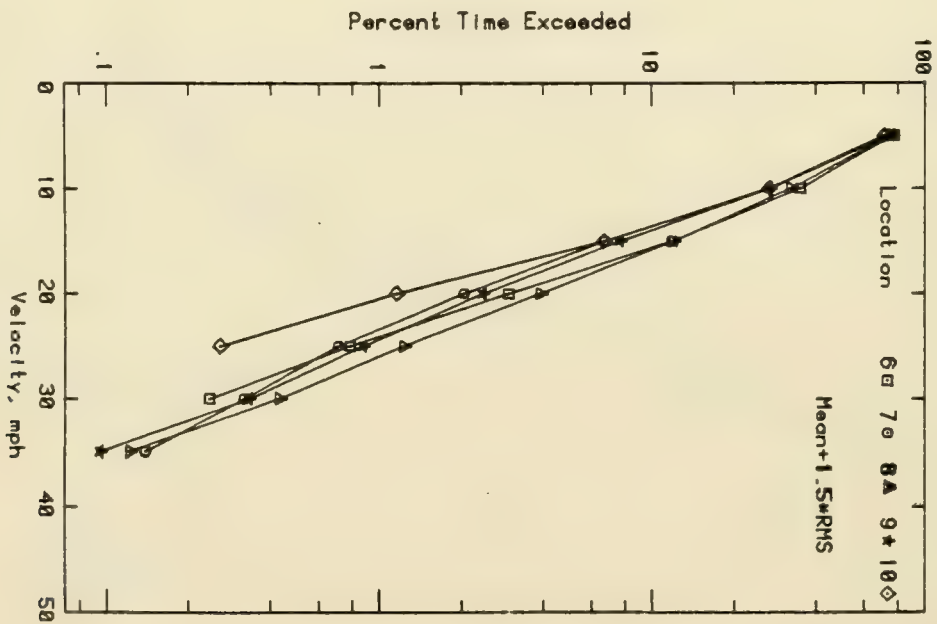
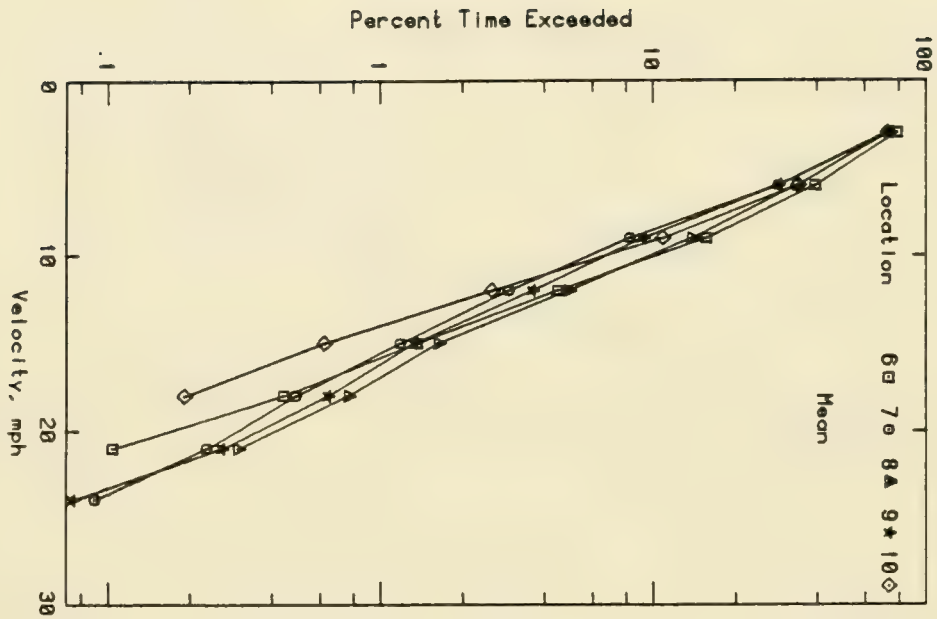




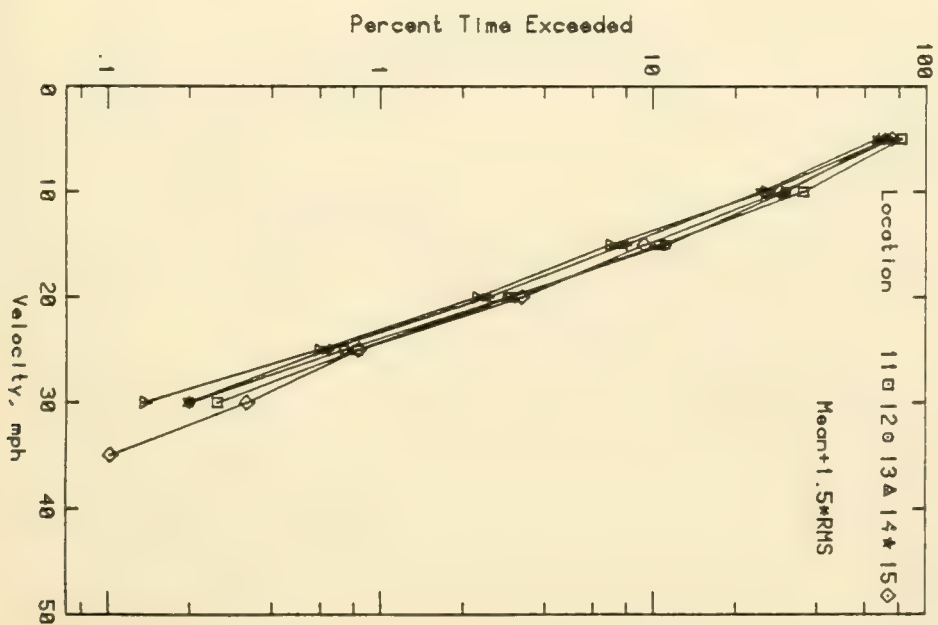
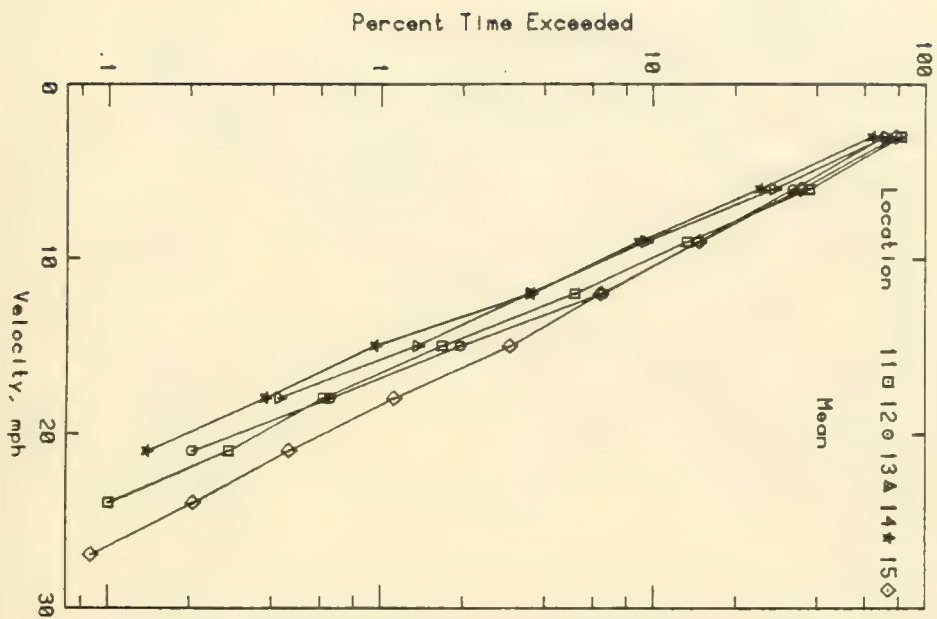
Percent Time Exceeded for PFE Configuration

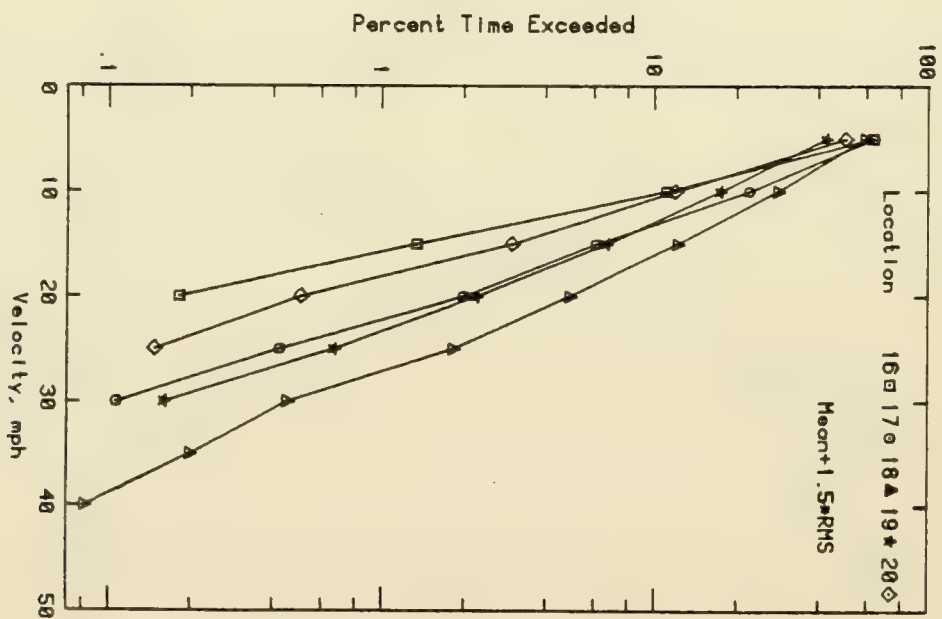
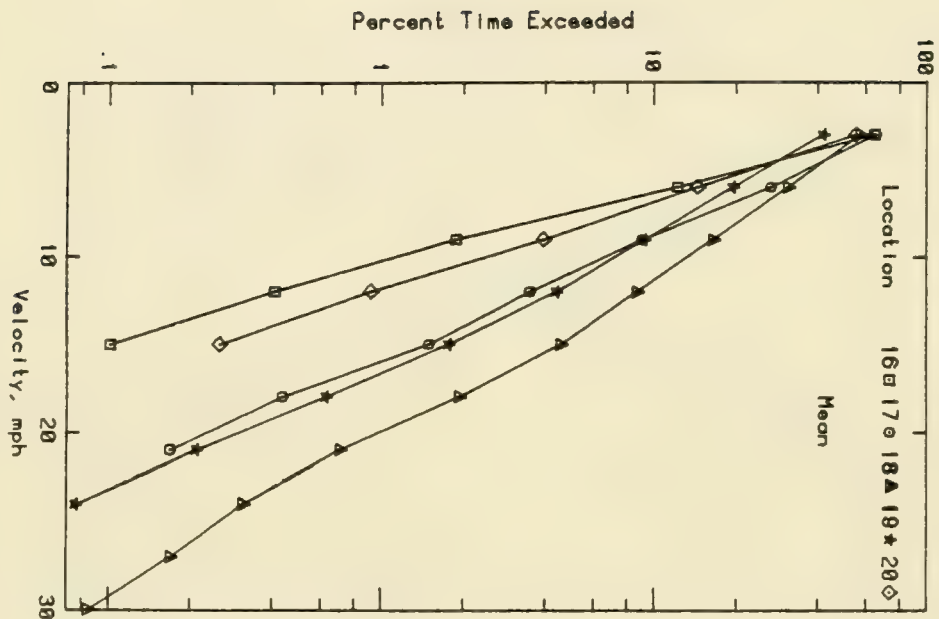




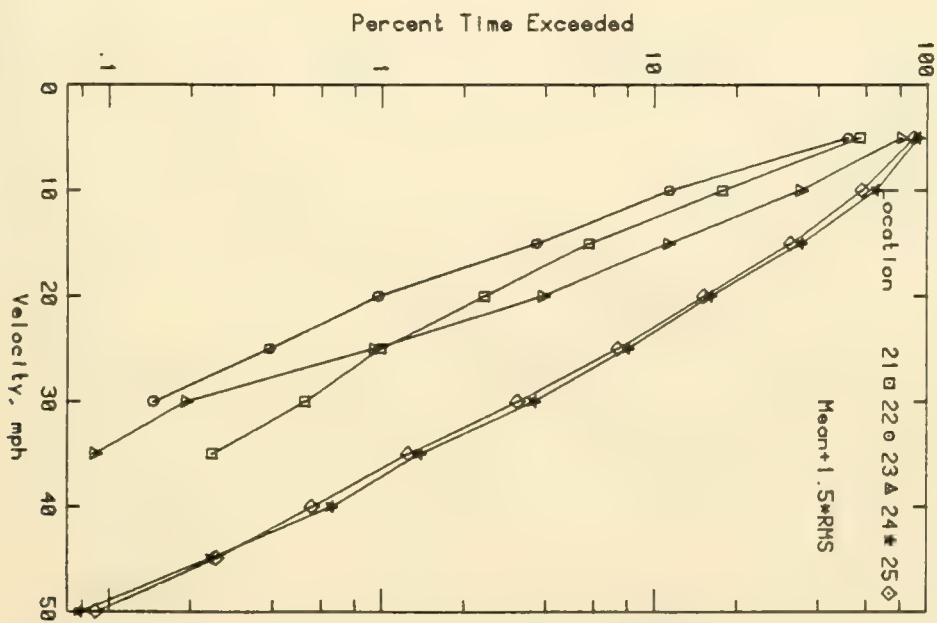
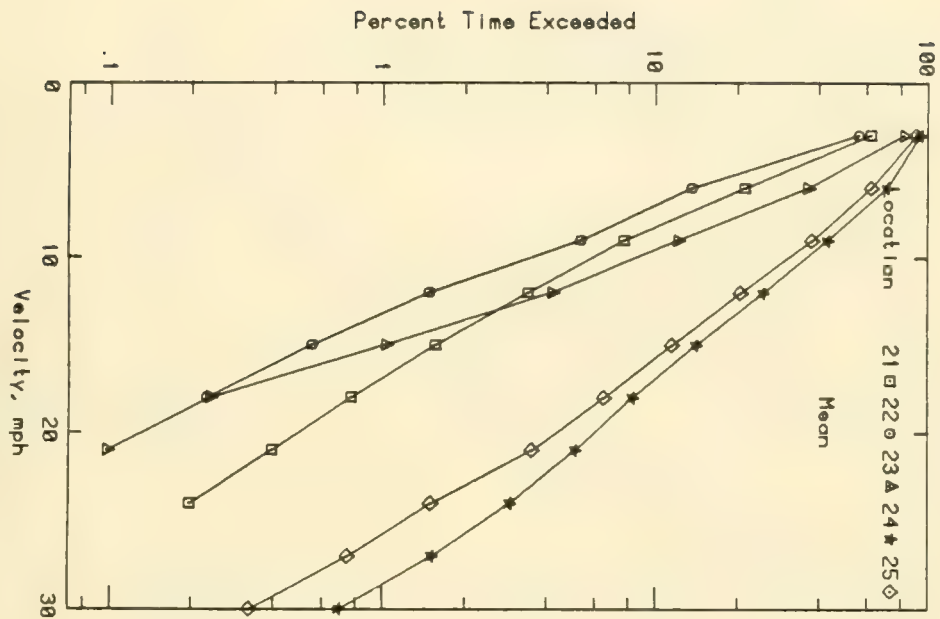


Percent Time Exceeded for PHI Configuration

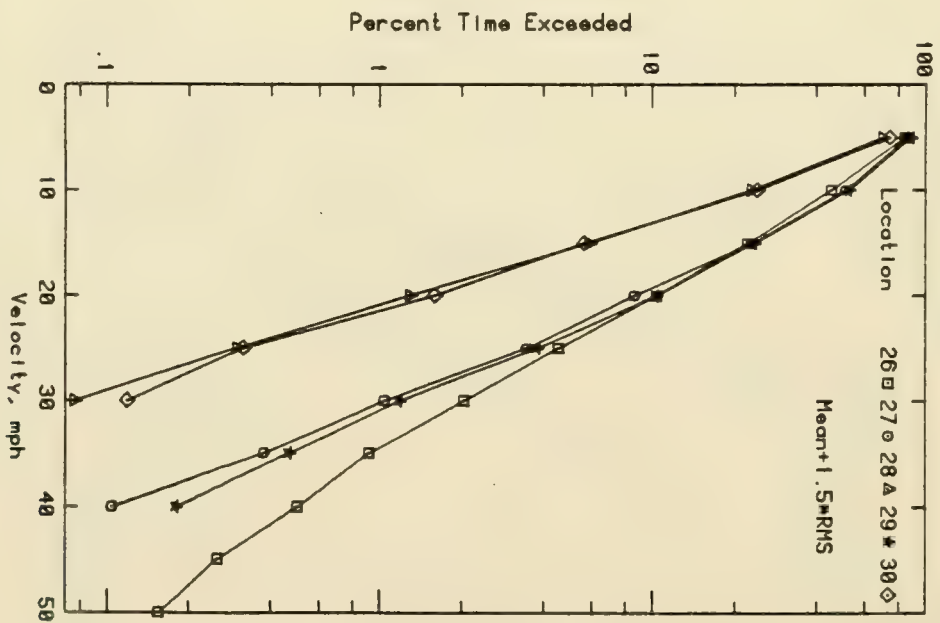
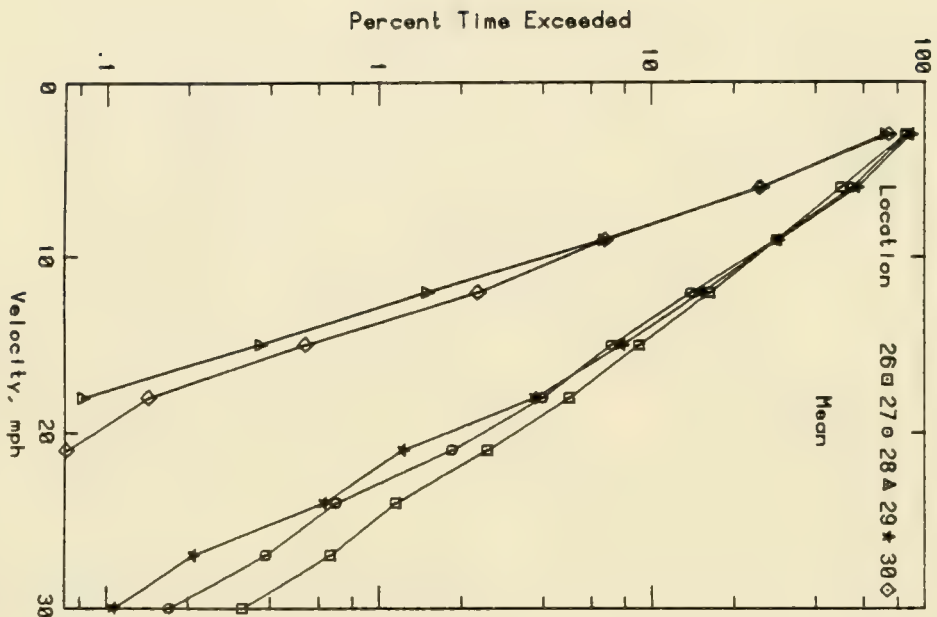




Percent Time Exceeded for PHL Configuration

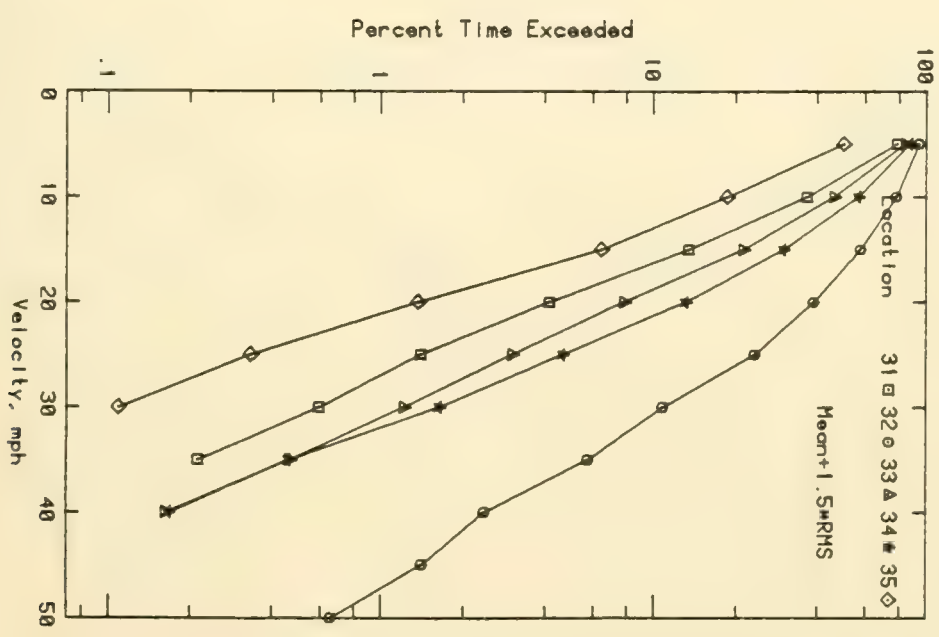
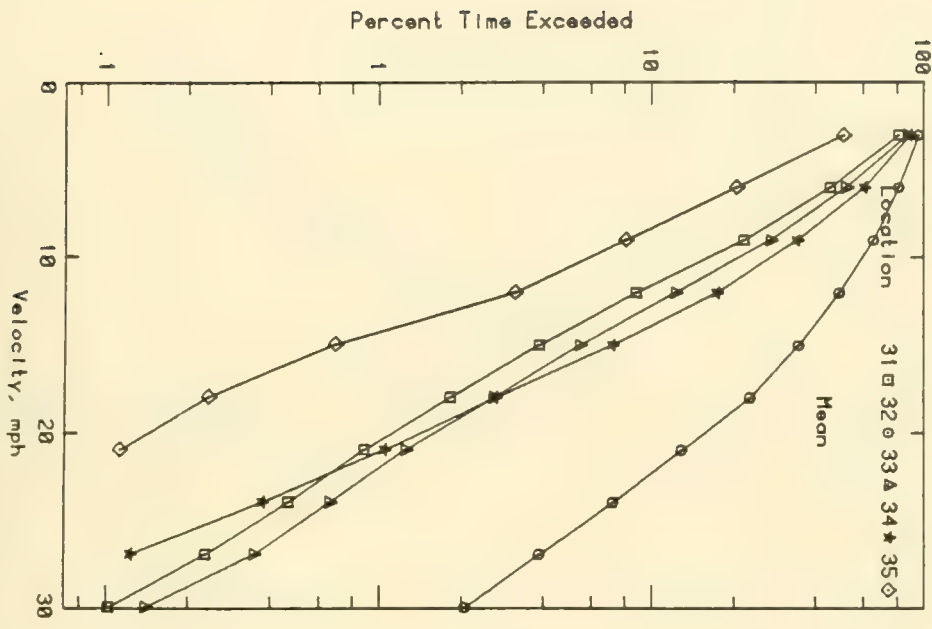


# Percent Time Exceeded for PH1 Configuration

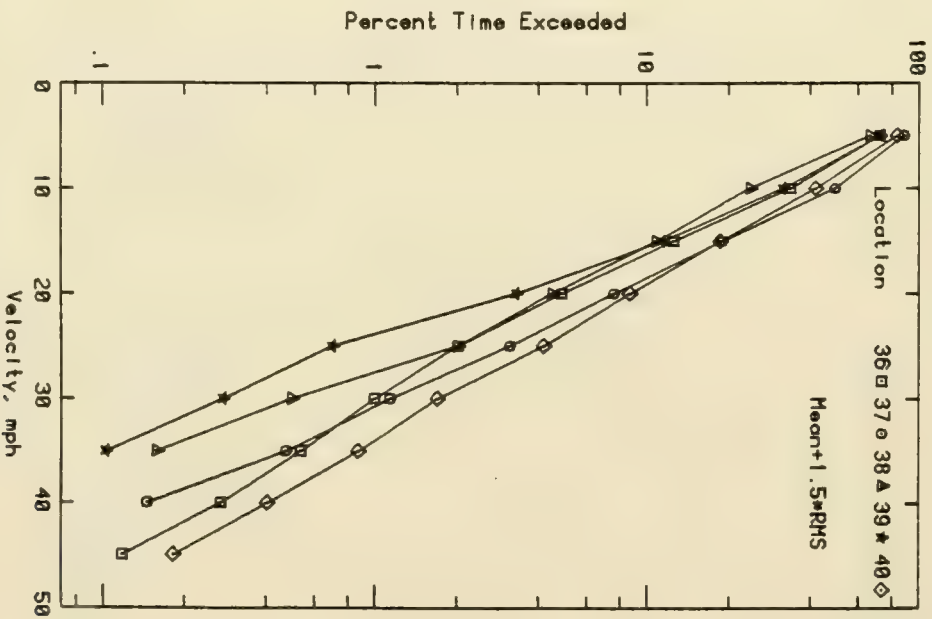
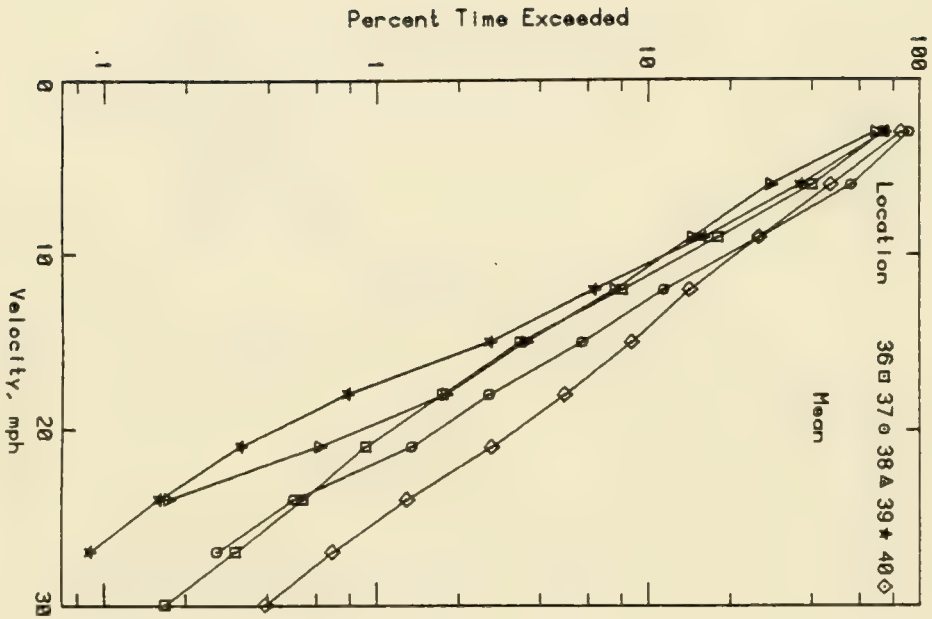


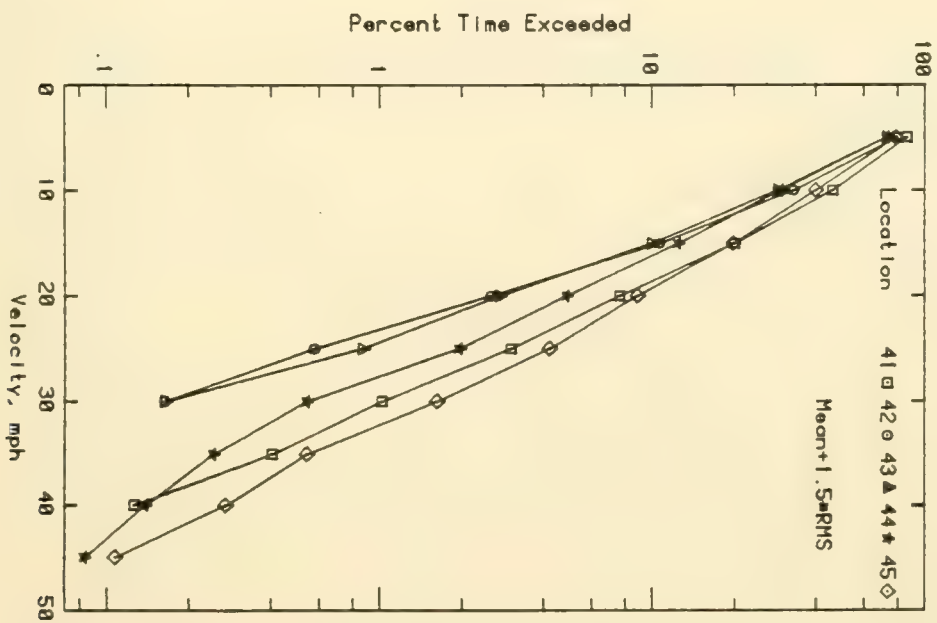
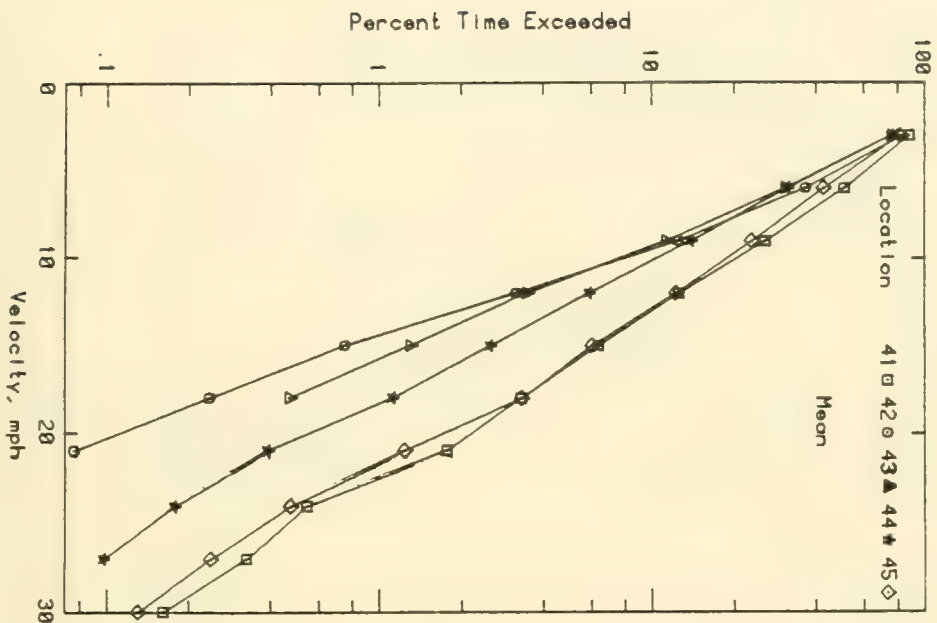


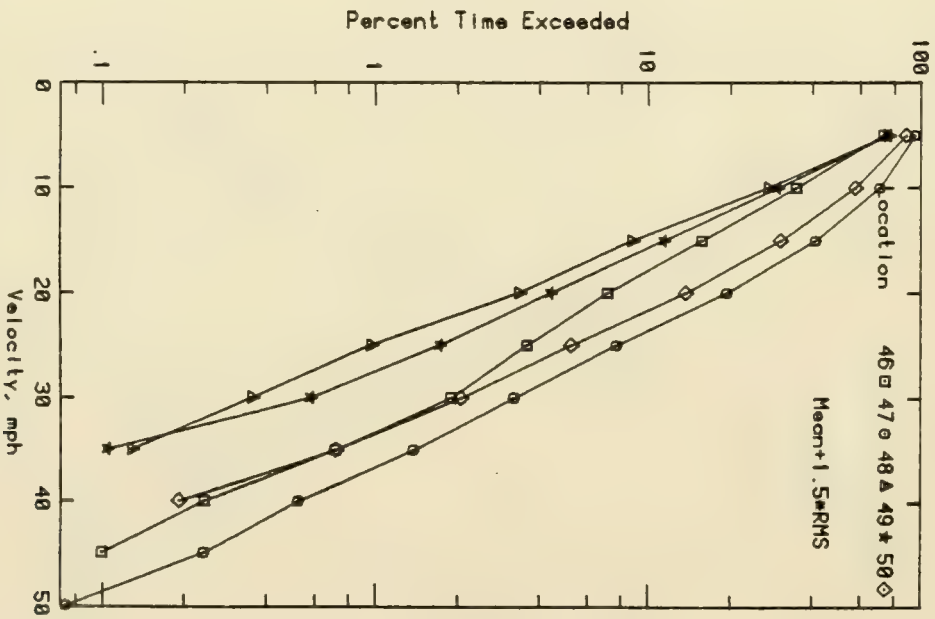
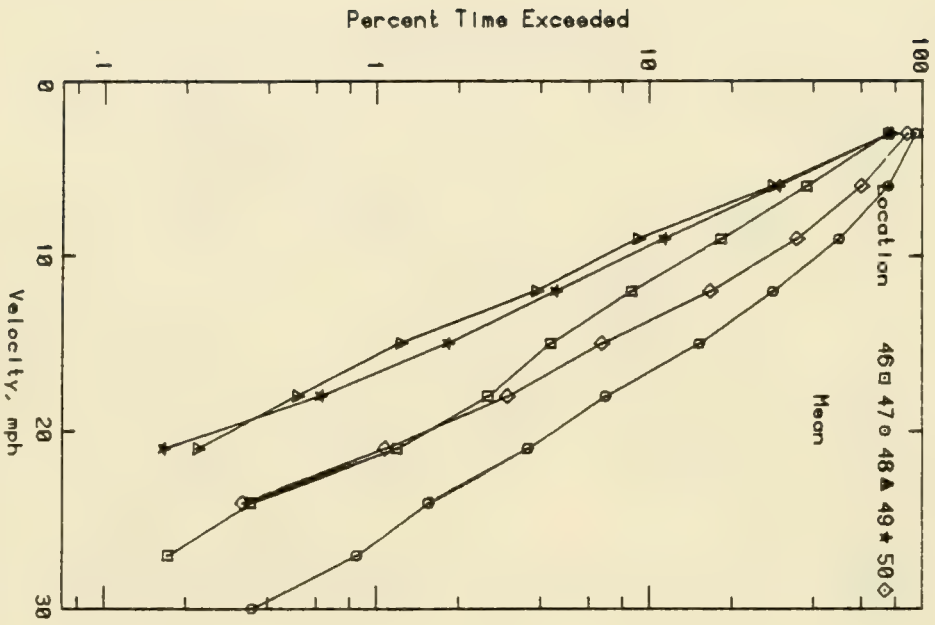
Percent Time Exceeded for PH1 Configuration



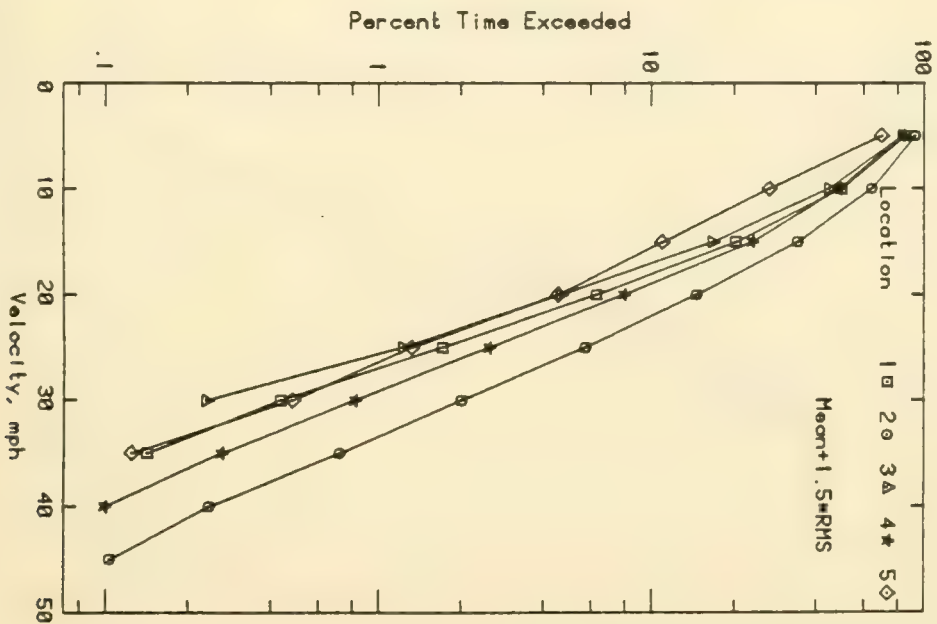
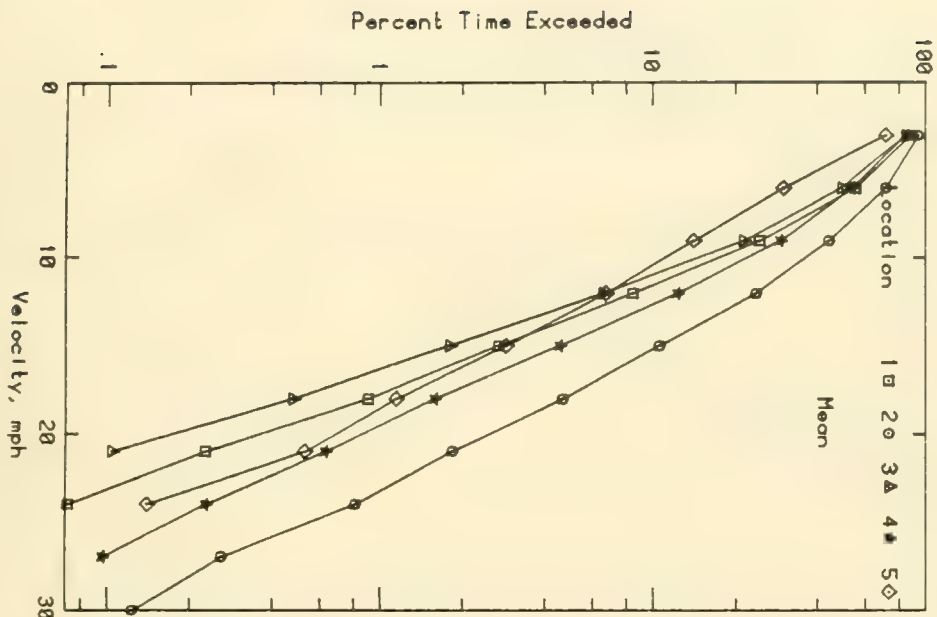
# Percent Time Exceeded for PHL Configuration





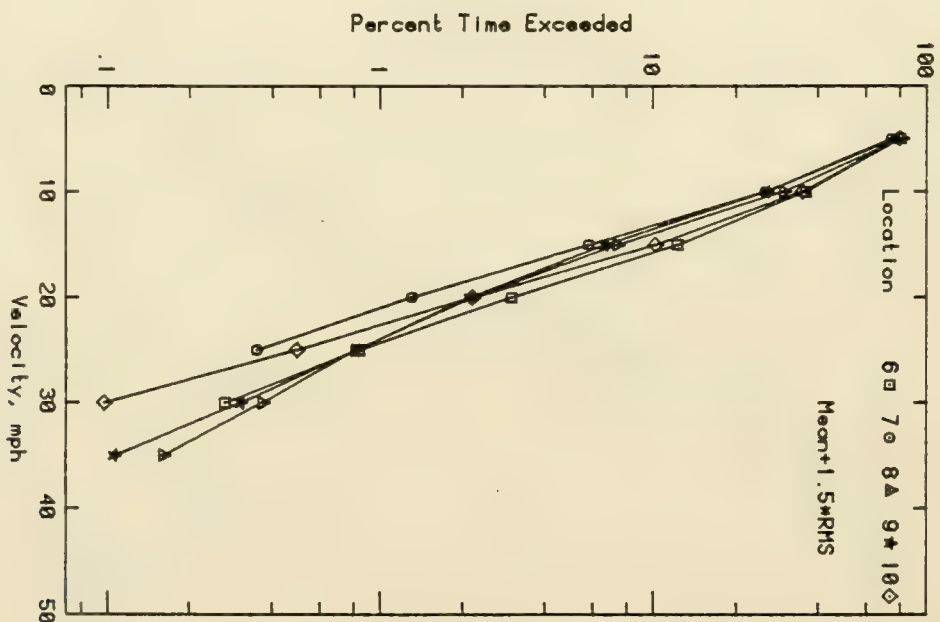
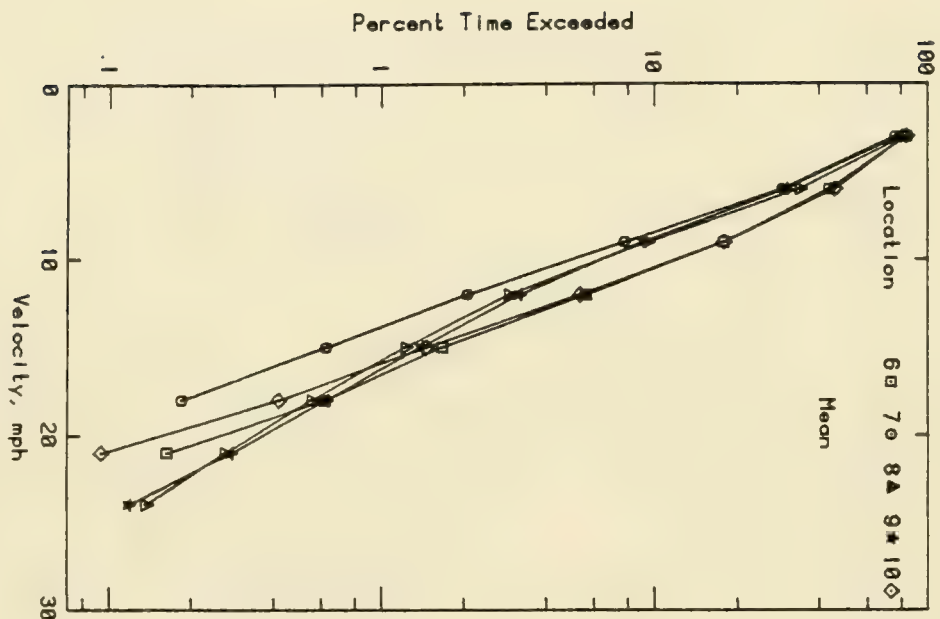


Percent Time Exceeded for PHI Configuration

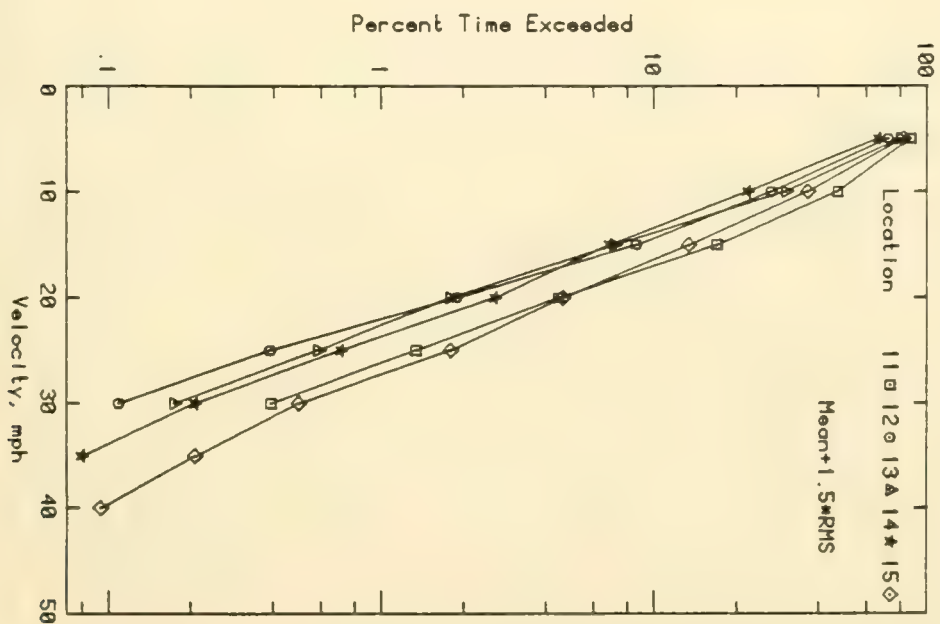
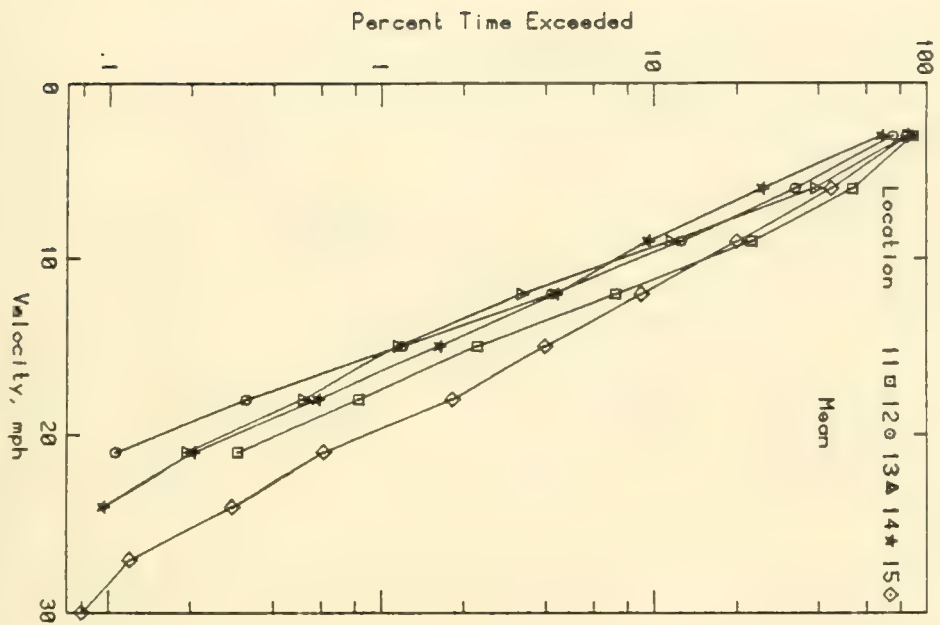


Percent Time Exceeded for PH2 Configuration

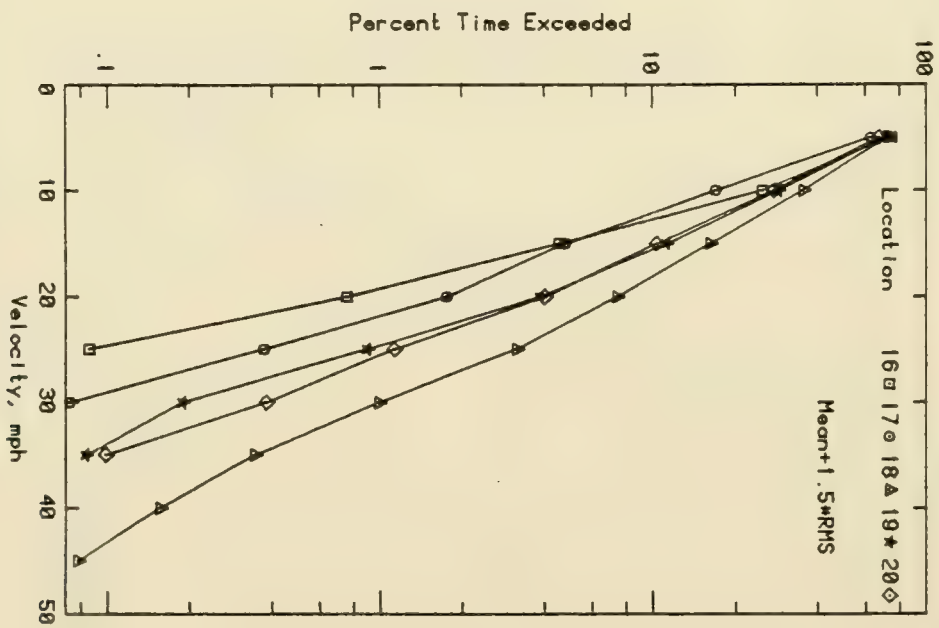
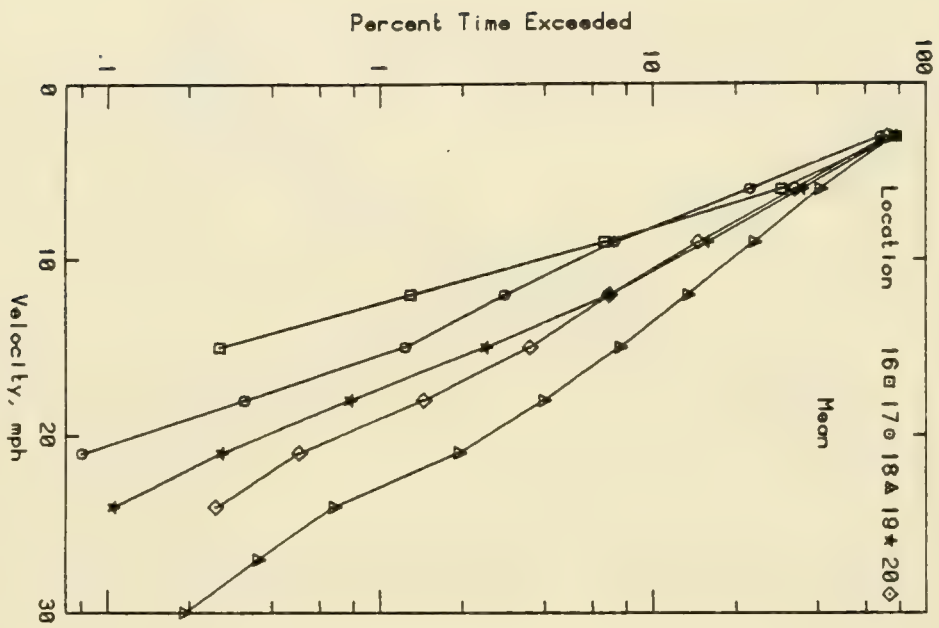




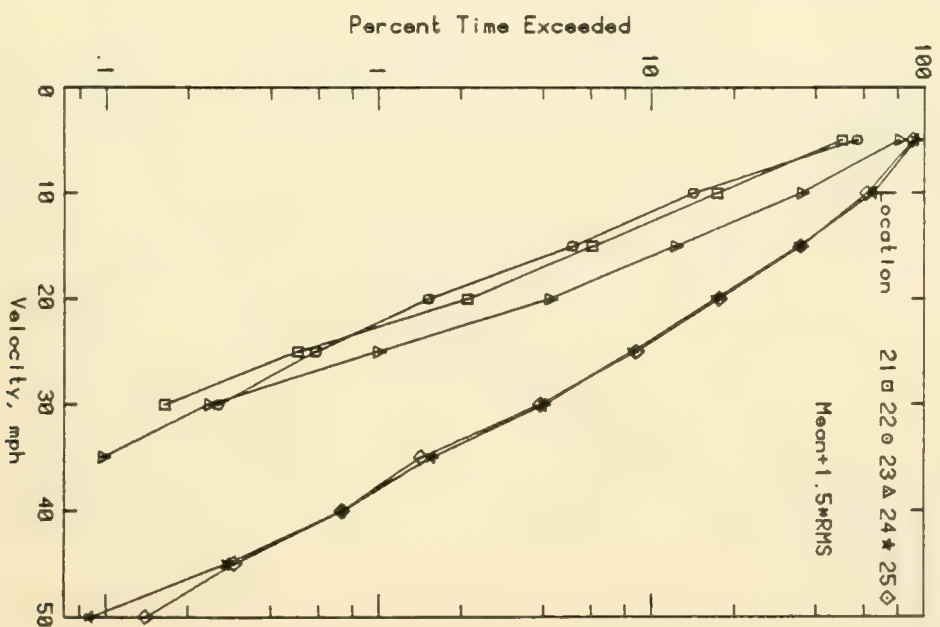
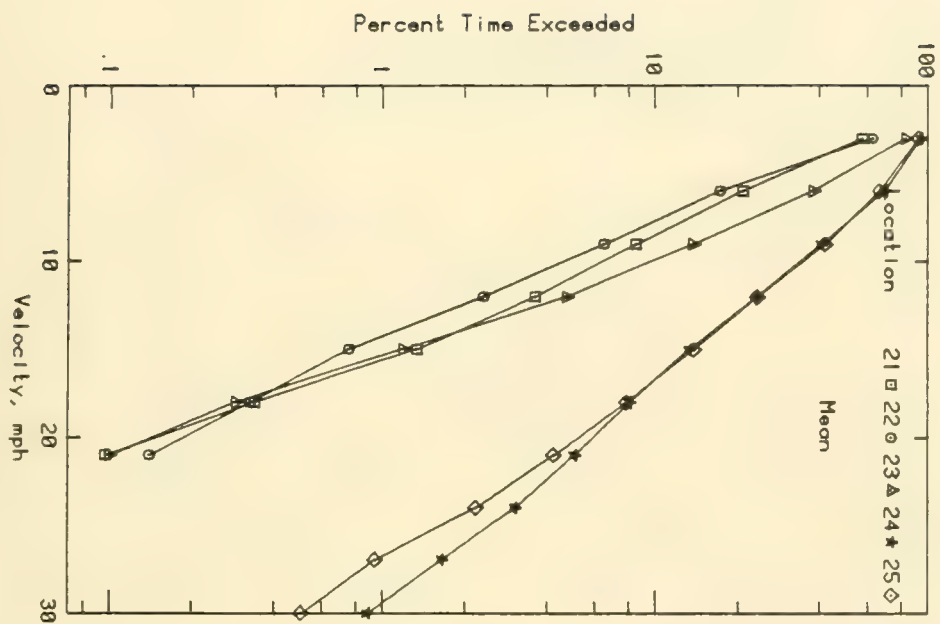
Percent Time Exceeded for PH2 Configuration

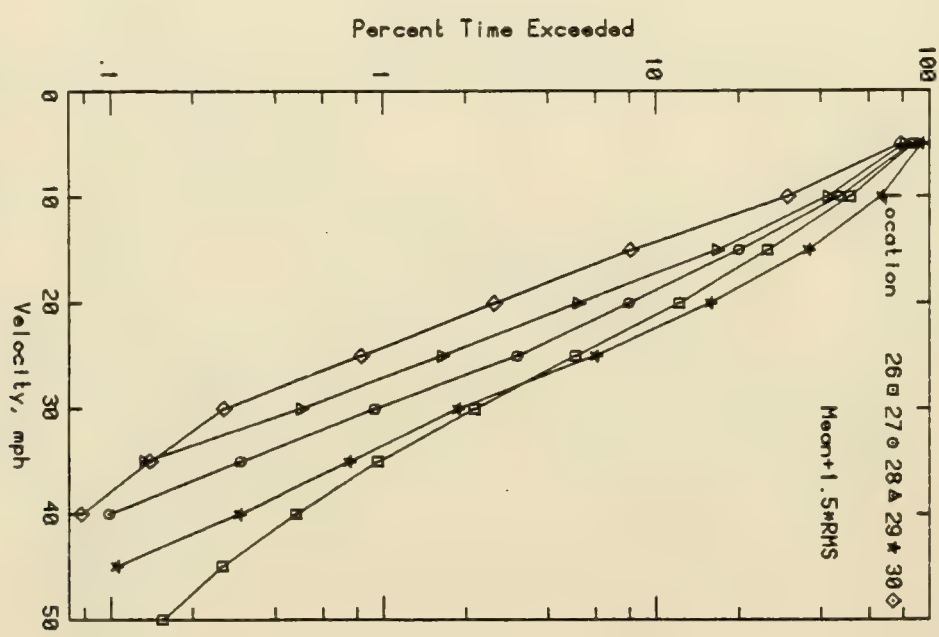
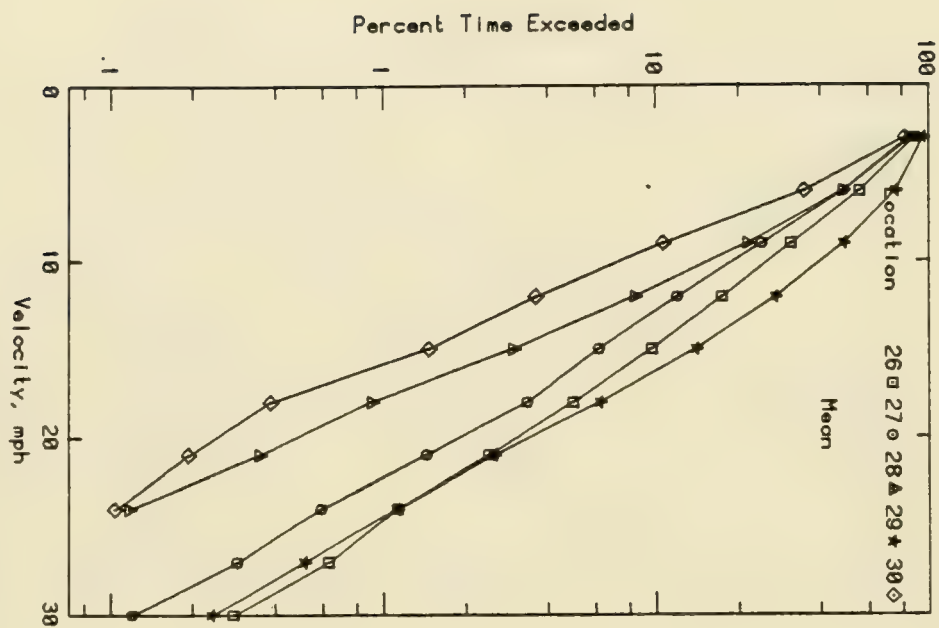


Percent Time Exceeded for PH2 Configuration



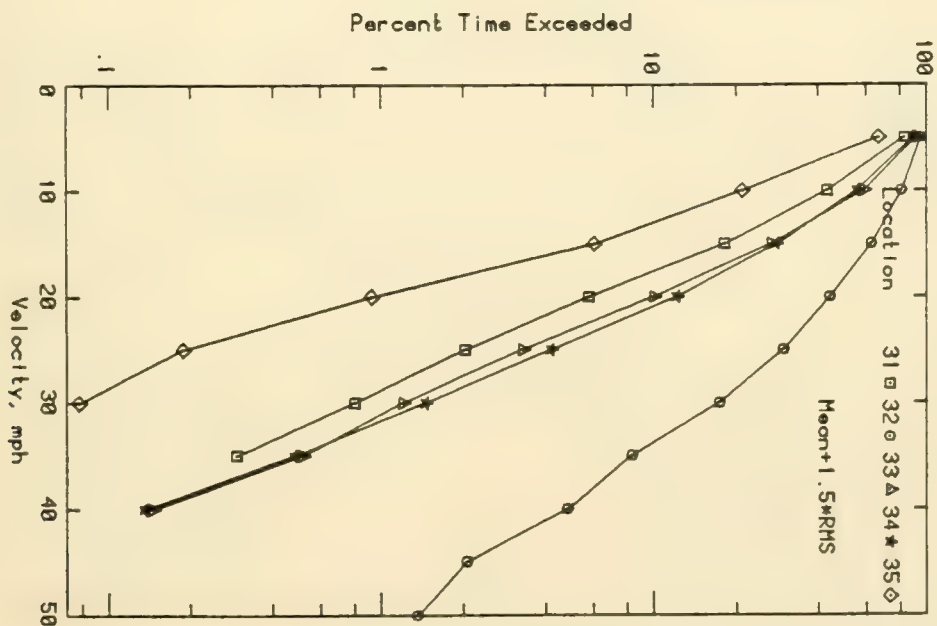
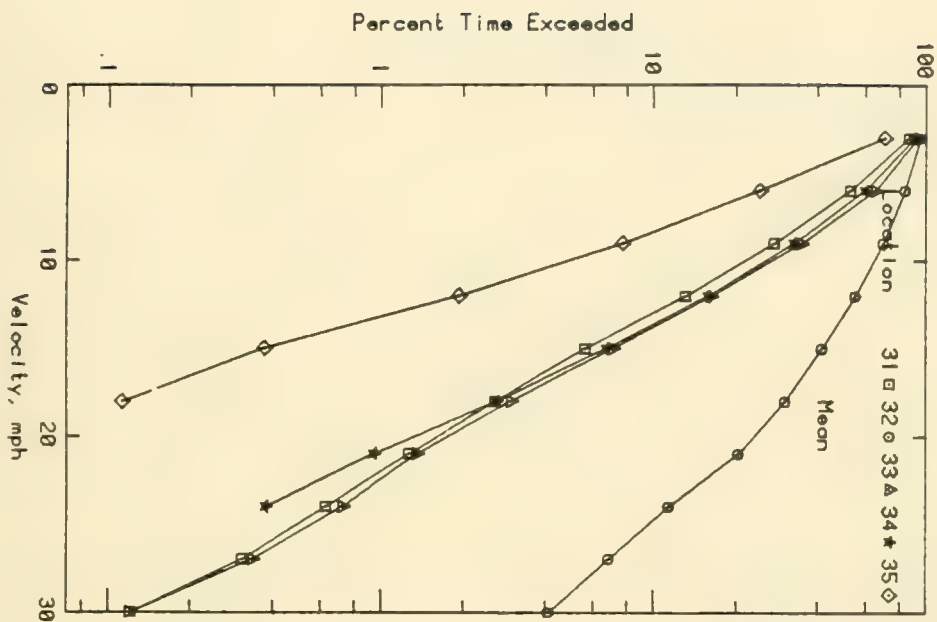
Percent Time Exceeded for PH2 Configuration



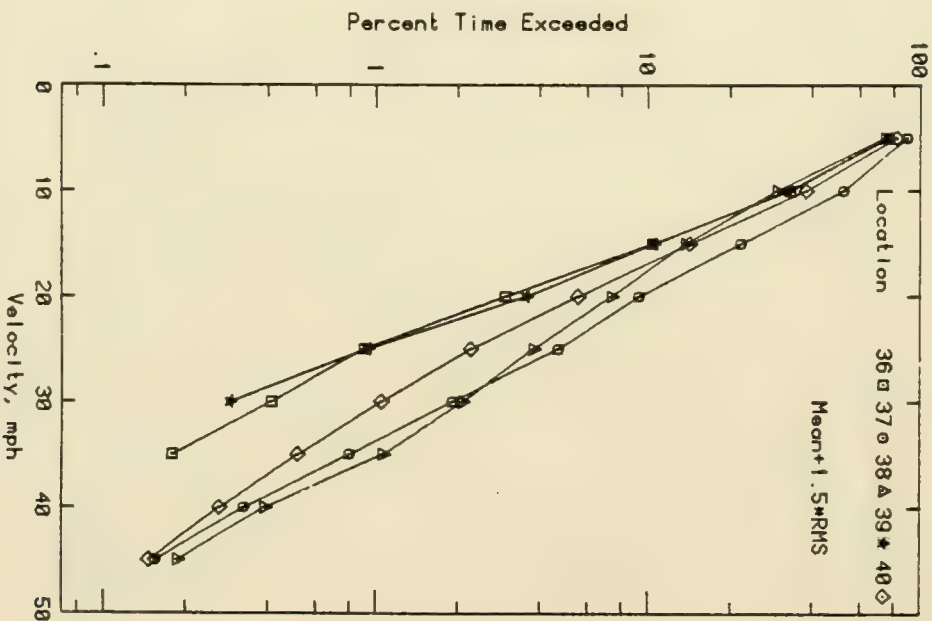
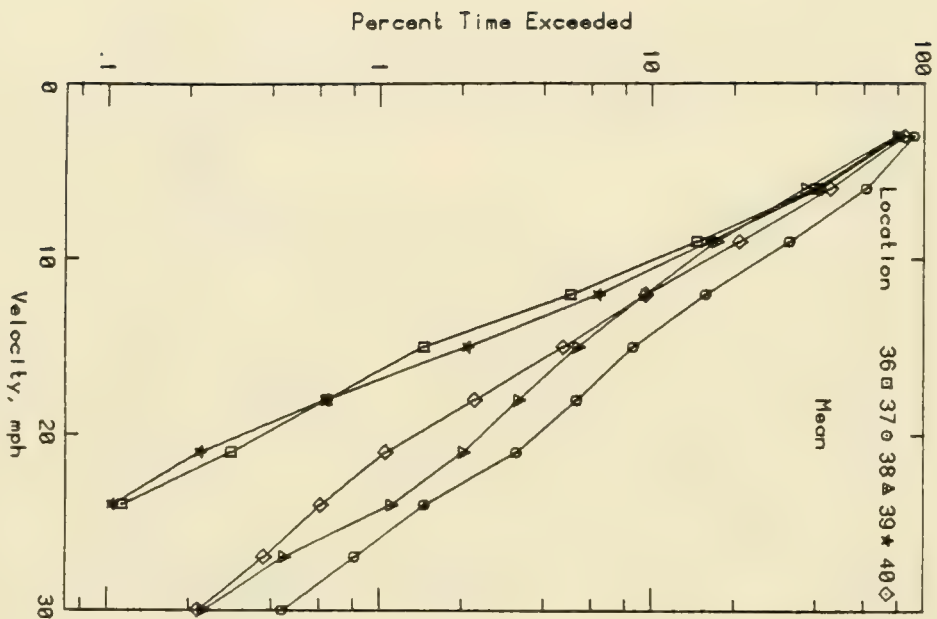


Percent Time Exceeded for PH2 Configuration



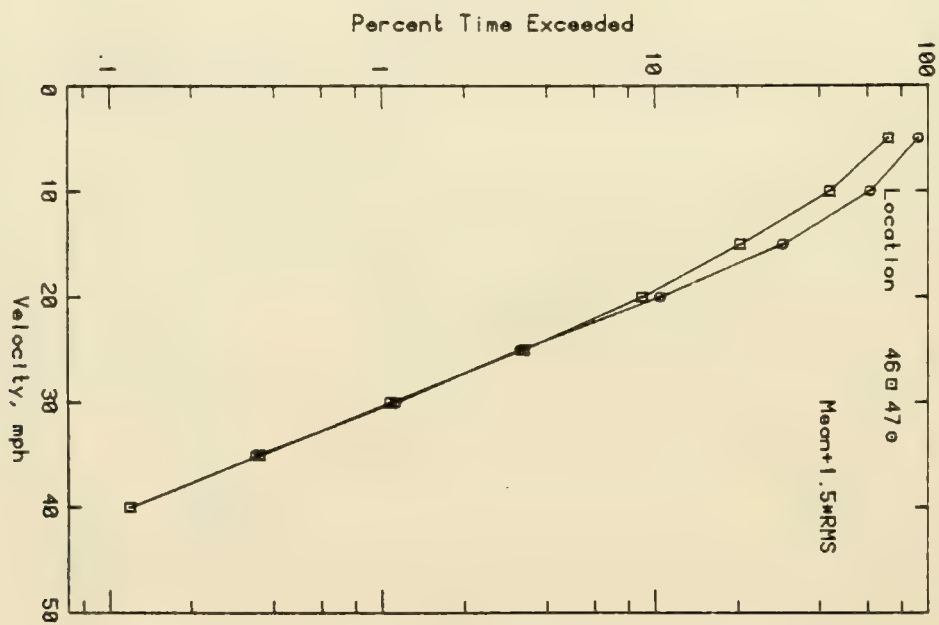
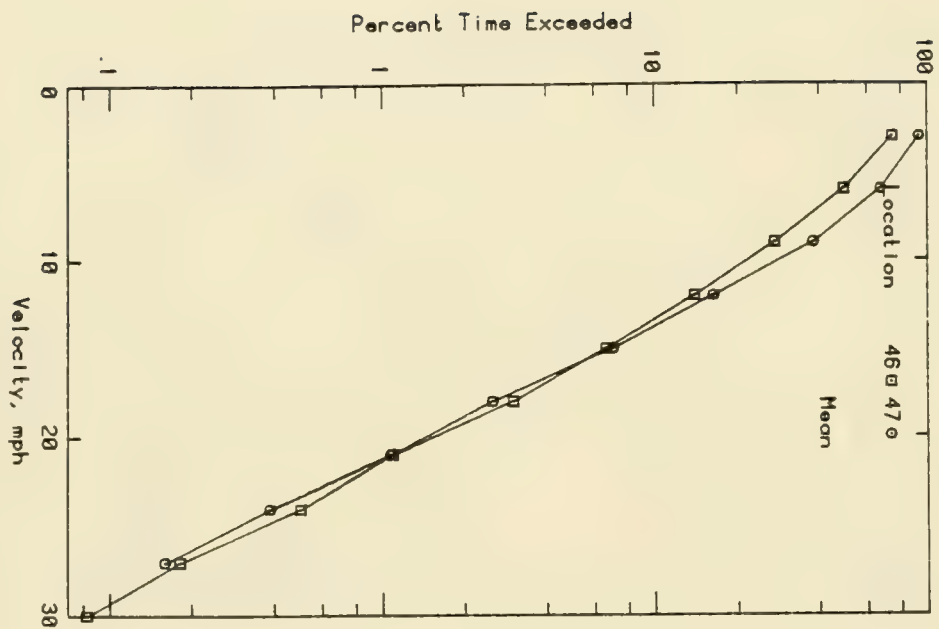


Percent Time Exceeded for PH2 Configuration



Percent Time Exceeded for PH2 Configuration





Percent Time Exceeded for PH2 Configuration





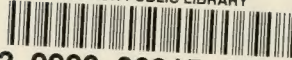








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